



# Investigation of Double RESURF P-GaN Gate AlGaIn/GaN Heterostructure Field-Effect Transistors with Partial N-GaN Channels

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## Abstract

In this paper, a double REduced SURface Field (RESURF) P-GaN gate AlGaIn/GaN heterostructure field-effect transistor with a partial N-GaN channel (DR-HFET) is proposed to improve the on-state performance in the high-voltage P-GaN gate AlGaIn/GaN heterostructure field-effect transistor (PG-HFET). The partial N-GaN channel between the gate and the drain increases the carrier density in the channel layer, and markedly reduces the on-resistance ( $R_{on}$ ). The P-top layer and the P-buffer layer modulate the distribution of the electric field along the GaN channel to achieve a high breakdown voltage. After validation of the simulation models and parameters, the DR-HFETs are optimized using the charge balance principle. The optimum DR-HFET with a gate-to-drain distance of  $L_{gd} = 6 \mu\text{m}$  shows a BV of 1100 V and  $R_{on}$  of 5.5  $\Omega \text{ mm}$ , which is 50.9% of the  $R_{on}$  in PG-HFET. The highest Baliga figure of merit (BFOM) of 2.3  $\text{GW/cm}^2$  is obtained when the channel charge density  $Q_{ch}$  is  $3.2 \times 10^{13} \text{ cm}^{-2}$  and the ratio of the P-top charge density  $Q_{pt}$  to the buffer charge density  $Q_{buf}$  is 1.625. We also examine the influence of the AlGaIn/GaN quality on the performance of the DR-HFETs. The simulation results indicate that the double RESURF structure may be less effective in the high-quality AlGaIn/GaN epitaxial layer. Overall, the DR-HFET shows a good balance between off-state blocking capability and on-state performance.

**Keywords** AlGaIn/GaN · heterostructure field-effect transistors · normally off · double RESURF · low on-resistance

## Introduction

In recent years, AlGaIn/GaN heterostructure-based power devices have attracted considerable attention due to the wide band gap and high critical field of GaN,<sup>1</sup> its high electron mobility in the two-dimensional electron gas (2DEG) channel,<sup>2–4</sup> and the low-cost fabrication of III-N epitaxy on silicon substrate.<sup>5</sup> Therefore, AlGaIn/GaN heterostructure field-effect transistors (HFETs) can operate at a high switching frequency ( $>1 \text{ MHz}$ ),<sup>6</sup> to reduce the volume of energy storage devices such as inductors and capacitors,<sup>7,8</sup> and miniaturize the power supply modules.<sup>9</sup> AlGaIn/GaN HFETs are already widely used in power supplies, electric vehicles, and fast chargers in consumer electronics.<sup>10–12</sup> The P-GaN gate AlGaIn/GaN HFET (PG-HFET) is a typical commercial

GaN power device, which can realize enhanced-mode operation by a simple and controllable fabrication process.<sup>8</sup> However, PG-HFETs often suffer from the concentration of the electric field (E-field) at the gate edge, which may cause a premature breakdown.<sup>13</sup>

Many recent research efforts have focused on improving the breakdown voltage (BV) of the PG-HFET using various approaches, including metal field plates,<sup>14,15</sup> junction or P-type field plates,<sup>16</sup> stripe array gates, and<sup>17</sup> alternate-island drains.<sup>18</sup> All these methods can smooth the E-field distribution along the channel and significantly improve the BV. However, these device structures often have a long drift region between the gate and the drain to withstand high voltages, resulting in relatively high on-resistance ( $R_{on}$ ). Therefore, improving the on-state performance of the high-voltage PG-HFET is essential.

The double REduced SURface Field (RESURF) structure is a widely used technology in high-voltage lateral diffusion metal–oxide–semiconductor field-effect transistors (LDMOSFET).<sup>19</sup> The double RESURF structure has a lateral N drift region that defines the  $R_{on}$  of the device and a vertical PNP structure which supports a space-charge

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depletion region enabling high breakdown voltage.<sup>20</sup> Compared to the single RESURF structure with a vertical PN junction, the double RESURF structure with a more highly doped N-drift region shows lower on-resistance under the same breakdown voltage.

In this work, we propose a double RESURF P-GaN gate AlGaIn/GaN HFET with a partial N-GaN (DR-HFET) channel to improve the BV and the  $R_{on}$  of the PG-HFETs. The partial N-GaN channel between the gate and the drain results in a remarkable reduction in the  $R_{on}$  by increasing the electron density in the channel layer. The P-top layer and the P-buffer layer modulate the distribution of the E-field along the N-type GaN channel to achieve a high breakdown voltage. After validation of the simulation models and parameters, the optimum DR-HFET achieves a BV of 1100 V and  $R_{on}$  of 5.5  $\Omega$  mm, while the PG-HFETs produce a BV of 600 V and  $R_{on}$  of 10.8  $\Omega$  mm under the same gate-to-drain distance of 6  $\mu$ m. We then discuss the influence of the AlGaIn/GaN quality on the performance of the DR-HFETs. When the quality of the AlGaIn/GaN epitaxial layer is improved, the relative reduction of  $R_{on}$  decreases from 53% to 40%, and the relative increase in BFOM decreases from 6.1 times to 4.6 times. The simulation results indicate that the double RESURF structure may be less effective in the high-quality AlGaIn/GaN epitaxial layer. Finally, we propose a series of fabrication steps for the DR-HFET, in which the fabrication of DR-HFETs may have more steps than that of PG-HFETs.

## Device Structures, Simulation Models and Mechanism

### Device Structures

The structures of the PG-HFET and the proposed DR-HFET are shown schematically in Fig. 1. The structure

parameters of the PG-HFET are consistent with reported results.<sup>21</sup> For vertical epitaxial layers, both structures are composed of a 2.6- $\mu$ m-thick GaN buffer layer, a 300-nm GaN channel layer, and a 12.5-nm AlGaIn barrier layer with 25% Al content. The gate stack is formed by an 80-nm-thick P-type GaN layer with a hole concentration of  $1 \times 10^{18}$   $\text{cm}^{-3}$ . The  $\text{Si}_3\text{N}_4$  passivation layer with a thickness of 500 nm is located on the top of the devices.

For the lateral structure parameters, both HFETs have a source and drain length ( $L_C$ ) of 1  $\mu$ m. The gate length ( $L_G$ ) is set as 0.8  $\mu$ m. The gate-to-source distance ( $L_{GS}$ ) and gate-to-drain distance ( $L_{GD}$ ) of the devices are defined as 0.75 and 6  $\mu$ m, respectively. As shown in Fig. 1b, the proposed DR-HFETs have a P-AlGaIn top layer, a partially doped N-GaN channel layer between the gate and the drain, and a P-type GaN buffer layer to form a double RESURF structure. All the structure parameters are given in Table 1.

