

# **A Photonic Crystal Fiber‑Based Biosensor with Quasi‑D‑shaped Layout and ITO‑Graphene Combination**

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#### **Abstract**

A quasi-D-shaped photonic crystal fber (PCF) biosensor in the near-infrared region (NIR) is proposed for the purpose of detecting the analytes/liquids of diferent refractive indices (RIs) ranging from 1.21 to 1.32. In order to realize sensing in the near-infrared region, we use indium tin oxide (ITO) as the plasma material. Then a fake of graphene is deposited on the ITO flm. Graphene has excellent molecular adsorption performance, which can improve the detection capability of the PCF sensor. Graphene becomes an ideal dielectric layer for sensing due to its large surface area and rich *π*-conjugation. To enhance the birefringence, we introduce two elliptical holes around the core. The proposed sensor is designed and numerically analyzed by fnite element method. Thickness of the ITO, graphene layer, and the ellipticity of ellipse of PCF are varied so as to study its efect on the sensing characteristics of the proposed sensor. Wavelength sensitivity of the proposed sensor is as high as 12,000 nm/RIU (refractive index unit), and a maximum resolution can be  $8.33 \times 10^{-6}$  RIU. Compared with the traditional D-shaped sensors, the proposed sensor has the advantages of easy manufacturing and high sensitivity.

**Keywords** Photonic crystal fber · Biosenor · Surface plasmon resonance

# **Introduction**

Surface plasmon resonance (SPR) is widely used in the feld of sensors. It has attracted the interest of many scholars in the past decade. The SPR sensor has great potential in the felds of medical diagnosis, biomolecular analyte detection, and organic chemistry detection  $[1-3]$  $[1-3]$ . Photonic crystal fibers are increasingly employed as the carrier of SPR sensors because of its fexible structure design and high birefringence. For example, Juan Liu designed a PCF-SPR sensor with a silver core [[4\]](#page-8-2). The average wavelength sensitivity of this sensor can reach to the value of 23,821 nm/refractive index unit

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(RIU) with a resolution of  $4.2 \times 10^{-6}$  RIU for an analyte refractive index (RI) ranging from 1.38 to 1.44. However, it is a technical challenge to deposit a silver flm in the air hole of the PCF. Fengning Zha proposed a PCF-SPR sensor that has a detection for RI of the analyte ranging from 1.30 to 1.42 [[5\]](#page-8-3). This sensor is structured with a D-shaped air hole inside the PCF, which increases the difficulty of processing. PCF is generally drawn at high temperature. However, how to make the D-shaped surface of the small hole smooth during the fabrication process is still a challenge at present. As all known, the smoothness of the coating plane seriously afects sensitivity of the sensor. In literature, the graphenesilver-based PCF-SPR sensor proposed by Ahmmed A. Rifat has a maximum amplitude sensitivity of 418 nm/RIU and resolution as high as  $2.4 \times 10^{-5}$  RIU [\[6](#page-8-4)]. However, the corresponding sensing range is as small as 1.46–1.49 only, and the detection range is too narrow to sense for practical applications. However, most of PCF-SPR sensors are applied to the detection of high refractive indexes. In practice, it is important to detect low refractive index analytes between 1.20 and 1.32, e.g., fuorine-containing organics, medical oxygen, liquid  $CO<sub>2</sub>$ , and sevoflurane serving as anesthetics in the biomedical feld [\[7,](#page-8-5) [8\]](#page-8-6).

