

First-Principles Study on the MAX Phases $\text{Ti}_{n+1}\text{GaN}_n$ $(n = 1, 2,$ and 3)

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We have performed first-principles density functional theory calculations within generalized-gradient approximation to obtain the structural, mechanical, electronic, and dynamic properties of $Ti_{n+1}GaN_n$ compounds. In order to examine the stability of these compounds, formation enthalpies, single-crystal elastic constants, and phonon dispersion curves were calculated. We show that all compounds are stable, while α -Ti₄GaN₃ is the most stable. The density of states calculations also demonstrate that all of the compounds are metallic. Additionally, bonding nature and related characteristics such as Mulliken atomic charges and bond overlap populations were investigated. Furthermore, thermodynamic properties were calculated by means of phonon dispersion curves. The results are compared in this work with available experimental values and theoretical calculations.

Key words: MAX phases, electronic properties, phonons, mechanical properties, first-principles

INTRODUCTION

The $M_{n+1}AX_n$ phases (where M, A, and X are a transition metal, A-group element, and either C or N, respectively) have attracted considerable attention due to their promising properties which establish connections between metallic and ceramic properties, such as high strength and stiffness at high temperatures, resistance to oxidation and thermal shock, good damage tolerance, good corrosion resistance, and good thermal and electrical conduction.^{1–3} Therefore, $M_{n+1}AX_n$ phases are promising materials for many applications such as rotating electrical contacts and bearings, heating elements, nozzles, heat exchangers, and tools for depressing, among many others.⁴

Several physical properties of $M_{n+1}AX_n$ phases have been studied by different researchers. For instance, Dahlqvist et al. investigated the phase stability of MAX $(M = Sc, Ti, V, Cr, or Mn, A = Al,$ and $X = C$ or N).^{[5](#page-8-0)} They reported that a maximum stability is reached around V as a transition metal, while for nitrogen, the maximum stability is reached for Ti for carbon-containing MAX phases. In addition, Keast et al. predicted the stability of an $M_{n+1}AX_n$ system containing α - and β -phases for different values of n^6 n^6 . Their results suggest that $Ti₂SiC, Ti₂SiN, and Ti₃AlN₂ have the potential to be$ synthesized as metastable compounds.

 M_2GaN (M is either Ti, V, or Cr) was investigated systematically to identify trends for structural, electronic, and elastic properties by Bouhemadou. Yang et al. performed comprehensive investigations on the compressive and electronic properties of Ti2GaN and applied high pressure to the compound up to 1000 GPa.² On the other hand, Manoun et al. measured the pressure dependency of the structural and mechanical properties of Gallium-con-(Received November 12, 2015; accepted April 28, 2016; $\frac{\text{tan at a mean}}{\text{tan in g}}$ polycrystalline $\frac{\text{Tr}_2\text{GaN}}{\text{Tr}_2\text{GaC}}$ as

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Fig. 1. Crystal structures of $Ti_{n+1}GaN_n$ (n = 1, 2, and 3) compounds.

experimental MAX phases.⁸ Shein and Ivanovskii systematically studied the trends in structural and electronic properties, as well as the relative stability of a representative group of very recently discovered materials prepared from de-intercalated MAX phases.⁹ Furthermore, as an important result, they reported that $M_{n+1}AX_n$ phases can be used as graphene-like structures. Systematic experimental studies of MAX-phase solid solutions to elucidate the role of chemistry on phase stability and proper-ties were carried out by Eklund et al.^{[10](#page-8-0)}

Despite a large number of theoretical and experimental studies devoted to the M_2AX phase, to our best knowledge, until now no other systematic results have been reported on the mechanical, electronic, and dynamic properties of $Ti_{n+1}GaN_n$ compounds. Hence, we report here the structural, mechanical, electronic, and dynamic properties of $Ti_{n+1}GaN_n$ compounds as investigated by first-principles calculations in our study. After well-converged geometry optimizations, we tested the energetic, mechanic, and dynamic stabilities of the compounds, and then compared the results to some experimental data and to those of similar compounds with the same structure.

