

# Graphene-Metal Hybrid Metamaterial for a Tunable Broadband Terahertz Linear-Polarization Conversion Switch and Linear-to-Circular Polarization

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#### Abstract

In this paper, we propose a tunable broadband terahertz (THz) linear polarization conversion switch (LPCS) and linear-tocircular polarization (LTCP) metamaterial. By tuning the Fermi energy level of graphene from  $E_F = 0$  eV to  $E_F = 1$  eV at 2.70–5.62 THz, it is possible to adjust the proposed structure from the linear polarization conversion (LPC) ON state to the LPC OFF state and also to tune the polarization conversion rate (PCR) from 1% to 99.99%. When  $E_F = 0.5$  eV and is in the range of 5.56–5.96 THz, the structure can achieve LTCP function with ellipticity ( $\eta$ ) exceeding 0.97 and an axial ratio (AR) of less than 1.5 dB. Based on the surface current and U-V decomposition, the LPC ON state, LPC OFF state and LTCP function are analyzed and well corroborated. Investigating graphene surface impedance at different fermi energy levels proves the polarization state tunable. The proposed structure can be applied to various fields of wireless communication, sensing and imaging.

Keywords Polarization conversion switch · graphene · metamaterial · linear-to-circular polarization

# Introduction

Polarization, a significant property of electromagnetic waves, can increase the capacity of wireless communication by more than a few times.<sup>1</sup> Traditional polarization control is achieved by fiber grating or birefringent crystals.<sup>2</sup> However, these methods have complex phase accumulation processes that result in bulky equipment that is no longer suitable for today's practical needs. In recent years, metamaterials (MMs), as artificial electromagnetic mediums, have emerged as one of the best alternatives for polarization control because of their electromagnetic properties and ability to control electromagnetic waves without natural materials and the possibility of periodic alignment.<sup>3–5</sup> In contrast to standard optical components, MMs, as artificial materials that

Zhongyin Xiao zhyxiao@shu.edu.cn can be tailored to the electromagnetic response on demand, provide inspiring possibilities for high-density integration and miniaturization of terahertz (THz) devices.<sup>6–8</sup> Polarization control of THz waves by periodically arranged MMs achieved fascinating results and have been widely applied in practice, such as coded metamaterials,<sup>9–11</sup> near-field imaging,<sup>12,13</sup> sensors,<sup>14</sup> and wireless communication.<sup>15</sup> However, most polarization control studies tend to be restricted to linear polarization conversion (LPC) and linear-to-circular polarization (LTCP) functions,<sup>16–18</sup> and thus certain tunability is needed. Therefore, it is urgent to design a structure with a controllable polarization state and realize the LPC ON state, LPC OFF state and LTCP function. Moreover, the control method is simple and explicit.

In practical applications, devices designed from graphene have ideal tunability. Graphene is a hexagonal honeycomb lattice nanomaterial composed of carbon atoms,<sup>19,20</sup> and by varying the chemical doping or gate voltage over a wide frequency range, the surface conductivity of graphene, which depends on the chemical potential, can be continuously varied.<sup>21,22</sup> Because of its surface conductivity,<sup>23</sup> tunable optical transparency<sup>24</sup> and high electron mobility,<sup>25</sup> the control of the polarization state of THz waves has attracted widespread attention. For example, in 2020,

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Li et al. proposed a dynamically tunable THz broadband polarization converter. This structure dynamically converts linear polarization waves to cross-linear or circular polarization waves by graphene.<sup>26</sup> However, it needs more bandwidth to control polarization conversion and more tunability. In 2020, Zhang et al. proposed a switchable reflective THz polarization converter<sup>27</sup> that can modulate graphene's Fermi energy level to switch the linear polarization between quarter-wave and half-wave plates, enabling LPC and LTCP function. Nevertheless, the bandwidth is smaller and the polarization conversion efficiency could be higher. In 2021, Chen et al. designed a monolayer graphene broadband tunable reflective polarization converter that can convert linear co-polarized waves to cross-polarized waves with relatively flexible tuning of the bandwidth of the polarization conversion by adjusting the Fermi energy level of the graphene.<sup>28</sup> Yet its single function and tunability need to be improved. In 2022, Yuan et al. devised a graphene metamaterial-based tunable reflective THz polarization converter. By varying the Fermi energy level of graphene, the converter can achieve dual-band LPC and LTCP,<sup>29</sup> but its polarization conversion bandwidth needs more stability and comparatively lower bandwidth.

