ORIGINAL RESEARCH ARTICLE



High Thermoelectric Performance of Large Size Bi₂Te_{2.7}Se_{0.3} Alloy Ingots

Wanwan Zhang¹ · Xin Liu¹ · Zengguo Tian¹ · Yingjiu Zhang¹ · Xin-Jian Li¹ · Hongzhang Song¹

Received: 23 November 2022 / Accepted: 29 June 2023 / Published online: 25 July 2023 © The Minerals, Metals & Materials Society 2023

Abstract

 Bi_2Te_3 -based alloys are currently the best room-temperature thermoelectric materials, and have been used widely in the field of thermoelectric refrigeration. Bi_2Te_3 ingots prepared by the zone-melting method provide convenience for large-scale commercial application. Currently, one trend is that the dimensionless thermoelectric figure-of-merit (*ZT*) value of the *n*-type $Bi_2Te_{2.7}Se_{0.3}$ is slightly lower than that of the *p*-type $Bi_{0.5}Sb_{1.5}Te_3$. In this paper, *n*-type $Bi_2Te_{2.7}Se_{0.3}$ alloy ingots with large size were successfully prepared through the optimized zone-melting preparation process, and achieved a high *ZT* value of 1.16 at 360 K. This value is higher than all the *n*-type Di_2Te_3 -based ingots in current commercial applications.

Keywords Thermoelectric $\cdot Bi_2Te_{2.7}Se_{0.3} \cdot large size ingots \cdot commercial applications$

Introduction

The ever-increasing population and rapidly developing economy have greatly increased the demand for energy and will inevitably bring about a series of environmental pollution problems. Energy diversification and efficient multilevel utilization have become an effective approach to solve the energy gap without adding additional environmental burdens.^{1,2} Thermoelectric materials can realize the direct conversion between thermal energy and electric energy.³ For example, it can convert a large amount of waste heat and residual heat which are difficult to utilize in industry into electric energy⁴, and has attracted extensive attention from industry and academia.⁵ Thermoelectric materials are mainly used in the fields of thermoelectric power generation and thermoelectric cooling.⁶ Due to their irreplaceable advantages and characteristics, such as adaptability, diversity, and reliability, thermoelectric materials are receiving unprecedented expectations as the key technology supporting many modern industries.7-9

The conversion efficiency of a thermoelectric material is characterized by its dimensionless thermoelectric figure-of-merit (ZT) value. The ZT value is closely related to mainly physical quantities, such as resistivity (ρ), Seebeck coefficient (S), thermal conductivity (κ), and absolute temperature (T). The specific relationship is $ZT = \frac{S^2}{\alpha\kappa}T$. The thermoelectric properties are divided into two parts: electrical transport properties and thermal transport properties. The electrical transport properties can be characterized by the power factor $\left(PF = \frac{\bar{s}^2}{\rho}\right)$. Good electrical conductivity is one of the characteristics of thermoelectric materials, so most of the research on thermoelectric materials initially focused on metals and their alloys with extremely low resistivity. However, it was later discovered that the Seebeck coefficient of metallic materials is too small. Metallic materials are not destined to be excellent thermoelectric materials. With the development of semiconductor materials, thermoelectric materials have again become a research boom and rapidly entered an explosive stage.^{10–13} In the 1950s, Bi₂Te₃-based thermoelectric materials quickly became the focus of researchers as soon as they were discovered, and entire research was centered on how to obtain high ZT values.¹⁴ In the following decades, Bi₂Te₃-based thermoelectric materials continued to refresh the highest ZT values.^{15–17} Bi₂Te₃ is a typical narrow-band semiconductor material.¹⁸ It has a high density of states and effective electronic mass due to its complex energy band structure. Furthermore, because of the small electronegativity difference between Bi and Te atoms, it helps to obtain higher carrier mobility.

