

# A Quantitative Study of the Synthesis of TiB<sub>2</sub> Particles *via* Salts-Metal Reaction at Different Temperatures



ZHIWEI LIU, QINGYOU HAN, ZHIFU HUANG, and JIANDONG XING

This research quantitatively studied the effect of temperature on the synthesis of TiB<sub>2</sub> particle reinforcement *via* a casing method in which a salts-metal reaction was involved. Experimental results showed that the yield of TiB<sub>2</sub> reached 89.5 pct and most TiB<sub>2</sub> particles ranged from 400 to 800 nm at 1173 K (900 °C) with a 10-minute reaction time; when the reaction time was 30 minutes, the TiB<sub>2</sub> particles had similar yield and size distribution. At 973 K (700 °C) with a 10-minute reaction time, most TiB<sub>2</sub> particles were less than 300 nm, whereas the yield was just 28.1 pct; as the time was prolonged to 30 minutes, some smaller-sized TiB<sub>2</sub> particles were synthesized and the yield of TiB<sub>2</sub> was 36.4 pct. At a higher temperature [1173 K (900 °C)], the synthesis of TiB<sub>2</sub> mainly followed the precipitation-growth process at reaction interface. At a lower temperature [973 K (700 °C)], the precipitation-growth process and dissolution reaction between Al<sub>3</sub>Ti and AlB<sub>2</sub> both contributed to the formation of TiB<sub>2</sub>.

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## I. INTRODUCTION

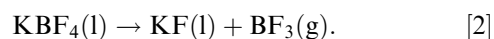
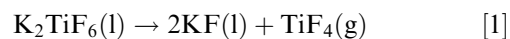
IT is well known that *in situ* TiB<sub>2</sub> particles can be synthesized *via* the salts-metal reaction by adding the mixed K<sub>2</sub>TiF<sub>6</sub>-KBF<sub>4</sub> salts into molten Al at high temperatures.<sup>[1,2]</sup> Due to its unique characteristics, such as low cost, high efficiency and short synthesizing time, the salts-metal reaction has been widely used in practical productions for producing *in situ* TiB<sub>2</sub>/Al composites and the existence of TiB<sub>2</sub> particles can improve the mechanical properties of the Al alloys significantly.<sup>[3,4]</sup> This type of material has been obtained more attentions in the aerospace and automobile industries. In nature, the salts-metal reaction belongs to a chemical reaction. The synthesizing temperature is one of the most important factors, which influences the formation of the products during the reaction. Generally, a high temperature is beneficial for the formation of TiB<sub>2</sub> particles, and the temperature used in the salts-metal reaction is usually higher than 1073 K (800 °C). It has been reported that a lower temperature can lead to the formation of Al<sub>3</sub>Ti and AlB<sub>2</sub> phases, which decrease the

yield of TiB<sub>2</sub> phase in the Al matrix.<sup>[5]</sup> Thereby, using a higher temperature of the Al melt is always recommended in order to improve the production of TiB<sub>2</sub> particles in the reaction.

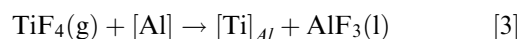
Although the salts-metal reaction has become the most common method for synthesizing *in situ* TiB<sub>2</sub>/Al composites, the relationship between the temperature and the formation of TiB<sub>2</sub>, however, has not been investigated clearly. A quantitative study of the effect of temperature on the synthesis of TiB<sub>2</sub> regarding the yield of TiB<sub>2</sub> particles and their size distribution has not been reported by other researchers. In addition, the understanding of the formation mechanism of TiB<sub>2</sub> in the salts-metal reaction is still unclear.

So far, two main viewpoints with regard to the formation process of TiB<sub>2</sub> have been proposed. One refers that TiB<sub>2</sub> particles are formed by a dissolution-precipitation mechanism when the concentrations of Ti and B reach saturation in molten Al (alloys).<sup>[6]</sup> The detailed mechanism can be summarized as follows.

First, K<sub>2</sub>TiF<sub>6</sub> and KBF<sub>4</sub> are melted on the Al surface, both of which are separately decomposed to KF (liquid), TiF<sub>4</sub> (gas), and BF<sub>3</sub> (gas), which are expressed as follows:



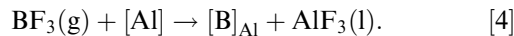
Then, Ti and B atoms are released and diffuse into liquid Al through the aluminothermic reduction of TiF<sub>4</sub> and BF<sub>3</sub> gases at the salts-melt interface, which are expressed as below:



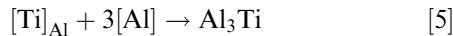
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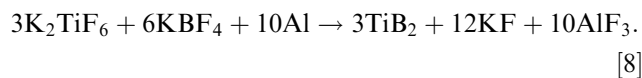
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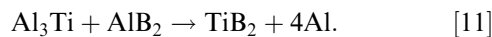
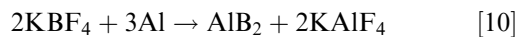
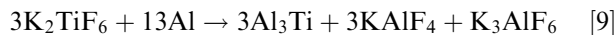
When the solutes [Ti] and [B] in liquid Al reach saturation, they might be separated out as compounds  $\text{Al}_3\text{Ti}$ ,  $\text{AlB}_2$ , and  $\text{TiB}_2$ , according to the following reactions:



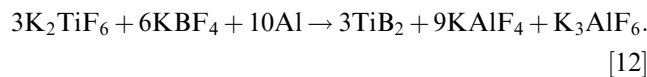
Among the compounds involved in the salts-metal reaction,  $\text{TiB}_2$  is the most thermodynamically stable phase due to its lowest free energy of formation.<sup>[7]</sup> The overall reaction showing the formation of  $\text{TiB}_2$  can be written as



The other one refers that  $\text{TiB}_2$  particles are synthesized resulting from the reaction between  $\text{Al}_3\text{Ti}$  and  $\text{AlB}_2$ , which are formed due to the reactions of  $\text{K}_2\text{TiF}_6\text{-Al}$  and  $\text{KBF}_4\text{-Al}$ .<sup>[8]</sup> The following reactions describe the formation process of  $\text{TiB}_2$ :



An overall reaction for synthesizing  $\text{TiB}_2$  can be given as follows:



Actually, the above two mechanisms are based on the equilibrium thermodynamics of the Al-Ti-B system. The practical salts-metal reaction, however, is a typical non-equilibrium thermodynamic reaction. An analysis considering the reaction temperature and reaction time might be more suitable to reflect the actual formation process of  $\text{TiB}_2$  during the reaction.

In order to investigate the influences of reaction temperature and time on the formation of  $\text{TiB}_2$  particles in molten Al regarding the yields and size distributions of  $\text{TiB}_2$  particulates, two reaction temperatures [1173 K and 973 K (900 °C and 700 °C)] with two reaction times (10 and 30 minutes) were studied. A quantitative analysis about the formation of  $\text{TiB}_2$  under different experimental parameters was firstly investigated in this research. The formation process of  $\text{TiB}_2$  particles was also explored from the perspective of the temperature.

