# Experimental Investigation of Phase Equilibria in the Cu-Fe-Zr Ternary System

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The phase equilibria in the Cu-Fe-Zr ternary system was experimentally investigated by optical microscopy, electron probe micro-analyzer and x-ray diffraction on the equilibriated alloys. Three isothermal sections of the Cu-Fe-Zr ternary system at 1000, 1100 and 1200 °C were experimentally determined, and no ternary compound was found in this system. The further result in the present work shows that the  $Fe_{23}Zr_6$  phase in the Cu-Fe-Zr ternary system is an equilibrium phase rather than oxygen-stabilized phase.

Keywords Cu-Fe-Zr ternary system, electron probe micro-analyzer, experimental phase equilibria, x-ray diffraction

#### 1. Introduction

Metallic glasses have stimulated widespread research enthusiasm due to its excellent properties of strength, hardness, magnetism, wear and corrosion resistance.<sup>[1-3]</sup> However, the applications of metallic glasses have been limited due to the poor plasticity caused by shear localization and work softening.<sup>[4]</sup> To solve this problem, great attention has been paid to crystalline/amorphous composite through liquid immiscibility.<sup>[5-7]</sup> The Cu-Fe-Zr-B is a good candidate for the composites, owing to its sufficiently high glass-forming ability (GFA) in the Fe-Zr-B system,<sup>[8]</sup> and a positive enthalpy of mixing in the Fe-Cu atomic pair.<sup>[9]</sup> The phase equilibria information in the Cu-Fe-Zr ternary subsystem is needed to pinpoint the alloy compositions with liquid immiscibility in the Cu-Fe-Zr-B quaternary system. However, until now, such information in the Cu-Fe-Zr ternary system has not been available in the relevant literature. Therefore, it is necessary to comprehensively determine the phase equilibria in the Cu-Fe-Zr ternary system.

Three binary phase diagrams of the Cu-Fe,<sup>[10]</sup> Cu-Zr<sup>[11]</sup> and Fe-Zr,<sup>[12]</sup> constituting the Cu-Fe-Zr ternary system, are shown in Fig. 1. The Cu-Fe binary system<sup>[10]</sup> is a simple system without any intermediate phase. The Cu-Zr binary system<sup>[11]</sup> has ten intermediate phases, Cu<sub>5</sub>Zr, Cu<sub>51</sub>Zr<sub>14</sub>, Cu<sub>8</sub>Zr<sub>3</sub>, Cu<sub>2</sub>Zr, Cu<sub>24</sub>Zr<sub>13</sub>, Cu<sub>10</sub>Zr<sub>7</sub>, CuZr, Cu<sub>5</sub>Zr<sub>8</sub>,  $\alpha$ CuZr<sub>2</sub>

and  $\beta$ CuZr<sub>2</sub>. The Cu<sub>5</sub>Zr phase forms through peritectic reaction at 1012 °C. The Fe-Zr binary system<sup>[12]</sup> has five intermediate phases, FeZr<sub>3</sub>, FeZr<sub>2</sub>,  $\alpha$ Fe<sub>2</sub>Zr,  $\beta$ Fe<sub>2</sub>Zr and Fe<sub>23</sub>Zr<sub>6</sub>. All the stable solid phases in the three binary systems are summarized in Table 1.

The purpose of the present work is to experimentally investigate the phase equilibrium the Cu-Fe-Zr ternary system at 1000, 1100 and 1200 °C by using optical microscopy (OM), electron probe micro-analyzer (EPMA) and x-ray diffraction (XRD), which will provide a better understanding of microstructures and information for the thermodynamic database of Cu-Fe-Zr-B quaternary phase diagram.

