# The Role of Iron in the Formation of Porosity in Al-Si-Cu– Based Casting Alloys: Part III. A Microstructural Model

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Iron has been shown to have a significant effect on the formation of porosity and shrinkage defects in Al-Si-Cu–based foundry alloys. This is not simply a direct consequence of the physical presence of the  $\beta$ -Al<sub>5</sub>FeSi platelets in the microstructure, but is also due to the effect that these platelets have on the nucleation and growth of eutectic silicon. The alloy-dependent critical iron content determines when the  $\beta$  phase first solidifies and, hence, when it can participate in the silicon nucleation event. At critical iron contents, the  $\beta$  phase solidifies as the initial component of the ternary eutectic. However, at supercritical iron contents, the  $\beta$  phase is already well developed when ternary eutectic solidification begins, while, at subcritical iron contents, the  $\beta$  phase forms as a component of the ternary eutectic only after the binary Al-Si eutectic is well established. Each of these paths of microstructural evolution leads to different variations in microstructural permeability and, hence, interdendritic feedability and porosity formation. The actual porosity-forming response to these alloyinduced microstructural changes is influenced by the solidification conditions in the casting.

**VOLUMETRIC** shrinkage occurs during the solidifica-<br>tion of most alloys. In order to produce a casting free from<br>slumping, contraction, and/or internal porosity, this shrink-<br>age must be compensated by an unimpeded suppl age-related defect. Various researchers have proposed that the presence of  $\beta$  platelets within the interdendritic spaces of iron-containing Al-Si alloys causes physical blockages to interdendritic fluid flow and that these make feeding more

mental observations described in two companion articles.<sup>[4,5]</sup> In that work, iron is shown to play an important role in the development of porosity and shrinkage defects in unmodified, nongrain-refined hypoeutectic Al-Si alloys that also contain approximately 1 pct Cu and 0.5 pct Mg. The role of iron is manifest as a distinctive threefold effect that is where  $f_L$  is the volume fraction of liquid, *n* is the number also dependent on the silicon content of the alloy and which of channels per unit cross-sectiona also dependent on the silicon content of the alloy and which

At a critical iron content, solidification proceeds directly from primary dendrite formation to the formation of the The parameters *n* and  $\tau$  are typically assumed to be conternary  $AI-Si-BAI<sub>s</sub>FeSi eutectic$ . The minimum total porosity stant and, consequently, the permeability of a solidifying occurs at this iron level. As the iron content varies to either structure is assumed to be solely dependent on the diminish-<br>side of the critical value, the overall porosity increases. At ing volume fraction of liquid. How side of the critical value, the overall porosity increases. At ing volume fraction of liquid. However, various microstruc-<br>supercritical iron contents, there is also an increase in the tural changes can lead to changes in likelihood of localized, interconnected sponge porosity occurring. In the subcritical iron regime, a change in pore unit area and the tortuosity increase as the microstructure morphology is evident.  $\bullet$  evolves. In such cases, it is reasonable to expect the perme-

**I. INTRODUCTION** that it is not the  $\beta$  phase *per se* that is the cause of the

$$
Q = \frac{K\Delta P}{\mu L} \tag{1}
$$

interdender of the fluid and defect formation easier.<sup>[1,2,3]</sup> where *Q* is the flow rate,  $\Delta P$  is the pressure drop along a difficult and defect formation easier.<sup>[1,2,3]</sup> ength *L*,  $\mu$  is the viscosity, and *K* is th This "restricted feeding" theory cannot explain the experi-<br>  $\begin{array}{ll}\n\text{length } L, \mu \text{ is the viscosity, and } K \text{ is the permeability of the potential observations described in two companion articles [4.5]}\n\end{array}$ expressed as<sup>[7]</sup>

$$
K = \frac{(f_L)^2}{8n\pi\tau^3} \tag{2}
$$

can be explained in terms of the solidification sequence. osity" factor (a term used to account for the fact that the At a critical iron content solidification proceeds directly channels are neither straight nor smooth).