In this manuscript, we proposed a novel type of quasi-Dtype PCF-SPR sensor coated with indium tin oxide (ITO) and a graphene layer. The operating range of the proposed sensor is in the IR region. The upward movement of the core allows us to polish away a small portion of the fber only, which reduces the difficulty of manufacturing and increases the strength of the fber. Generally speaking, gold and silver are commonly used for sensing materials. However, gold and silver have their SPR wavelength in the visible region. Gold is chemically stable and has a large shift in the resonance wavelength. But the refractive index change in this sensing area is a little [[9\]](#page-8-7). Silver is a chemically active material and can be oxidized very quickly, which leads to degradation of its sensing performance [\[10\]](#page-8-8). Based on the reasons above, in this article we employ ITO as the sensing material. The plasma frequency of ITO can be tuned by means of changing the doping concentration of tin oxide to indium oxide to ensure that it works within the selected wavelength range  $[11, 12]$  $[11, 12]$  $[11, 12]$ . There are several advantages of choosing the working wavelength in the near-infrared region. Firstly, some proteins and biomolecules are marked in the NIR region. If the SPR-based sensing method is considered to detect such molecules, it is too difficult to use gold or silver as the sensing material. Secondly, the near-infrared evanescent wave can penetrate deeply into the analyte, which makes the high sensitivity. Finally, the fber-based SPR sensor in NIR has low loss because of the low fber transmission loss in this region. However, the ITO sensors cannot be used directly for biosensing because they do not have an ideal affinity for biomolecules. Therefore, we add a layer of graphene on its surface for the purpose of improving the affinity. As a new material, graphene is extensively explored by scholars [[13](#page-9-1)[–15\]](#page-9-2). Graphene can not only improve the performance of the sensor but also

be helpful in signifcant adsorption of biomolecules due to *π*-−*π* stacking [[16](#page-9-3), [17\]](#page-9-4).

A fnite element method (FEM) is used to numerically analyze the performance of the D-shaped PCF-SPR sensor. Because the structure of the proposed sensor does not change in the *z*-direction (longitudinal), we built a twodimensional model for our simulation. The establishment of a two-dimensional model also greatly reduces the running time of the calculation. By tuning the structural parameters, the maximum spectral sensitivity of up to 12,000 nm/RIU is obtained for analyte RIs ranging between 1.21 and 1.32, corresponding to the theoretical resolution of 8.33  $\times$  10<sup>-6</sup> RIU.

## **Structure Design and Numerical Simulation**

In this article, we use the loss spectrum analysis method. Firstly, obtain the efective refractive index of the mode feld according to the fnite element method, and then draw the loss spectrum of the sensing model according to the imaginary part of the refractive index. In order to improve the calculation accuracy, the scattering boundary is fxed, and a perfectly matched layer (PML) is used to absorb the scattered energy. Figure [1](#page-1-0) shows the schematic diagram of the PCF-SPR sensor based on fused silica. The diagram in the bottom right corner is the divided grid picture in the calculation, and the outermost layer is the perfect matching layer. Silica is set as the substrate material. The diameters of the big air hole and the small air hole are  $d_1 = 1.2 \mu m$  and  $d_2 = 1.6 \mu m$ , respectively. The pitch of the adjacent air holes is  $\Lambda = 1.8$  μm, and the polished depth  $D = 4.6 \mu$ m. There are two elliptical holes beside the core. The long axis length is  $d<sub>v</sub> = 1.5 \mu m$ , the short axis length is  $d_x = 0.6 \, \mu \text{m}$ . ITO film is plated on the surface of

<span id="page-1-0"></span>

the optical fber with a thickness of 45 nm. A monolayer of graphene is deposited on the ITO flm with a thickness of 0.34 nm. The values of real and imaginary parts of the permittivity of ITO are calculated as [[18\]](#page-9-5):

$$
\varepsilon_m(\lambda) = \varepsilon_\infty - \frac{\lambda^2 \lambda_c}{\lambda_p^2(\lambda_c + i\lambda)}
$$
 (1)

where  $\varepsilon_{\infty}$  is the dielectric constant for the infinite value of the frequency,  $\lambda$  is the wavelength of the incident light,  $\lambda_p$  = 5.6497 m ×10<sup>7</sup> in the plasma wavelength of ITO, and  $\lambda_c = 11.21076 \text{ m} \times 10^6 \text{ in the collision wavelength of ITO.}$ 

Graphene is deposited on the ITO flm. The complex RI of graphene can be obtained from the equation below [[19\]](#page-9-6):

$$
n_g = 3 + \frac{iC_1\lambda}{3} \tag{2}
$$

where constant  $C_1$  is approximated as 5.446  $\mu m^{-1}$  and  $\lambda$  is the vacuum wavelength in micrometer. The fxed thickness of single-layer graphene is 0.34 nm. Moreover, the total thickness of the graphene layer can be calculated using the following equation  $t<sub>g</sub> = 0.34$  nm  $\times$  *L*, where *L* is the number of graphene layers.