## II. EXPERIMENTAL

### A. Synthesis of $\text{TiB}_2$ Particles via Salts-Metal Reaction

A 500 g pure Al ingot was melted in a graphite crucible in an electrical resistant furnace. After the temperature of the Al melt reached and kept stable at 1173 K (900 °C) [or 973 K (700 °C)], the mixed  $\text{K}_2\text{TiF}_6\text{-KBF}_4$  salt powders were added into the Al melt, and the addition of the mixed salts corresponded to the composition of Al-5 wt pct  $\text{TiB}_2$ . Then the melt was stirred manually for a few seconds by using a niobium bar. After 10 min, the Al melt containing reaction products was stirred again, for the newly formed products might deposit during the reaction due to the higher density than pure Al. After the slag on the melt surface was removed, the melt was poured into a steel mold to form an ingot. For the samples fabricated in 30 min, the melt was stirred in 10-minute intervals. 4 samples were fabricated in total. For simplicity, the 4 samples were referred as S900-10, S900-30, S700-10, and S700-30, respectively (the first and second numbers stands for the reaction temperature (°C) and time (minutes) in each sample).

### B. Extraction Procedure for Obtaining $\text{TiB}_2$ Particles

In this research, some  $\text{TiB}_2$  particles were extracted from each sample for calculating the yield of  $\text{TiB}_2$  particles and measuring their size distribution. The detailed extraction procedure for obtaining  $\text{TiB}_2$  particles is given as (1) A small ingot was cut from the sample, and the surface of which was cleaned by sand paper. (2) The small ingot was dissolved in a 15 vol pct aqueous HCl solution in a beaker at room temperature. After dissolution, a layer of particles were deposited at the bottom of the beaker, and then the HCl solution was decanted. (3)  $\text{TiB}_2$  particles were washed with water for several times until the supernatant displayed neutral pH. (4) These  $\text{TiB}_2$  particles were washed with ethanol, and then dried by using an electric hair dryer. According to our proceeding work,<sup>[9]</sup> pure  $\text{TiB}_2$  phase can be obtained through the above process and no other phases can influence the calculation of the yield of  $\text{TiB}_2$  particles and the measurement of their size distribution.

### C. Examination of Samples

In each group of experiment, the products generated in the reaction were consisted of ingot and slag. A small sample was cut from the ingot, and ground using SiC sand papers successively following the order of 180, 240, 400, and 600 mesh. Then the ground sample was polished using micro-sized diamond compound, following the order of 3 and 1  $\mu\text{m}$ . After that the polished sample was cleaned in the ultrasonic cleaner for a few minutes to clean the polished surface. The by-product slag was milled to powders by using a glass mortar.

The sample and slag powder were both examined by X-ray diffraction (XRD, Bruker D8, AXS, Karlsruhe, Germany) using Cu K $\alpha$  radiation at 40 kV and 40 mA and a scan rate of 0.10°/s. The microstructures of

samples were analyzed by scanning electron microscopy (SEM, S-4800, Hitachi, Ltd., Tokyo, Japan) equipped with an energy dispersive spectroscope (EDS) device for identifying the components in the samples. An optical microscopy (OM) was also applied to observe the microstructures of samples.

#### D. Calculation of the Yield of $TiB_2$ Particles

Three small ingots with a weight of about 8 grams cut from each sample were treated by a completed extraction process, respectively. Three groups of extracted powders were weighted by using an electric balance. Then the actual weight percentage of  $TiB_2$  phase in the Al matrix could be calculated. Since the sample was fabricated corresponding to the composition of Al-5 wt pct  $TiB_2$ , the yield of  $TiB_2$  could be further obtained. An average value of the yield was computed in order to decrease the experimental error.

#### E. Measurement of the Size Distributions of $TiB_2$ Particles

Zetasizer Nano ZS (Malvern) was used to measure the size distributions of  $TiB_2$  particulates extracted from each sample. This device was able to measure the particles with the size ranging from 3 nm to 5  $\mu m$ . Before the test, a small amount of  $TiB_2$  powders were diluted with DI water. In order to reduce error, 10 measurements were conducted for each sample.

### III. RESULTS AND DISCUSSION

#### A. S900-10 Sample

##### 1. XRD analysis

Figure 1 shows the XRD patterns of the slag and sample produced at 1173 K (900 °C) with a 10-minute reaction time. It is obvious that  $KAlF_4$  and  $K_3AlF_6$  were the two main phases in the slag, as shown in Figure 1(a), indicating that Ti and B elements were both transferred from the molten mixed salts to molten Al. In the

S900-10 sample,  $TiB_2$  was the only newly formed phase during the salts-metal reaction, the diffraction peaks of which could be observed clearly, as shown in Figure 1(b) (inset graph). The results of the two XRD patterns indicate that the chemical formula shown in reaction [12] is more suitable to describe the process of the reaction of  $K_2TiF_6$ - $KBF_4$ -Al system.

##### 2. SEM analysis

Figure 2 shows the typical microstructure of the S900-10 sample. Only one type of newly formed phase existed in the Al matrix, which was identified as  $TiB_2$  by EDS. These small-sized  $TiB_2$  particulates aggregated to form clusters at  $\alpha$ -Al grain boundaries, as shown in Figure 2(a). Figure 2(b) clearly shows that these  $TiB_2$  particles synthesized *via* the salts-metal reaction had different sizes, and most of them were much smaller than 1  $\mu m$ . In Figure 2(c), it can be found that some  $TiB_2$  particles had a larger size exceeding 1  $\mu m$ .

#### B. S900-30 Sample

##### 1. XRD analysis

Figure 3 shows the XRD patterns of the slag and sample (S900-30) produced at 1173 K (900 °C) with a 30-minute reaction time. Similar to the products produced at 1173 K (900 °C) with a 10-minute reaction time,  $KAlF_4$  and  $K_3AlF_6$  were the two main phases in the slag (Figure 3(a)), and  $TiB_2$  was the only newly formed phase in the sample (Figure 3(b)).

##### 2. SEM analysis

The typical microstructure of the S900-30 sample is presented in Figure 4. Overall, it had similar microstructural features with the S900-10 sample. Only  $TiB_2$  particulates were *in situ* formed, which existed in the Al matrix as clusters located at the grain boundaries (Figure 4(a)). Most  $TiB_2$  particles were smaller than 1  $\mu m$  in size (Figure 4(b)), whereas a very small amount of  $TiB_2$  particles were greater than 1  $\mu m$ , as shown in Figure 4(c).

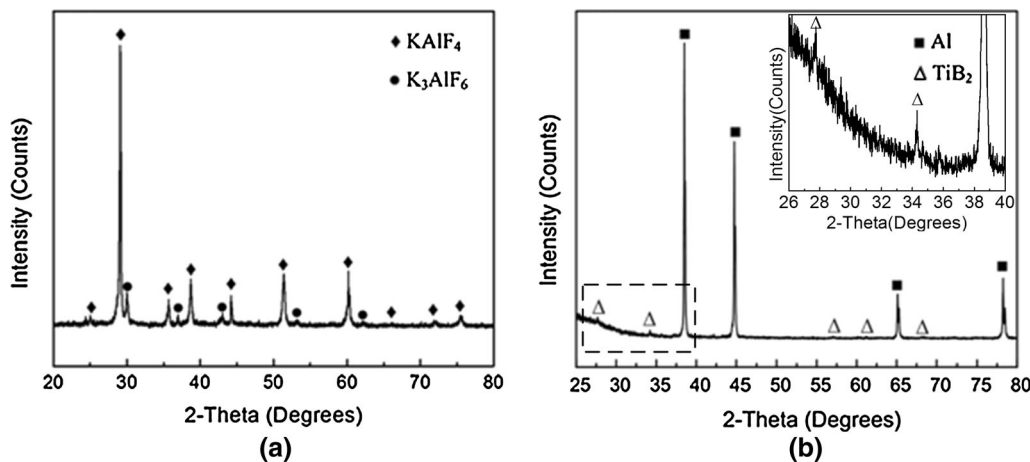


Fig. 1—XRD patterns of the slag (a), and S900-10 sample (b) produced at 1173 K (900 °C) with a 10-min reaction time.