Microstructural examination has shown that the  $\beta$  phase ability to drop to a value incapable of sustaining interdenis present at all iron levels from 0.1 to 1.0 pct. This suggests dritic flow earlier than if it depended solely upon the decreasing fraction of liquid. The microstructural evolution can, therefore, be important.

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CRC for Alloy and Solidification Technology (CAST), Department of the microstructural evolution of Al-Si-Cu alloys. In particu-<br>Mining Minerals and Materials Engineering. The University of Oueensland. In the avenue the rel

# **II. EXPERIMENTAL**

Metallographic sections (polished to a colloidal silica finish and unetched) taken from several castings of the two experimental alloys $[4,5]$  at various iron levels were examined, using optical microscopy, to study the relationship between the  $\beta$  phase and the eutectic silicon.

Selected metallographic samples were deep etched by immersion in a 1 pct aqueous solution of NaOH at 55  $^{\circ}$ C to 60  $\degree$ C for a period of 10 minutes. This process removed the aluminum phase, leaving the iron-containing intermetallics and the eutectic silicon exposed. The deep-etched samples were then examined using a JEOL\* JSM-6400F scan-

\*JEOL is a trademark of Japan Electron Optics Ltd., Tokyo.

ning electron microscope with a Link X-ray analytical facility. Several apparent nucleation events of unmodified eutec-<br>tic silicon on the  $\beta$  platelets were studied in both<br>experimental alloys. The etching depth was on the order of<br>10  $\mu$ m. Since the large intermetallic platel typically  $>100 \mu$ m, the ratio of exposed surface to the is Mg<sub>2</sub>Si. submerged surface was low.

## **III. RESULTS**

Unmodified silicon eutectic was present in all samples (all alloy compositions/casting configurations/casting locations) and occurred as both fine acicular structures between the aluminium dendritic structure and as larger, isolated pools of coarse acicular structure. The most consistent observation regarding the formation of the unmodified eutectic silicon was the manner of its nucleation. In samples of both the AA309 alloy (approximately Al-5 pct Si-1 pct Cu-0.5 pct Mg) and the Al-10 pct silicon variant (approximately Al-10 pct Si-1 pct Cu-0.5 pct Mg), the  $\beta$ -Al<sub>5</sub>FeSi platelets appeared to be the main nucleation sites for the eutectic silicon. (These  $\beta$  platelets also appeared to be the favored nucleation sites for other late-forming phases such as  $Mg_2Si$  and CuAl<sub>2</sub>). Nucleation of silicon (both acicular and polygonal) occurred on both the large "binary"  $\beta$  platelets (formed as a compo-  $\left(\alpha\right)$ nent of the  $AI- $\beta$ A<sub>1</sub> F<sub>e</sub> S<sub>i</sub> binary eutectic complex) and on$ the smaller "ternary"  $\beta$  platelets (formed as a component of the Al-Si- $\beta$ Al<sub>5</sub>FeSi ternary eutectic complex). Examples of these events in both alloy systems are shown in Figures 1 and 2.

The silicon was frequently observed to grow from multiple locations along a single  $\beta$  platelet and even, on occasion, to have completely engulfed small  $\beta$  platelets. The reverse situation of  $\beta$  platelets nucleating on or covering silicon was not observed. The iron-containing  $\pi$ -phase particles  $(Al<sub>8</sub>FeMg<sub>3</sub>Si<sub>6</sub>)$  did not appear to participate in the nucleation of eutectic silicon. Scanning electron microscopy (SEM) of deep-etched samples also showed that eutectic silicon grows directly on the  $\beta$  phase. Figure 3 shows an example of an embryonic eutectic silicon cell nucleating on a  $\beta$  substrate. This silicon cell is not continuous with the background aluminum matrix, which implies that it nucleated on the  $\beta$  (*b*) substrate and not on another source. (*b*)

current experimental evidence (both optical microscopy and (*b*)1.00 pct.