### Simulation Models and Validation

The technology computer-aided design (TCAD) simulation was conducted using the Shockley–Read–Hall (SRH) model to calculate the carrier generation and recombination, and the carrier in the simulated devices obey Fermi–Dirac statistics. The high field mobility and the polarization model of the III-N materials was adopted with default parameter values from the Silvaco ATLAS TCAD tool.<sup>22,23</sup> Acceptor-like traps of 0.59 eV under the conduction band were added into the buffer layer of the PG-HFET with density of  $1 \times 10^{16}$   $\text{cm}^{-3}$ .<sup>24</sup>

The Selberherr impact ionization model was used to emulate the breakdown characteristics of the GaN-based electronic devices.<sup>25</sup> The impact ionization coefficients for electrons ( $\alpha_n$ ) and holes ( $\alpha_p$ ) are based upon the following expressions.

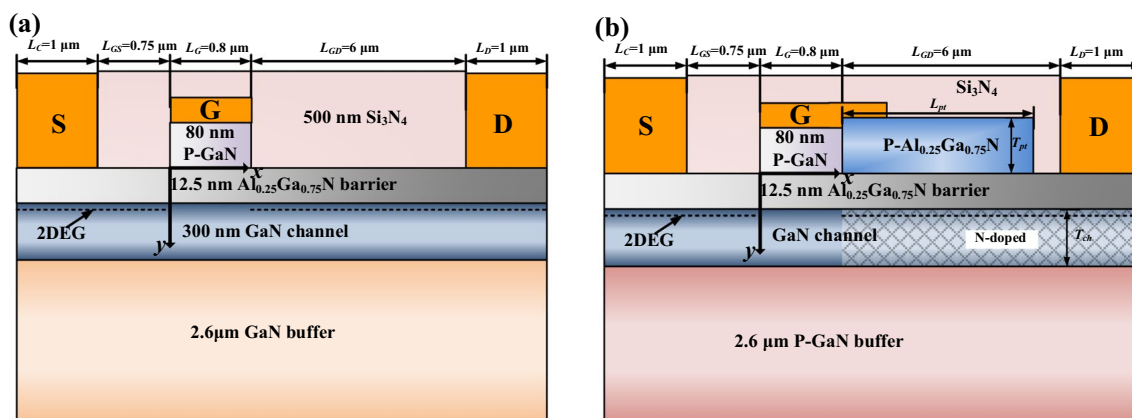


Fig. 1 Device structures of (a) PG-HFETs, (b) DR-HFETs.

**Table I** Simulated device specifications

Parameters	Values	Parameter captions
$L_G$	0.8 $\mu\text{m}$	Gate length
$L_{GS}$	0.75 $\mu\text{m}$	Distance from gate to source
$L_{GD}$	6 $\mu\text{m}$	Distance from gate to drain
$T_{\text{barr}}$	12.5 nm	Thickness of $\text{Al}_{0.25}\text{Ga}_{0.75}\text{N}$ barrier layer
$T_{\text{buf}}$	2.6 $\mu\text{m}$	Thickness of GaN buffer layer
$T_{\text{GaN}}$	80 nm	Thickness of P-GaN gate
$N_{\text{pGaN}}$	$1 \times 10^{18} \text{ cm}^{-3}$	Density of holes in the P-GaN gate
$N_{\text{pt}}$	$3.6\text{--}6.8 \times 10^{17} \text{ cm}^{-3}$	Density of holes in the P-top layer
$T_{\text{pt}}$	500 nm	Thickness of the P-top layer
$L_{\text{pt}}$	1–5.6 $\mu\text{m}$	Length of the P-top layer
$T_{\text{ch}}$	100–500 nm	Thickness of the channel layer
$N_{\text{ch}}$	$0.01\text{--}100 \times 10^{18} \text{ cm}^{-3}$	Density of electrons in the N-GaN channel
$N_{\text{buf}}$	$3.1\text{--}9.2 \times 10^{16} \text{ cm}^{-3}$	Density of holes in the buffer layer

$$\alpha_n = a_n \exp \left[ - \left( \frac{b_n}{E} \right)^m \right], \tag{1}$$

$$\alpha_p = a_p \exp \left[ - \left( \frac{b_p}{E} \right)^m \right], \tag{2}$$

where  $E$  is the electric field in the direction of current flow at a particular position in the structure, and  $a_n$ ,  $a_p$ ,  $b_n$ ,  $b_p$ ,  $m$  are parameters. The parameters were set as  $a_n = a_p = 1.1438 \times 10^7 \text{ cm}^{-1}$ ,  $b_n = b_p = 23.8933 \text{ MV/cm}$  and  $m = 1$ .<sup>26</sup>

The Lombardi mobility model was conducted as the low field mobility model in the simulation.<sup>27</sup> In the Lombardi mobility model, the electron mobility is limited by the surface acoustic phonon scattering mobility  $\mu_{\text{ac}}$ , doping-dependent bulk carrier mobility  $\mu_{\text{b}}$  and interface roughness scattering  $\mu_{\text{int}}$ . The total electron mobility  $\mu_n$  was calculated using Matthiessen’s rule.

$$\frac{1}{\mu_n} = \frac{1}{\mu_{\text{ac}}} + \frac{1}{\mu_{\text{b}}} + \frac{1}{\mu_{\text{int}}}, \tag{3}$$

$$\mu_{\text{ac}} = \left( B \frac{T}{E_{\perp}} + C \frac{1}{E_{\perp}^{1/3}} \right) \frac{1}{T}, \tag{4}$$

$$\mu_{\text{b}} = \mu_0 + \frac{\mu_{\text{max}} - \mu_0}{1 + (N/C_r)^{\alpha 1}}, \tag{5}$$

$$\mu_{\text{int}} = \frac{\delta}{E_{\perp}^2}, \tag{6}$$

where  $E_{\perp}$  is the transverse field,  $T$  is the temperature,  $\mu_{\text{max}}$  is the Hall mobility at room temperature,  $N$  is the impurity concentration of the semiconductor, and  $B$ ,  $C$ ,  $\mu_0$ ,  $C_r$ ,  $\alpha 1$ ,

**Table II** Parameters for  $\mu_{\text{ac}}$ ,  $\mu_{\text{b}}$ , and  $\mu_{\text{int}}$  in the mobility model

Parameters	Units	Values
$B$	cm/s	$2.6 \times 10^7$
$C$	K cm/s	$3.3 \times 10^2$
$\mu_{\text{max}}$	$\text{cm}^2/\text{V s}$	1600
$\mu_0$	$\text{cm}^2/\text{V s}$	100
$C_r$	$\text{cm}^{-3}$	$9.68 \times 10^{16}$
$\alpha 1$		0.7
$\delta$	V/s	$4.6 \times 10^{14}$

$\delta$  are fitting parameters. The values of  $\mu_0$ ,  $C_r$  and  $\mu_{\text{max}}$  are defined based upon other research results.<sup>28–30</sup> We tuned the parameters of  $B$ ,  $C$ ,  $\alpha 1$  and  $\delta$  to fit the experimental results reported by Li et al.<sup>21</sup>. The parameters used in the Lombardi mobility model are listed in Table II.