#### 2. Experimental Procedure

Highly-pure copper (99.9 wt.%), iron (99.9 wt.%) and zirconium (99.9 wt.%) were used as starting materials. Bulk alloy buttons were prepared from pure elements by arc melting under a highly-pure argon atmosphere using a non-consumable tungsten electrode. The ingots were melted at least five times in order to achieve their homogeneity. The sample weight was around 10 g and the weight loss during melting was generally less than 0.20%. Afterwards, the ingots were cut into small pieces for heat treatment and further observations.

All samples were put into quartz capsules evacuated and backfilled with argon gas. The specimens were annealed at 1000, 1100 and 1200 °C, respectively. The time of heat treatment varied from several hours to several days depending on the annealing temperature and the composition of the specimen. After the heat treatment, the specimens were quenched into ice water.

After annealing standard metallographic preparation, the microstructural observations were carried out by OM. The equilibrium compositions of the phases were measured by EPMA (JXA-8800R, JEOL, Japan). Pure elements were used as standards and measurements were carried out at 20.0 kV. The XRD was used to identify the crystal structure of the constituent phases. The XRD measurement was

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Fig. 1 Binary phase diagrams constituting the Cu-Fe-Zr ternary system<sup>[10-12]</sup>

carried out on a Bruker D8 Advance X-pert diffractometer using  $CuK_{\alpha}$  radiation at 35.0 kV and 20 mA. The data were collected in the range of 2 $\theta$  from 20° to 120° at a step of 0.02°.

## 3. Results and Discussion

#### 3.1 Microstructure and Phase Equilibria

Back-scattered electron (BSE) images of typical ternary Cu-Fe-Zr alloys are shown in Fig. 2(a)-(j). Phase identification was based on the equilibrium composition measured by EPMA and XRD results. Figure 2(a) shows the two-phase microstructure (( $\alpha$ Fe) + Liquid) of the Cu<sub>49.5</sub>Fe<sub>49.5</sub>Zr<sub>1</sub> (at.%) alloy annealed at 1200 °C for 1 day. In the Cu<sub>5</sub>Fe<sub>85</sub>Zr<sub>10</sub> (at.%) alloy annealed at 1100 °C for 60 days, the two-phase microstructure (Fe<sub>23</sub>Zr<sub>6</sub> + ( $\alpha$ Fe)) was observed (Fig. 2b) and substantiated by the XRD result, as shown in Fig. 3(a), where the characteristic peaks of the Fe<sub>23</sub>Zr<sub>6</sub> and ( $\alpha$ Fe) phases were found and well marked by different symbols. The ( $\alpha$ Fe) phase at room temperature came from the phase transition in ( $\gamma$ Fe) phase during quenching. Moreover, the composition of the ( $\alpha$ Fe) phase at room temperature and the ( $\gamma$ Fe) phase at high temperature are the same. The oxygen-content detected by EPMA in the Fe<sub>23</sub>Zr<sub>6</sub> phase in all samples is very low in the Cu-Fe-Zr ternary system, which is different from the Fe<sub>23</sub>Zr<sub>6</sub> phase stabilized by oxygen in the Fe-Zr system.<sup>[26]</sup> Combined with the EPMA element mapping (Fig. 4) of the selected area of the Cu<sub>5</sub>Fe<sub>85</sub>Zr<sub>10</sub> (at.%) alloy annealed at 1100 °C for 60 days, the Fe<sub>23</sub>Zr<sub>6</sub> phase is an equilibrium phase in the Cu-Fe-Zr ternary system.