Confnement loss is a basic parameter normally used for the purpose of estimating sensor performance, which can be obtained from the following equation [[2,](#page-8-10) [20\]](#page-9-7):

<span id="page-2-0"></span>
$$
\alpha(\text{dB/cm}) = 8.686 \times k_0 \times \text{Im}\left(n_{\text{eff}}\right) \times 10^4 \tag{3}
$$

where  $k_0 = \lambda/2\pi$  is the wavenumber, here unit of  $\lambda$  is micrometers. Im( $n_{\text{eff}}$ ) represents the imaginary part of the efective refractive index. It can be known from Eq. [\(3](#page-2-0)) that the confnement loss is proportional to the imaginary part of the efective refractive index.

Here, we intentionally design the layout with two elliptical holes around the core for the purpose of destroying the symmetry and obtain a signifcant polarization efect. The length of long axis is  $d_v$ , the short axis is  $d_x$ , and the corresponding ellipticity  $\eta = d_v/d_v$ . As can be seen from Fig. [2](#page-2-1), the green solid line and the dashed line, respectively, indicate the loss of *y*-pol and *x*-pol when the elliptical air holes are not introduced. The red solid line and the dashed line, respectively, represent the loss of *y*-pol and *x*-pol for the layout of the elliptical air holes. In comparison, it can be seen clearly that after the structure is improved, the polarization of the fundamental mode in the *y*-direction is nearly doubled, and the confnement loss is red-shifted. Confnement loss is one of the important parameters of the biosensors like PCF-SPR. The higher the loss, the easier of the sensor detection will be. At the same time, we can also see from Fig. [2](#page-2-1) that the polarization loss of the fundamental mode in *x*-direction is extremely low. Thus, in this article, our study concentrates on the confnement loss of *y*-pol.

At present, the manufacturing and drawing technology of PCF are well developed [[21,](#page-9-8) [22](#page-9-9)]. The manufacturing



<span id="page-2-1"></span>**Fig. 2** Confnement loss for before and after introducing the oval air holes with *x* direction (dashed) and y direction (solid)

technology of ITO film is also mature and has many applications in industry. In addition, it was reported that graphene can be deposited on ITO [[23](#page-9-10)]. Therefore, we believed that the proposed quasi-D-shaped PCF-based SPR sensor can be practically realized.

## **Results and Discussion**

In this section, we perform preliminary numerical calculations on the proposed structure. Various modes such as core-guided mode, surface plasmon polaritons (SPPs) mode, and coupled mode are shown in the fgure below. Moreover, the relationship between confnement loss and dispersion is observed.

## **Loss Spectra and Dispersion Relations**

We investigate the mechanism of plasma wave transduction in more detail in this sub-section. A typical fber optical plasmonic sensor operates near the phase matching point between the core-guided mode and the metalized surface plasmon wave. We show the dispersion relationship between the core-guided mode (green curve) and the surface plasmon polaritons mode (SPPs mode, see blue curve), as shown in Fig. [3.](#page-3-0) The phase matching point is 1748 nm, at which the refractive index of the fundamental mode and the plasma mode are equal. Near the phase matching point, the effective refractive index of the fundamental mode has a sudden rise, while the effective refractive index of the plasma mode has a sudden drop. In the vicinity of the phase matching point, the two modes are strongly mixed, as energy is transferred from the fundamental mode to the plasmonic mode, the loss of the fundamental mode increases dramatically. Confnement loss reaches its peak at this point, as shown by the red curve. Detecting the increase of confnement loss near the phase matching point has become the crucial issue for many sensor designs.