In this paper, we propose a tunable broadband THz linear polarization conversion switch (LPCS) and LTCP metamaterial. By tuning the Fermi energy level of graphene from  $E_F = 0$  eV to  $E_F = 1$  eV at 2.70–5.62 THz, it is feasible to adjust the proposed structure from LPC ON state to the LPC OFF state and also to tune the polarization conversion rate (PCR) from 1% to 99.99%. When  $E_F = 0.5$  eV and in the range of 5.56-5.96 THz, the structure can achieve LTCP function with ellipticity ( $\eta$ ) exceeding 0.97 and an axial ratio (AR) of less than 1.5 dB. Based on the surface current and U-V decomposition, the LPC ON state, LPC OFF state and LTCP function are analyzed and well corroborated. Investigating graphene surface impedance at different Fermi energy levels proves the polarization state tunable. Compared to the previously reported article, the proposed device has more functions and easily tunable and integrated features. We believe that the proposed structure has potential applications in tunable devices for THz communications.

## **Structural Design and Theory**

The proposed reflective structure is shown in Fig. 1. Figure 1a shows that the structure consists of five layers: a double-graphene layer, a spacer layer, an I-type gold resonator, a dielectric layer and gold substrate. The double-graphene layer is a patterned sandwich structure consisting of two periodically patterned graphene layers and a Topas polymer ( $\epsilon = 2.35$ ). Both spacer and dielectric layers are also constructed as Topas polymers, where the spacer is  $t_1 = 0.1 \, \mu m$ 

and the dielectric layer is d = 15 µm. Figure 1b shows the double-graphene layer with opening size  $P_3 = 14.6 \text{ µm}$  and opening direction of  $-45^{\circ}$  with respect to the x-axis. Figure 1c shows the I-type gold resonator placed in the x-axis direction with the following parameters: P = 39 µm,  $l_1 = 23.4 \text{ µm}$ ,  $l_2 = 12.5 \text{ µm}$ ,  $w_1 = 4.3 \text{ µm}$ ,  $w_2 = 4.5 \text{ µm}$ ,  $t_2 = 0.1 \text{ µm}$ . As the gold film is perfectly reflective in the THz band, and its thickness has little effect on the performance of the structure, we set its thickness as t = 1 µm to reduce the simulation time. The permittivity of gold follows the Drude model  $\epsilon(\omega) = 1 - \omega_p^2/(\omega^2 + i\gamma\omega)$  with the plasma frequency  $\omega_p = 1.37 \times 10^{16} rad/s$  and the damping constant is  $\gamma = 4.07 \times 10^{13} \text{ rad/s}$ .

Graphene can be simulated as a 2D conductive surface impedance material,<sup>28,30,31</sup> with surface impedance<sup>14</sup>  $Zg = 1/\sigma_s$ . In the THz band, the graphene surface complex conductivity can be expressed by the classical Kubo formula.<sup>32</sup>

$$\sigma_{\text{intra}} = j \frac{e^2 k_B T}{\pi h^2 (\omega - j2\Gamma)} \left( \frac{E_F}{k_B T} + 2 \ln \left( e^{-\frac{E_F}{k_B T}} + 1 \right) \right)$$
(1)

$$\sigma_{\text{inter}} = \frac{je^2}{4\pi h} \ln\left(\frac{2|E_F| - (\omega - j2\Gamma)h}{2|E_F| + (\omega - j2\Gamma)h}\right)$$
(2)

where  $\sigma_{intra}$  and  $\sigma_{inter}$  represent intraband and interband leap conductivity of graphene, respectively,  $\omega$  is the angular frequency of the incident electromagnetic wave, $E_F$  is the fermi energy level, *e* represents the charge of the electron,  $k_B$  denotes Boltzmann's constant. *T* indicates ambient temperature, *h* means approximate Planck constants.  $\Gamma$  indicates scattering rate,  $\Gamma = 1/2\tau$ ,  $\tau$  represents electron relaxation time. The Fermi energy level of graphene with applied bias voltage is expressed as<sup>16,22</sup>:

$$E_F \approx h v_f \sqrt{\frac{\pi \varepsilon_r \varepsilon_0 V_g}{e t_2}} \tag{3}$$



Fig. 1 (a) 3D model, (b) graphene layer, (c) I-type gold resonator.