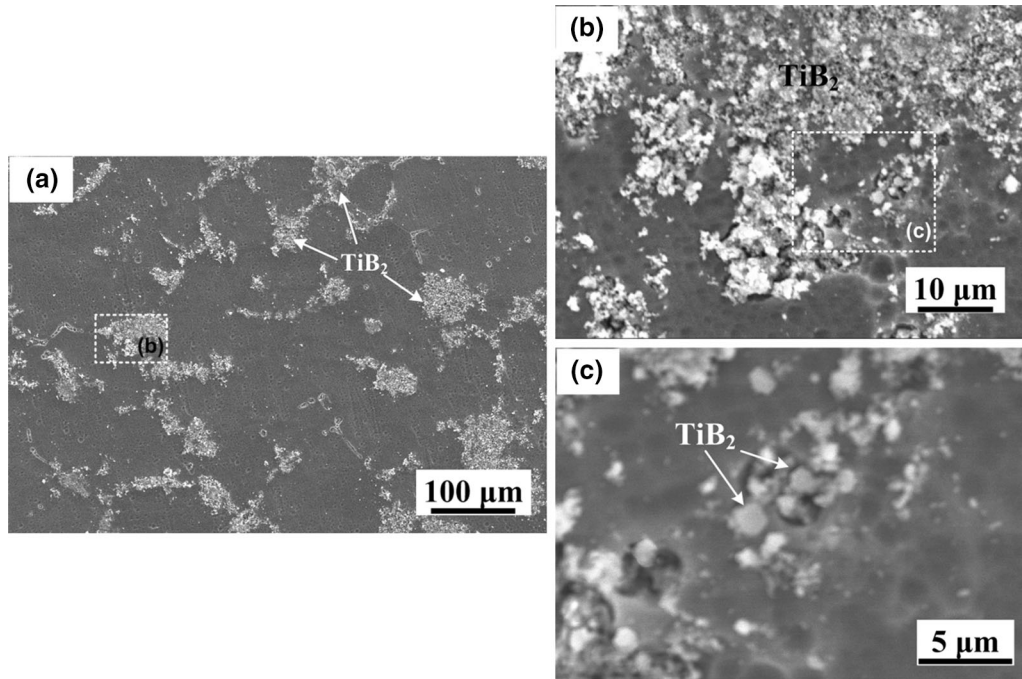


Fig. 2—(a) Typical microstructure of the S900-10 sample, (b) higher magnification of the area marked in image (a), and (c) higher magnification of the area marked in image (b).

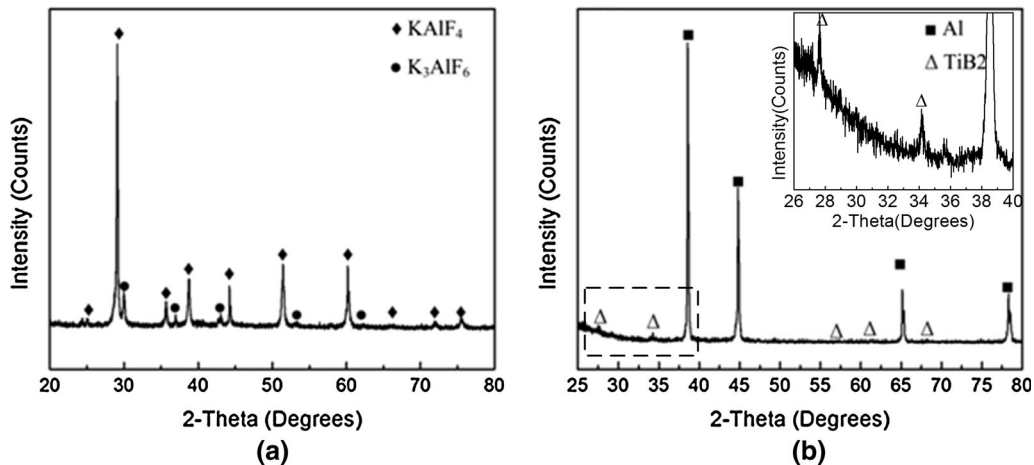


Fig. 3—XRD patterns of the slag (a), and S900-30 sample (b) produced at 1173 K (900 °C) with a 30-min reaction time.

### C. S700-10 Sample

#### 1. XRD analysis

Figure 5 shows the XRD patterns of the slag and S700-10 obtained in the salts-metal reaction at 973 K (700 °C) with a 10-minute reaction time.  $KAlF_4$  and  $K_3AlF_6$  detected by XRD were the main phases in the slag, as shown in Figure 5(a). No phase containing obvious Ti or B was found in the slag, suggesting that Ti and B elements were both transferred to molten Al from salts. Some rather weak diffraction peaks of  $TiB_2$  phase were found in the S700-10 sample (Figure 5(b)), indicating that the mixed-salts reaction proceeded according to the chemical formula shown in reaction [12] at the low temperature of 973 K (700 °C).

#### 2. SEM analysis

Figure 6 shows the typical microstructure of the S700-10 sample. Three types of reinforcements existed in the Al matrix. Some blocky particles ranged in size from 1 to 3  $\mu m$  were detected as  $Al_3Ti$  by EDS. Some rather small-sized  $TiB_2$  particles were also found in the matrix, most of which existed along the chain-like reinforcement. After examined by EDS, the main phase of chain-like reinforcement was identified as  $Al_3Ti$ , and also some separately tiny  $TiB_2$  particles were located in  $Al_3Ti$ , as shown in Figure 6(b). Since the content of  $Al_3Ti$  phase in the matrix was rather low, it is hard to detect in the XRD examination (Figure 5(b)). In addition, a little amount of  $AlB_2$  phase might exist in the Al



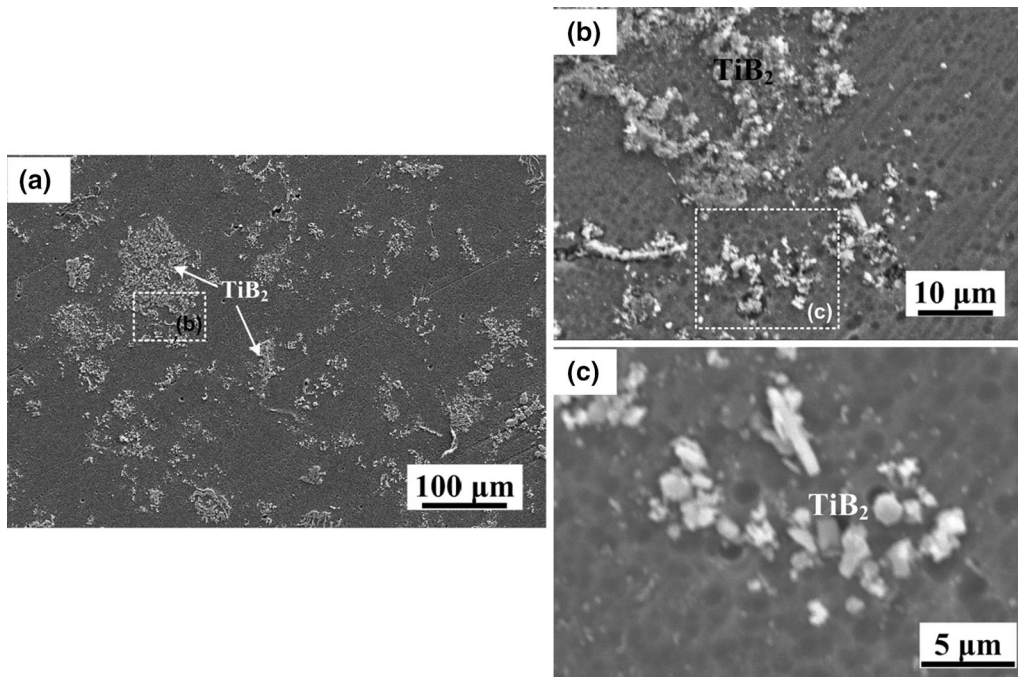


Fig. 4—(a) Typical microstructure of the S900-30 sample, (b) higher magnification of the area marked in image (a), and (c) higher magnification of the area marked in image (b).

