

# Determination of Gibbs Free Energy of Formation from Elements for $\text{Ca}_4\text{Fe}_9\text{O}_{17}$ by Solid-state Galvanic Cell

HUI-YU LI and XING-MIN GUO

Aiming to fill the thermodynamic blank in  $\text{CaO-FeO-Fe}_2\text{O}_3$  system, the determination of the Gibbs free energy of formation from elements for ternary  $\text{Ca}_4\text{Fe}_9\text{O}_{17}$  was carried out using a solid-state galvanic cell with air and calcium zirconate material, respectively, as the reference electrode and electrolyte. The ternary system  $\text{Ca}_2\text{Fe}_2\text{O}_5\text{-CaFe}_2\text{O}_4\text{-Ca}_4\text{Fe}_9\text{O}_{17}$  was selected as the measuring electrode and its equilibrium was confirmed. The essential thermodynamic data of  $\text{Ca}_2\text{Fe}_2\text{O}_5$  and  $\text{CaFe}_2\text{O}_4$  were cited from the reassessed data from a previous investigation. The reversible electromotive forces of the cell were determined from 1273 K to 1473 K (1000 °C to 1200 °C). The Gibbs free energy of formation from elements for  $\text{Ca}_4\text{Fe}_9\text{O}_{17}$  was derived and given by:

$$\Delta_f G_m^\circ(\text{Ca}_4\text{Fe}_9\text{O}_{17}) = -6218.862 \times 10^3 + 1247.762T + 31.32T \ln T \pm 2694 \text{ (J mol}^{-1}\text{)}$$

The increment of enthalpy and entropy of formation from elements for  $\text{Ca}_4\text{Fe}_9\text{O}_{17}$  at 298 K (25 °C) are calculated to be  $\Delta_f H_{m,298}^\circ = -6209.529 \times 10^3 \text{ (J mol}^{-1}\text{)}$  and  $\Delta_f S_{m,298}^\circ = -1038.009 \text{ (J mol}^{-1} \text{K}^{-1}\text{)}$ . The Ellingham diagram was developed in temperature range 1273 K to 1473 K (1000 °C to 1200 °C). The oxygen potential of  $\text{Ca}_4\text{Fe}_9\text{O}_{17}$  was found to be slightly higher than  $\text{CaFe}_2\text{O}_4$  and much higher than  $\text{Ca}_2\text{Fe}_2\text{O}_5$ .

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## I. INTRODUCTION

BECAUSE of the outstanding applications in iron-making industrial process, the Fe-Ca-O ternary system including various compounds has been focused on for decades. As the basic binders of iron ore, the amount and status of calcium ferrite compounds are viewed to be of central importance for iron ore sintering. The basic thermodynamic data play a key role in the estimation and evaluation of calcium ferrite compounds in iron ore. Unfortunately, the serious insufficiency of basic data on calcium ferrite compounds makes these works difficult to carry out. For three known binary compounds, the thermodynamic data of  $\text{Ca}_2\text{Fe}_2\text{O}_5$  ( $\text{C}_2\text{F}$ ) and  $\text{CaFe}_2\text{O}_4$  ( $\text{CF}$ ) have been reported repeatedly and can be identified more precisely, whereas the data of  $\text{CaFe}_4\text{O}_7$  ( $\text{CF}_2$ ) is unknown.<sup>[1-8]</sup> With respect to the large group of ternary calcium ferrite compounds in a  $\text{CaO-FeO-Fe}_2\text{O}_3$  system, only four of them,  $\text{CaFe}_3\text{O}_5$  ( $\text{CWF}$ ),  $\text{CaFe}_5\text{O}_7$  ( $\text{CW}_3\text{F}$ ),  $\text{Ca}_4\text{Fe}_9\text{O}_{17}$  ( $\text{C}_4\text{WF}_4$ ), and  $\text{Ca}_4\text{Fe}_{17}\text{O}_{29}$  ( $\text{C}_4\text{WF}_8$ ), are generally under consideration because of their well-documented existence.<sup>[9-14]</sup> The Gibbs free energy of reaction from oxides for  $\text{CaFe}_3\text{O}_5$  has been determined separately by Björkman<sup>[6]</sup> and Lykasov and Popova.<sup>[15]</sup> Björkman provided the only recorded Gibbs free energy of formation from elements for  $\text{CaFe}_5\text{O}_7$ .<sup>[6]</sup> Except for the measurements

mentioned above, no specific investigation concerning the Gibbs free energy of formation for ternary calcium ferrites can be found. Hence, much basic thermodynamic data is unknown and an urgent solution is required.

Two types of solid-state electrolytes of  $\text{CaF}_2$  and  $\text{ZrO}_2$ -based materials have been frequently employed to determine the Gibbs free energy of calcium ferrite compounds. However, the mostly used  $\text{CaF}_2$  cannot afford a high-temperature environment,<sup>[8]</sup> whereas the  $\text{ZrO}_2$ -based material is vulnerable to the  $\text{CaO}$  even below 1273 K (1000 °C).<sup>[16-18]</sup> The nonstoichiometric  $\text{Ca}_{1+x}\text{Zr}_{1-x}\text{O}_{3-x}$  material was reported as an excellent oxygen ionic conductor with almost pure ionic conduction and great chemical and thermal stability from the investigation provided by Janke.<sup>[19]</sup> It has been used as an electrolyte in a solid-state galvanic cell for thermodynamic determination by some investigations.<sup>[20-22]</sup>

In the current work, efforts were made to determine the Gibbs free energy of formation for a ternary calcium ferrite  $\text{Ca}_4\text{Fe}_9\text{O}_{17}$  ( $\text{C}_4\text{WF}_4$ ) using a solid-state galvanic cell embracing nonstoichiometric calcium zirconate ( $\text{CZO}$ ) electrolyte. Measurements were performed by the aid of the electromotive force (emf) method through a relative high temperature range of 1273 K to 1473 K (1000 °C to 1200 °C).