Here,  $V_{\rho}$  is the bias voltage,  $\varepsilon_0$  represents vacuum dielectric constant, and  $\varepsilon_r$  represents relative dielectric constant of the medium.  $t_2$  is the thickness of the Topas polymer in the middle of the bilayer graphene pattern. $v_f = 1 \times 10^6 m/s$ expresses the Fermi wave vector. Graphene's Fermi energy level  $E_F$  can be dynamically tuned from 0 eV to 1 eV.<sup>21</sup> The rapidly developing micro and nano process technology provides methods for fabricating the proposed structures. First, a thin layer of Topas polymer is spin-coated on a silicon substrate, and a thick layer of Topas dielectric with the desired thickness is prepared by growing the spin-coated and cured layer using a thermal evaporation system.<sup>16,30</sup> The I-type gold resonator is then designed using conventional optical techniques. Finally, bilayer graphene patterns are prepared in the Topas dielectric layer by repeated growth and transfer processes. Assuming ambient temperature T = 300 K,  $\tau = 0.6$  ps, the higher relaxation time has easy tuning features, and in calculations, the single-layer graphene with a thickness of 0.34 nm is modeled as a 2D conductive layer.<sup>31</sup> Using CST Microwave Studio 2020 for numerical simulations, the simulated results in this work were calculated by using the three-dimensional finite-difference time-domain (FDTD) method. In all simulations, period boundaries are applied in both x- and y-directions, and the perfectly matching layers are assigned along the z-direction. The incident THz waves are set to y-polarized TE mode employing the frequency domain solver.<sup>33</sup>

In this paper, a reflective graphene-metal hybrid structure is proposed, and now we analyze the operating principles of the reflective graphene-metal hybrid structure from the theory. Assuming the incident electromagnetic wave propagates in the -Z direction of linear polarization, the relationship between the incident linear component  $\left(E_x^i; E_y^i\right)$  and the reflected linear polarization component  $\left(E_x^r; E_y^r\right)$  can be expressed as<sup>12</sup>:

$$\begin{pmatrix} E_x^r \\ E_y^r \end{pmatrix} = \begin{pmatrix} r_{xx} & r_{xy} \\ r_{yx} & r_{yy} \end{pmatrix} \begin{pmatrix} E_x^i \\ E_y^i \end{pmatrix} = r \begin{pmatrix} E_x^i \\ E_y^i \end{pmatrix}$$
(4)

Here  $r_{xx}$  and  $r_{yy}$  are co-polarization transmission coefficients for linear polarization horizontal and vertical, respectively, r is the linear polarization of the Jones matrix. To better evaluate LPC performance, the PCR is introduced to describe the polarization conversion effectiveness<sup>18</sup> and is defined as:

$$PCR(x) = \frac{|r_{yx}|^2}{|r_{xx}|^2 + |r_{yx}|^2}$$
(5)

. 7

$$PCR(y) = \frac{|r_{xy}|^2}{|r_{xy}|^2 + |r_{yy}|^2}$$
(6)

where PCR(*x*) indicates the linear polarization horizontal polarization conversion efficiency and PCR(*y*) indicates the vertical polarization conversion efficiency. Furthermore, for the measurement of the degree of LTCP, the  $\eta$  and AR are defined as follows<sup>29</sup>:

$$\beta = \frac{1}{2} \sin^{-1} \left( \frac{2|r_{ii}| |r_{ji}| \sin \Delta \varphi}{|r_{ii}|^2 + |r_{ji}|^2} \right)$$
(7)