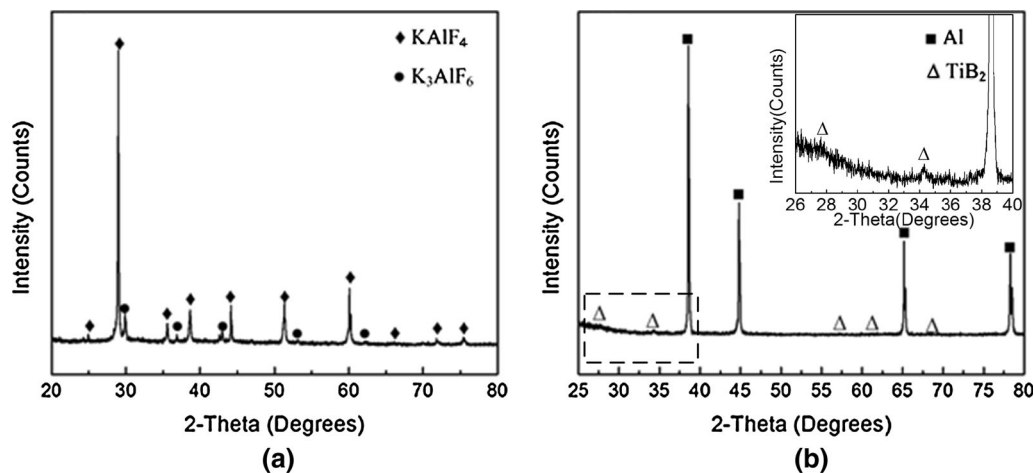


Fig. 5—XRD patterns of the slag (a), and S700-10 sample (b) produced in the mixed-salts reaction at 973 K (700 °C) with a 10-min reaction time.

matrix, but it is hard to examine them out in the present research due to the limitation of device.

#### D. S700-30 Sample

##### 1. XRD analysis

Figure 7 shows the XRD patterns of the slag and S700-30 sample obtained in the salts-metal reaction at 973 K (700 °C) with a 30-minute reaction time. As shown in Figure 7(a), the slag was consisted of  $KAlF_4$  and  $K_3AlF_6$  phases. Weak  $TiB_2$  peaks were also found in the sample, showing that the content of  $TiB_2$  phase was still low (Figure 7(b)) in the Al matrix by a 30-minute reaction.

##### 2. SEM analysis

Figure 8 shows the microstructure of the S700-30 sample. Long chain-like reinforcements and cluster-like reinforcements were both found in the Al matrix, as shown in Figure 8(a). It is found that the chain-like reinforcement was composed of  $Al_3Ti$  and some small-sized  $TiB_2$  particles which were located in the  $Al_3Ti$  phase, as shown in Figure 8(b). The cluster-like reinforcement was consisted of some large-sized blocky  $Al_3Ti$  particles and some nanometer-sized  $TiB_2$  particles, as shown in Figure 8(c). One more thing should be mentioned is that the size of long chain-like reinforcement in S700-30 sampler was smaller than that in the

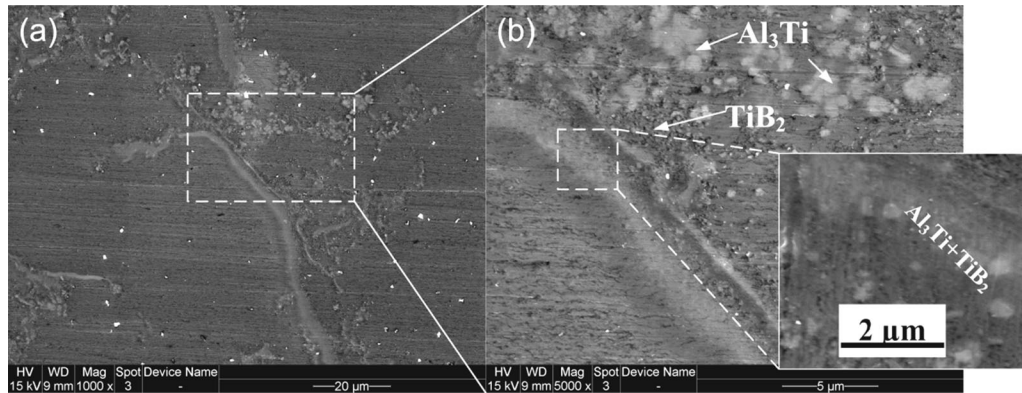


Fig. 6—(a) Typical microstructure of the S700-10 sample, and (b) higher magnification of the area marked in image (a).

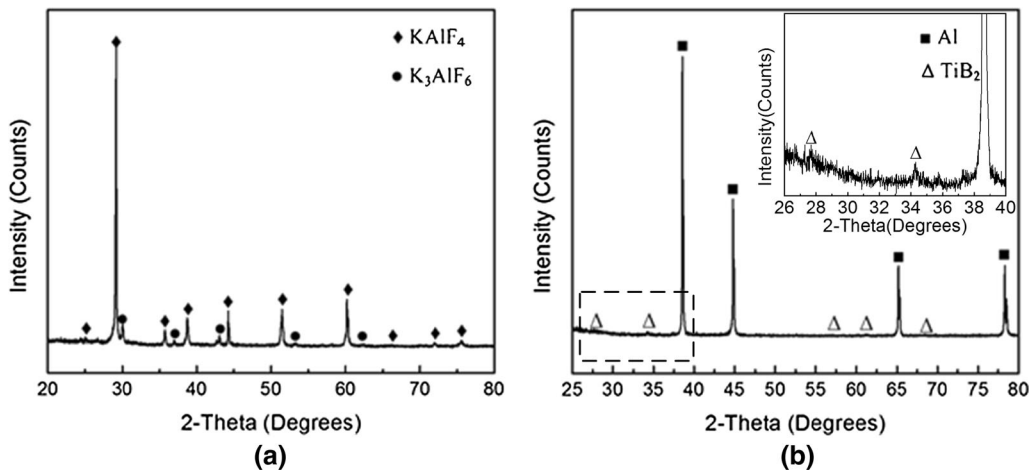


Fig. 7—XRD patterns of the slag (a), and S700-30 sample (b) produced in the mixed-salts reaction at 973 K (700 °C) with a 30-min reaction time.

S700-10 sample, which indicated that part of it might dissolve or react as the reaction time was increased.  $\text{AlB}_2$  phase also might exist in the sample, which was hard to examine out clearly in this research.