System	Phase	Pearson's symbol	Prototype	Space group	Lattice parameters, nm	References
Cu-Fe	(Cu)	cF4	Cu	Fm-3m	<i>a</i> = 0.3613	[10,13]
	(δFe)	cI2	W	Im-3m	a = 0.29315	[10,14]
	(yFe)	cF4	Cu	Fm-3m	a = 0.343	[10,15]
	(aFe)	cI2	W	Im-3m	a = 0.2866	[10,14]
Cu-Zr	(Cu)	cF4	Cu	Fm-3m	a = 0.3613	[11,13]
	Cu <sub>5</sub> Zr	cF24	AuBe <sub>5</sub>	F-43m	a = 0.687	[11,16]
	Cu <sub>51</sub> Zr <sub>14</sub>	hP65	$Ag_{51}Gd_{14}$	P6/m	a = 1.12444, c = 0.82815	[11,17]
	Cu <sub>8</sub> Zr <sub>3</sub>	oP44	Cu <sub>8</sub> Hf <sub>3</sub>	Pnma	a = 0.78693, b = 0.81547, c = 0.99848	[11,17]
	Cu <sub>2</sub> Zr					[11]
	Cu <sub>24</sub> Zr <sub>13</sub>	o*37				[11]
	Cu <sub>10</sub> Zr <sub>7</sub>	oC68	Ni <sub>10</sub> Zr <sub>7</sub>	C2ca	a = 1.26729, b = 0.93163, c = 0.93466	[11,17]
	CuZr	cP2	CsCl	Pm-3m	a = 0.32620	[11,18]
	Cu <sub>5</sub> Zr <sub>8</sub>	o*26				[11]
	$\beta CuZr_2$	tI6	MoSi <sub>2</sub>	I4/mmm	a = 0.32204, c = 1.11832	[11,19]
	$\alpha CuZr_2$	tP150				[11]
	(βZr)	cI2	W	Im-3 m	a = 0.3568	[11,20]
	(aZr)	hP2	Mg	$P6_3/mmc$	a = 0.3232, c = 0.5147	[11,21]
Fe-Zr	(δFe)	cI2	W	Im-3m	a = 0.29315	[12,14]
	(yFe)	cF4	Cu	Fm-3m	a = 0.343	[12,15]
	(aFe)	cI2	W	Im-3m	a = 0.2866	[12,14]
	Fe <sub>23</sub> Zr <sub>6</sub>	cF116	Th <sub>6</sub> Mn <sub>23</sub>	Fm-3m	a = 1.169	[12,22]
	βFe <sub>2</sub> Zr	hP24	MgNi <sub>2</sub>	$P6_3/mmc$		[12]
	αFe <sub>2</sub> Zr	cF24	Cu <sub>2</sub> Mg	Fd-3m	a = 0.70721	[12,23]
	FeZr <sub>2</sub>	tI12	Al <sub>2</sub> Cu	I4/mcm	a = 0.6385, c = 0.5596	[12,24]
	FeZr <sub>3</sub>	oC16	BRe <sub>3</sub>	Cmcm	a = 0.3324, b = 1.0990, c = 0.8810	[12,25]
	(βZr)	cI2	W	Im-3m	a = 0.3568	[12,20]
	(aZr)	hP2	Mg	$P6_3/mmc$	a = 0.3232, c = 0.5147	[12,21]