## II. EXPERIMENTAL

### A. Materials

Analytical reagent-grade chemicals  $\text{CaCO}_3$ ,  $\alpha\text{-Fe}_2\text{O}_3$ ,  $\text{Al}_2\text{O}_3$ , and electrolytic Fe supplied by the Sinopharm Chemical Reagent Company were served as starting materials.

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The essential  $\text{CaFe}_2\text{O}_4$ ,  $\text{Ca}_2\text{Fe}_2\text{O}_5$ , and wüitite were synthesized by a simple solid-state reaction. The dried  $\text{CaCO}_3$  and  $\alpha\text{-Fe}_2\text{O}_3$  were completely mixed in a stoichiometric ratio of  $\text{Ca}_2\text{Fe}_2\text{O}_5$  and  $\text{CaFe}_2\text{O}_4$ . The mixtures were pressed into cylindrical specimens under 5 MPa pressure and then sintered at 1473 K (1200 °C) for 8 hours in air. The wüitite was selected as another basic material for the preparation of electrode mixture. To obtain wüitite, calculated amounts of  $\alpha\text{-Fe}_2\text{O}_3$  and electrolytic iron powder in 1.1:1 molar ratio were fully mixed and then compacted into cylindrical specimens under 5 MPa pressure. The wüitite was synthesized by heating the mixture at 1173 K (900 °C) for 5 hours under Ar inert condition in a steel crucible and followed by quenching operation in liquid nitrogen. The compositions of resultant specimen were identified by X-ray diffraction (XRD) determination. Single-phase samples were qualified.

For further synthesis, the obtained high pure  $\text{Ca}_2\text{Fe}_2\text{O}_5$ ,  $\text{CaFe}_2\text{O}_4$  and wüitite were toughly ground to pass 300 meshes. Besides, adopted as filler material, amounts of high pure  $\text{Al}_2\text{O}_3$  agent powder was calcined at 1473 K (1200 °C) for 3 hours in air and then ground to pass 300 meshes as well.

### B. Phase Exploration

A thermodynamically stable system performing a reversible oxidation–reduction reaction and providing a constant oxygen partial pressure should be adequate for working as measuring electrode in electrochemical determination. According to the ACerS-NIST Phase Equilibrium Diagrams (No. 05038 and No. 02110), a ternary phase system of  $\text{Ca}_2\text{Fe}_2\text{O}_5\text{-CaFe}_2\text{O}_4\text{-Ca}_4\text{Fe}_9\text{O}_{17}$  came into our sight, which was theoretically confirmed to be stable within 1273 K to 1473 K (1000 °C to 1200 °C) by Imlach and Glasser<sup>[23]</sup> and by Phillips and Muan.<sup>[10]</sup> The composition relations of all possible compounds on the section of  $\text{Fe}_2\text{O}_3\text{-CaO-FeO}$  system are depicted in Figure 1. No possible fourth substance exists in the field of the selected  $\text{Ca}_2\text{Fe}_2\text{O}_5\text{-CaFe}_2\text{O}_4\text{-Ca}_4\text{Fe}_9\text{O}_{17}$  system. Hence, the  $\text{Ca}_2\text{Fe}_2\text{O}_5$ ,  $\text{CaFe}_2\text{O}_4$ , and  $\text{Ca}_4\text{Fe}_9\text{O}_{17}$  are suggested to perform at thermodynamic equilibrium.

To examine and synthesize *in situ* the expected equilibrium ternary phase system, the previously prepared  $\text{CaFe}_2\text{O}_4$ ,  $\text{Ca}_2\text{Fe}_2\text{O}_5$ , and wüitite were completely mixed and poured into an alumina crucible then tamped toughly until it was difficult to insert a thin needle. For filling, the previously calcined  $\text{Al}_2\text{O}_3$  powder was continuously poured and tamped into crucible until it was filled up and the inner powder was hard. At last, the crucible was sealed using cement seal. After drying for 2 days at room temperature in air, the sealed sample was heated at 1473 K (1200 °C) for 2 days then followed by quenching in liquid nitrogen. The resulting composition of mixture was identified by the XRD method. It would be qualified if the products are identical to the ideal system  $\text{Ca}_2\text{Fe}_2\text{O}_5\text{-CaFe}_2\text{O}_4\text{-Ca}_4\text{Fe}_9\text{O}_{17}$  with no other phase detected. Ascribed to the further formation of  $\text{CaFe}_2\text{O}_4$  and inevitable oxidation of wüitite caused by the introduced oxygen during sample assembling, the

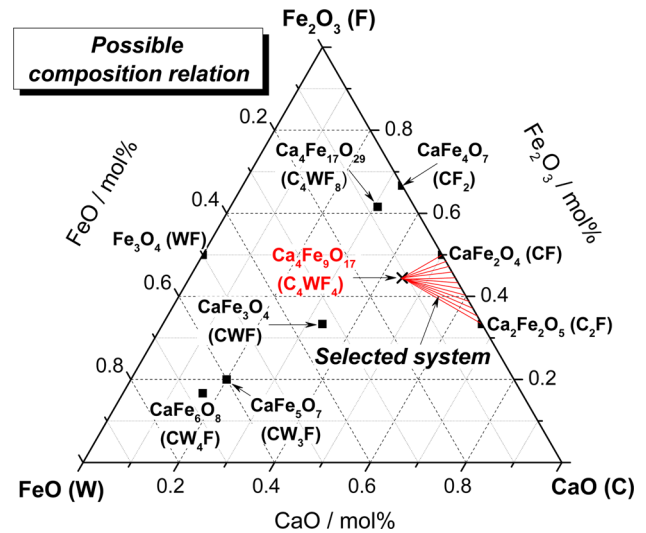
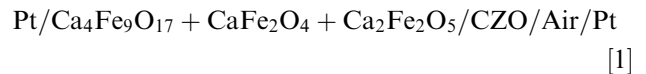


Fig. 1—Composition relations of possible compounds in  $\text{FeO-CaO-Fe}_2\text{O}_3$  system.

mixture with a molar ratio  $\text{Ca}_2\text{Fe}_2\text{O}_5\text{:CaFe}_2\text{O}_4\text{:FeO} = 2\text{:}1\text{:}7$  was experimentally proved to be adequate.