The validation of our simulation was conducted by comparison of the simulation curve and the experimental data for PG-HFETs reported by Li et al.<sup>21</sup> The validation results are illustrated in Fig. 2. The PG-HFET has a threshold voltage  $V_{\text{TH}}$  of 1.6 V, a linear area current  $I_{\text{dlin}}$  of 9.3 mA/mm and a BV of 600 V. The method for calculating  $R_{\text{on}}$  is to divide the  $V_{\text{DS}}$  by the  $I_{\text{dlin}}$  current. During the transfer curves simulation, the  $V_{\text{DS}}$  was set as 0.1 V, and the  $R_{\text{on}}$  was obtained as 10.8  $\Omega \text{ mm}$ . These simulation results match the characteristics of the experimental results reported by Li et al.<sup>21</sup> As shown in Fig. 2, the output (Fig. 2a), transfer (Fig. 2b), and off-state (Fig. 2c) characteristics of the PG-HFET are basically consistent with the experimental results.

### Device Mechanism

The electron density and band diagram at  $x = 4 \mu\text{m}$  for the PG-HFETs, the PG-HFETs with only N-GaN channels (NC-HFET) and the DR-HFETs are compared and discussed in

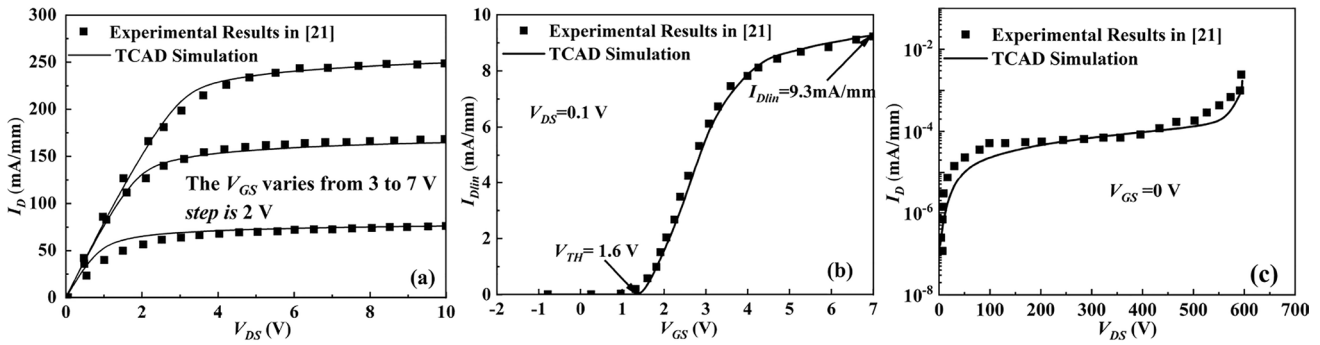


Fig. 2 Simulation validation by comparison of the experimental curves of (a) output (b) transfer (c) off-state characteristics.

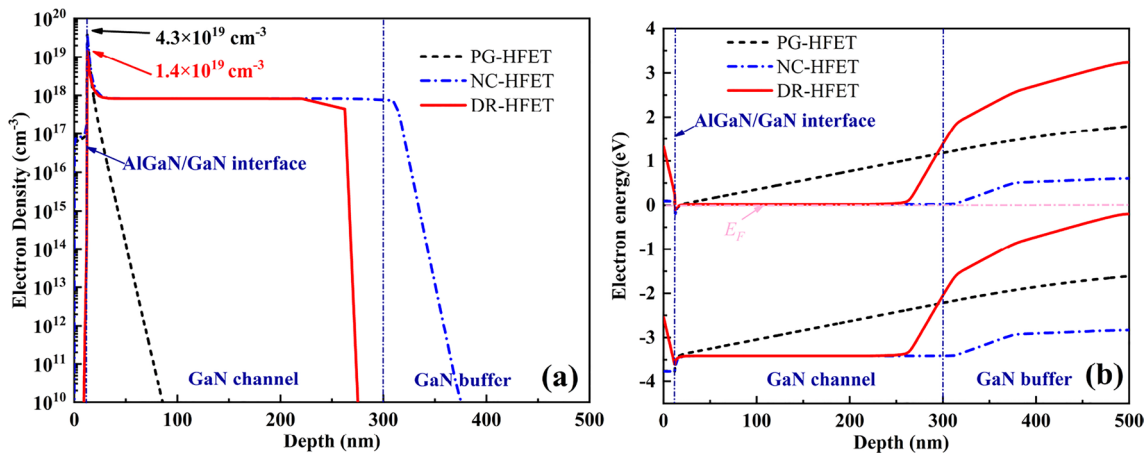


Fig. 3 (a) Electron density and (b) band diagram of the PG-HFET, NC-HFET and DR-HFET with a  $T_{ch}$  of 300 nm in thermal equilibrium.

Fig. 3 under thermal equilibrium conditions. As shown in Fig. 3a, the NC-HFET and DR-HFET have partial N-GaN channels with an electron concentration  $N_{ch}$  of  $8 \times 10^{17} \text{ cm}^{-3}$ , which is placed between the gate and the drain; thus the channel electron density in the NC-HFET and DR-HFET become much higher than that of the PG-HFET. For the DR-HFET, the P-top layer induces a decrease in 2DEG density, and the P-buffer layer can extend the depletion region in the channel layer. Therefore, DR-HFETs may have a lower  $R_{on}$  than PG-HFET but a higher  $R_{on}$  than NC-HFET. In Fig. 3b, it is obvious that the DR-HFETs have the highest electron barrier in the buffer layer due to a concentration of  $6.2 \times 10^{16} \text{ cm}^{-3}$  acceptors in the P-GaN buffer, and thus DR-HFETs may show low leakage current.