Table 1 The stable solid phases in the three binary systems

The Cu<sub>5</sub>Fe<sub>45</sub>Zr<sub>50</sub> (at.%) and Cu<sub>5</sub>Fe<sub>10</sub>Zr<sub>85</sub> (at.%) alloys annealed at 1100 °C are located in two two-phase equilibrium regions of the (Fe<sub>2</sub>Zr + Liquid) and (( $\beta$ Zr) + Liquid), respectively, as characterized in Fig. 2(c) and (d). A threephase equilibrium of the  $(Fe_{23}Zr_6 + (\alpha Fe) + (Cu))$  was observed (Fig. 2e) in the  $Cu_{49.5}Fe_{49.5}Zr_1$  (at.%) alloy annealed at 1000 °C for 60 days and the XRD results is shown in Fig. 3(b), where the characteristic peaks of  $Fe_{23}Zr_6$ , ( $\alpha Fe$ ) and (Cu) phases were confirmed. Figure 2(f) presents the three-phase equilibrium microstructures of the  $(Fe_{23}Zr_6 + (\alpha Fe) + Liquid)$  in the  $Cu_{45}Fe_{45}Zr_{10}$  (at.%) alloy annealed at 1200 °C for 2 days, and Fig. 2(g) shows a three-phase equilibrium of the  $(Fe_{23}Zr_6 + Fe_2Zr + Liquid)$ in the Cu<sub>38</sub>Fe<sub>38</sub>Zr<sub>24</sub> (at.%) alloy annealed at 1200 °C for 2 days. There is a three-phase equilibrium of the  $(Fe_{23}Zr_6 + Fe_2Zr + (Cu))$ in the  $Cu_{41}Fe_{41}Zr_{18}$  (at.%) annealed at 1000 °C (Fig. 2h) and the XRD results is shown in Fig. 3(c). Two three-phase equilibria of the  $(Fe_2Zr + (Cu) +$ Liquid) and  $(Fe_2Zr + Cu_{51}Zr_{14} + Liquid)$  were observed in the  $Cu_{37}Fe_{37}Zr_{26}$  (at.%) and  $Cu_{60}Fe_{10}Zr_{30}$  (at.%) alloys annealed at 1000 °C, and were indicated in Fig. 2(i) and (j), respectively. XRD results of the Cu47.5Fe47.5Zr5 (at.%) and Cu<sub>5</sub>Fe<sub>85</sub>Zr<sub>10</sub> (at.%) alloys annealed at 1000 °C are presented in Fig. 3(d) and (e), respectively. According to the XRD results, the lattice parameters of phases in the Cu<sub>49.5</sub>Fe<sub>49.5</sub>Zr<sub>1</sub> (at.%), Cu<sub>47.5</sub>Fe<sub>47.5</sub>Zr<sub>5</sub> (at.%), Cu<sub>5</sub>Fe<sub>85</sub>Zr<sub>10</sub> (at.%), Cu<sub>41</sub>Fe<sub>41</sub>Zr<sub>18</sub>

(at.%) alloys annealed at 1000 °C and  $Cu_5Fe_{85}Zr_{10}$  (at.%) alloy annealed at 1100 °C have been calculated, respectively (Table 2).

#### 3.2 Isothermal Section

The equilibrium compositions of the Cu-Fe-Zr ternary system at 1000, 1100 and 1200 °C obtained from EPMA are listed in Tables 3-5, respectively. Base on the experimental data determined by this work, three isothermal sections of 1000, 1100 and 1200 °C were constructed in Fig. 5(a)-(c), respectively.

Figure 5(a) shows the isothermal section at 1000 °C. In the section, four three-phase regions of  $(Fe_{23}Zr_6 + (\gamma Fe) + (Cu))$ ,  $(Fe_{23}Zr_6 + Fe_2Zr + (Cu))$ ,  $(Fe_2Zr + (Cu) + Liquid)$  and  $(Fe_2Zr + Cu_{51}Zr_{14} + Liquid))$  appear. The results show that the maximum solubility of Cu in the Fe<sub>2</sub>Zr and Fe<sub>23</sub>Zr<sub>6</sub> phases are about 15 and 5 at.%, respectively. In the isothermal section of 1100 °C shown in Fig. 5(b), two three-phase regions of  $(Fe_{23}Zr_6 + (\gamma Fe) + Liquid)$  and  $(Fe_{23}Zr_6 + Fe_2Zr + Liquid)$  were experimentally determined in this work. The maximum solubility of Cu in the Fe<sub>2</sub>Zr phase was found to be about 12.5 at.%, and the maximum solubility of Cu in the Fe<sub>23</sub>Zr<sub>6</sub> phase was approximately 4.5 at.%. The phase relationships in the isothermal section of 1200 °C