Hongzhang Song hzsong@zzu.edu.cn

¹ Key Laboratory of Material Physics of Ministry of Education, School of Physics and Microelectronics, Zhengzhou University, Zhengzhou 450001, China

Under the influence of multiple factors, Bi_2Te_3 alloys became the optimal thermoelectric material systems near room temperature.^{15,19}

Furthermore, Bi₂Te₂ thermoelectric materials are currently the only thermoelectric material system widely used in business, such as refrigeration near room temperature.²⁰⁻²² However, the ZT value of commercial Bi₂Te₃ is mostly below 0.9. The development of high-performance Bi₂Te₃ thermoelectric materials is conducive to further seize the thermoelectric material market. On the whole, the performance of *n*-type materials is not yet comparable to that of *p*-type materials.^{4,23–27} Therefore, the research and development of high-performance *n*-type Bi₂Te₂₇Se₀₃ alloys is more important. The common preparation methods of thermoelectric materials include hot pressing (HP),^{28,29} spark plasma sintering (SPS), 30,31 zone melting, 32,33 etc. The ZT values of $Bi_{2}Te_{2,7}Se_{0,3}$ thermoelectric materials prepared by different methods are not the same.³⁴ In this paper, the zone-melting method was used to prepare *n*-type $Bi_2Te_{2,7}Se_{0,3}$ crystals. Compared with other preparation methods, its products have a large size and higher thermoelectric properties due to texturing, which is beneficial for commercial applications. Especially, compared to the conventional zone-melting process, the zone-melting method in this paper was optimized by using quartz tubes instead of common glass tubes, and two vacuum pumps instead of one mechanical pump, and adding a process of swing furnace.

Experimental

All samples in this experiment were prepared using the zone-melting method. The *n*-type $Bi_2Te_{2.7}Se_{0.3}$ ingredients were weighed according to the stoichiometric ratio, mixed, and sealed in a high-vacuum quartz tube. In the swing furnace, the raw materials were shaken for 10 h at 1023 K to achieve the effect of uniform mixing of the ingredients. Cooled to room temperature, the quartz tube was fixed on a zone fusion furnace. The melted ingot underwent zone fusion crystal growth at a temperature of 973 K with a growing rate of 8 mm/h. After the zone-melting temperature dropped to room temperature, the *n*-type $Bi_2Te_{2,7}Se_{0,3}$ ingot were removed from the broken quartz tube. The ingot was cut into the required size for testing the electrical and thermal properties using a wire-cut electrical discharge machining. The sample size for electrical performance testing was $2 \text{ mm} \times 3 \text{ mm} \times 13 \text{ mm}$, and the sample size for thermal performance testing was $2 \text{ mm} \times 10 \text{ mm} \times 10 \text{ mm}$.

The treated samples were subjected to various microstructure characterization and performance tests. The phase structure of the material was characterized by an x-ray diffraction analyzer (XRD), and the micromorphology was observed by scanning electron microscopy (SEM). Regarding thermoelectric performance, this mainly includes two aspects: electrical transport performance (Seebeck coefficient and resistivity) and thermal transport performance (thermal conductivity). The LSR system (LSR-3/800 Seebeck coefficients/electrical resistance measuring system; Linseis, Germany) can simultaneously measure the Seebeck coefficient and the resistivity of the sample. The inert gas environment during the test was provided by argon. The thermal conductivity was calculated by the formula $\kappa = dDC_p$. The physical symbols d, D, and C_p represent the density, thermal diffusion coefficient, and specific heat capacity of the material, respectively. They were calculated using the Archimedes principle, tested by the LFA457 system (Netzsch, Germany), and measured by differential scanning calorimetry (DSC) independently.

Results and Discussion

The $Bi_2Te_{2.7}Se_{0.3}$ alloy in this paper has two distinct advantages. The first is that the thermoelectric properties are generally higher than those of the $Bi_2Te_{2.7}Se_{0.3}$ currently on the market. The second is that $Bi_2Te_{2.7}Se_{0.3}$ can be produced at large scale to meet the needs of commercialization. The ingot length was 28 cm and its diameter was 2.6 cm, as shown in Fig. 1. In order to obtain more reliable data, three sets of samples taken from different areas of the ingot (Fig. 1) were tested separately for thermoelectric performance. In addition, the thermoelectric properties were tested along two different directions, one parallel to the zone melting direction (results are shown in Fig. 3), and the other perpendicular to the zone-melting direction.

Figure 2 shows the XRD pattern for the Bi₂Te_{2.7}Se_{0.3} ingot. By comparing the standard cards and several published reports, the diffraction peaks of this group of samples match well, with no impurity diffraction peaks, confirming that this group of samples is the target material.

In Fig. 3a, the resistivity of all the samples is proportional to temperature, exhibiting typical degenerate semiconductor characteristics. In Fig. 3b, the Seebeck coefficient of all the samples is negative, indicating that the samples are all



Fig. 1 The $Bi_2Te_{2.7}Se_{0.3}$ ingot; the red box refers to the area of the sample (Color figure online).