Fig. 2—Typical optical micrographs showing eutectic silicon phase (medium gray, marked as 1) nucleating on small-scale  $\beta$ -Al<sub>5</sub>FeSi platelets **IV.** DISCUSSION (light gray colour, marked as 2), which may have formed as part of the Al-Si-Al-FeSi ternary eutectic. These samples are from the C6 segments It has been suggested,<sup>[8,9]</sup> and this is supported by the of 10 pct silicon alloy castings with iron contents of  $\alpha$ ) 0.7 pct and



tic silicon cell (radiating plates of silicon) that has nucleated and grown on the surface of a  $\beta$ -Al<sub>5</sub>FeSi platelet in a deep-etched sample from a B7 segment of an AA309 alloy casting containing 0.7 pct Fe.

SEM), that the unmodified eutectic silicon phase nucleates on the surface of the  $\beta$  platelets (Figures 1 through 3). However, the implications of this observation on the development of porosity do not appear to have been considered previously. The development of shrinkage porosity in hypo-<br>
eutectic Al-Si–based alloys may arise during the interden- (*a*) (*b*) dritic feeding stage, when large volume fractions of eutectic silicon are solidifying. Any changes to the microstructural evolution which alter interdendritic permeability during these crucial feeding stages may, therefore, have a significant impact on the formation of porosity.

It can be shown that a feasible orientation relationship exists for the nucleation and growth of silicon on  $\beta$  platelets. This relationship is

$$
(210)_{\beta} \parallel (200)_{\text{Si}} \cdot [001]_{\beta} \parallel [001]_{\text{Si}} \tag{c}
$$

the latter must pre-exist the former. This is the case for the dendrite tips and a pool of interdendritic liquid (dotted). The gray needles platelets that form as either a primary  $\beta$  phase or as binary<br>  $\beta$  phase (a co Such platelets are well developed by the time the ternary<br>enterties white/black striped cells of various sizes are the Al-Si faceted<br>eutectic silicon begins to grow. However, whether the ternary<br>eutectic (the silicon compo eutectic silicon begins to grow. However, whether the ternary eutectic (the silicon component is black). Note that in (a) the eutectic cells (left  $\beta$  platelets of the ALSi- $\beta$ Al-FeSi eutectic can participate in uncleat  $\beta$  platelets of the Al-Si- $\beta$ Al<sub>3</sub>FeSi eutectic can participate in the nucleate only on small ternary  $\beta$  platelets. In (b), large eutectic cells (left and right) nucleate independently and prior to the smaller eutect Al-10 pct Si variant) at all iron concentrations show that  $\beta$  nucleate on the ternary  $\beta$  platelets.

platelets of all possible sizes apparently participate in the nucleation of unmodified eutectic silicon. Since platelet size is likely to be a reasonably useful indicator of origin (*i.e.*, larger platelets are more likely to be primary or binary  $\beta$ rather than ternary  $\beta$ , because they had longer to grow), it can be inferred that the ternary  $\beta$  platelets must be the first component of the ternary eutectic to form. The  $\beta$ -Al<sub>5</sub>FeSi phase is known to nucleate on aluminium oxide<sup>[10]</sup> and, since this is common in all aluminum-based melts, the nucleation of  $\beta$  is probably very easy. This assumption is also supported by the absence of any significant undercooling for the  $\beta$ related inflections on the measured cooling curves. The silicon component of the ternary eutectic may, therefore, nucleate either on the small ternary  $\beta$  phases or on any of the larger binary  $\beta$  platelets already in existence.

Solidification in a simple binary hypoeutectic Al-Si alloy results in two distinct microstructural regimes with differing permeability characteristics. These are the growth of the coherent network of aluminium dendrites and the growth of faceted eutectic silicon cells in the interdendritic spaces. The presence of iron in the hypoeutectic Al-Si alloy system is a complicating factor, with other microstructural regimes becoming possible. The interdendritic permeability and feedability of each regime are likely to be quite different from the others. These regimes are illustrated schematically in Figure 4.