### C. Electrochemical Measurements

Based on the qualification of  $\text{Ca}_2\text{Fe}_2\text{O}_5\text{-CaFe}_2\text{O}_4\text{-Ca}_4\text{Fe}_9\text{O}_{17}$  system, materials of  $\text{Ca}_2\text{Fe}_2\text{O}_5$ ,  $\text{CaFe}_2\text{O}_4$ , and  $\text{FeO}$  in identical molar ratio were repeatedly mixed to produce the measuring electrode. The Gibbs free energy of formation from elements for  $\text{Ca}_4\text{Fe}_9\text{O}_{17}$  was determined by the cell



The air electrode was adopted as positive electrode on the right-hand side. A gas electrode is said to hold more precise oxygen pressure than the metal–metal oxide electrode.<sup>[24,25]</sup>

The apparatus for electrochemical measurements was depicted in Figure 2. A nonstoichiometric CZO electrolyte ceramic tube with one end closed and measuring 0.7 cm in diameter and 3.1 cm in length was used as the solid-state electrolyte. The employed CZO tube was synthesized *via* a co-precipitation method as described in our previous work<sup>[26]</sup> and shaped by injection molding process. The tube was tested for leaks and found to be impervious. The porous Pt electrode coats were fabricated by uniformly applying Pt paste over both the inner and outer bottom surfaces of CZO tube. Two Pt wires including one twining on the outer bottom and the other spirally adhering to the inner bottom were co-fired with the Pt paste at 1123 K (850 °C) for 3 hours in air. Consequently, uniform and porous Pt electrode films with Pt leads adhering on the inner and outer bottom surfaces were obtained simultaneously. The assembly of a galvanic cell is similar to the process described in a previous phase equilibrium exploration. The whole apparatus was placed inside a vertical furnace with Pt wires

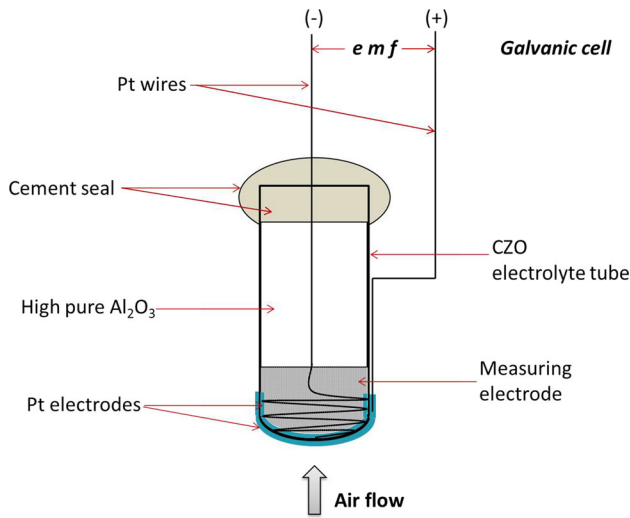


Fig. 2—Schematic diagram of the assembled galvanic cell for electrochemical measurement.

extending out and connecting to the CHI660B Electrochemical Workstation, which possesses the accuracy of  $\pm 0.1$  mV. A Faraday cage made of stainless steel foil was placed between the furnace tube and the cell. The air reference electrode was served by a constant dry air flow at a rate of  $300 \text{ mL min}^{-1}$  over the outer Pt electrode.

As the cell was heated to a specific temperature, because of the different oxygen pressures of measuring electrode and reference electrode, an emf can be established on both Pt electrode sides of electrolyte and the signal can be continuously picked up by the CHI660 Electrochemical Workstation. Before measurement, the cell was heated for 1 day to equalize the measuring electrode system. The time taken for the cell to attain a nearly constant emf value is no longer than 50,000 seconds. The reversibility of cell was checked by microcoulometric titration method in both directions.<sup>[27,28]</sup> A small voltage was applied in both directions, and whether the emf returned to the value before titration was observed.

### III. RESULTS AND DISCUSSION

#### A. Phase Identification

The XRD patterns of synthesized  $\text{Ca}_2\text{Fe}_2\text{O}_5$ ,  $\text{CaFe}_2\text{O}_4$  and wüsite are shown in Figure 3. Highly pure  $\text{Ca}_2\text{Fe}_2\text{O}_5$ ,  $\text{CaFe}_2\text{O}_4$  and wüsite can be identified without any trace of a possible second phase detected. They are qualified for subsequent phase exploration.

The XRD patterns of long-term-heated products from  $\text{Ca}_2\text{Fe}_2\text{O}_5$ - $\text{CaFe}_2\text{O}_4$ -FeO mixture are presented in Figure 4. A ternary phase system consisting of  $\text{Ca}_2\text{Fe}_2\text{O}_5$ ,  $\text{CaFe}_2\text{O}_4$ , and  $\text{Ca}_4\text{Fe}_9\text{O}_{17}$  can be confirmed. After being checked by the standard PDF (The Powder Diffraction File from The Joint Committee on Powder Diffraction Standards) data, no obvious shift in peak location was detected, which indicates a low possibility of forming a solid-solution system. Actually, the significant

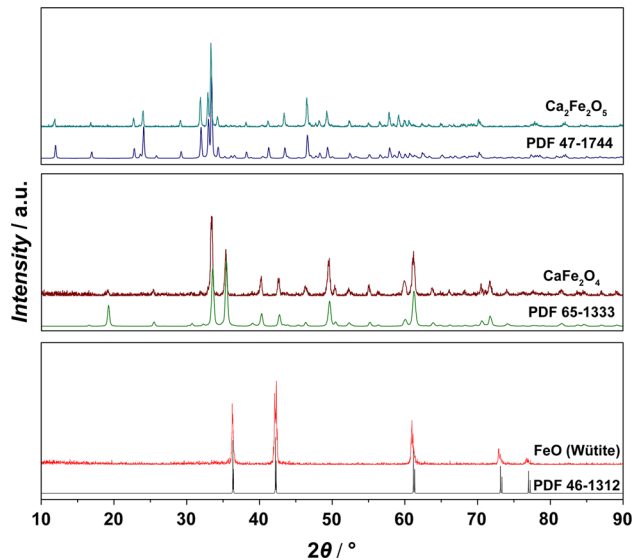


Fig. 3—XRD patterns of synthesized  $\text{Ca}_2\text{Fe}_2\text{O}_5$ ,  $\text{CaFe}_2\text{O}_4$  and Wüsite.