$$\eta = \frac{2|r_{ii}| |r_{ji}| \sin \Delta \varphi}{|r_{ii}|^2 + |r_{ji}|^2}$$
(8)

$$AR = 10 \times \log(\tan\beta) \tag{9}$$

where  $r_{ii}$  denotes co-polarization coefficient of the linear polarization,  $r_{ji}$  denotes cross-polarization coefficient of the linear polarization,<sup>4</sup> and  $\eta$  and AR are used to evaluate the performance of circular polarization.<sup>34</sup> When  $r_{ii} = r_{ij}$ , that is PCR = 0.5, and  $\Delta \varphi = \varphi i i - \varphi i j = \pi/2 + 2k\pi$  (*k* is an integer), at this time, AR is less than 3 dB, and the incident linear polarization wave can be converted into a circular polarization reflected wave. When  $\eta$  is +1/-1, the reflected wave is left-handed circular polarization (LHCP) wave/righthanded circular polarization (RHCP) wave, respectively.

# **Results and Discussion**

## Tunable Linear Polarization Transfer Switch Function

The structure of the proposed I-type gold resonator and double-graphene layer are symmetrically placed about the diagonal. The co-polarization and cross-polarization coefficients of the reflections are the same when the y-polarized and x-polarized waves are incident, so here we only use the case of the incident y-polarized waves for consideration. Figure 2a shows that at  $E_F = 0$  eV, from 2.70 THz to 5.62 THz,  $|r_{xy}| > 0.55$ ,  $|r_{yy}| < 0.25$ , and in the range of 4.17–5.62 THz,  $|r_{xy}| > 0.9$  and more extensive than |ryy|. Figure 2b shows that PCR is greater than 90% from 2.70 THz to 5.62 THz and reaches the maximum value of 99.99% at 4.96 THz. At this point, the proposed structure acts as a linear polarization converter by the cross-polarization output; the LPC ON



**Fig. 2** (a) amplitude of the reflection coefficient at  $E_F = 0$  eV ( $|\mathbf{r}_{yy}|$  and  $|\mathbf{r}_{xy}|$ ), (b) PCR at  $E_F = 0$  eV, (c) amplitude of the reflection coefficient at  $E_F = 1$  eV ( $|\mathbf{r}_{yy}|$  and  $|\mathbf{r}_{xy}|$ ), (d) PCR at  $E_F = 1$  eV.

state can be achieved. Figure 2c shows that modulating the fermi energy level to  $E_F = 1 \text{ eV}$ , in the range of 2.70 THz–5.62 THz,  $|r_{yy}| > 0.77$ ,  $|r_{xy}| < 0.16$ . In this case, the output is by co-polarization. Figure 2d shows that PCR < 5% from 2.70 THz to 5.62 THz. It can achieve the LPC OFF state at this time. By tuning the Fermi energy level from 0 eV to 1 eV, PCR can be adjusted from 1% to 99.99%. Dynamically, the proposed structure acts as a broadband LPCS.

#### **Tunable Linear-to-Circular Polarization**

When the Fermi energy level is regulated to  $E_F = 0.5 \text{ eV}$ , Fig. 3a shows that  $|r_{xy}| = |ryy| = 0.46 \sim 0.50$  and  $\Delta \varphi = \varphi_{yy} - \varphi_{xy} = -90^\circ - 10^\circ/270^\circ - 10^\circ$  in the range of 5.56–5.96 THz. Figure 3b, c and d show that in this frequency band PCR =  $0.5 \pm 0.01$ , ellipticity  $\eta < -0.97$  and AR < 1.5dB < 3dB. To summarize, Fig. 3 explicitly illustrates the reflected *rxy* and *ryy* synthesized RHCP waves when y-polarized waves are incident on the structure at  $E_F = 0.5 \text{ eV}$  in the range of 5.56–5.96 THz. As the proposed structure of the gold resonator and double graphene layers are symmetrically placed about the diagonal, the x-polarized waves at 5.56–5.96 THz are reflected by *ryx* and *rxx*  synthesized LHCP waves. It can achieve LTCP function at this time.