CALCULATION METHOD

First-principles density functional plane wave calculations were performed using the CASTEP package under generalized gradient approximation (GGA-PW91).[11,12](#page-8-0) To define interactions between electrons and ion cores, norm-conserving pseudopotentials were used. 13,14 13,14 13,14 The wave functions were expanded in plane waves up to a kinetic-energy cutoff of 880 eV. The numerical integration over the Brillouin zone was performed using a $14 \times 14 \times 4$, $10 \times$ 10×2 , $14 \times 14 \times 2$, $10 \times 10 \times 2$ and $14 \times 14 \times 14$ 2 Monkhorst–Pack k -point grids for Ti₂GaN,

 α -Ti₃GaN₂, β -Ti₃GaN₂, α -Ti₄GaN₃, and β -Ti₄GaN₃ crystal structures, respectively.[15](#page-8-0) During the geometry optimizations, there are no restrictions on lattice parameters and atomic locations, and the structures were relaxed using the Broyden, Fletcher, Goldfarb, and Shannon (BFGS) method.¹⁶ The convergence criteria are (i) 5×10^{-6} eV/atom for total energy, (ii) 0.01 eV/A for maximum ionic Hellmann–Feynman force, (iii) 5×10^{-4} Å for maximum ionic displacement, and (iv) 0.02 GPa for maximum stress.

RESULTS AND DISCUSSION

Structural and Electronic Properties

The $M_{n+1}AX_n$ phases crystallize in a hexagonal structure (space group P63/mmc) with two formula units per unit cell.^{[3](#page-8-0)} Crystal structures of $Ti_{n+1}GaN_n$ $(n = 1, 2, \text{ and } 3)$ compounds are formed by ceramiclike strongly bonded MX atomic layers and interleaved A layers (see Fig. 1). Structural optimizations were performed, including lattice parameters and internal coordinates. The calculated lattice parameters (a, c) and atomic positions are given in Table [I](#page-2-0).

Our results for $Ti₂GaN$ agree well with previous theoretical and experimental reports.^{[7,8](#page-8-0)} Since there are no experimental and theoretical data for the other compounds, the results for these compounds are compared to those of the compounds including $A = Si$ and Al.^{[6](#page-8-0)} The lattice parameters of α -type (β type) compounds are smaller (higher) than those of the $A = Ga$ case.

For $Ti_{n+1}GaN_n$ compounds, formation enthalpies were also calculated using the following common relation:

$$
E_{\text{from}}^{\text{Ti}_{n+1}\text{GaN}_n}=E_{\text{total}}^{\text{Ti}_{n+1}\text{GaN}_n}-\left[(n+1)\ E_{\text{solid}}^{\text{Ti}}+E_{\text{solid}}^{\text{Ga}}+nE_{\text{solid}}^{\text{N}}\right] \hspace{2cm}(1)
$$

| | \boldsymbol{a} 3.02 | \boldsymbol{c} | Atomic positions | | ΔH_f |
|--|--------------------------|--------------------|-------------------------------------|---|--------------|
| Ti ₂ GaN | | 13.31 | Ti 4f $(1/3, 2/3, 0.088)$ | Ti 4f $(1/3, 2/3, 0.092)^c$ | -1.25 |
| | 3.00 ^a | 13.33^{a} | Ga 2d $(1/3, 2/3, 3/4)$ | Ti 4f $(1/3, 2/3, 0.085)^d$ | |
| | 3.02 ^b | $13.32^{\rm b}$ | N 2a $(0, 0, 0)$ | | |
| | 2.99 ^c | 12.88° | | | |
| | 2.99 ^d | $13.64^{\rm d}$ | | | |
| α -Ti ₃ GaN ₂ | 3.01 | 18.21 | Ti ₁ 2a (0, 0, 0) | Ti_2 4f (2/3, 1/3, 0.136) ^c | -1.42 |
| | 2.99 ^c | 17.84^c | $Ti2$ 4f (2/3, 1/3, 0.130) | Ti_2 4f (2/3, 1/3, 0.129) ^d | |
| | 3.00 ^c | 18.49 ^d | Ga $2b(0, 0, 1/4)$ | N 4f $(1/3, 2/3, 0.069)^c$ | |
| | | | N 4f $(1/3, 2/3, 0.069)$ | N 4f $(1/3, 2/3, 0.068)^d$ | |
| β -Ti ₃ GaN ₂ | 2.99 | 18.47 | Ti ₁ 2a (0, 0, 0) | Ti_2 4f (2/3, 1/3, 0.136) ^c | -1 |
| | 2.96 ^c | 2.99 ^d | $Ti2$ 4f (2/3, 1/3, 0.129) | $Ti2$ 4f (2/3, 1/3, 0.128) ^d | |
| | 2.99 ^d | 18.67 ^d | Ga 2d $(2/3, 1/3, 1/4)$ | N 4f $(1/3, 2/3, 0.068)^c$ | |
| | | | N 4f (1/3, 2/3, 0.068) | N 4f $(1/3, 2/3, 0.067)^d$ | |
| α -Ti ₄ GaN ₃ | 3.00 | 23.22 | $Ti1$ 4e (0, 0, 0.155) | Ti_1 4e (0, 0, 0.160) ^c | -1.54 |
| | 3.00 ^c | 22.58° | Ti ₂ 4f(2/3, 1/3, 0.054) | Ti_1 4e (0, 0, 0.154) ^d | |
| | 3.00 ^d | $23.51^{\rm d}$ | Ga 2c (2/3, 1/3, 1/4) | $Ti2 4f(2/3, 1/3, 0.055)^c$ | |
| | | | N_1 4a $(0, 0, 0)$ | Ti_2 4f(2/3, 1/3, 0.054) ^d | |
| | | | N_2 4f (2/3, 1/3, 0.106) | N_2 4f (2/3, 1/3, 0.109) ^c | |
| | | | | N_2 4f (2/3, 1/3, 0.106) ^d | |
| β -Ti ₄ GaN ₃ | 2.98 | 23.60 | Ti_1 4f (1/3, 2/3, 0.055) | Ti_1 4f (1/3, 2/3, 0.055) ^c | -1.46 |
| | 2.99 ^c | 22.87 ^c | $Ti2$ 4f (2/3, 1/3, 0.657) | Ti_1 4f (1/3, 2/3, 0.054) ^d | -1.46 |
| | 2.98 ^d | 23.60 ^d | Ga 2c $(1/3, 2/3, 1/4)$ | $Ti2$ 4f (2/3, 1/3, 0.159) ^c | |
| | | | N_1 2a $(0, 0, 0)$ | Ti_2 4f (2/3, 1/3, 0.154) ^d | |
| | | | N_2 4f (2/3,1/3, 0.110) | N_2 4f (2/3, 1/3, 0.107) ^c | |
| | | | | N_2 4f $(2/3,1/3, 0.105)^d$ | |