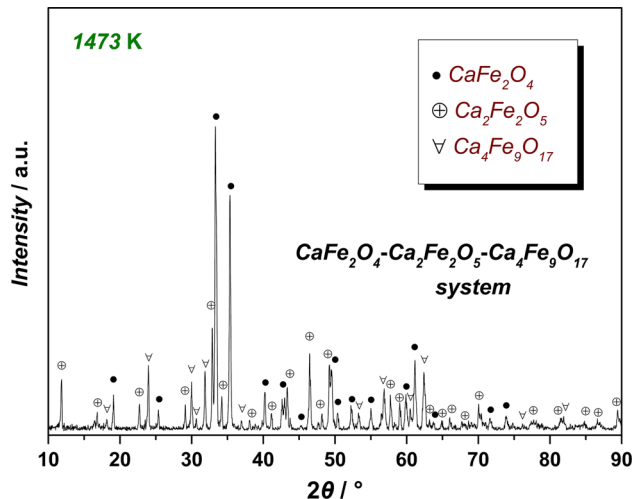


Fig. 4—XRD patterns of synthesized  $\text{Ca}_4\text{Fe}_9\text{O}_{17}$ - $\text{CaFe}_2\text{O}_4$ - $\text{Ca}_2\text{Fe}_2\text{O}_5$  ternary system.

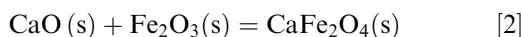
difference in lattice structure between  $\text{Ca}_4\text{Fe}_9\text{O}_{17}$  and binary calcium ferrites of  $\text{CaFe}_2\text{O}_4$  and  $\text{Ca}_2\text{Fe}_2\text{O}_5$ , suggests the  $\text{Ca}_4\text{Fe}_9\text{O}_{17}$ -contained solid solution is hard to form in this system. In contrast, the phase diagram of  $\text{CaO}$ - $\text{Fe}_2\text{O}_3$  binary system from investigation by Phillips and Muan clearly shows no solid solution appearing between  $\text{CaFe}_2\text{O}_4$  and  $\text{Ca}_2\text{Fe}_2\text{O}_5$  below 1489 K (1216 °C).<sup>[29]</sup> Therefore, the formation of a solid solution among this equilibrium phases is excluded.

In the transition process from initial  $\text{Ca}_2\text{Fe}_2\text{O}_5$ - $\text{CaFe}_2\text{O}_4$ -FeO mixture to the equilibrium  $\text{Ca}_2\text{Fe}_2\text{O}_5$ - $\text{CaFe}_2\text{O}_4$ - $\text{Ca}_4\text{Fe}_9\text{O}_{17}$  system, the FeO in the starting components plays an important role as Figure 5 shows. Partial FeO combines with  $\text{CaFe}_2\text{O}_4$  to produce the  $\text{Ca}_4\text{Fe}_9\text{O}_{17}$ , whereas the other FeO is thought of being oxidized to  $\text{Fe}_2\text{O}_3$  and subsequently consumed between

$\text{Ca}_2\text{Fe}_2\text{O}_5$  and  $\text{CaFe}_2\text{O}_4$ . Finally, the  $\text{Ca}_2\text{Fe}_2\text{O}_5$ ,  $\text{CaFe}_2\text{O}_4$  and produced  $\text{Ca}_4\text{Fe}_9\text{O}_{17}$  form the equilibrium ternary phase system.

### B. Essential Thermodynamic Data

In the light of phase exploration, the  $\text{Ca}_2\text{Fe}_2\text{O}_5$ - $\text{CaFe}_2\text{O}_4$ - $\text{Ca}_4\text{Fe}_9\text{O}_{17}$  system is confirmed to be qualified for working as the measuring electrode. As a key to the determination of the unknown thermodynamic properties of  $\text{Ca}_4\text{Fe}_9\text{O}_{17}$ , reliable standard thermodynamic data of  $\text{CaFe}_2\text{O}_4$  and  $\text{Ca}_2\text{Fe}_2\text{O}_5$  are essential. The standard data of  $\text{CaFe}_2\text{O}_4$  and  $\text{Ca}_2\text{Fe}_2\text{O}_5$  are rarely included in thermodynamic compilations except for the records by Knacke *et al.*<sup>[30]</sup> In contrast, their available experimental data have been frequently reported, for instance by Rezukhina and Baginska,<sup>[3]</sup> by Rajagopalan *et al.*,<sup>[4,5]</sup> by Björkman,<sup>[6]</sup> by Jacob *et al.*,<sup>[7]</sup> and the latest by Forsberg *et al.*<sup>[8]</sup> The Gibbs free energy of formation from elements for  $\text{Ca}_2\text{Fe}_2\text{O}_5$  was always given directly. Regarding the  $\text{CaFe}_2\text{O}_4$ , the Gibbs free energy of formation from oxides based on Reaction [2] was mostly provided.