#### **Physical Mechanism of the Polarization State**

To analyze the LPC ON state's physical mechanism, we simulated the proposed structure's surface currents at 3.30 THz and 4.96 THz when  $E_F = 0$  eV. Figure 4a, b and c show the surface currents distribution of the graphene layers, gold resonator and gold substrate at 3.30 THz. Graphene layers and the long arms of the I-type gold resonator together form inverse parallel currents with the gold substrate at low frequency. The reversed parallel currents form magnetic dipoles that produce a magnetic reaction, forming an induced magnetic field H<sub>1</sub>. While at 4.96 THz, the surface currents of graphene layers are relatively weakly distributed as shown in Fig. 4d, e and f, the currents on the short arm of the I-type gold resonator form homogeneous parallel currents with the currents on the gold substrate, leading to an electrical reaction that produces an induced electric field E. For the polarization conversion, the component  $H_{1v}$  of the induced magnetic field  $H_1$  in the y-direction is parallel to the direction of the incident electric field E<sub>i</sub>; this ensures that cross-polarization coupling can be generated at low frequency. The component  $E_{1x}$  of the induced electric field



**Fig. 3** (a) Amplitude of the reflection coefficient at  $E_F = 0.5$  eV ( $|\mathbf{r}_{yy}|$  and  $|\mathbf{r}_{xy}|$ ) and phase difference value ( $\Delta \varphi$ ), (b)PCR at  $E_F = 0.5$  eV, (c) ellipticity ( $\eta$ ) at  $E_F = 0.5$  eV, (d) axial ratio (AR) at  $E_F = 0.5$  eV.



**Fig. 4** (a), (b) and (c) surface currents of graphene layers, I-type gold resonator and gold substrate with  $E_F = 0$  eV at 3.30 THz. (d), (e) and (f) surface currents graphene layers, I-type gold resonator and gold substrate with  $E_F = 0$  eV at 3.30 THz.

E in the *x*-direction is perpendicular to the direction of the incident electric field  $E_i$ ; this ensures that cross-polarization coupling can be generated at high frequency, allowing cross-polarization to occur, so that *y*-polarized waves can be converted into *x*-polarized waves.

To analyze the reason for LPC OFF state, we also simulated the surface currents of the proposed structure at the points 3.30 THz and 4.96 THz when  $E_F = 1$  eV. As shown in Fig. 5a, b and c, the graphene layers and the long arms of the I-type gold resonator at 3.30 THz have weak current strengths and cannot form reverse parallel currents with the gold substrate, thus failing to generate a magnetic resonance. Figure 5d, e and f shows the short arm of the I-type gold resonator with the gold substrate at 4.96 THz point, which could not form isotropic parallel currents at high frequency,

resulting in an electrical resonance. In summary, the proposed structure forms broadband LPC ON state at  $E_F = 0$  eV and LPC OFF state at  $E_F = 1$  eV.

To explain the physical mechanism of converting the reflected y-polarized waves into RHCP waves after incidence, we simulate the surface currents distribution at 5.65 THz when  $E_F = 0.5$  eV. From the above, the high-frequency resonance point is mainly determined by the surface currents of the short arm of the I-type gold resonator independent of the surface currents of the surface currents of the short arm of the I-type gold resonator at 5.65 THz, and Fig. 6a, b, c, and d shows the surface currents of the short arm surface currents at 5.65 THz with 0°, 90°, 180° and 270° counterclockwise



Fig. 5 (a), (b) and (c) surface currents of graphene layers, I-type gold resonator and gold substrate at 3.30 THz with  $E_F = 1$  eV. (d), (e) and (f) surface currents of graphene layers, I-type metal resonator and metal substrate at 4.96 THz with  $E_F = 1$  eV.



**Fig.6** (a), (b), (c) and (d) I-type gold resonator surface currents at 5.65 THz with 0°, 90°, 180° and 270° counterclockwise rotations when  $E_F = 0.5$  eV.

rotations, indicating that the *y*-polarized waves are reflected to form the RHCP waves after incidence.