At the critical iron content ( $Fe<sub>crit</sub>$ ), the alloy will solidify in two stages (Figure 4(a)): (1) development of the  $\alpha$ -aluminum dendritic network, and (2) the formation of the ternary Al-



where  $d_{(210)\beta} = 2.736$  nm and  $d_{(200)Si} = 2.715$  nm (a mis-<br>match of 0.77 pct).<br>Fig. 4—Schematic representations of the developing microstructure at the<br>interesting Al-Si- $\beta$ Al<sub>5</sub>FeSi eutectic begins to form in an unmo below Fe<sub>crit</sub>, and  $(c)$  above Fe<sub>crit</sub>. In each diagram, there are five aluminum dendrite tips and a pool of interdendritic liquid (dotted). The gray needles





( $\leq$ Fe<sub>crit</sub>), the alloy solidifies in three stages (Figure 4(b)): Si on  $2^{\circ} \beta$ " fields are unknown. (1) development of the  $\alpha$ -aluminum dendritic network, (2) the formation of the Al-Si binary eutectic cells that nucleate at non- $\beta$  sites, and (3) the formation of independently nucle- amounts of higher-order Cu and Mg-containing phases are ated ternary eutectic cells that nucleate on ternary  $\beta$  platelets. ignored, as they account for less than 5 vol pct). At supercritical iron contents ( $\geq$ Fe<sub>crit</sub>), the alloy solidifies The large binary  $\beta$ -Al<sub>5</sub>FeSi platelets that form in alloys in either three or, possibly, four stages (Figure 4(c)): (1) the with supercritical iron c development of the  $\alpha$ -aluminum dendritic network, (2) the tion of significant regions of interconnected shrinkage porosformation of the Al- $\beta$  binary eutectic, (3) the growth of ity through a number of mechanisms, including (1) direct ternary eutectic cells that nucleate on binary  $\beta$  platelets, physical obstruction to liquid flow during the interdendritic and (4) the growth of other independently nucleated ternary feeding stage, (2) indirect obstruction to liquid flow by eutectic cells. The latter two stages may occur simultane- induced changes to the freezing pattern of the eutectic silicon ously. These microstructural changes and their effect on phase, and/or (3) by physically strengthening the dendritic permeability and, therefore, on feeding are described in network against collapse and burst feeding.<br>Table I. As the iron content increases above Fe<sub>crit</sub>

of the alloy's critical iron content, the relative proportions spaces. This creates a rapid multiplication in the number of of each microstructural type formed and the fraction solid channels per unit area and a decrease in the average channel at which there is a transition from one microstructural type size. The permeability decreases according to Eq. [2] and, to another will vary with both the iron and silicon content. hence, feedability also decreases. At the ternary eutectic Figure 5 provides estimates of the sequence of formation and point, the small channels become rapidly narrowed, choked, the approximate proportions of the various microstructural and roughened as faceted eutectic silicon cells nucleate and constituents for the two experimental alloys (the small grow from the already existing binary  $\beta$  platelets (Figure



Fig. 5—Graphs showing estimates of the relative proportions of various microstructural types that are predicted to form during solidification at various iron contents in two alloys: (*a*) AA309 alloy and (*b*) Al-10 pct Si alloy. The abbreviations  $1^{\circ},2^{\circ}$ , and  $3^{\circ}$  stand for primary, binary, and ternary, respectively. A vertical line drawn at any iron content can be used to silicon components of the ternary eutectic grow on the easier-<br>to-nucleate ternary  $\beta$  platelets. At subcritical iron contents<br>to-nucleate ternary  $\beta$  platelets. At subcritical iron contents<br>to-nucleate ternary  $\beta$  pla