A comparison of Gibbs free energy of formation from elements for  $\text{Ca}_2\text{Fe}_2\text{O}_5$  in different investigations is

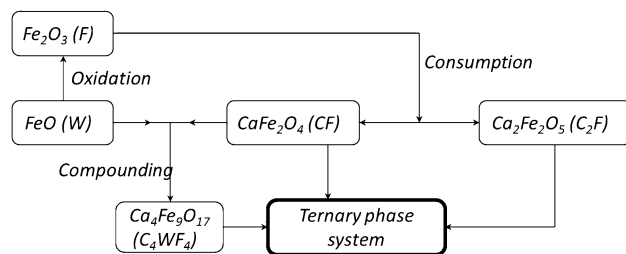


Fig. 5—Transition path from starting mixture to the equilibrium system.

performed in Figure 6(a), whereas the Gibbs free energy of formation from oxides for  $\text{CaFe}_2\text{O}_4$  is drawn in Figure 6(b). For  $\text{Ca}_2\text{Fe}_2\text{O}_5$ , the agreement between the study by Björkman and by Forsberg *et al.* is excellent, whereas the result given by Rajagopalan *et al.* deviates somewhat. In contrast with the situation of  $\text{Ca}_2\text{Fe}_2\text{O}_5$ , the relative larger deviation of reference data for  $\text{CaFe}_2\text{O}_4$  can be clearly seen. The result provided by Jacob *et al.* shows a positive slope, which is entirely different to the negative slope values by Forsberg *et al.* and by Rezukhina and Baginska. Actually, there is controversy on the thermodynamic data of  $\text{CaO}$  in various compilations, which may give rise to the discrepancies in resultant data of  $\text{Ca}_2\text{Fe}_2\text{O}_5$  and  $\text{CaFe}_2\text{O}_4$ . Taking this into account and considering the suggestion provided by Jacob and Varghese,<sup>[31]</sup> Forsberg *et al.* cited the essential data from the more accurate JANAF Thermochemical Tables<sup>[32]</sup> and demonstrated a series experimental work of high quality. Hence, the data reported by Forsberg *et al.* are more reliable. However, the essential data of  $\text{CaO}$  dedicated by Forsberg *et al.* were derived *via* a nonlinear simulation in a narrow temperature range of 1000 K to 1400 K (727 °C to 1127 °C). Obviously, a fitting work through a wide temperature range is necessary to obtain more accurate essential data for subsequent citation. Thus, a nonlinear simulation was carried out by the aid of the least squares regression analysis from 300 K to 1700 K (27 °C to 1427 °C) for the extracted data from JANAF Thermochemical Tables.<sup>[32]</sup> The results are shown in Figure 7.

The wide-range nonlinear simulation by the current work exhibits higher accuracy especially at a lower temperature range. It is expected to be more accurate for the extrapolation of the resultant data in a low temperature range. Extracted from JANAF Thermochemical Tables,<sup>[32]</sup> the mathematical expressions of new simulated Gibbs free energy of formation from elements for  $\text{CaO}$  and  $\text{Fe}_2\text{O}_3$  are respectively denoted as Eqs. [3] and [4], and the methods taken for reassessing thermodynamic data of  $\text{CaFe}_2\text{O}_4$  and  $\text{Ca}_2\text{Fe}_2\text{O}_5$  are described in Figure 8.

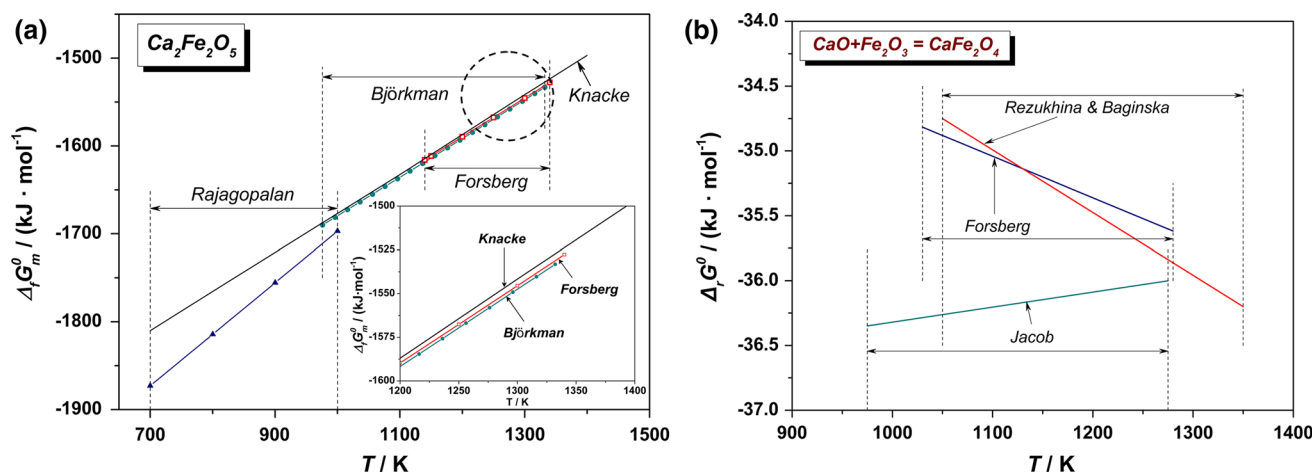
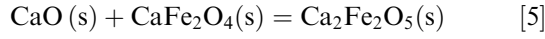


Fig. 6—Comparisons of (a)  $\Delta_f G_m^\circ(\text{Ca}_2\text{Fe}_2\text{O}_5)$  and (b)  $\Delta_r G^\circ$  for reaction  $\text{CaO} + \text{Fe}_2\text{O}_3 = \text{CaFe}_2\text{O}_4$  from different references.



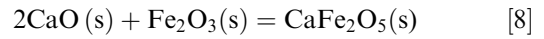
$$\Delta_f G_m^\circ(\text{CaO}) = -629.623 \times 10^3 + 45.161T + 7.83T \ln T \text{ (J mol}^{-1}\text{)} \quad [3]$$

$$\Delta_f G_m^\circ(\text{Fe}_2\text{O}_3) = -807.662 \times 10^3 + 246.109T \text{ (J mol}^{-1}\text{)} \quad [4]$$



$$\Delta_r G^\circ(2) = -2E_1 F \quad [6]$$

$$\Delta_r G^\circ(5) = -2E_2 F \quad [7]$$



$$\Delta_r G^\circ(8) = -2(E_1 + E_2)F \quad [9]$$

$$E_1 = 163.3 + 0.01664T (\pm 2.2 \text{ mV})^{[8]} \quad [10]$$

$$E_2 = -31.2 + 0.1267T (\pm 2.9 \text{ mV})^{[8]} \quad [11]$$

$$\Delta_r G^\circ(\text{CaFe}_2\text{O}_4) = -31.512 \times 10^3 - 3.211T \pm 425 \text{ (J mol}^{-1}\text{)} \quad [12]$$