Suppose the electric field vector of the vertically incident electromagnetic wave along the MM is decomposed along the direction of the orthogonal coordinate axes. In that case, the polarization converter works as shown in Fig. 7a. The coordinate axis uOv is rotated by 45° from the coordinate axis xOy. According to the classical electromagnetic field theory, a phase difference of 0° indicates that the reflection is a co-polarized wave, a phase difference of 90°/270° signals that the reflection is a circularly polarized wave, and a phase difference of  $\pm 180^{\circ}$  represents that the reflection is a crosspolarized wave. With the incident y-polarized wave as an example, Fig. 7b shows the phase response of the structure under Eu and  $E_V$  excitation at  $E_F = 0$  eV. From 2.70 THz to 5.62 THz, the phase difference  $\varphi uv = \varphi vv - \varphi uu \approx \pm 180^\circ$ , indicates that the structure achieves a broadband LPC ON state. According to Fig. 7c, at  $E_F = 0.5$  eV from 5.56 THz to 5.96 THz,  $\varphi uv = \varphi vv - \varphi uu \approx 270^{\circ}$  indicates that the structure achieves LTCP function. According to Fig. 7d, at  $E_F = 1$  eV from 2.70 THz to 5.62 THz,  $\varphi uv = \varphi vv - \varphi uu \approx 0^\circ$  indicates that the structure achieves a broadband LPC OFF state.

We also elucidate the mechanism of the polarization state and analyze the polarization state of graphene at different fermi energy levels and its surface impedance. As shown in Fig. 8a, when  $E_F = 0.05 \sim 0.20 \, eV$ , as the Fermi energy level rises, the frequency band of the proposed structure with PCR > 90% decreases. Figure 8b and c shows the surface impedance of graphene  $Zg = 1/\sigma_s$ , graphene surface impedance with  $E_F = 0$  eV ranges from 465  $\Omega$  at 2 THz to 2200  $\Omega$  at 6 THz, when graphene is considered a dielectric film, it allows significant electromagnetic waves to be incident. While at  $E_F = 0.05$  eV, surface impedance 260  $\Omega$  to 530  $\Omega$ , at  $E_F = 0.10 \text{ eV}$ ,  $E_F = 0.15 \text{ eV}$  and  $E_F = 0.20 \text{ eV}$ , surface impedance 145  $\Omega$ , 94  $\Omega$  and 70  $\Omega$ . At this point, graphene gradually transitions from a dielectric film to a semi-metallic material, allowing a portion of the electromagnetic waves to be incident into the structure, producing the LPC ON state. For low frequency, the resonance point is mainly due to the action of the graphene layers and the long arms of gold resonator together with the gold substrate which produces magnetic resonance, while for high frequency, the resonance point is mainly due to the short arm of the gold resonator acting with the gold substrate to produce electrical resonance. Therefore, as the Fermi energy level of graphene rises, a blueshift of the low-frequency





**Fig.7** (a) Electric field vector Ey decomposed into two orthogonal electric vectors Eu and Ev, (b) reflection phases ( $\varphi uu$  and  $\varphi vv$ ) and phase difference ( $\varphi uv$ ) at  $E_F=0$  eV, (c) reflection phases ( $\varphi uu$  and

 $\varphi vv$ ) and phase difference ( $\varphi uv$ ) at  $E_F = 0.5$  eV, (d) reflection phases ( $\varphi uu$  and  $\varphi vv$ ) and phase difference ( $\varphi uv$ ) at  $E_F = 1$  eV.



Fig. 8 (a) PCR with  $E_F = 0.05$  to 0.2 eV, (b) graphene surface impedance with  $E_F = 0$  eV and  $E_F = 1$  eV, (c) graphene surface impedance with  $E_F = 0.05$  to 0.2 eV.



Fig. 9 (a) PCR with frequency and incidence angle at  $E_F = 0$  eV, (b) PCR with frequency and incidence angle at  $E_F = 0.5$  eV. PCR with frequency and incidence angle at  $E_F = 1$  eV.

resonance point occurs at  $E_F = 0.05 \sim 0.20 \, eV$ , while the high-frequency resonance point remains almost unchanged. When  $E_F = 0.50 \, eV$  with a graphene surface resistance of 28  $\Omega$ , graphene layers transition from semi-metallic material to metallic material, and only a few electromagnetic waves are incident to the structure. At this time, the low-frequency resonance point does not exist, while the high-frequency resonance point will move down, resulting in LTCP function. At  $E_F = 1 \, eV$ , the graphene surface impedance of 14  $\Omega$ is transformed to a metallic state, and many electromagnetic waves on the direct reflection will not produce a resonance point, thus playing a role in the LPC OFF state.