Figure 4 illustrates the results of our in-depth research on the relationship between the structural parameters of the N-GaN channel and  $R_{on}$  in the NC-HFETs. When the  $N_{ch}$  and the  $T_{ch}$  of the N-GaN channel increase, the  $R_{on}$  decreases monotonically. When  $R_{on}$  is lower than  $\sim 4 \Omega \text{ mm}$ , a larger change in  $N_{ch}$  or  $T_{ch}$  has a relatively smaller impact on the  $R_{on}$ , and it is inefficient to reduce  $R_{on}$  by increasing the  $N_{ch}$  or  $T_{ch}$  of the N-GaN channel. Therefore, the benefit threshold

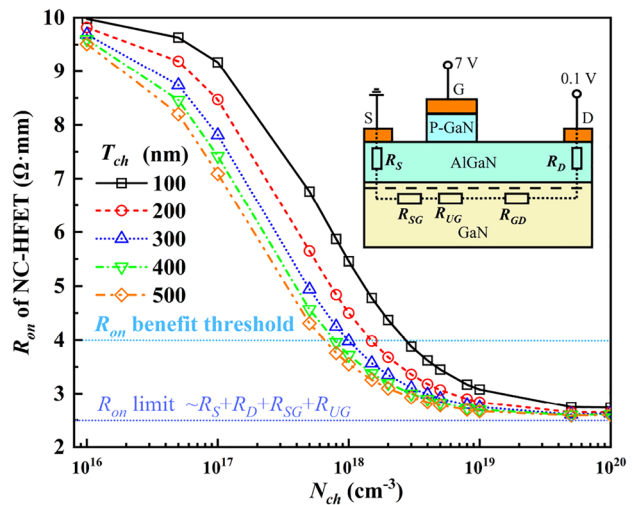


Fig. 4 The  $T_{ch}$  and  $N_{ch}$  dependence of the  $R_{on}$  in the NC-HFET.

of  $R_{on}$  is obtained as  $4 \Omega \text{ mm}$ , and we choose  $T_{ch} = 400 \text{ nm}$ ,  $N_{ch} = 8 \times 10^{17} \text{ cm}^{-3}$  as the optimum value of the N-GaN channel.

In Fig. 4, the  $R_{on}$  of the PG-HFET can be expressed as

$$R_{on} = R_S + R_D + R_{SG} + R_{UG} + R_{GD}, \quad (7)$$

where  $R_S$  and  $R_D$  are the resistance between the metal contacts and the 2DEG channel,  $R_{SG}$  and  $R_{GD}$  are the access region resistance, and  $R_{UG}$  is the channel resistance under the gate. Although increasing  $T_{ch}$  and  $N_{ch}$  can reduce the  $R_{GD}$ ,  $R_{on}$  is limited to  $\sim 2.5 \Omega \cdot \text{mm}$ , where the sum of  $R_S$ ,  $R_D$ ,  $R_{SG}$  and  $R_{UG}$  become the main part of the  $R_{on}$  in the NC-HFETs.

## Results and Discussion

### Device Characteristics and Optimization

The DC characteristics of the PG-HFETs, NC-HFETs and DR-HFETs are illustrated in Fig. 5. DR-HFETs and PG-HFETs have a  $T_{ch}$  of 400 nm, a  $N_{ch}$  of  $8 \times 10^{17} \text{ cm}^{-3}$ . According to the charge balance principle of the RESURF structure, the DR-HFETs are optimized and have a total charge density in P-top layer  $Q_{tp}$  of  $2.6 \times 10^{13} \text{ cm}^{-2}$  ( $N_{pt} = 5.2 \times 10^{17} \text{ cm}^{-3}$ ,  $T_{pt} = 500 \text{ nm}$ ), and a total charge density in P-GaN buffer layer  $Q_{buf}$  of  $1.6 \times 10^{13} \text{ cm}^{-2}$  ( $N_{buf} = 6.2 \times 10^{16} \text{ cm}^{-3}$ ,  $T_{buf} = 2.6 \mu\text{m}$ ).

Facilitated by the high electron density in the N-GaN channel, the NC-HFET and DR-HFET show a higher saturation current  $I_{dsat}$  and a lower  $R_{on}$  than that of PG-HFET. As shown in Fig. 5a, owing to the electron depletion caused by the P-top and P-buffer layer, a degradation of on-state performance can be observed in the DR-HFET. In Fig. 5b, the  $R_{on}$  is extracted by the transfer characteristic at  $V_{DS} = 0.1 \text{ V}$ . The  $R_{on}$  of the NC-HFET is achieved as  $\sim 4 \Omega \cdot \text{mm}$ , which is the benefit threshold value mentioned in above section. Then,

the DR-HFET have a  $R_{on}$  of  $5.5 \Omega \cdot \text{mm}$ , which is 50.9% that of PG-HFET, indicated that double RESURF structure can significantly reduce the  $R_{on}$ . As shown in Fig. 5b, the threshold voltage  $V_{TH}$  of the PG-HFET and NC-HFET is 1.6 V with non-doped GaN buffers, while the  $V_{TH}$  of the DR-HFET becomes 1.7 V due to the P-type doping in the buffer layer.

The off-state breakdown characteristics of PG-HFETs, NC-HFETs and DR-HFETs are compared at  $V_{GS} = 0 \text{ V}$  in Fig. 6. The BV is extracted when the reverse leakage current reaches  $1 \mu\text{A}/\text{mm}$ . The on-state and off-state simulations have identical structural parameters. As shown in Fig. 6a, the DR-HFETs show a BV of 1100 V, while the PG-HFETs have a BV of 600 V. Compared to the PG-HFETs and NC-HFETs, the DR-HFETs display reverse leakage current of  $\sim 10^{-6} \text{ mA}/\text{mm}$  at  $V_{DS} = 600 \text{ V}$ , which indicates that the P-GaN buffer can effectively suppress the leakage currents. The E-field distribution along the channel at  $y = 13 \text{ nm}$  is shown in Fig. 6b. When breakdown occurs, all devices have the maximum E-field strength of  $\sim 3.4 \text{ MV}/\text{cm}$ . It is clearly shown that the E-field distribution of the DR-HFET spread more uniformly than that of the PG-HFETs and the NC-HFETs; thus, the DR-HFETs have the highest BV of 1100 V among all three kinds of HFETs.

The potential distributions of PG-HFET and the proposed DR-HFET at  $V_{DS} = 600 \text{ V}$  are shown in Fig. 7. For the PG-HFET in Fig. 7a, the potential contours are closely packed at the gate edge due to the incomplete depletion of the gate-to-drain access region, which suggests the crowding of the electric field lines at the gate edge. As shown in Fig. 7b, the potential distribution of the DR-HFETs is more uniform than that of the PG-HFETs. It can be observed that the potential contours are relatively concentrated at the gate edge and the P-top edge. Therefore, two electric field peaks at these edges can also be found in the E-field distribution of the DR-HFETs in Fig. 6b.