#### **Sensitivity**

The proposed sensor is surrounded by analyte, as shown in Fig. [1](#page-1-0). Firstly, we review the principle of SPR sensor. When the propagation constant of the incident light is equal to the collective oscillation of electrons on the metal surface, their momentum can be matched and resonance occurs. Therefore, SPR is highly sensitive to changes of the refractive index (RI). When RI of the analyte changes,  $\lambda_{\text{peak}}$  has blue-shift or red-shift accordingly. Figure [4](#page-4-0) shows the loss spectrum of the fundamental mode when the RI changes from 1.21 to 1.32. As shown in the pictures, as the RI increases,  $\lambda_{\text{peak}}$  moves toward the long wavelength direction, i.e., a red shift occurs. When the RI reaches 1.33, the loss peak is broadened, which is not easy to be measured and cannot meet the performance requirements of the sensor. Thus, it is not considered here. Wavelength sensitivity is one of the important parameters for analyzing sensor performance. The overall wavelength sensitivity can be estimated with the following formula [\[24\]](#page-9-11):

<span id="page-3-0"></span>**Fig. 3** Dispersion relation of the core-guided mode (green), plasmonic mode (blue), and the loss spectrum (red); inset of (**a**) shows the electric feld of the plasmonic mode and inset of (**b**) shows the electric feld of core-guided mode; (**c**) shows the electric feld on the phase matching point with design parameters of  $n_a = 1.31$ ,  $d<sub>x</sub> = 1.2 \text{ µm}, d<sub>y</sub> = 1.6 \text{ µm},$ thickness of  $ITO = 45$  nm, and number of graphene layer  $L = 1$ 



<span id="page-4-0"></span>



$$
S(nm/RIU) = \frac{\Delta \lambda_{\text{peak}}}{\Delta n_a}
$$
 (4)

$$
R(RIU) = \Delta n_a \frac{\Delta \lambda_{\text{min}}}{\Delta \lambda_{\text{peak}}} \tag{5}
$$

where  $\Delta n_a$  is the variation of analyte RIs and  $\Delta \lambda_{\text{peak}}$  is the diference between the two resonance wavelengths. There is a maximum peak shift of  $\Delta \lambda_{\text{peak}} = 120 \text{ nm}$  with RIs varying from 1.31 to 1.32, and a maximum spectral sensitivity of 12,000 nm/RIU is achieved. Resolution of a sensor is another important parameter, which can be expressed by the following equation [[24\]](#page-9-11):

where  $\Delta \lambda_{\text{min}}$  is the resolution of the instrument, which is assumed to be 0.1,  $\Delta \lambda_{\text{peak}}$  represents the difference of the wavelength peak shift, and  $\Delta n_a$  indicates the change in refractive index (0.01) of the analyte. When the RI of the analyte changes from 1.31 to 1.32, the resolution of this sensor reaches the value of  $8.33 \times 10^{-6}$  RIU.

Furthermore, the comparison between the sensor we designed and the reported sensor is shown in Table [1.](#page-5-0) It can be seen from the table that our sensor is very competitive.

### **Investigation of Various Structural Parameters**

As a type of microstructure fber, the structure of PCF has a great infuence on its performance. In this section, the infuence of structural parameters of the quasi D-shaped PCF such as ellipse parameters, ITO layer thickness, and the number of graphene layer can be observed on the sensing performance of the proposed sensor.

## **Impact of the Parameters of Elliptical Holes on the Sensing Performance**

In this section we discuss the influence of  $\eta$  of the elliptical hole surrounding the core on the performance of the proposed sensor. We know that  $\eta$  affects not only the birefringence of the structure but also the distribution of light transmission energy. Therefore, in order to obtain good polarization characteristics and effective transmission quality, it is necessary to optimize the size of the elliptical hole.

Figure [5](#page-6-0) depicts the variation in the peak loss with different  $\eta$ . In order to change the ellipticity, we fix geometrical parameter of  $d_x = 0.6 \mu$ m and only change *dy* from 1.4 to 1.7 μm. As can seen from Fig. [5](#page-6-0)a that when  $d_x = 0.6 \mu m$  and  $d_y = 1.5 \mu m$ , the peak value of the confnement loss reaches the maximum value, and its peak loss is the sharpest. In the same way, we fix  $d<sub>v</sub> = 1.5 \mu m$  and change  $d_x$  from 0.4 to 0.7  $\mu$ m, and we obtain the results, as shown in Fig. [6b](#page-7-0). When  $d<sub>v</sub> = 1.5 \text{ }\mu\text{m}$  and  $d<sub>v</sub> = 0.6 \text{ }\mu\text{m}$ , the confnement loss reaches the maximum value.