#### E. Yields and Size Distributions of $\text{TiB}_2$ Particles

The yields of  $\text{TiB}_2$  particles and their size distributions of each sample are presented in Figure 9. For the S900-10 sample, the yields of  $\text{TiB}_2$  particles could reach 89.5 pct; most  $\text{TiB}_2$  particles were less than 1  $\mu\text{m}$  in size, in which about 81 pct of the  $\text{TiB}_2$  particles ranged in size from 400 to 800 nm, and a very small amount of  $\text{TiB}_2$  ranged in size from 1 to 2  $\mu\text{m}$ . For the S900-30 sample, the yield of  $\text{TiB}_2$  particles was about 90.3 pct; overall, the most  $\text{TiB}_2$  particles were smaller than 1  $\mu\text{m}$ , in which about 83 pct of the  $\text{TiB}_2$  particles ranged in size from 400 to 800 nm, and a rather small amount of  $\text{TiB}_2$  particles had the size in the range of 1 to 2  $\mu\text{m}$ . It is clear that the S900-10 and S900-30 samples had similar yield and size distribution of  $\text{TiB}_2$  particles. For the S700-10 sample, the yield of  $\text{TiB}_2$  particles was rather low, about 28.1 pct; the size of  $\text{TiB}_2$  particles was less than 1  $\mu\text{m}$ , in which about 95 pct  $\text{TiB}_2$  particles were smaller than 300 nm. For the S700-30 sample, the yield of particles could

reach 36.4 pct; more than 95 pct of the  $\text{TiB}_2$  had the size less than 300 nm. Comparing with the S700-10 sample, the content of  $\text{TiB}_2$  particles with a smaller size was increased in the S700-30 sample, and the ratio of  $\text{TiB}_2$  smaller than 100 nm was about 30 pct, indicating a certain amount of  $\text{TiB}_2$  particles with a smaller size were formed as the reaction time was prolonged from 10 to 30 minutes.

The results in this research displayed the differences in the formation of  $\text{TiB}_2$  at different temperatures [1173 K and 973 K (900 °C and 700 °C)], such as the yields of  $\text{TiB}_2$  particulates and their size distributions. It is noted that the reaction temperature played a critical role in the salts-metal reaction of  $\text{K}_2\text{TiF}_6\text{-KBF}_4\text{-Al}$  system in this research. Accordingly, the related formation mechanism of  $\text{TiB}_2$  might be different at different temperatures. The following discussion about the formation process of  $\text{TiB}_2$  will be conducted considering the Al melt temperature.

#### F. Formation of $\text{TiB}_2$ at a Higher Temperature [1173 K (900 °C)]

In this research, when the reaction temperature was 1173 K (900 °C) and the reaction time was 10 minutes,

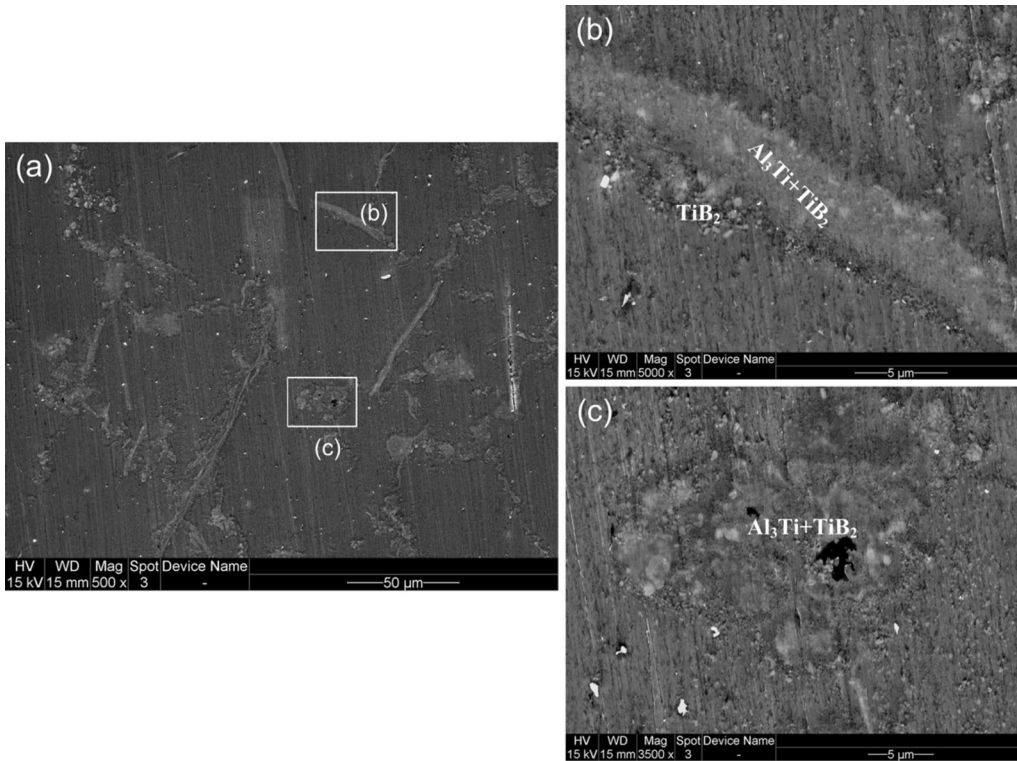


Fig. 8—(a) Typical microstructure of the S700-30 sample, and (b), (c) higher magnification of the areas marked in image (a).

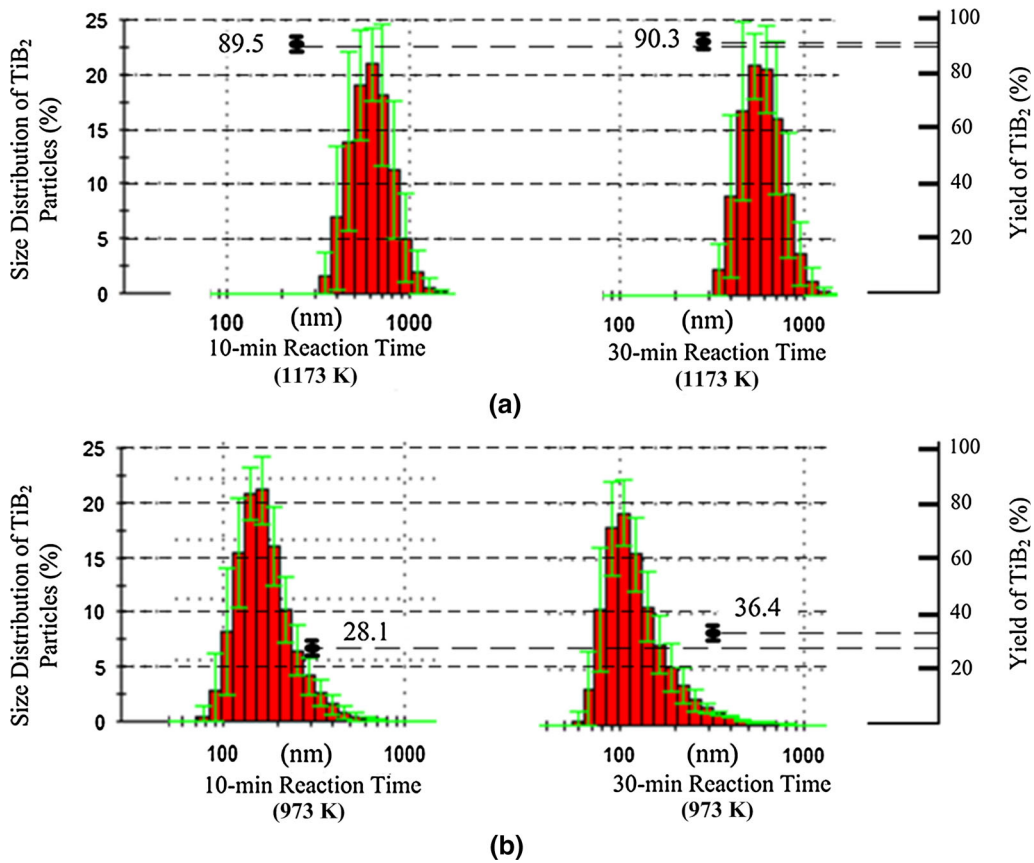


Fig. 9—The yields and size distributions of TiB<sub>2</sub> particles synthesized *via* the salts-metal reactions at 1173 K (900 °C) (a) and 973 K (700 °C) (b).