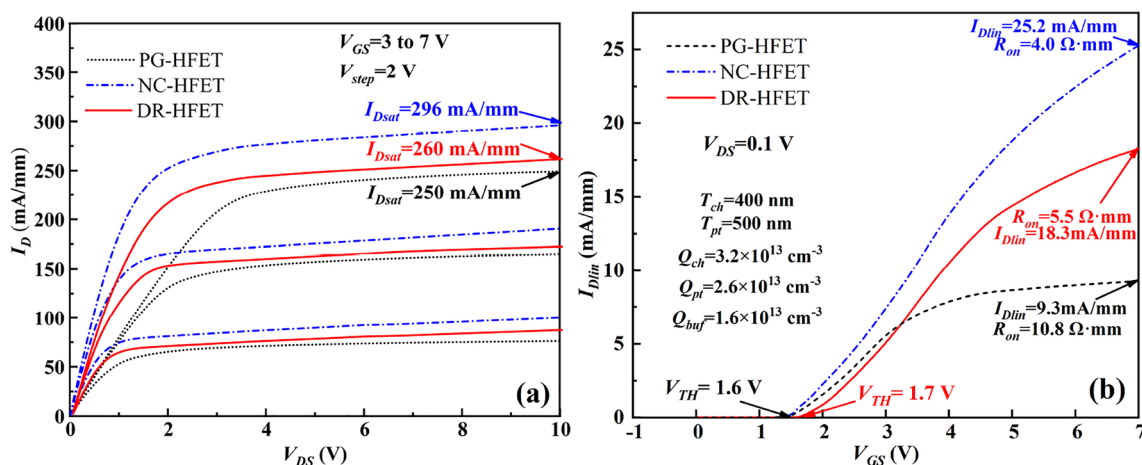


Fig. 5 The DC characteristics of PG-HFETs, NC-HFETs and DR-HFETs: (a) output curves, (b) transfer curves.



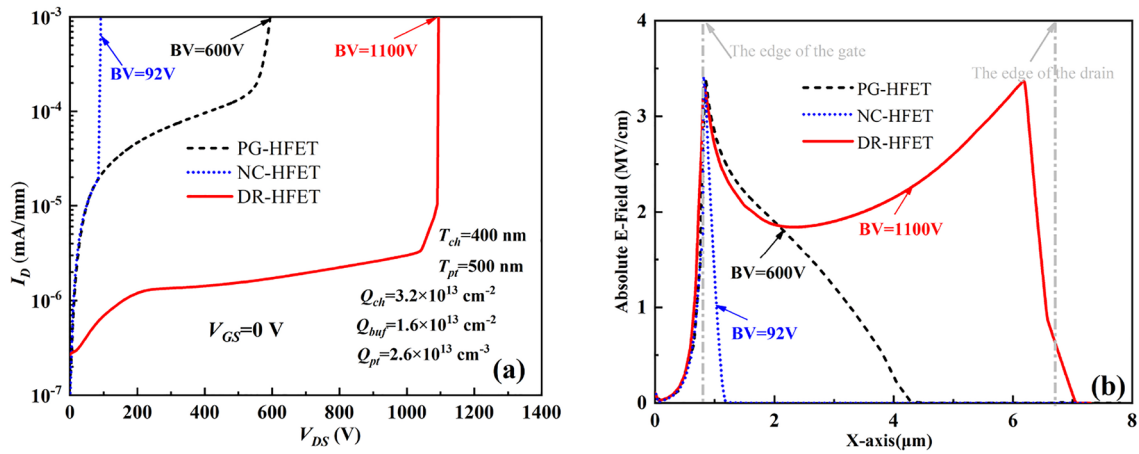


Fig. 6 (a) The BV curves, (b) the E-field distribution along the channel of the PG-HFETs, NC-HFETs and DR-HFETs at the BV.

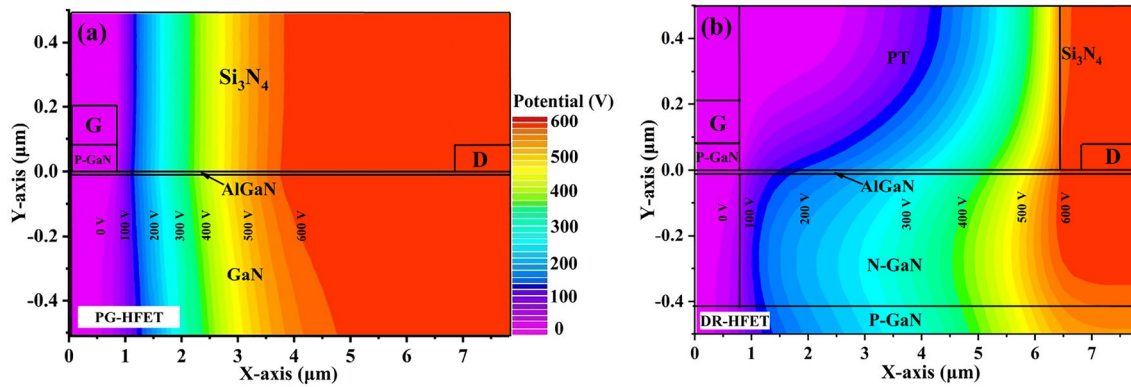


Fig. 7 Potential distribution at  $V_{DS}=600$  V: (a) PG-HFETs, (b) DR-HFETs.

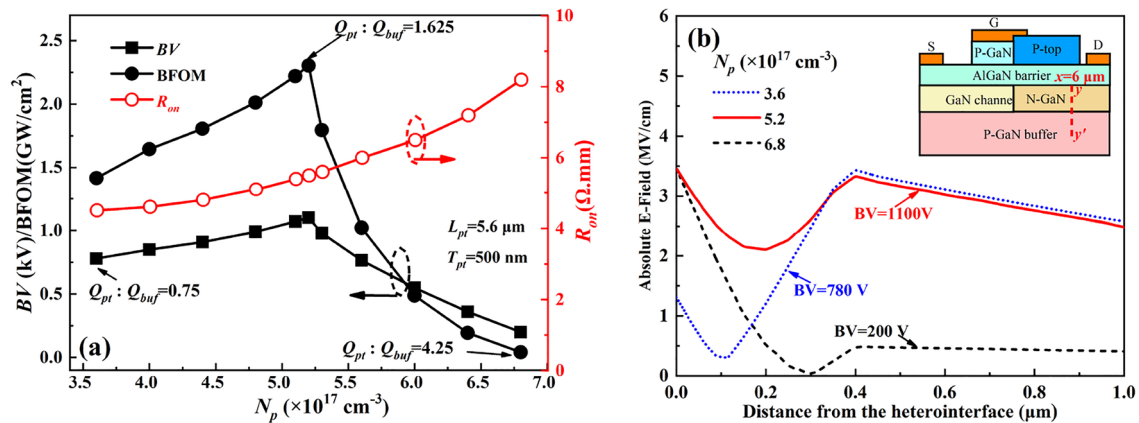


Fig. 8 (a) The  $N_p$  dependence of the BV,  $R_{on}$  and BFOM with charge balance at  $T_{pt}=500$  nm, and (b) the E-field distribution at  $x=6$   $\mu$ m with different  $N_p$ .