**Fig. 2** Typical ternary BSE images obtained from: (a)  $Cu_{49,5}Fe_{49,5}Zr_1$  (at.%) alloy annealed at 1200 °C for 1 day; (b)  $Cu_5Fe_{85}Zr_{10}$  (at.%) alloy annealed at 1100 °C for 60 days; (c)  $Cu_5Fe_{45}Zr_{50}$  (at.%) alloy annealed at 1100 °C for 4 days; (d)  $Cu_5Fe_{10}Zr_{85}$  (at.%) alloy annealed at 1100 °C for 4 days; (e)  $Cu_{49,5}Fe_{49,5}Zr_1$  (at.%) alloy annealed at 1000 °C for 60 days; (f)  $Cu_5Fe_{45}Zr_{10}$  (at.%) alloy annealed at 1000 °C for 60 days; (g)  $Cu_{38}Fe_{38}Zr_{24}$  (at.%) alloy annealed at 1200 °C for 2 days; (h)  $Cu_{41}Fe_{41}Zr_{18}$  (at.%) alloy annealed at 1000 °C for 4 days; (i)  $Cu_{37}Fe_{37}Zr_{26}$  (at.%) alloy annealed at 1000 °C for 4 days; (at.%) alloy annealed at 1000 °C for 12 h



**Fig. 3** X-ray diffraction patterns obtained from: (a) the  $Cu_5Fe_{85}Zr_{10}$  (at.%) alloy annealed at 1100 °C for 60 days; (b) the  $Cu_{49.5}Fe_{49.5}Zr_{1}$  (at.%) alloy annealed at 1000 °C for 60 days; (c) the  $Cu_4Fe_{41}Zr_{18}$  (at.%) alloy annealed at 1000 °C for 4 days; (d)  $Cu_{47.5}Fe_{47.5}Zr_{5}$  (at.%) alloy annealed at 1000 °C for 60 days; and (e) the  $Cu_5Fe_{85}Zr_{10}$  (at.%) alloy annealed at 1000 °C for 60 days;

containing two three-phase regions of  $(Fe_{23}Zr_6 + (\gamma Fe) + Liquid)$  and  $(Fe_{23}Zr_6 + Fe_2Zr + Liquid)$  (Fig. 5c), is quite similar to that at 1100 °C. Undetermined three-phase equilibria in Fig. 5(a) and (b) are shown in dashed

lines. Compared with the above mentioned three isothermal sections, it should be noted that the area of liquid phase increases at the temperature range from 1000 to 1200 °C.



Fig. 4 Fe<sub>23</sub>Zr<sub>6</sub>-enriched region of the Cu5Fe85Zr10 (at.%) alloy annealed at 1100 °C for 60 days: (a) BSE micrograph of the region with ( $\alpha$ Fe) (dark areas), and Fe<sub>23</sub>Zr<sub>6</sub> (white areas); (b, c, and d) EPMA element mappings of the respective region for zirconium, oxygen, and iron, respectively

Alloys, at.%	Annealing temperature, °C	XRD pattern	Phase	Calculating lattice parameters, nm
Cu <sub>49.5</sub> Fe <sub>49.5</sub> Zr <sub>1</sub>	1000	Figure 3(b)	(aFe)	a = 0.2870
			Fe23Zr6	a = 1.1659
			(Cu)	a = 0.3616
Cu <sub>47.5</sub> Fe <sub>47.5</sub> Zr <sub>5</sub>	1000	Figure 3(d)	(aFe)	a = 0.2868
			Fe23Zr6	a = 1.1675
			(Cu)	a = 0.3618
Cu <sub>5</sub> Fe <sub>85</sub> Zr <sub>10</sub>	1000	Figure 3(e)	(aFe)	a = 0.2871
			Fe23Zr6	a = 1.1713
Cu <sub>41</sub> Fe <sub>41</sub> Zr <sub>18</sub>	1000	Figure 3(c)	Fe2Zr	a = 0.7037
			Fe23Zr6	a = 1.1668
			(Cu)	a = 0.3620
Cu <sub>5</sub> Fe <sub>85</sub> Zr <sub>10</sub>	1100	Figure 3(a)	(aFe)	a = 0.2868
			Fe23Zr6	a = 1.1695