Table I. The calculated equilibrium lattice parameters $(a,$ and c in \dot{A}), atomic positions, and formation energies (ΔH_f in eV/atom) for $Ti_{n+1}GaN_n$ compounds

where $E_{\text{solid}}^{\text{Ti}}$, $E_{\text{solid}}^{\text{Ga}}$ and $E_{\text{solid}}^{\text{N}}$ are calculated from Ti₂GaN, α -Ti₃GaN₂, β -Ti₃GaN₂, α -Ti₄GaN₃, and β -Ti4GaN3 structures, respectively. It is shown in Table I that all compounds are energetically stable due to the negative formation enthalpy values, indicating that it should be possible to synthesize the considered phases. Among the compounds, α -Ti₄GaN₃ is relatively the most stable.

The calculated partial and total density of states (DOS) are shown in Fig. [2](#page-3-0). It is clear that all compounds are metallic due to the fact that the DOS values differ from zero at the Fermi level. The most significant contribution to DOS comes from Ti dstates at the vicinity of the Fermi level. In addition, the delocalized bands in the energy range from -16 eV to -15 eV are dominated by an s orbital and from -15 eV to -13.5 eV they are dominated by a d orbital for all calculated compounds. Also, a strong hybridization exists between s and p orbitals that are from -9.5 eV to -7 eV, which indicates the presence of covalent interactions. A p orbital is dominant from -3 eV to -2 eV while a d orbital is dominant from -2 eV to 4 eV for all compounds.

On the other hand, DOS curves can be used to discuss the stability of the compounds by means of band filling theory.^{17,18} According to this theory; if the numbers of bonding (anti-bonding) states increase (decrease), the stability of the material increases. Thus, the ratio W_{occ} (the width of the occupied states)/ W_b (the width of the bonding states) may give information about the stability of the material. If the value of this ratio is closer to 1.0, the stability increases. In this study, the parameters given in Table [II](#page-4-0) for $Ti_{n+1}GaN_n$ suggest that $W_{\text{occ}}/W_{\text{b}}$ values are very closer to 1.0. On account of this, the $Ti_{n+1}GaN_n$ compounds turn out to be stable materials.