In Figs. 8 and 9, we optimize the structure parameters of the DR-HFETs. The optimization of hole concentration  $N_p$  in the P-top layer is shown in Fig. 8a. It should be noted that the optimization of  $N_p$  is in accordance with the charge balance principle. Once a value of  $N_p$  is defined, the hole concentration of the P-buffer layer  $N_{\text{buf}}$  can be expressed as

$$N_{\text{buf}} = \frac{N_{\text{ch}} \cdot T_{\text{ch}} - N_p \cdot T_{\text{pt}}}{T_{\text{buf}}}, \quad (8)$$

where  $N_{\text{ch}} = 8 \times 10^{17} \text{ cm}^{-3}$ ,  $T_{\text{ch}} = 400 \text{ nm}$ , and  $T_{\text{pt}}$  is the thickness of the P-top layer. The  $T_{\text{pt}}$  has no influence on  $R_{\text{on}}$ . When a thick P-top layer is grown, the  $N_p$  can be smaller upon the same  $Q_{\text{pt}}$ . When the value of  $N_p$  is relatively small, the depletion effect of the P-top layer on the N-GaN channel is decreased, and the DR-HFET will show a low  $R_{\text{on}}$ . Therefore, the  $T_{\text{pt}}$  is set as 500 nm, which was the highest value in our previous work.<sup>16</sup> The  $T_{\text{buf}}$  is the thickness of the P-GaN buffer layer, which is defined as 2.6  $\mu\text{m}$  in the compared experimental PG-HFETs.

When the charge balance principle is followed during the optimization, the proportion of  $Q_{\text{pt}}$  to  $Q_{\text{buf}}$  has an optimum value of 1.625 (2.6:1.6). According to the double RESURF theory, the selection of the charge density in P-top and P-sub should maintain the full depletion in the N-drift region under the breakdown voltage. For a uniformly doped drift region, the charge in the P-top layer is usually half of that in the drift region.<sup>20</sup> However, there is a 2DEG channel in the N-GaN drift region of the DR-HFET in our simulation, so the determination of  $Q_{\text{pt}}$  should ensure the depletion of both the 2DEG channel and the half of the N-GaN drift region. The charge density in the 2DEG channel  $Q_{\text{2DEG}}$  is calculated as  $\sim 1 \times 10^{13} \text{ cm}^{-2}$  in our simulation.<sup>16</sup> Thus, the optimum value of  $Q_{\text{pt}}$  should be the sum of  $Q_{\text{2DEG}}$  and  $1/2Q_{\text{ch}}$ , and is calculated as  $2.6 \times 10^{13} \text{ cm}^{-2}$ . The above results can also

be confirmed in the vertical E-field distribution between  $y-y'$  under the heterointerface at  $x = 6 \mu\text{m}$  in Fig. 7b. When  $N_p = 3.6$  or  $6.8 \times 10^{17} \text{ cm}^{-3}$ , high E-field strength can be observed only at the N-GaN/P-buffer interface or only at the AlGaN/GaN heterointerface. When the  $N_p = 5.2 \times 10^{17} \text{ cm}^{-3}$ , two E-field peaks can be found, at both the N-GaN/P-buffer interface and AlGaN/GaN heterointerface; thus the DR-HFET with  $N_p = 5.2 \times 10^{17} \text{ cm}^{-3}$  shows a relatively uniform distribution of the E-field in the vertical direction.

The  $L_{\text{pt}}$  dependence of the BV,  $R_{\text{on}}$  and BFOM is shown in Fig. 9a. When the  $L_{\text{pt}}$  increases from 1  $\mu\text{m}$  to 5.8  $\mu\text{m}$ , the value of the BV,  $R_{\text{on}}$  and BFOM increase monotonically. The reason for the increase in BV can be found in Fig. 9b. When the  $L_{\text{pt}}$  increases, the depletion region under the P-top also extends several microns in the lateral direction, so the E-field along the channel can spread more uniformly, thus improving the BV. Therefore, the optimum  $L_{\text{pt}}$  is obtained as 5.8  $\mu\text{m}$  in our simulation.

In comparison with other experimental P-GaN gate AlGaN/GaN HFETs in the literature (Fig. 10),<sup>14,15,17,18,21,31-35</sup> our device shows a high BV of 1100 V with a remarkably low  $R_{\text{on,sp}}$  of  $0.53 \text{ m}\Omega \text{ cm}^2$ , leading to a BFOM of  $2.3 \text{ GW/cm}^2$ , which suggests a good balance between the off-state blocking capability and on-state performance.

### The Influence of the AlGaN/GaN Quality

Epitaxial growth methods and fabrication process parameters may influence the quality of the AlGaN/GaN heterostructure. Typical growth methods for AlGaN/GaN include molecular-beam epitaxy (MBE) and metal-organic vapor-phase epitaxy (MOVPE), and the low field mobility is most affected by different growth methods.<sup>36</sup> According to experimental results, the electron mobility may vary from