Table 2 The calculating lattice parameters of phases in typical ternary Cu-Fe-Zr alloys

			Composition, at.%									
		Dhasa squilibuis		Phase 1			Phase 2			Phase 3		
Alloys, at.%	Annealing time	Phase equilibria Phase 1/Phase 2/Phase 3	Cu	Fe	Zr	Cu	Fe	Zr	Cu	Fe	Zr	
Cu <sub>49.5</sub> Fe <sub>49.5</sub> Zr <sub>1</sub>	60 days	(γFe)/Fe <sub>23</sub> Zr <sub>6</sub> /(Cu)	7.3	92.7	0.0	6.0	73.5	20.5	93.6	6.4	0.0	
Cu47.5Fe47.5Zr5	60 days	$(\gamma Fe)/Fe_{23}Zr_6/(Cu)$	7.2	92.8	0.0	5.2	74.2	20.6	94.1	5.8	0.1	
Cu <sub>5</sub> Fe <sub>85</sub> Zr <sub>10</sub>	60 days	$(\gamma Fe)/Fe_{23}Zr_6$	5.1	94.9	0.0	3.3	76.0	20.7				
Cu <sub>41</sub> Fe <sub>41</sub> Zr <sub>18</sub>	4 days	Fe <sub>2</sub> Zr/Fe <sub>23</sub> Zr <sub>6</sub> /(Cu)	6.3	68.1	25.6	4.6	75.8	19.6	94.6	5.4	0.0	
Cu37Fe37Zr26	4 days	Fe <sub>2</sub> Zr/Liquid/(Cu)	7.1	64.1	28.8	87.8	4.0	8.2	96.6	3.4	0.0	
Cu <sub>60</sub> Fe <sub>10</sub> Zr <sub>30</sub>	12 h	Fe <sub>2</sub> Zr/Liquid/Cu <sub>51</sub> Zr <sub>14</sub>	14.0	54.0	32.0	58.5	6.0	35.5	78.3	1.0	20.7	
Cu <sub>30</sub> Fe <sub>30</sub> Zr <sub>40</sub>	21 days	Fe <sub>2</sub> Zr/Liquid	11.2	56.4	32.4	29.3	14.1	56.6				
Cu10Fe50Zr40	4 days	Fe <sub>2</sub> Zr/Liquid	5.2	60.8	34.0	22.7	20.5	56.8				
Cu <sub>27.5</sub> Fe <sub>27.5</sub> Zr <sub>45</sub>	21 days	Fe <sub>2</sub> Zr/Liquid	11.1	56.5	32.4	29.8	13.5	56.7				
Cu25Fe25Zr50	21 days	Fe <sub>2</sub> Zr/Liquid	3.0	64.0	33.0	19.8	22.8	57.4				
Cu10Fe40Zr50	4 days	Fe <sub>2</sub> Zr/Liquid	2.7	63.2	34.1	13.3	20.9	65.8				
Cu <sub>5</sub> Fe <sub>45</sub> Zr <sub>50</sub>	21 days	Fe <sub>2</sub> Zr/Liquid	1.2	66.2	32.6	8.0	26.7	65.3				
Cu <sub>9</sub> Fe <sub>9</sub> Zr <sub>82</sub>	21 days	(βZr)/Liquid	0.1	0.1	99.8	10.6	13.7	75.7				
Cu <sub>5</sub> Fe <sub>10</sub> Zr <sub>85</sub>	4 days	(βZr)/Liquid	0.0	0.1	99.9	7.1	16.6	76.3				
Cu <sub>5</sub> Fe <sub>5</sub> Zr <sub>90</sub>	4 days	(βZr)/Liquid	2.9	2.8	94.3	15.5	14.6	69.9				