$$\Delta_r G^\circ(\text{Ca}_2\text{Fe}_2\text{O}_5) = -25.491 \times 10^3 - 27.66T \pm 984 \text{ (J mol}^{-1}\text{)} \quad [13]$$

$$\Delta_f G_m^\circ(\text{CaFe}_2\text{O}_4) = -1468.797 \times 10^3 + 288.059T + 7.83T \ln T \pm 425 \text{ (J mol}^{-1}\text{)} \quad [14]$$

$$\Delta_f G_m^\circ(\text{Ca}_2\text{Fe}_2\text{O}_5) = -2092.399 \times 10^3 + 308.771T + 15.66T \ln T \pm 984 \text{ (J mol}^{-1}\text{)} \quad [15]$$

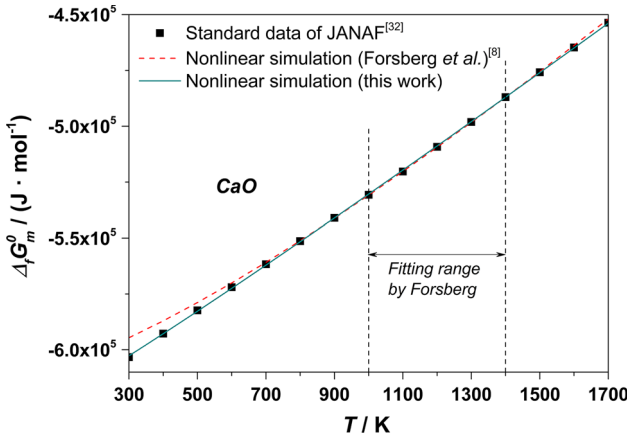


Fig. 7—Nonlinear simulations of  $\Delta_f G_m^\circ(\text{CaO})$  through different temperature range.

The Gibbs free energy of Reactions [2] and [5] are formulated as Eqs. [6] and [7]. Equation [6] directly relates to the Gibbs free energy of formation from oxides for  $\text{CaFe}_2\text{O}_4$ , whereas that of  $\text{Ca}_2\text{Fe}_2\text{O}_5$  has to be deduced by a simple addition and expressed in Eq. [9].

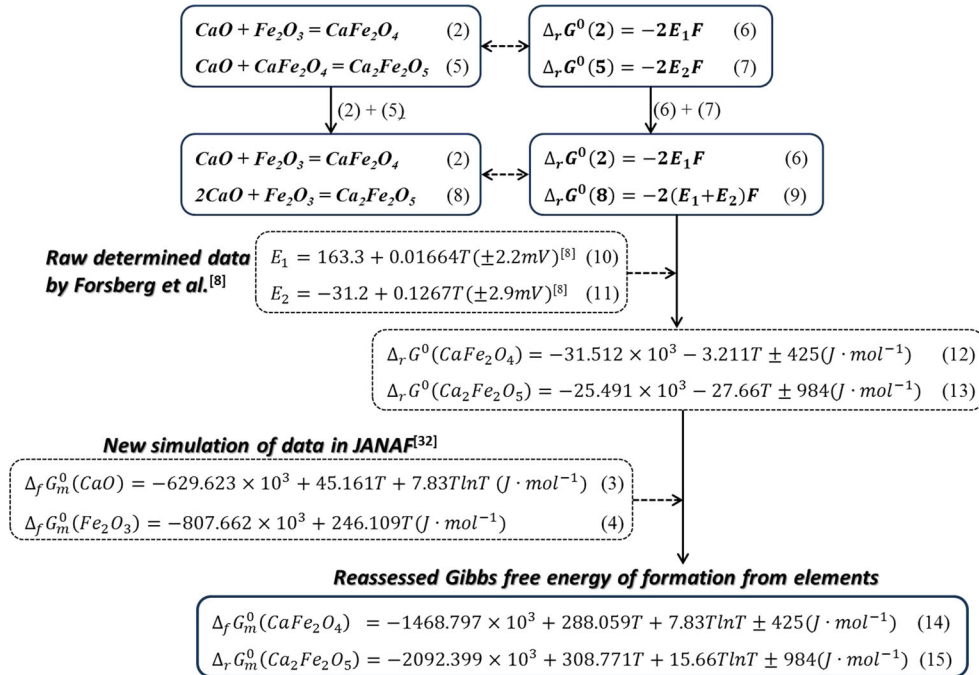
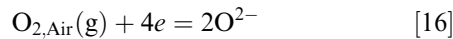


Fig. 8—The reassessing path of  $\Delta_f G_m^\circ(\text{CaFe}_2\text{O}_4)$  and  $\Delta_f G_m^\circ(\text{Ca}_2\text{Fe}_2\text{O}_5)$  based on investigation by Forsberg et al.<sup>[8]</sup> and JANAF Thermochemical Tables.<sup>[32]</sup>

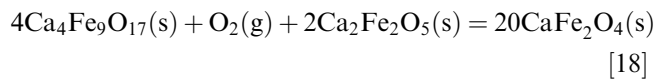
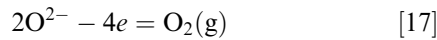
The  $F$  represents the Faraday constant with a recommended value of  $96,485.3 \text{ C mol}^{-1}$  advised by NIST.<sup>[33]</sup> The emfs of  $E_1$  and  $E_2$  dependent on temperature are determined as Eqs. [10] and [11] by Forsberg *et al.*<sup>[8]</sup> By introducing the raw determined data of Forsberg *et al.*<sup>[8]</sup> the Gibbs free energy of formation from oxides for  $\text{CaFe}_2\text{O}_4$  and  $\text{Ca}_2\text{Fe}_2\text{O}_5$  can be calculated as Eqs. [12] and [13]. In this way, the Gibbs free energy of formation from elements for  $\text{CaFe}_2\text{O}_4$  and  $\text{Ca}_2\text{Fe}_2\text{O}_5$  can be obtained by taking our new simulation data from Eqs. [3] and [4] into [12] and [13]. The final results are presented as Eqs. [14] and [15].