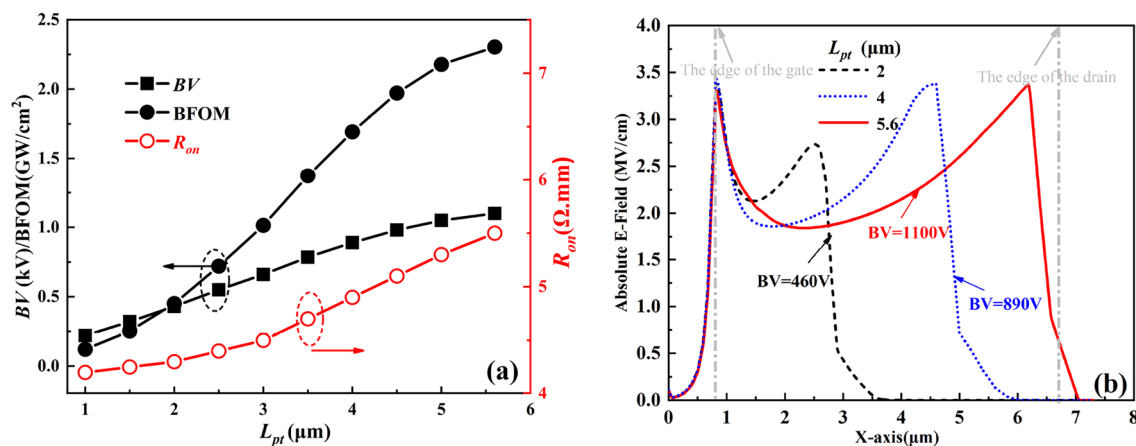


Fig. 9 (a) The  $L_{\text{pt}}$  dependence of the BV,  $R_{\text{on}}$  and BFOM, and (b) the E-field distribution at  $y = 13 \text{ nm}$  with different  $L_{\text{pt}}$ .

2000 cm<sup>2</sup>/(V s) to 500 cm<sup>2</sup>/(V s) under different growth conditions.

In our simulation, we use the Lombardi model to calculate the mobility under low electric field conditions. As described in the Lombardi model, the electron mobility is limited by surface acoustic phonon scattering, doping-dependent scattering and interface roughness scattering, while surface acoustic phonon scattering and interface roughness scattering are related to the quality of the AlGaIn/GaN heterostructure.<sup>36</sup> Therefore, we tune the parameters of *B*, *C* and  $\delta$  in the Lombardi model to simulate the impact of the AlGaIn/GaN material quality. Otherwise, we make no changes to the  $\mu_{max}$ ,  $\mu_0$ , *C<sub>t</sub>* or  $\alpha 1$  values in the doping-dependent scattering part of the Lombardi model during the low field mobility simulation. Finally, the low field electron

mobility  $\mu_n$  varies from 500 cm<sup>2</sup>/(V s) to 2000 cm<sup>2</sup>/(V s) when we tune the parameters in the simulation.

Figure 11a shows the relationships between the *R<sub>on</sub>* and the *N<sub>ch</sub>* and *T<sub>ch</sub>* of the NC-HFETs with varied  $\mu_n$ . The  $\mu_n$  in the previous simulation results is 700 cm<sup>2</sup>/(V s). When the growth quality of the AlGaIn/GaN is improved, the  $\mu_n$  will increase while the *R<sub>on</sub>* of PG-HFET will decrease. When the mobility is higher, the *R<sub>on</sub>* of the PG-HFET is lower, and thus the impact of the *N<sub>ch</sub>* and the *T<sub>ch</sub>* on the *R<sub>on</sub>* is decreased. When  $\mu_n = 2000$  cm<sup>2</sup>/(V s), the *R<sub>on</sub>* of the PG-HFET is 14.2 Ω mm, and when  $\mu_n = 500$  cm<sup>2</sup>/(V s), the *R<sub>on</sub>* of the PG-HFET is 3.5 Ω mm. After considering the benefit threshold of *R<sub>on</sub>*, by increasing the channel doping concentration, the *R<sub>on</sub>* of the NC-HFET with  $\mu_n = 500$  cm<sup>2</sup>/(V s) can be reduced by 8.4 Ω mm, while for the NC-HFET with  $\mu_n = 2000$  cm<sup>2</sup>/(V s), the *R<sub>on</sub>* can be reduced from 3.5 Ω mm to 1.5 Ω mm. When *T<sub>ch</sub>* = 400 nm, the optimum *N<sub>ch</sub>* is around  $\sim 8 \times 10^{17}$  cm<sup>-3</sup>, while the *R<sub>on</sub>* for each NC-HFET with different  $\mu_n$  reaches the benefit threshold. Therefore, when the quality of the material is improved, the effects of the *R<sub>on</sub>* reduction by increasing *N<sub>ch</sub>* or *T<sub>ch</sub>* become weak.

As shown in Fig. 11b, when the  $\mu_n$  increases to 2000 cm<sup>2</sup>/(V s), the *I<sub>dlin</sub>* of the DR-HFET reaches 47.6 mA/mm, while the *R<sub>on</sub>* of the devices is as low as 2.1 Ω mm. The reduction in *R<sub>on</sub>* with the double RESURF structure is 1.4 Ω mm, which is the lowest *R<sub>on</sub>* improvement among the emulated DR-HFETs.

The graph inset in Fig. 11b shows the dependence of the relative increase in the *R<sub>on</sub>* and BFOM on the  $\mu_n$ . It should be noted that the relationship between the BV and the material quality is unclear. If the GaN buffer is of poor quality, the buffer leakage current may increase, causing a premature breakdown.<sup>37</sup> Otherwise, in our simulation case, we add acceptor traps into the GaN buffer of the PG-HFETs, and we

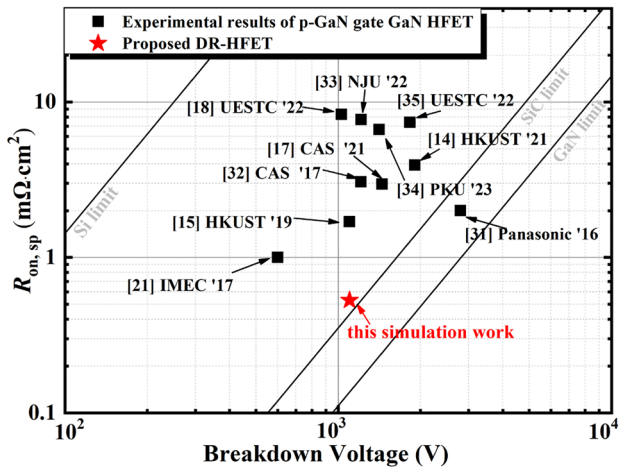


Fig. 10 Comparison plots of BV versus *R<sub>on,sp</sub>* for the P-GaN gate HFET.