Fig. 2 XRD patterns for the $Bi_2Te_{2,7}Se_{0,3}$ ingot.

n-type semiconductors with electrons as the main carrier. The Seebeck coefficient gradually increases with increasing temperature, reaching its maximum value at a certain temperature, and then begins to decrease. This phenomenon is attributed to the bipolar effect. At higher temperatures, due to the intrinsic thermal excitation, electron and hole pairs are produced in thermoelectric materials, while due to the opposite sign of the Seebeck coefficients of the electrons and holes, the minority carrier would decrease the Seebeck coefficient. Thus an S peak appears. The highest values of the Seebeck coefficient for the *n*-type $Bi_2Te_{2,7}Se_{0,3}$ sample prepared by hot pressing were about 140–160 $\mu V/K$.³⁵ The absolute value of the Seebeck coefficient of the *n*-type $Bi_2Te_2 Se_{0.3}$ sample prepared by SPS is below 200 $\mu V/K$,^{36,37} but the absolute value of the Seebeck coefficient in this experiment is 205–230 $\mu V/K$. Compared with other experimental methods, the ZT values of the Bi₂Te_{2.7}Se_{0.3} samples in this study may be not the highest, but their high Seebeck values make them more competitive because of their high detection sensitivity. The power factor calculated by the resistivity and the Seebeck coefficient is shown in Fig. 3c. The highest power factor can be achieved near room temperature.

The physical quantity that characterizes the thermal transport properties of materials is the thermal conductivity (κ). This is composed of three parts: electronic thermal conductivity, lattice thermal conductivity, and bipolar thermal conductivity. There is a strong correlation between the electronic thermal conductivity and the electrical resistivity. Low resistance and large electronic thermal conductivity always occur together. So, the electronic thermal conductivity is not

easy to individually control. The lattice thermal conductivity is a relatively independent parameter, and research on thermal conductivity generally focuses on reducing the lattice thermal conductivity.^{38–40} In the Bi₂Te_{2.7}Se_{0.3} materials, both Bi and Te atoms have large atomic masses, and the melting point of the system is lower (about 858 K), so the system has a lower lattice thermal conductivity, as shown in Fig. 3d. In Fig. 3e, the total thermal conductivity first decreases due to the enhanced phonon scattering, and then increases with increasing temperature due to the bipolar effect. It changes in the range of 1.3–1.7 *W/m.K*.

Under the combined effect of the Seebeck coefficient, resistivity, and thermal conductivity, the *ZT* of the material first increases and then decreases with temperature, as shown in Fig. 3f. In the temperature range of 300–400 K, *ZT* values of more than 1 are achieved. At 360 K, the *n*-type $Bi_2Te_{2.7}Se_{0.3}$ obtains an optimum *ZT* value as high as 1.16. This value may be lower than some reported values whose bulk samples are prepared by HP, SPS, HTHP, LSM, etc., 4,25,26,41-50 is a highly competitive one in the zone-melting field due to the high vacuum, high pure raw materials, and swing sintering in this experiment.^{32,33,51} In particular, four Bi_2Te_3 -based alloy ingots can be simultaneously prepared in the zone-melting furnace. So, the preparation process in this paper can be directly industrialized.

On the whole, the three groups of samples show similar patterns, but the performance of the area 2 sample is better than the other two samples. This is because the areas 1 and 3 are located at the two ends of the ingot, respectively. The samples in these two areas are prone to component segregation during the zone-melting process, which reduces the thermoelectric properties. That is to say, some samples with poor performance may be produced at the two ends of the ingot, while the size of the two specific areas needs to be further studied.

The samples prepared by zone melting are polycrystalline with oriented growth characteristics, and their mechanical properties are better than those of single crystals. Element doping was used to adjust the carrier concentration to achieve a uniform distribution of impurities, and the thermoelectric performance is then more stable. Figure 4 shows the fracture morphology of the $Bi_2Te_{2.7}Se_{0.3}$ sample. The observed directions in Fig. 4a and b are parallel and perpendicular to the zone-melting direction, respectively. The morphology is a typical layered density structure. The test results of the thermoelectric properties of the $Bi_2Te_{2.7}Se_{0.3}$ sample taken from area 2 along two directions are shown in Fig. 5.