PHONON DISPERSION CURVES

The phonon frequencies and phonon dispersion curves of $Ti_{n+1}GaN_n$ compounds were calculated using the ''finite-displacement method'' in the CASTEP package[.19](#page-8-0) Specifically, the phonon dispersion curves were calculated along high symmetry directions using $a 2 \times 2 \times 2$ super cell. The obtained phonon dispersion curves are shown in Fig. [3.](#page-5-0) The calculated phonon frequencies in all directions and in all bands are real, demonstrating that these compounds are dynamically stable. Although there exist some works in the literature dedicated to these compounds, no experimental or theoretical works exist on the lattice dynamics for comparison with our results.

Fig. 2. Calculated partial density of states for $Ti_{n+1}GaN_n$ ($n = 1, 2$, and 3) compounds.

Table II. The width of occupied states W_{occ} (eV) and bonding states W_b (eV) for $Ti_{n+1}GaN_n$ compounds

| | $W_{\alpha ee}$ | $W_{\rm h}$ | $W_{\rm occ}/W_{\rm b}$ |
|--|-----------------|-------------|-------------------------|
| Ti ₂ GaN | 10.30 | 9.70 | 1.06 |
| α -Ti ₃ GaN ₂ | 10.20 | 9.40 | 1.09 |
| β -Ti ₃ GaN ₂ | 10.10 | 10.30 | 0.99 |
| α -Ti ₄ GaN ₃ | 10.25 | 10.23 | 1.00 |
| β -Ti ₄ GaN ₃ | 10.33 | 10.32 | 1.00 |

ELASTIC AND MECHANICAL PROPERTIES

The elastic constants (C_{ii}) provide information about the stability and stiffness of materials, and their first- principles calculation requires accurate methods. 20 In this study, the elastic constants are calculated by using both the ''slope technique'' from the phonon dispersion curves and the ''stress– strain" method. $21-23$ For a stable hexagonal structure, there are five independent elastic constants C_{ii} (i.e. C_{11} , C_{12} , C_{13} , C_{33} , and C_{44}), and they should satisfy the well-known Born–Huang criteria for mechanical stability 24 24 24 :

$$
C_{44} > 0, C_{11} > |C_{12}|, (C_{11} + 2C_{12}) C_{33} > 2C_{13}^2 \qquad (2)
$$

In the slope technique, the elastic modulus (C_{ii}) is obtained via the sound velocities (V) as derived from the initial slope of the acoustic phonon branches along specific high-symmetry and Christoffel's equation.² Thus, the elastic constants $(C_{11} = \rho (V_{LA} \[100])^2$, $C_{33} = \rho (V_{LA} [001])^2$, $C_{66} = \rho (V_{TA} [110]_{001>})^2$, $C_{44} =$ $\rho(\widetilde{V}_{TA}[110]_{\sim 001>}^2)$, and \widetilde{C}_{13} contributes to the sound velocity only for nonpure directions, where ρ is the density) are calculated from the acoustic phonon dispersion curves. The velocity of the longitudinal acoustic (LA) phonon branches along the [100] and [001] direction, that of the two transverse acoustic (TA) branches along the [110] direction, and that of the quasi longitudinal phonon branches along the [101] direction. The sound velocities which are calculated using the acoustic phonon branches are given in Table [III](#page-6-0).

The calculated elastic constants along with the other theoretical values in literature are given in Table $\text{IV.}^{2,7}$ $\text{IV.}^{2,7}$ $\text{IV.}^{2,7}$ $\text{IV.}^{2,7}$ $\text{IV.}^{2,7}$ $\text{IV.}^{2,7}$ $\text{IV.}^{2,7}$ It is seen that the present elastic constants of Ti₂GaN are in good agreement with the reported values. 2.7 To the best of our knowledge, no experimental data or theoretical calculations of elastic constants for other phases have been reported. It is shown from Table [IV](#page-6-0) that all compounds satisfy all the stability conditions (Eq. 2), and thus, $Ti_{n+1}GaN_n$ compounds are mechanically stable. From Table [IV](#page-6-0), it is also easily seen that α - Ti_4GaN_3 has the largest C_{11} , C_{12} , and C_{44} . Also, C_{11} is higher than C_{33} for all considered phases, showing that the incompressibility along the [1010] and [0110] directions is stronger than that along the

[0001] direction, implying that the bonding strength along the [1010] and [0110] directions is stronger than that along the $[0001]$ direction.^{[25](#page-8-0)}

The mechanical properties, such as bulk modulus (B) , Young's modulus (E) , shear modulus (G) and Poisson's ratio (v) , which are functions of the elastic constants, are calculated by using the Voigt–Reuss–Hill approximation, and are listed in Table [V](#page-6-0).^{[22,26](#page-8-0)}

The bulk modulus indicates the resistance to fracture, while the shear modulus indicates the resistance to plastic deformation. α -Ti₄GaN₃ has the highest bulk and shear moduli. If the value of E increases, the covalent nature of the material also increases.^{[27](#page-8-0)} Therefore, the covalent character of α - $Ti₄GaN₃$ is more dominant than that of other phases. Furthermore, Young's modulus provides a measure of the stiffness of the solid. 28 The highest E value occurs for β -Ti₄GaN₃ among the other phases, implying that it is stiffer as compared to other phases.