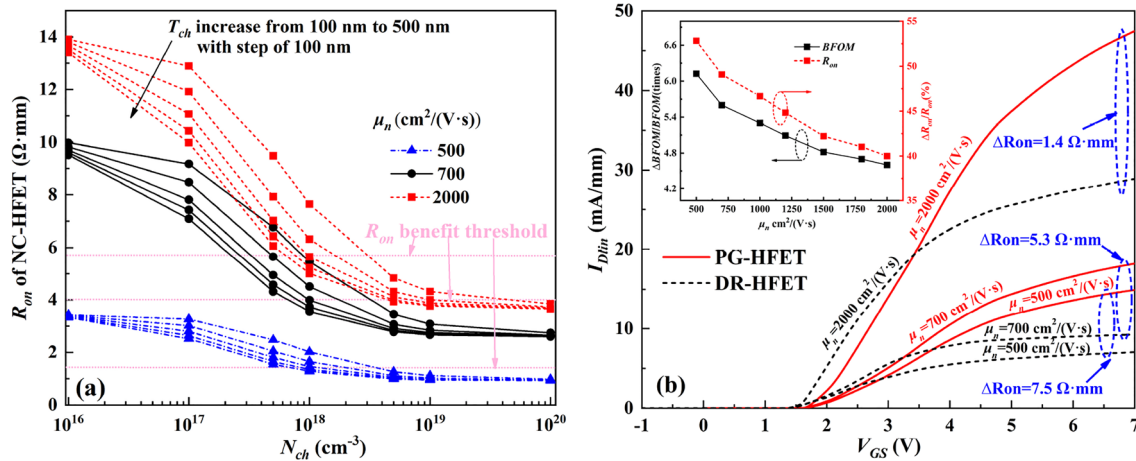
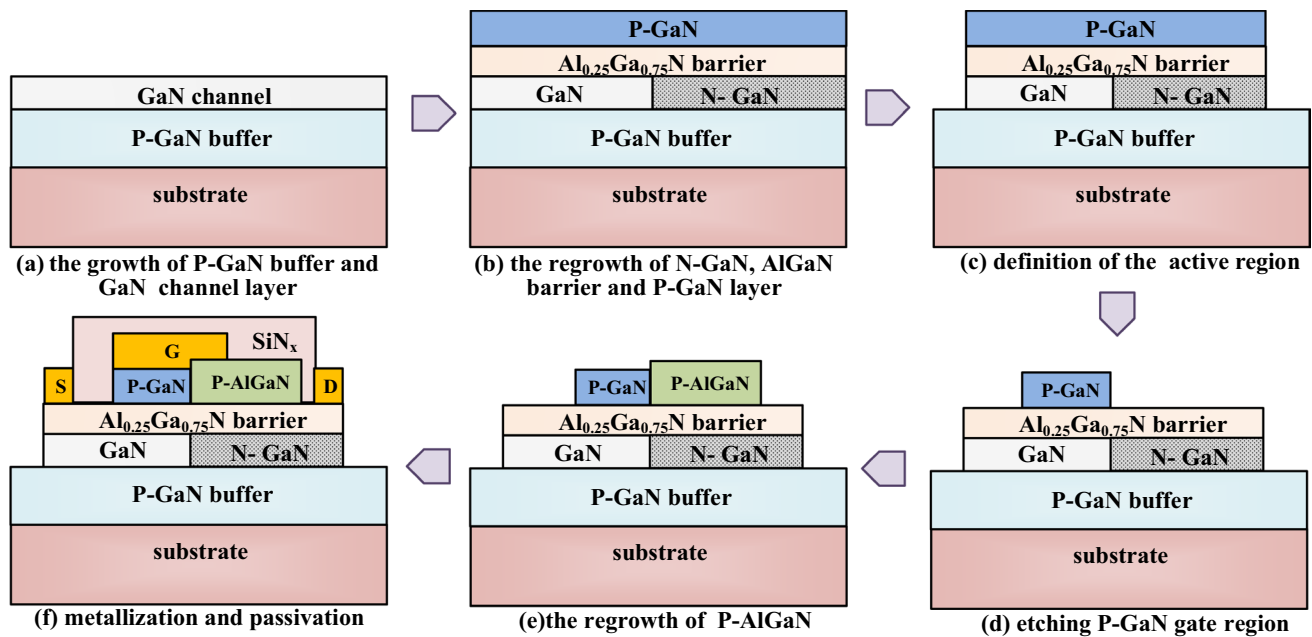


Fig. 11 (a) The relationships between the *R<sub>on</sub>* and the *N<sub>ch</sub>* and *T<sub>ch</sub>* of the NC-HFETs with varied electron mobility  $\mu_n$ , and (b) the dependence of PG-HFETs and transfer curves, the relative variation of the *R<sub>on</sub>* and the BFOM on the  $\mu_n$ .





**Fig. 12** Schematic for the fabrication steps of the DR-HFET: (a) the growth of P-GaN buffer and GaN channel layer, (b) the regrowth of N-GaN, AlGaIn barrier and P-GaN layer, (c) the definition of the

active region, (d) etching P-GaN gate region, (e) the regrowth of P-AlGaIn, (f) metallization and passivation.

use P-GaN as a buffer layer in the DR-HFETs. The P-GaN buffer or acceptor trap-doped buffer shows low leakage current, and avoids premature breakdown.<sup>38,39</sup> Thus, in our simulation case, the BV of the PG-HFETs remains 600 V, while the BV of the DR-HFETs remains 1100 V. When the  $\mu_n$  increases from  $500 \text{ cm}^2/(\text{V s})$  to  $2000 \text{ cm}^2/(\text{V s})$ , the relative reduction of the  $R_{\text{on}}$  decreases from 53% to 40%, while the relative increase in the BFOM decreases from 6.1 times to 4.6 times. Therefore, the enhancement of forward characteristics and BFOM of the DR-HFETs would gradually weaken when the quality of the AlGaIn/GaN is improved.

### Key Fabrication Steps

Figure 12 shows the main fabrication steps for the DR-HFET. After growth of the P-GaN buffer/GaN channel epitaxy by metal–organic chemical vapor deposition (MOCVD) (Fig. 12a), the Si-doped GaN channel, the AlGaIn barrier and the P-GaN are regrown on the dielectric patterned wafer after selective etching of the GaN channel (Fig. 12b). Then, mesa isolation is conducted to define the active region of the devices (Fig. 12c). The P-GaN gate region is formatted after selective etching of the P-GaN layer (Fig. 12d). Then, a patterned dielectric is deposited after a surface treatment, and the patterned dielectric is used to perform selective area growth of P-AlGaIn (Fig. 12e). Finally, a passivation layer is deposited and patterned after the formation of metal contacts (Fig. 12f).

### Conclusion

A method for improving on-state performance utilizing double RESURF technology is presented for a P-GaN gate GaN HFET by TCAD simulation. With the simulation validation and the optimization of the  $Q_{\text{ch}}$ ,  $Q_{\text{pt}}$  and  $Q_{\text{buf}}$  in the double RESURF structure, a BV of 1100 V and BFOM of  $2.3 \text{ GW/cm}^2$  can be achieved, which indicates a good balance between off-state blocking capability and on-state performance.

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