Fig. 3 Variation of thermoelectric properties with temperature for different regions of $Bi_2Te_{2.7}Se_{0.3}$: (a) resistivity, (b) Seebeck coefficients, (c) power factors, (d) lattice thermal conductivity, (e) total thermal conductivity, and (f) ZT values.



Fig. 4 SEM fracture morphology diagram of $Bi_2Te_{2.7}Se_{0.3}$ along two tested directions: (a) parallel to the zone melting direction, (b) perpendicular to the zone melting direction.

Figure 5a shows the change trend of the sample's resistivity with temperature in two directions. The resistivity increases with increasing temperature, differs significantly in the two directions and has obvious anisotropy. The numerical ratio of the resistivity in the two directions is called the anisotropy ratio of resistivity.⁴⁰ In this experiment, the electrical resistivity perpendicular and parallel to the zone-melting directions at room temperature was 17.66 $\mu\Omega.m$ and 9.95 $\mu\Omega.m$, respectively. The calculated anisotropy ratio was 1.78, which is lower or comparable to the data in the literature.^{33,52} This anisotropy of electrical conductivity in the *n*-type $Bi_2Te_{2,7}Se_{0,3}$ ingot is well understood by the anisotropic nature in carrier mobility as the crystallographic directions, as demonstrated by its texturing and layered microstructure shown in Figs. 1 and 4. Figure 5b shows the variation range of the Seebeck coefficient in two directions. Within the experimental error range, the experimental data in the two directions are roughly the same. In other words, the Seebeck coefficient is isotropic.⁵³ This is consistent with the theoretical calculation results based on the relaxation time approximation.⁵⁴ Through the above analysis, the samples with parallel zone-melting directions have a high Seebeck coefficient and low resistivity at the same time. The sample in the parallel zone-melting direction has a higher power factor, which is about 1.9 times that of the perpendicular zone-melting direction. Their power factors calculated by resistivity and Seebeck coefficient are shown in Fig. 5c.

The lattice thermal conductivity and the total thermal conductivity of $Bi_2Te_{2.7}Se_{0.3}$ ingot in two directions varies with temperature, as shown in Fig. 5d and e, respectively. The test results indicate that the total thermal conductivity in the parallel zone melting direction is 1.41 *W/m.K* near room temperature, which is larger than that in the

perpendicular zone melting direction of 0.9 W/m.K. This is because the preferred orientation of the sample favors the heat transport of carriers and phonons along the crystal plane. The anisotropic ratio of thermal conductivity is 1.56, which is much smaller than the value of the single crystal sample (2.1–2.4) as well as smaller than the textured Bi₂Te₂Se₁ bulk sample.^{55,56}

Figure 5f shows the ZT value obtained by calculation. The Seebeck coefficient of the $Bi_2Te_{2.7}Se_{0.3}$ sample prepared by zone melting is isotropic, and the thermal conductivity and resistivity have different degrees of anisotropy. Since the resistivity ratio of the two directions is greater than the thermal conductivity ratio, the ZT value of the material shows that the parallel zonemelting direction is better than the perpendicular zonemelting direction. This is the same as the conclusion of Wang et al.⁵⁷

Conclusions

The emergence of thermoelectric materials provides new ideas for solving the energy crisis and environmental pollution.^{58–64} As typical excellent room-temperature thermoelectric materials, $Bi_2Te_{2.7}Se_{0.3}$ alloys have successfully achieved commercial applications. However, the current commercial $Bi_2Te_{2.7}Se_{0.3}$ alloys have low *ZT* values. The $Bi_2Te_{2.7}Se_{0.3}$ sample in this article has achieved a *ZT* value of more than 1.0 near room temperature, and the highest value can reach 1.16. The ingot size is large, which improves its utilization. By testing the thermoelectric properties in different directions, it is confirmed that the $Bi_2Te_{2.7}Se_{0.3}$ ingot has anisotropy, and that the thermoelectric properties in the



Fig. 5 Variation of thermoelectric properties of $Bi_2Te_{2.7}Se_{0.3}$ with temperature along the two tested directions: (a) resistivity, (b) Seebeck coefficients, (c) power factors, (d) lattice thermal conductivity,

(e) total thermal conductivity, and (f) ZT values; N- \perp perpendicular to the zone-melting direction, N-// parallel to the zone melting direction.

parallel zone-melting direction are greatly improved, which is consistent with the results in the literature.

Conflict of interest There are no conflicts to declare.

Data availability Data will be made available on reasonable request.

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