no  $\text{Al}_3\text{Ti}$  phase was found in the Al matrix, the yield of  $\text{TiB}_2$  reached 89.5 pct, and the size of most of *in situ* formed  $\text{TiB}_2$  particulates was in the range of 400 to 800 nm. As the reaction time was increased to 30 minutes, no obvious change occurred in the S900-30 sample, in which the yield of  $\text{TiB}_2$  was about 90.3 pct and the size of most  $\text{TiB}_2$  particles was in the range of 400 to 800 nm, as shown in Figure 9(a). It is clear that a higher reaction temperature is beneficial for the formation of  $\text{TiB}_2$  with a larger size in a short time.

The salts-metal reaction of  $\text{K}_2\text{TiF}_6$ - $\text{KBF}_4$ -Al system is an interface reaction. Based on the results of the S900 samples, the possible formation process of  $\text{TiB}_2$  phase in the salts-metal reaction is discussed below, in which three critical steps in the reaction are listed, respectively.

### 1. Formation of the Interface Between Molten Salts and Al Melt

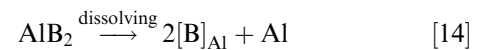
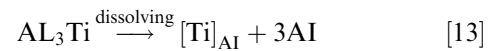
First all of, no obvious KF and  $\text{AlF}_3$  phases were found in the slags produced in the salts-metal reaction at different temperatures. Thereby, the Ti and B in Al are not from the reactions of  $\text{TiF}_4$  (gas)-Al and  $\text{BF}_3$  (gas)-Al, in which the  $\text{TiF}_4$  and  $\text{BF}_3$  gases are from the decomposition of  $\text{K}_2\text{TiF}_6$  and  $\text{KBF}_4$ . Accordingly, the formation processes described in reactions [1], [2], [3], and [4] are not suitable to explain the formation of  $\text{TiB}_2$  phase. At least, the formation of most  $\text{TiB}_2$  phase in the reaction does not follow the chemical reaction shown in reaction [8].

Actually, it has been reported by Biro<sup>[10]</sup> that even though  $\text{K}_2\text{TiF}_6$  has a higher melting point than  $\text{KBF}_4$ ,  $\text{K}_2\text{TiF}_6$  can be reduced by Al, releasing Ti at

approximately 493 K (220 °C);  $\text{KBF}_4$  starts to be reduced by Al a while later at round 798 K (525 °C), possibly after its polymorphic transformation from orthorhombic to cubic structure is over. In this research, after the mixed salts are added into the molten Al at 1173 K (900 °C), the mixed salts melt quickly on the Al melt surface, and an interface between molten salts and Al melt is formed.

### 2. Precipitation of $\text{TiB}_2$

Once the reaction interface is formed, Ti released from  $\text{K}_2\text{TiF}_6$  and B released from  $\text{KBF}_4$  both react with Al at the interface between salts and Al to form  $\text{Al}_3\text{Ti}$  and  $\text{AlB}_2$  by reduction reactions [9] and [10]. According to Al-Ti and Al-B phase diagrams,<sup>[11]</sup> as shown in Figure 10,  $\text{Al}_3\text{Ti}$  and  $\text{AlB}_2$  are both soluble in molten Al. The newly formed  $\text{Al}_3\text{Ti}$  and  $\text{AlB}_2$  phases can dissolve in molten Al immediately, and then a thin layer of liquid Al containing Ti and B adjacent to the interface can be formed. The processes can be expressed as follows:



Actually, the above processes are significantly influenced by the temperature of molten Al. Higher contents of [Ti] and [B] in the thin layer are obtained easily at a higher reaction temperature [1173 K (900 °C)]. On the one hand, the reduction reactions between salts and Al become more active, and more  $\text{Al}_3\text{Ti}$  and  $\text{AlB}_2$  phases

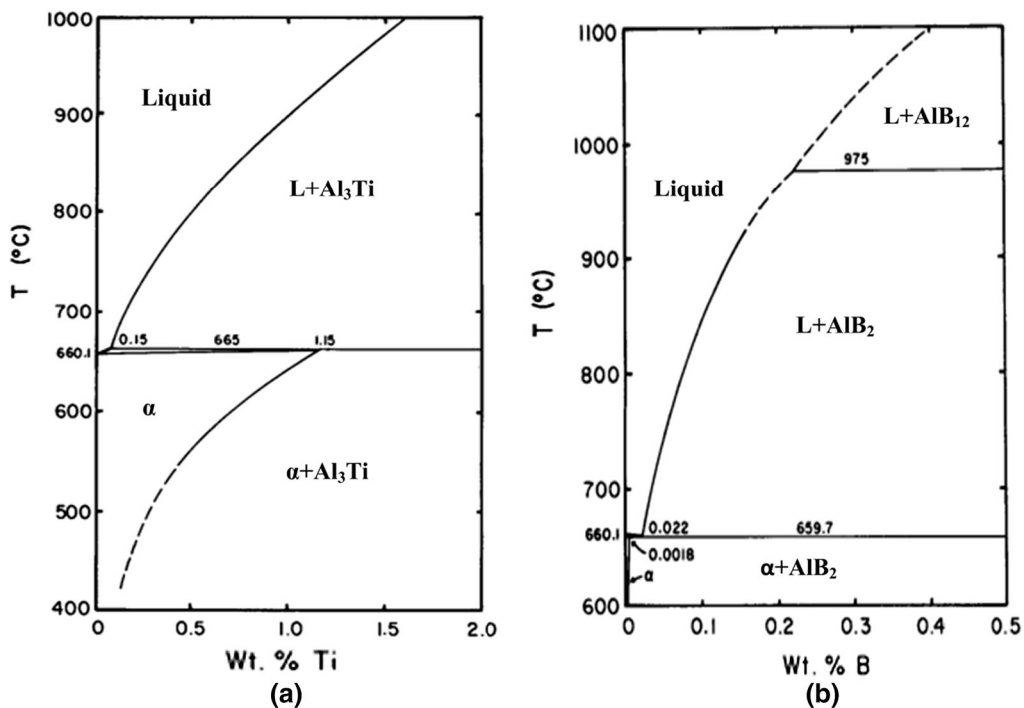


Fig. 10—The aluminum-rich side of the Al-Ti phase diagram (a), and the aluminum-rich side of the Al-B phase diagram (b). Both of which were reproduced according to Sigworth.<sup>[9]</sup>



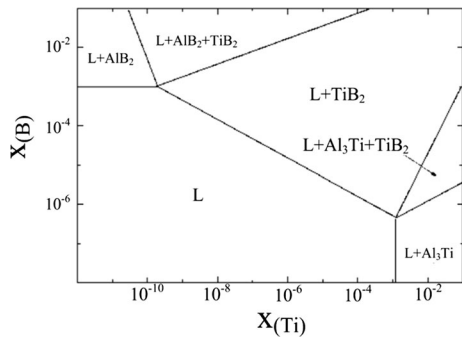


Fig. 11—Phase diagram for Al-Ti-B system at 1000 K (727 °C) (Al corner),  $x$  represents the molar fraction, which is reproduced according to Jones and Pearson.<sup>[10]</sup>

can be obtained at a higher temperature. On the other hand, according to the phase diagrams in Figure 11, the solubilities of  $\text{Al}_3\text{Ti}$  and  $\text{AlB}_2$  phases in molten Al become larger as the temperature is increased. Thereby, increasing the temperature can accelerate the transfer speed of Ti and B to molten Al effectively.