with supercritical iron contents may contribute to the forma-

As the iron content increases above  $Fe<sub>crit</sub>$ , an increasing Although the previous sequences are described in terms amount of binary  $\beta$  platelets form in the interdendritic further decrease in permeability. The proportion of the related porosity defects. Evidence from Iwahori *et al.*<sup>[2]</sup> has microstructure that evolves in this deleterious manner shown that the elements Mn and Be improve the feeding increases with iron content (Figure 5). There is, therefore, characteristics and reduce shrinkage-porosity formation in a corresponding increase in the probability of localized feed- an Al-6.8 pct Si-3.2 pct Cu alloy (Japanese code AC2B) ing problems occurring with increasing iron content. In such that contains detrimentally high levels of iron. Clearly, this high-iron alloys, major shrinkage-porosity defects are, there-<br>could be a useful area for future w high-iron alloys, major shrinkage-porosity defects are, therefore, more typically found to be located in regions where marginal thermal and feeding conditions exist. In addition, large  $\beta$  platelets that form "bridges" between dendrites may **VI. CONCLUSIONS** 

also provide additional strength to the dendritic nework. In unmodified, nongrain-refined hypocutectic Al-Si alloys<br>Such strengthening could restrict the later solid feeding<br>mechanisms, and this may explain why massive in iron content diverges to either side of Fe<sub>crit</sub>.<br>Not only is the dendritic network permeability likely to

Not only is the dendritic network permeability likely to<br>be maximized at Fe<sub>crit</sub>, but the amount of ternary eutectic is<br>also maximized (Figure 5). It may be possible in the early The Cooperative Research Centre for All stages of ternary eutectic solidification that the small, embry- cation Technology (CAST) was established under and is onic eutectic cells are capable of behaving in a slurry-like funded in part by the Australian Government's Cooperative manner for a short period prior to becoming a coherent Research Centre Scheme. eutectic network (Figure 4(a)). Such interdendritic liquid behavior would optimize feeding.

mura: *Casting*, 1988, vol. 60(9), pp. 590-95.<br>It is well documented that iron has a deleterious effect 3. J.E. Eklund: Ph.D. Thesis, Helsinki University of Technology, Helon the mechanical properties of Al-Si-based casting sinki, Finland, 1993.<br>alloys,<sup>[11,12]</sup> due to the presence of the large  $\beta$ -Al<sub>5</sub>FeSi plate- 4. J.A. Taylor, G.B. Schaffer, and D.H. StJohn: *Metall. Mater. Trans. A*, Lets favored by slow cooling rates (i.e.,  $5^{\circ}C/s$ ).<sup>[13]</sup> Conse-<br>Quently, various approaches to controlling the formation of<br>the  $\beta$  phase have been developed. These generally encourage on R. Roy, A.M. Samuel, and F.H. the  $\beta$  phase have been developed. These generally encourage 6. N. Roy, A.M. Samuel, and the formation of alternative iron-containing intermetallic 1996, vol. 27A, pp. 415-29. phases, by either the addition of iron-controlling elements<br>such as Mn, Cr, Co, and Be<sup>[12-15]</sup> or by the application of<br>8. M.H. Mulazimoglu, N. Tenekediev, B.M. Closset, and J.E. Gruzleski: thermal treatments to the melt.<sup>[10,16,17]</sup><br> *Cast Met.* 1993, vol. 6 (1), pp. 16-28.<br> **Cast Met.** 1993, vol. 6 (1), pp. 16-28.<br> **Cast Met.** 1993, vol. 6 (1), pp. 16-28.<br> **Cast Met.** 1993, vol. 6 (1), pp. 16-28.

If, as the present theory suggests, the presence of the  $\beta$  9. L. Anantha Narayanan, F.H. Satelets arising from the binary AL  $RA1$ . FeSi eutectic are 1992, vol. 100, pp. 383-91. platelets arising from the binary  $AI-\beta AI_5FeSi$  eutectic are  $1992$ , vol. 100, pp. 383-91.<br>
10. L. Anantha Narayanan, F.H. Samuel, and J.E. Gruzleski: Metall. Mater. responsible (directly or indirectly) for the development of Trans. A, 1994, vol. 25A, pp. 1761-73.<br>
localized shrinkage defects, then it might be possible to 11. D. Vorren, J.E. Evensen, and T.B.Pederson: AFS Trans., 1984, extend the application of these iron-controlling principles 92, pp. 459-66.

4(c)). This results in an increase in the tortuosity and a for mechanical-property improvement to the control of iron-

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