Figure 9 show the effect of PCR with frequency and incidence angle. The proposed structure at  $E_F = 0$  eV shown in Fig. 9a maintains a stable bandwidth for incidence angles from 0° to 10° and decreases continuously as the incidence angle increases. Figure 9b shows the proposed structure at  $E_F = 0.50$  eV, where the linear to circular polarization remains stable at an incidence angle of 0° ~ 10°. Figure 9c shows the  $E_F = 1$  eV, structure satisfies the LPC OFF state at an incidence angle of 0° ~ 40°.

Finally, we compare some results with those of the devices reported in Table I for the graphene-based controlled polarization state THz simulation papers to demonstrate the innovation and performance of our proposed structure. In Table I, we list the functions, types, frequency ranges and bandwidths of the working implementations used in different studies. Table I shows that most studies focus on one or two modes of LPC and LTCP. Our proposed functional device can implement both LPC ON, LPC OFF state and LTCP function.

### Conclusion

In this paper, we propose a device to dynamically control the polarization state of terahertz waves in the range of 2.70–5.62 THz by tuning the Fermi level of graphene from  $E_F = 0$  eV to  $E_F = 1$  eV, which can adjust the proposed structure from the LPC ON state to the LPC OFF state, and the PCR can be tuned from 1% to 99.99%. When  $E_F = 0.5$  eV and is in the range of 5.56–5.96 THz, the structure can achieve LTCP function with  $\eta$  exceeding 0.97 and AR is less than 1.5 dB. We

 Table I
 Comparison of previous

 THz simulation papers on
 graphene-based devices with

 controlled polarization states
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References	Function	Туре	Frequency range (THz)	Bandwidth (THz)
26	LPC LTCP	Dual function	2.24~2.74 THz 2.30~2.68 THz	0.5 0.38
27	LPC LTCP	Dual function	1.38~1.85 THz 1.38~1.72 THz	0.47 0.34
28	LPC	Single function	2.15~4.00 THz	1.85
29	LPC LTCP	Dual function	2.34~3.54, 3.38~4.43 THz 2.14~2.62 THz	1.2, 1.05 0.48
This work	LPC ON state LTCP LPC OFF state	Triple function	2.70~5.62 THz 5.56~5.96 THz 2.70~5.62 THz	2.92 0.40 2.92

simulated PCR at the Fermi level  $E_F = 0 \sim 0.2$  eV, for which the structure is tunable for polarization conversion. Based on the surface current and U-V decomposition, the LPC ON state, LPC OFF state and LTCP function are analyzed and well corroborated. Investigating graphene surface impedance at different Fermi energy levels proves the polarization state tunable. We believe that the proposed structure has potential applications in tunable devices for THz communications.

Author Contributions XW: Conceptualization, Methodology, Software, Writing—Original Draft, Writing—Review Editing. ZX: Conceptualization, Validation, Writing—Review & Editing, Supervision. XM: Software, Data Curation. Writing—Review Editing. XJ: Software, Formal analysis. Investigation, Supervision. AL: Software, Investigation, Supervision.

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Availability of Data and Materials All data generated or analyzed during this study are included in this published article.

**Conflict of interest** The authors declared that they have no conflicts of interest to this work. We declare that we do not have any commercial or associative interest that represents a conflict of interest in connection with the work submitted.

**Consent for Publication** Written informed consent for publication was obtained from all participants.

**Consent to Participate** Written informed consent for participation was obtained from all participants.

**Ethical Approval** We declare that this article is original, has not been published before, and is not currently considered for publication elsewhere. We confirm that the manuscript has been read and approved by all named authors and that there are no other persons who satisfied the

criteria for authorship but are not listed. We further confirm that the order of authors listed in the manuscript has been approved by all of us.

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