As mentioned above, Ti and B can be easily obtained in the thin layer of Al at the reaction interface, and the Ti/B ratio in the reaction layer is much closer to  $\frac{1}{2}$  at a higher temperature. When the solutes [Ti] and [B] in liquid Al reaches saturation, they might be separated out as the compounds  $\text{Al}_3\text{Ti}$ ,  $\text{AlB}_2$ , and  $\text{TiB}_2$  in the ternary system of Al-Ti-B.  $\text{TiB}_2$  is the most thermodynamically stable phase due to its lowest free energy of formation among the three compounds. In addition, according to the phase diagram of Al-Ti-B shown in Figure 11,<sup>[12]</sup> rather low contents of Ti and B can lead to the formation of  $\text{TiB}_2$  phase. In addition, once the concentrations of [Ti] and [B] reach saturation in the Al melt,  $\text{TiB}_2$  nuclei precipitate from the saturation region in the Al melt.

### 3. Growth of $\text{TiB}_2$

As the reaction time is increased, more Ti and B are transferred from the molten salts to the reaction layer.  $\text{TiB}_2$  particles start to grow up due to the deposition of more Ti and B. It is known that the mass transfers of Ti and B from salts to the reaction interface become faster at a higher temperature, and a higher concentration of solutes in liquid Al can be obtained in a shorter time. Thereby, more Ti and B can be provided in the growth process of  $\text{TiB}_2$ , and then the  $\text{TiB}_2$  particles can grow larger easily. Meanwhile, the salts-melt reaction for synthesizing  $\text{TiB}_2$  phase becomes faster.

### G. Formation of $\text{TiB}_2$ at a Lower Temperature [973 K (700 °C)]

Figure 9(b) shows the yields and size distributions of  $\text{TiB}_2$  particulates in the S700 samples. When the salts-metal reaction proceeded at 973 K (700 °C) with a 10-minute reaction time, some  $\text{Al}_3\text{Ti}$  ( $\text{AlB}_2$  also should exist) phase existed in the Al matrix, the yield of  $\text{TiB}_2$  was just about 28.1 pct, and most of  $\text{TiB}_2$  particulates were smaller than 300 nm in size. The yield of  $\text{TiB}_2$

fabricated at 973 K (700 °C) with a 30-minute reaction time was 36.4 pct, which was higher than that of  $\text{TiB}_2$  in the S700-10 sample by about 29.5 pct. Furthermore, the ratio of  $\text{TiB}_2$  particles with a smaller size was increased, which indicated that a certain amount of smaller-sized  $\text{TiB}_2$  particles were synthesized as the reaction time was prolonged from 10 to 30 minutes. In addition, according to the SEM analysis (Figures 6 and 8), the products in the S700 samples were more complicated, in which blocky  $\text{Al}_3\text{Ti}$  particulates, tiny  $\text{TiB}_2$  particulates, and chain-like  $\text{Al}_3\text{Ti}$  reinforcement containing  $\text{TiB}_2$  phase were all formed.

Similarly, a reaction interface between the molten mixed salts and Al is firstly formed in the reaction at a lower temperature. However, more Ti and B might exist as  $\text{Al}_3\text{Ti}$  and  $\text{AlB}_2$ , respectively, at the reaction interface, because of the limited solubilities of the two phases at a lower temperature (as shown in Figure 10). It has been proved that the reaction between  $\text{K}_2\text{TiF}_6$  and Al occurs at a much higher rate than that between  $\text{KBF}_4$  and Al.<sup>[13]</sup> Thereby, the ratio of Ti/B in the thinner layer located at the reaction interface is easy to be greater than  $\frac{1}{2}$ , and this ratio will become greater as the temperature of molten Al is decreased. Part of Ti reacts with B to form  $\text{TiB}_2$  phase, following the precipitation-growth process, and the rest of Ti will react with Al to form  $\text{Al}_3\text{Ti}$  phase. As reported by Mohanty *et al.*,<sup>[14]</sup> the growth of  $\text{Al}_3\text{Ti}$  could engulf the entire  $\text{TiB}_2$  particles. Alternatively, the  $\text{Al}_3\text{Ti}$  might also nucleate as individual particulates.<sup>[15]</sup>

At a lower temperature, since the content of B is rather low in the reaction interface, the growth of  $\text{TiB}_2$  will be limited. As a result, the size of  $\text{TiB}_2$  in the S700-10 sample was much smaller than that of  $\text{TiB}_2$  produced in the S900-10 sample.

In the S700-30 sample, the newly formed  $\text{TiB}_2$  particulates had a smaller size. It is reasonable that the newly formed  $\text{TiB}_2$  particulates in the S700-30 sample were obtained according to reaction [11], by which  $\text{Al}_3\text{Ti}$  reacted with  $\text{AlB}_2$  to form  $\text{TiB}_2$ . The detailed formation process has been studied by Emamy *et al.*<sup>[16]</sup> and Michael Rajan *et al.*,<sup>[17]</sup> respectively. The basic sequence of  $\text{TiB}_2$  formation can be proposed as follows:

1. The B from  $\text{AlB}_2$  moves toward  $\text{Al}_3\text{Ti}$  phase;
2. Reaction takes place between Ti and B in a gap from  $\text{Al}_3\text{Ti}$  surface to form  $\text{TiB}_2$ ;
3. Dissolution of  $\text{Al}_3\text{Ti}$  phase due to natural cracking and fragmentation of  $\text{Al}_3\text{Ti}$  which lead to increased rate of  $\text{TiB}_2$  formation.

These steps involve the dissolutions of  $\text{AlB}_2$  and  $\text{Al}_3\text{Ti}$  phases and the reaction for synthesizing  $\text{TiB}_2$ . Thereby, the related formation process of  $\text{TiB}_2$  is a dissolution-reaction process. The detailed process in the present research is give below.

$\text{Al}_3\text{Ti}$  phase in the S700-10 sample mainly existed in the chain-like reinforcements. The area surrounding  $\text{Al}_3\text{Ti}$  phase was a [Ti]-rich region.  $\text{AlB}_2$  phase also existed in molten Al, which could dissolve in Al to generate B atoms. When B atoms contacted with the  $\text{Al}_3\text{Ti}$  phase, Ti and B could react to form  $\text{TiB}_2$ . The concentrations of [Ti] and [B] were rather low due to the

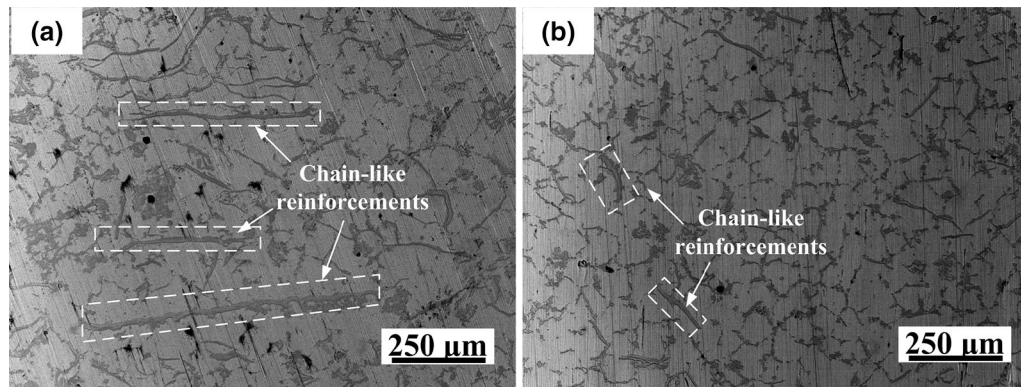


Fig. 12—Microstructures of the S700-10 sample (a) and S700-30 sample (b).

low temperature of molten Al; thereby, the  $\text{TiB}_2$  particles synthesized in this period were not able to grow large, and more  $\text{TiB}_2$  particles with a smaller size were formed. As a result, the percentage of  $\text{TiB}_2$  particles with smaller size in the S700-30 sample was increased compared with the S700-10 sample, as shown in Figure 9(b).