## Table 3 Equilibrium compositions of the Cu-Fe-Zr system at 1000 °C

## Table 4 Equilibrium compositions of the Cu-Fe-Zr system at 1100 °C

			Composition, at.%									
				Phase 1			Phase 2		I	Phase 3		
Alloys, at.%	Annealing time	Phase 1/Phase 2/Phase 3	Cu	Fe	Zr	Cu	Fe	Zr	Cu	Fe	Zr	
Cu <sub>49.5</sub> Fe <sub>49.5</sub> Zr <sub>1</sub>	2 days	(yFe)/Liquid	7.0	93.0	0.0	90.7	4.5	4.8				
Cu48.5Fe48.5Zr3	4 days	(yFe)/Liquid	6.7	93.3	0.0	94.1	5	0.9				
Cu47.5Fe47.5Zr5	4 days	(yFe)/Liquid	6.8	93.2	0.0	93.6	4.3	2.1				
Cu46.5Fe46.5Zr7	4 days	(yFe)/Fe23Zr6/Liquid	6.5	93.3	0.2	7.4	72.4	20.2	92.4	5	2.6	
Cu45.5Fe45.5Zr9	4 days	(yFe)/Fe23Zr6/Liquid	6.7	93.3	0.0	7.6	72.6	19.8	90.5	4.9	4.6	
Cu45Fe45Zr10	4 days	(yFe)/Fe23Zr6/Liquid	7.4	92.6	0.0	7.1	72.0	20.9	90.8	5.2	4	
Cu <sub>5</sub> Fe <sub>85</sub> Zr <sub>10</sub>	60 days	(γFe)/Fe <sub>23</sub> Zr <sub>6</sub>	5.1	94.8	0.1	3.6	75.8	20.6				
Cu43.5Fe43.5Zr13	4 days	Fe2Zr/Fe23Zr6/Liquid	5	67.5	27.5	6.8	73.2	20.0	93.20	3.0	3.8	
$Cu_{41}Fe_{41}Zr_{18}$	4 days	Fe2Zr/Fe23Zr6/Liquid	5.3	67.6	27.1	6.3	73.7	20.0	92.0	3.1	4.9	
Cu38Fe38Zr24	1 day	Fe <sub>2</sub> Zr/Liquid	13.6	55.7	30.7	71.0	8.1	20.9				
Cu37Fe37Zr26	1 day	Fe <sub>2</sub> Zr/Liquid	7	62.5	30.5	83.3	4.5	12.2				
Cu30Fe30Zr40	12 h	Fe <sub>2</sub> Zr/Liquid	9.9	57.6	32.5	68.1	6.6	25.3				
$Cu_{10}Fe_{50}Zr_{40}$	4 days	Fe <sub>2</sub> Zr/Liquid	8.5	58.5	33	52.5	11.2	36.3				
Cu25Fe25Zr50	1 day	Fe <sub>2</sub> Zr/Liquid	9.1	57.8	33.1	41.4	11.6	47.0				
Cu10Fe40Zr50	4 days	Fe <sub>2</sub> Zr/Liquid	4.5	63.0	32.5	19.1	21.4	59.5				
Cu <sub>5</sub> Fe <sub>45</sub> Zr <sub>50</sub>	4 days	Fe <sub>2</sub> Zr/Liquid	3	65.8	31.2	12.3	24.1	63.6				
Cu <sub>9</sub> Fe <sub>9</sub> Zr <sub>82</sub>	4 days	(βZr)/Liquid	0.3	0.1	99.6	12.2	9.4	78.4				
Cu10Fe5Zr85	4 days	(βZr)/Liquid	0.4	0.1	99.5	15.3	6.3	78.4				
$Cu_5Fe_{10}Zr_{85}$	4 days	(βZr)/Liquid	0.1	0.1	99.8	9.0	11.5	79.5				