We have also predicted other mechanical properties such as brittleness and ductility, as the B/G ratio can be used to predict the brittle or ductile behavior of materials. According to the Pugh criterion (B/G), a material is brittle (ductile) if the B/G ratio is less (higher) than 1.75. The present values of B/G for $Ti_{n+1}GaN_n$ compounds are less than $1.75²⁹$ Hence, these materials will behave in a brittle manner. The $Ti₂GaN$ is the most brittle in these phases with the lowest Pugh value. Furthermore, the value of the Poisson's ratio is small $(v = 0.1)$ for covalent materials, whereas a typical value of v is 0.25 for ionic m materials.^{[30](#page-8-0)} From Table [V](#page-6-0), it can be seen that the calculated Poisson's ratio values approach 0.22. Thus, it can be expected that ionic nature of these materials is high. However, α -Ti₄GaN₃has the smallest Poisson's ratio, where this implies the covalent nature of the compound, and agrees with the high stability and high mechanical properties mentioned above.

Hardness is another important mechanical property of the materials and it can be theoretically calculated through different methods. A similar semi-empirical method was developed by Chen et al.^{[31](#page-8-0)} In this method, hardness of a given material that should be related to bulk and shear moduli can be calculated as;

$$
H_V = 2(k^2 G)^{0.585} - 3\tag{3}
$$

where $k = G/B$ is Pugh's modulus ratio. The calculated hardness values are given in Table [V.](#page-6-0) According to Table [V,](#page-6-0) these compounds are hard materials $(H_v > 10$ GPa) and the hardness order is β - $\mathrm{Ti}_3\mathrm{GaN}_2<\mathrm{a}\mathrm{Ti}_3\mathrm{GaN}_2<\mathrm{Ti}_2\mathrm{GaN}<\beta\mathrm{\cdot Ti}_4\mathrm{GaN}_3<\alpha\mathrm{\cdot}$ Ti4GaN3. As an important result, the most stable structure $(\alpha - Ti_4GaN_3)$ has the highest hardness.

THERMODYNAMIC PROPERTIES

The calculated phonon dispersion can be used to compute energy (E) , entropy (S) , free energy (F) , and heat capacity (C_v) as functions of temperature on $0-1000$ K range. The quantities were calculated by the following relations $32,33$;

| | V_{LA} [100] | V_{TA} [100] | V_{LA} [110] | V_{TA} [110] |
|--|----------------|----------------|----------------|----------------|
| Ti ₂ GaN | 7243 | 4409 | 4740 | 6922 |
| α -Ti ₃ GaN ₂ | 6295 | 3942 | 4001 | 6017 |
| β -Ti ₃ GaN ₂ | 5825 | 3626 | 3285 | 5699 |
| α -Ti ₄ GaN ₃ | 6622 | 4044 | 4044 | 6218 |
| β -Ti ₄ GaN ₃ | 6060 | 3733 | 3327 | 5938 |

Table III. The calculated sound velocity (V in m/s) using the acoustic phonon branches for $Ti_{n+1}GaN_n$ compounds

Table IV. The calculated Elastic constants $(C_{ij}$, in GPa) for $Ti_{n+1}GaN_n$ compounds