As the reaction time was increased, the quantities of  $\text{Al}_3\text{Ti}$  and  $\text{AlB}_2$  were both decreased, and more  $\text{TiB}_2$  could be formed. A comparison about the chain-like reinforcements between the S700-10 sample and the S700-30 sample is given in Figure 12. It is clear that the size of long chain-like reinforcements became small due to the dissolution of  $\text{Al}_3\text{Ti}$  phase in the formation of  $\text{TiB}_2$  particulates. In this research, because the temperature was rather low, a complete formation of  $\text{TiB}_2$  was hard to achieve in a short holding time. In order to obtain more  $\text{TiB}_2$  phase, a longer reaction time is needed. Chen *et al.*<sup>[2]</sup> reported that a completed reaction for synthesizing  $\text{TiB}_2$  could not be achieved with a 60-minute holding time after salt addition at 1023 K (750 °C), and large areas of  $\text{AlB}_2$  and  $\text{Al}_3\text{Ti}$  were observed along the grain boundary of the composites. One more thing should be mentioned is about the  $\text{AlB}_2$  phase. In this research, the phases in the slags produced in the fabrications of the S700-10 and S700-30 samples were similar; on the other hand, as the content of  $\text{TiB}_2$  was increased in the S700-30 sample, it is reasonable to think some  $\text{AlB}_2$  should exist in the S700 samples. As reported by Wang *et al.*,<sup>[18]</sup> blocky  $\text{AlB}_2$  could be formed in the Al-B master alloy at 1023 K (750 °C) with a 10-minute reaction time. Wang *et al.*<sup>[19]</sup> continued proving that the similar  $\text{AlB}_2$  particles still existed in the Al-B master alloy at 1023 K (750 °C) with a 30-minute reaction time. Due to the rather small amount of  $\text{AlB}_2$ , it was hard to be detected by XRD in this research.

#### IV. CONCLUSIONS

In this research, the influence of reaction temperature on the formation of  $\text{TiB}_2$  via the salts-metal reaction regarding the yield and size distribution of  $\text{TiB}_2$  particles was quantitatively analyzed firstly and the formation processes of  $\text{TiB}_2$  at a higher temperature [1173 K (900 °C)] and a lower temperature [973 K (700 °C)] were

both investigated as well. The following conclusions are drawn:

1. Reaction temperature has an important influence on the synthesis of  $\text{TiB}_2$  in molten Al via the salts-metal reaction. A high temperature [1173 K (900 °C)] is beneficial for the formation of  $\text{TiB}_2$ . A higher temperature can lead to a higher yield of  $\text{TiB}_2$  particles with a larger size. In contrast, smaller-sized  $\text{TiB}_2$  particles can be obtained at a lower temperature [973 K (700 °C)], but the formation of  $\text{TiB}_2$  can be limited significantly, resulting in a rather low yield of  $\text{TiB}_2$ .
2. At a higher reaction temperature [1173 K (900 °C)], the salts-metal reaction for synthesizing  $\text{TiB}_2$  phase mainly follows the precipitation-growth process, in which the precipitation and growth of  $\text{TiB}_2$  phase proceed quickly at the reaction interface between salts and liquid Al.
3. At a lower temperature [973 K (700 °C)], the precipitation-growth process and dissolution reaction between  $\text{AlB}_2$  and  $\text{Al}_3\text{Ti}$  both contribute to the formation of  $\text{TiB}_2$ . As the reaction time is prolonged,  $\text{TiB}_2$  particles with a smaller size can be formed through the process of the dissolution reaction.

#### REFERENCES

1. A. Mandal, R. Maiti, M. Chakraborty, and B.S. Murty: *Mater. Sci. Eng. A*, 2004, vol. 386, pp. 296–300.
2. Y.F. Han, X.F. Liu, and X.F. Bian: *Compos. A*, 2002, vol. 33, pp. 133–38.
3. M.L. Wang, D. Chen, Z. Chen, Y. Wu, F.F. Wang, N.H. Ma, and H.W. Wang: *Mater. Sci. Eng. A*, 2014, vol. 590, pp. 246–254.
4. G. Han, W.Z. Zhang, G.H. Zhang, Z.J. Feng, and Y.J. Wang: *Mater. Sci. Eng. A*, 2015, vol. 633, pp. 161–68.
5. Z.N. Chen, T.M. Wang, Y.P. Zheng, Y.F. Zhao, H.J. Kang, and L. Gao: *Mater. Sci. Eng. A*, 2014, vol. 605, pp. 301–09.
6. S. Lakshmi, L. Lu, and M. Gupta: *J. Mater. Process. Tech.*, 1998, vol. 73, pp. 160–66.
7. T.X. Fan, G. Yang, and D. Zhang: *Metall. Mater. Trans. A*, 2005, vol. 36, pp. 225–33.
8. C.F. Feng and L. Froyen: *J. Mater. Sci.*, 2000, vol. 35, pp. 837–50.
9. Z.W. Liu, M. Rakita, W. Xu, X.M. Wang, and Q.Y. Han: *Chem. Eng. J.*, 2015, vol. 263, pp. 317–24.
10. Y. Birol: *J. Alloy. Compd.*, 2009, vol. 480, pp. 311–14.
11. G.K. Sigworth: *Metall. Trans. A*, 1984, vol. 15, pp. 277–82.

12. G.P. Jones and J. Pearson: *Metall. Trans. B*, 1976, vol. 7, pp. 223–34.
13. C.D. Mayers, D.G. McCartney, and G.J. Tatlock: *Mater. Sci. Technol. Lond.*, 1993, vol. 9, pp. 97–103.
14. P.S. Mohanty and J.E. Gruzleski: *Acta Metall. Mater.*, 1995, vol. 43, pp. 2001–12.
15. M.M. Guzowski, G.K. Sigworth, and D.A. Sentner: *Metall. Trans. A*, 1987, vol. 18, pp. 603–19.
16. M. Emany, M. Mahta, and J. Rasizadeh: *Compos. Sci. Technol.*, 2006, vol. 66, pp. 1063–66.
17. H.B. Michael Rajan, S. Ramabalan, I. Dinaharan, and S.J. Vijay: *Mater. Design.*, 2013, vol. 44, pp. 438–45.
18. T.M. Wang, Z.N. Chen, H.W. Fu, J. Xu, Y. Fu, and T.J. Li: *Scrip. Mater.*, 2011, vol. 64, pp. 1121–24.
19. T.M. Wang, H.W. Fu, Z.N. Chen, J. Xu, J. Zhu, F. Cao, and T.J. Li: *J. Alloy. Compd.*, 2012, vol. 511, pp. 45–49.