## Table 5 Equilibrium compositions of the Cu-Fe-Zr system at 1200 °C

		Phase equilibria Phase 1/Phase 2/Phase 3	Composition, at.%									
			Phase 1			Phase 2			Phase 3			
Alloys, at.%	Annealing time		Cu	Fe	Zr	Cu	Fe	Zr	Cu	Fe	Zr	
$\begin{array}{l} Cu_{49.5}Fe_{49.5}Zr_{1}\\ Cu_{48.5}Fe_{48.5}Zr_{3} \end{array}$	1 day 2 days	(γFe)/Liquid (γFe)/Liquid	8.4 8.0	91.6 92	0.0 0.0	95.9 95.0	4.1 5.0	0.0 0.0				

#### Table 5 continued

			Composition, at.%									
		Phase equilibria Phase 1/Phase 2/Phase 3	Phase 1			Phase 2			Phase 3			
Alloys, at.%	Annealing time		Cu	Fe	Zr	Cu	Fe	Zr	Cu	Fe	Zr	
Cu <sub>47.5</sub> Fe <sub>47.5</sub> Zr <sub>5</sub>	2 days	(yFe)/Liquid	7.7	92.3	0.0	96.8	3.2	0.0				
Cu45Fe45Zr10	2 days	(γFe)/Fe <sub>23</sub> Zr <sub>6</sub> /Liquid	7.1	92.9	0.0	10.9	68.4	20.7	90.1	5.2	4.7	
$Cu_{41}Fe_{41}Zr_{18}$	2 days	Fe2Zr/Fe23Zr6/Liquid	5.2	68.5	26.3	7.1	72.5	20.4	92.8	3.3	3.9	
Cu38Fe38Zr24	2 days	Fe2Zr/Fe23Zr6/Liquid	6.9	64.7	28.4	9.0	70.9	20.1	89.3	2.7	8.0	
Cu30Fe30Zr40	6 h	Fe <sub>2</sub> Zr/Liquid	10.1	54.6	35.3	69.7	6	24.3				
$Cu_{20}Fe_{40}Zr_{40}$	2 days	Fe <sub>2</sub> Zr/Liquid	10.5	57.6	31.9	76.9	7.9	15.2				
Cu10Fe50Zr40	2 days	Fe <sub>2</sub> Zr/Liquid	7.7	59.2	33.1	43.6	12.7	43.7				
Cu <sub>27.5</sub> Fe <sub>27.5</sub> Zr <sub>45</sub>	2 days	Fe <sub>2</sub> Zr/Liquid	9.9	55.0	35.1	72.6	7.2	20.2				
Cu25Fe25Zr50	1 h	Fe <sub>2</sub> Zr/Liquid	5.7	62.2	32.1	23.6	19.8	56.6				
Cu10Fe40Zr50	2 days	Fe <sub>2</sub> Zr/Liquid	3.2	64.1	32.7	19.8	17.9	62.3				
Cu5Fe45Zr50	2 days	Fe <sub>2</sub> Zr/Liquid	1.3	65.5	33.2	8.9	25.5	65.6				
Cu <sub>9</sub> Fe <sub>9</sub> Zr <sub>82</sub>	2 days	(βZr)/Liquid	0.2	0.0	99.8	11.7	9.5	78.8				
Cu <sub>5</sub> Fe <sub>10</sub> Zr <sub>85</sub>	2 days	(βZr)/Liquid	0.1	0.0	99.9	7.8	12.1	80.1				
Cu <sub>5</sub> Fe <sub>5</sub> Zr <sub>90</sub>	2 days	(βZr)/Liquid	0.2	0.0	99.8	6.8	8.8	84.4				



Cu

(c)

20

40

60

Fe / at.%

80





Fe

(yFe)

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## 4. Conclusions

The isothermal sections of the Cu-Fe-Zr ternary system at 1000, 1100 and 1200 °C were experimentally determined by the means of EPMA and XRD. The area of liquid phase increases at the temperature ranging from 1000 to 1200 °C.

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