| | C_{11} | C_{12} | C_{13} | C_{33} | C_{44} |
|--|------------------|--------------|-----------------|---------------|------------------|
| Ti ₂ GaN | | | | | |
| Present (stress-strain) | 299.90 | 77.28 | 91.83 | 275.80 | 126.22 |
| Present (slope technique) | 297.41 | 77.00 | 115.57 | 271.64 | 127.34 |
| Theory ^a | $297^{\rm a}$ | $83^{\rm a}$ | 91 ^a | $273^{\rm a}$ | $119^{\rm a}$ |
| Theory ^b | 296 ^b | $84^{\rm b}$ | 92 ^b | $275^{\rm b}$ | 119 ^b |
| α -Ti ₃ GaN ₂ | | | | | |
| Present (stress-strain) | 337.49 | 82.80 | 123.64 | 308.25 | 133.98 |
| Present (slope technique) | 336.43 | 72.50 | 122.93 | 307.34 | 135.90 |
| β -Ti ₃ GaN ₂ | | | | | |
| Present (stress-strain) | 344.21 | 91.85 | 99.73 | 334.66 | 110.46 |
| Present (slope technique) | 342.74 | 77.06 | 100.70 | 328.08 | 109.04 |
| α -Ti ₄ GaN ₃ | | | | | |
| Present (stress-strain) | 401.37 | 103.38 | 108.72 | 357.78 | 154.70 |
| Present (slope technique) | 399.95 | 101.62 | 131.20 | 352.59 | 149.13 |
| β -Ti ₄ GaN ₃ | | | | | |
| Present (stress-strain) | 400.00 | 100.49 | 101.01 | 389.62 | 117.96 |
| Present (slope technique) | 398.14 | 96.08 | 110.84 | 382.21 | 119.96 |
| ^a Ref. 2 ^b Ref. 7. | | | | | |

Table V. The calculated bulk modulus (B, in GPa), Shear Modulus (G, in GPa), Young's modulus (E in GPa), Poisson's ratio (v) , and Hardness (H_v) in GPa) for $\mathrm{Ti}_{n+1}\mathrm{GaN}_n$ compounds

 $^{\rm a}$ Ref. [2](#page-8-0). $^{\rm b}$ Ref. [6](#page-8-0).

$$
E(T) = E_{\rm wt} + E_{\rm zp} + \int \frac{\hbar w}{\exp(\frac{\hbar w}{kT}) - 1} F(w) dw \qquad (4)
$$

$$
S(T) = k \left\{ \int \frac{\hbar w}{\exp(\frac{\hbar w}{kT}) - 1} F(w) dw \right\} \qquad (5)
$$

$$
-\int F(w)\bigg[1-\exp\bigg(-\frac{\hbar w}{kT}\bigg)\bigg]dw\bigg\}\tag{5}
$$

$$
F(T) = E_{\text{tot}} + E_{\text{zp}} + kT \int F(w) \ln\left[1 - \exp\left(-\frac{\hbar w}{kT}\right)\right] dw
$$
\n(6)

$$
C_v(T) = k \int \frac{\left(\frac{\hbar w}{kT}\right)^2 \exp\left(\frac{\hbar w}{kT}\right)}{\left[\exp\left(\frac{\hbar w}{kT}\right) - 1\right]^2} F(w) dw \hspace{1cm} (7)
$$

where E_{zp} is the zero-point energy, k is the Boltzmann's constant, \hbar is the Planck's constant and $F(\omega)$ is the phonon density of states. All energy-related properties including the enthalpy, entropy, and free energy for $Ti_{n+1}GaN_n$ are plotted in Fig. 4a–c, respectively. In an ensemble where the sample volume and temperature are independent variables, the relevant potential is the Helmholtz free energy, $F = E - T.S.$ So, the entropy is presented as a T.S product to allow comparison with the enthalpy and Helmholtz free energy.

Above 200 K, the free energy decreases gradually with increasing temperature and the value of the entropy, which is multiplied by the temperature, increases rapidly as the temperature increases, resulting in an almost linear relationship between enthalpy and temperature. The rate of change of entropy, enthalpy, and free energy with increasing temperature can be sorted from the highest to lowest as β -Ti₄GaN₃, α -Ti₄GaN₃, α -Ti₃GaN₂, β - $Ti₃GaN₂$, $Ti₂GaN$, respectively.

From Fig. 4d, C_v increases rapidly with temperature below 400 K, whereas the increase is slower above 400 K. In addition, the heat capacity approaches a constant known as the Dulong–Petit limit at higher temperatures.

CONCLUSIONS

First-principles calculations were performed to investigate the structural, electronic, mechanical, and dynamic properties of $Ti_{n+1}GaN_n$ compounds, among which α -Ti₄GaN₃ was found to be energetically the most stable. The calculated elastic constants showed that these compounds are mechanically stable. The polycrystalline elastic parameters have been further calculated within the scheme of Voigt–Reuss–Hill (VRH) approximation. These phases are brittle in nature with respect to the B/ G and hard materials. The computed density of states of $Ti_{n+1}GaN_n$ compounds reveals a metallic character. Phonon calculations confirm the dynamical stability of the studied phases. We believe that

our results can serve as a prediction for future investigations.

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