### C. Electrochemical Determination

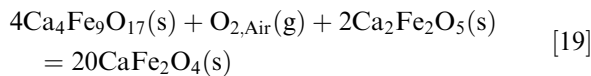
For the measured cell, the oxygen pressure on the right-hand positive electrode depends on the following reaction:



On the left-hand negative electrode, the oxygen chemical potential is fixed by the equilibrium inside ternary phase system, which is described as



Then overall cell reaction is illustrated by



The electrochemical relation for Reaction [19] can be directly established as

$$\Delta_r G = -4EF \quad [20]$$

The  $\Delta_r G$  and  $E$ , respectively, represent the Gibbs free energy of Reaction [19] and the determined emfs of cell. Theoretically, by another transformation, the calculation for Gibbs free energy of formation from elements for  $\text{Ca}_4\text{Fe}_9\text{O}_{17}$  can be achieved as

$$\Delta_f G_m^\circ(\text{Ca}_4\text{Fe}_9\text{O}_{17}) = 5\Delta_f G_m^\circ(\text{CaFe}_2\text{O}_4) - \frac{1}{2}\Delta_f G_m^\circ(\text{Ca}_2\text{Fe}_2\text{O}_5) - \frac{1}{4}RT \ln p_{\text{O}_2,\text{air}} + EF \quad [21]$$

Taking the determined equilibrium emfs and the prepared essential data  $\Delta_f G_m^\circ(\text{CaFe}_2\text{O}_4)$  and  $\Delta_f G_m^\circ(\text{Ca}_2\text{Fe}_2\text{O}_5)$  into Eq. [21], the expected  $\Delta_f G_m^\circ(\text{Ca}_4\text{Fe}_9\text{O}_{17})$  can be obtained.

The varying lines of emfs during the measuring process at different temperatures are shown in Figure 9. More time is spent to attain steady value at a lower temperature. The emf values are found decrease with the rise of temperature. Generally, the equilibrium reaction in the measuring electrode results in higher oxygen pressure as temperature increases, whereas the oxygen pressure on air reference electrode is constant. Consequently, the difference of oxygen potential between electrodes is produced to be closer. It should be responsible for the reducing emf values.

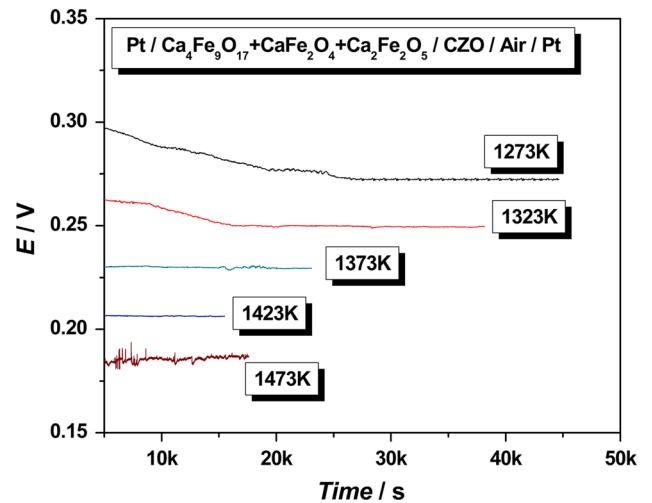


Fig. 9—The determined emf values at different temperatures between 1273 K and 1473 K (1000 °C to 1200 °C).

The obtained emf values dependent on temperature were plotted in Figure 10. A highly linear relation can be clearly observed and its mathematical expression was obtained by the linear fitting method. According to the mathematical relation [21], the Gibbs free energy of formation from elements for  $\text{Ca}_4\text{Fe}_9\text{O}_{17}$  is obtained as

$$\Delta_f G_m^\circ(\text{Ca}_4\text{Fe}_9\text{O}_{17}) = -6218.862 \times 10^3 + 1247.762T + 31.32T \ln T \pm 2694 \text{ (J mol}^{-1}\text{)} \quad [22]$$

The uncertainty in  $\Delta_f G_m^\circ(\text{Ca}_4\text{Fe}_9\text{O}_{17})$  should be attributed to the data taken from the references, especially for the introduced data of  $\text{CaFe}_2\text{O}_4$ , which possesses a significant high stoichiometric coefficient in Reaction [19]. In such a situation, even a tiny uncertainty is apt to be amplified several times.

### D. Oxygen Potential

Developed from the results in the current work, the Ellingham diagram for substances with available thermodynamic data in  $\text{FeO-CaO-Fe}_2\text{O}_3$  system from 1273 K to 1473 K (1000 °C to 1200 °C) is revealed in Figure 11. Obviously, the  $\text{Ca}_2\text{Fe}_2\text{O}_5$  exhibits the best thermodynamic stability, followed by  $\text{CaFe}_2\text{O}_4$  and  $\text{Ca}_4\text{Fe}_9\text{O}_{17}$ . The oxygen potential of  $\text{CaFe}_2\text{O}_4$  and  $\text{Ca}_4\text{Fe}_9\text{O}_{17}$  seems close to each other with the  $\text{CaFe}_2\text{O}_4$  showing slightly more stable.