#### **Impact of ITO Layer Thickness**

In this section, we discuss the infuence of ITO flm thickness on sensor performance. The thickness of the ITO layer varies from 40 to 60 nm, and the maximum confnement loss occurs at 45 nm, as shown in Fig. [6](#page-7-0). When the thickness exceeds this value, high damping loss can result in an overall reduction in confnement loss.

#### **Impact of Graphene Layer Thickness**

The number of graphene layers also greatly affects the performance of the sensor. As can be seen in Fig. [7](#page-7-1), with the number of graphene layers increases from  $L = 1$  to  $L = 5$ , the confnement loss decreases from 886 to 613 dB/cm accordingly. The reason is that as the number of graphene layers increases, the electronic behavior of graphene will approach to that of bulk graphite according to the infrared conductivity spectrum mentioned in the literature [[29\]](#page-9-12).

## **Impact of Polishing Depth**

The smooth sensing surface of the D-shaped sensor can be manufactured by means of polishing; hence, the impact of the polishing depth on the performance of the sensor also needs to be considered here. Figure [8](#page-8-11) shows the loss spectrum when the polishing depth *d* changes from 2.7 to 2.9 μm. It can be seen from the fgure that the peak value reaches the highest point in the case of  $d = 2.8 \text{ }\mu\text{m}$ .

# **Conclusions**

A highly sensitive biosensor designed on the basis of grapheme layers coated with ITO layer structured in quasi-D-shaped is proposed. In order to achieve the desired performance, we optimize the sensor structure parameters. The advantage of using ITO is that its resonance wavelength can be tuned in the near-infrared regime, and graphene layers ensure the affinity of the sensor for biomolecules. The structure is numerically analyzed using a fnite element method. The resolution of the proposed sensor can reach to the level of 8.33  $\times 10^{-6}$  RIU, with wavelength sensitivity of as high as 12,000 nm RIU<sup>-1</sup> for RI variation of the analytes ranging from 1.21 to 1.32. The sensor has excellent sensing performance and huge commercial potential in biosensing and environmental monitoring. At the same time, it should be noted that this type of sensor (including our proposed) cannot obtain excellent sensing performance in the entire efective sensing range. This should be the direction of our future work.



<span id="page-5-0"></span>**Table 1** Comparative analysis of previously reported RI sensor

<span id="page-6-0"></span>**Fig. 5** Confnement loss for diferent ellipticities of elliptical holes. **a** Fix  $d_x$  and change  $d_y$ from 1.4 μm to 1.7 μm. **b** Fix  $d_y$  and change  $d_x$  from 0.4 to  $0.7 \mu m$ 



<span id="page-7-0"></span>**Fig. 6** Variation of confnement loss with diferent ITO thickness



<span id="page-7-1"></span>**Fig. 7** Variation of loss peaks with varying the number of graphene layer



<span id="page-8-11"></span>**Fig. 8** Variation of loss with diferent polishing depths



**Authors' Contributions** All authors contributed to the study conception and design. Material preparation, data collection, and analysis were performed by Jiaguo Tian, Cheng Xu, and Songya Cui. The frst draft of the manuscript was written by Jiaguo Tian. The revision of the manuscript was completed by Jiaguo Tian and Yongqi Fu. All authors read and approved the fnal manuscript.

**Data Availability** All data generated or analyzed during this study are included in this published article.

#### **Compliance with Ethical Standards**

**Competing Interests** The authors declare that they have no confict of interest.

**Ethical Approval** This research is an original research, and there is no plagiarism from others.

**Consent to Participate** Informed consent was obtained from all individual participants included in the study.

**Consent to Publish** The participant has consented to the submission of the case report to the journal.

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