### E. The Enthalpy and Entropy of $\text{Ca}_4\text{Fe}_9\text{O}_{17}$ at 298 K (25 °C)

Indicated by the mathematical expression (Eq. [22]), we cannot directly read the enthalpy  $\Delta_f H_{298}^\circ$  and entropy  $\Delta_f S_{298}^\circ$  of  $\text{Ca}_4\text{Fe}_9\text{O}_{17}$  by the constant term and coefficients of the temperature-dependent term because of the nonzero increment of heat capacity  $\Delta C_p$  at specific temperature for the formation reaction of  $\text{Ca}_4\text{Fe}_9\text{O}_{17}$ . In

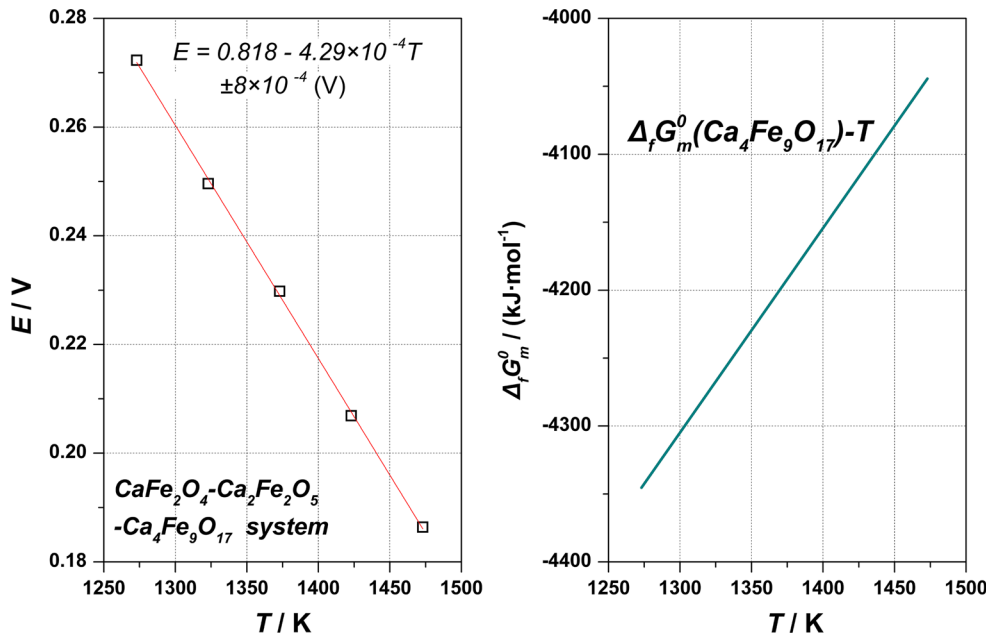


Fig. 10—The emf and derived  $\Delta_f G_m^{\circ}(\text{Ca}_4\text{Fe}_9\text{O}_{17})$  values dependent on temperature.

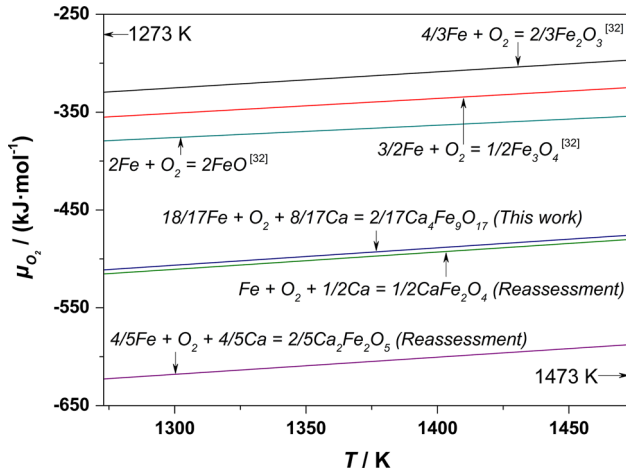


Fig. 11—The Ellingham diagram for important oxides of FeO-CaO- $\text{Fe}_2\text{O}_3$  system in 1273 K to 1473 K (1000 °C to 1200 °C).

this situation, according to the Kirchhoff relation, the increment of enthalpy  $\Delta_f H_T^{\circ}$  can be obtained by

$$\int_{298}^T d\Delta_f H_T^{\circ} = \Delta C_p \int_{298}^T dT \quad [23]$$

and further computed as

$$\Delta_f H_T^{\circ} = \Delta_f H_{298}^{\circ} + \Delta C_p T - 298\Delta C_p \quad [24]$$

Taking Eq. [24] into the Gibbs-Helmholtz equation

$$d\left(\frac{\Delta G_T^{\circ}}{T}\right) = -\frac{\Delta H_T^{\circ}}{T^2} dT \quad [25]$$

one can obtain

$$\Delta_f G_T^{\circ} = (\Delta_f H_{298}^{\circ} - 298\Delta C_p) + (\Delta C_p + \Delta C_p \ln 298 - \Delta_f S_{298}^{\circ})T - \Delta C_p T \ln T \quad [26]$$

Comparing Eq. [26] with the corresponding terms in Eq. [22], the increment of enthalpy and entropy of formation from elements for  $\text{Ca}_4\text{Fe}_9\text{O}_{17}$  at 298 K (25 °C) can be obtained as  $\Delta_f H_{m,298}^{\circ} = -6209.529 \times 10^3$  (J mol<sup>-1</sup>) and  $\Delta_f S_{m,298}^{\circ} = -1038.009$  (J mol<sup>-1</sup> K<sup>-1</sup>).

#### IV. CONCLUSIONS

The Gibbs free energy of formation from elements for a ternary calcium ferrite compound  $\text{Ca}_4\text{Fe}_9\text{O}_{17}$  was determined through a temperature range of 1273 K to 1473 K (1000 °C to 1200 °C). A solid-state galvanic cell was employed embracing an air reference electrode and calcium zirconate electrolyte. The ternary phase system  $\text{CaFe}_2\text{O}_4$ - $\text{Ca}_2\text{Fe}_2\text{O}_5$ - $\text{Ca}_4\text{Fe}_9\text{O}_{17}$  was confirmed to be thermodynamically stable within the measuring temperature range and was selected for working as a measuring electrode. During the measuring process, the increase in oxygen pressure in ternary equilibrium phases can be clearly read by the decreasing emf value with the increase of temperature. Revealed by the determined thermodynamic data, the  $\text{Ca}_4\text{Fe}_9\text{O}_{17}$  possesses a slightly lower thermodynamic stability than that of  $\text{CaFe}_2\text{O}_4$  and is remarkably unstable compared with  $\text{Ca}_2\text{Fe}_2\text{O}_5$ .

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