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Effects of tide-surge interactions on storm surges along the coast of the Bohai Sea, Yellow Sea, and East China Sea

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Abstract A two-dimensional coupled tide-surge model was used to investigate the effects of tide-surge interactions on storm surges along the coast of the Bohai Sea, Yellow Sea, and East China Sea. In order to estimate the impacts of tide-surge interactions on storm surge elevations, Typhoon 7203 was assumed to arrive at 12 different times, with all other conditions remaining constant. This allowed simulation of tide and total water levels for 12 separate cases. Numerical simulation results for Yingkou, Huludao, Shijiusuo, and Lianyungang tidal stations were analyzed. Model results showed wide variations in storm surge elevations across the 12 cases. The largest difference between 12 extreme storm surge elevation values was of up to 58 cm and occurred at Yingkou tidal station. The results indicate that the effects of tide-surge interactions on storm surge elevations. It is therefore essential that these are taken into account when predicting storm surge elevations.

Keywords Storm surges, Astronomical tides, Tide-surge interactions, Typhoon 7203, Coupled tide-surge model

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1. Introduction

People in coastal areas can be affected by storm surges, with these being abnormal increases or decreases in sea level induced by typhoons and atmospheric pressure disturbances (You and Seo, 2009; Yang et al., 2014). Storm surges can be positive or negative. A positive storm surge can result in significant loss of life and property damage, for example through the destruction of coastal infrastructure (Lin et al., 2012; Olbert et al., 2013; Haigh et al., 2014). Negative surges (Pousa et al., 2013) mainly jeopardise maritime safety and coastal engineering structures. It is vitally important to study storm surges along the coast, as results can provide useful information for risk-based flood man-

agement and engineering planning (Olbert et al., 2013).

Typhoons can bring about significant storm surges in coastal regions (Zhang et al., 2015; Yang et al., 2015), such as storm surges. To improve coastal storm surge forecasting, Peng et al. (2006) constructed a four-dimensional variational data assimilation algorithm using a tangent linear model and an adjoint model of the Princeton Ocean Model (POM). Peng et al. (2007) and Li et al. (2013) used this adjoint optimal technique to adjust initial conditions, boundary conditions, and the wind stress drag coefficient in the POM. Yin et al. (2009) simulated five typhoon storm surges in the East China Sea using a coupled model and suggested that a storm surge-wave coupled model should be used for storm surge prediction.

Storm surges can be aggravated if coinciding with a high spring tide or with a low neap tide (Maspataud et al., 2013; Olbert et al., 2013). In recent years, researchers have ex-

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plored the interactions between storm surges and astronomical tides in certain coastal areas using different methods. Zhang et al. (2007) utilised the two-way nested coupled tide-surge model to study the combined effects of storm surges and astronomical tides in the Taiwan Strait. Simulation results indicated that the influence of astronomical tides on storm surges should be taken into account in prediction models. Park et al. (2012) analysed the effects of water depth and astronomical tides on storm surges using the coupled numerical model PBL-ADCIRC. Results confirmed that the coupling of storm surges and tides is an essential consideration in coastal areas with shallow water depth and large tides. Antony et al. (2013) examined the dependency of surge maxima on tide magnitudes and phases, quantifying their interaction along the east coast of India and the head of the Bay of Bengal. They found that the strength of interaction tended to increase northward when tidal ranges and surge heights increased. Kong (2014) calculated and analysed 57 cases of Typhoon 7203 to study the impact of tidal waves on storm surges in the north of Liaodong Bay, using DHI Mike21.

However, little attention has been paid to the impacts of tide-surge interactions on storm surges along the coasts of the Bohai Sea, Yellow Sea, and East China Sea, all of which are vulnerable to such phenomena. In the present paper, we investigate the effects of tide-surge interactions on storm surge elevations during Typhoon 7203 using a two-dimensional coupled tide-surge model. Eight principal constituents (M2, S2, K1, O1, N2, K2, P1, and Q1) were introduced into the numerical model through open boundary conditions and tidal potentials. Meteorological driving forces that generate storm surges were provided by the wind forcing module and pressure field.

2. **Coupled tide-surge model**

The coupled tide-surge model is based on a depth-averaged two-dimensional flow model. This section describes the model framework in detail.

2.1 Basic equations

The governing equations used in the two-dimensional flow model are composed of depth-averaged equations of continuity and momentum.

$$\frac{\partial \zeta}{\partial t} + \frac{1}{a} \frac{\partial \left[\left(h + \zeta \right) u \right]}{\partial \lambda} + \frac{1}{a} \frac{\partial \left[\left(h + \zeta \right) v \cos \varphi \right]}{\partial \varphi} = 0, \qquad (1)$$

$$\frac{\partial u}{\partial t} + \frac{u}{a} \frac{\partial u}{\partial \lambda} + \frac{v}{R} \frac{\partial u}{\partial \varphi} - \frac{uv \tan \varphi}{R} - fv + \frac{ku\sqrt{u^2 + v^2}}{h + \zeta} - A\Delta u + \frac{g}{a} \frac{\partial (\zeta - \overline{\zeta})}{\partial \lambda} + \frac{1}{\rho_w a} \frac{\partial P_a}{\partial \lambda} - \frac{\rho_a}{\rho_w} \frac{C_d W_x \sqrt{W_x^2 + W_y^2}}{h + \zeta} = 0, \quad (2)$$

$$\frac{\partial v}{\partial t} + \frac{u}{a}\frac{\partial v}{\partial \lambda} + \frac{v}{R}\frac{\partial v}{\partial \varphi} + \frac{u^2 \tan \varphi}{R} + fu + \frac{kv\sqrt{u^2 + v^2}}{h + \zeta} - A\Delta v + \frac{g}{R}\frac{\partial(\zeta - \overline{\zeta})}{\partial \varphi} + \frac{1}{\rho_w R}\frac{\partial P_a}{\partial \varphi} - \frac{\rho_a}{\rho_w}\frac{C_d W_y \sqrt{W_x^2 + W_y^2}}{h + \zeta} = 0, \quad (3)$$

where t is time; λ and ϕ are east longitude and north latitude, respectively; h is depth of undisturbed water; ζ is sea surface elevation, relative to the undisturbed level; $h+\zeta$ is total water depth; u and v are the east and north components of the current, respectively; $\overline{\zeta}$ is the adjusted height of equilibrium tides; R is the radius of the earth and $a=R\cos\phi$; $f=2\Omega\sin\phi$ is the Coriolis parameter (here, Ω is the angular speed of the Earth's rotation); k is the bottom friction coefficient; A is the horizontal eddy viscosity coefficient; Δ is the Laplace operator and $\Delta(u,v) = a^{-1} \left[a^{-1} \partial_{\lambda} (\partial_{\lambda}(u,v)) \right]$

$$+R^{-1}\partial_{\varphi}\left(\cos\varphi\partial_{\varphi}\left(u,v\right)\right)$$
; g is gravitational acceleration; P_{a}

is atmospheric pressure on the sea surface; $\rho_w = 1025 \text{ kg m}^{-1}$ is seawater density; $\rho_a=1.27$ kg m⁻³ is air density, and W_x and W_y are the x and y components of the surface wind field. In this paper, the wind-stress coefficient C_d was calculated on the basis of wind velocity U_{10} measured at 10 m above mean sea surface (Wu, 1982):

$$C_d = (0.8 + 0.065 \times U_{10}) \times 10^{-3}.$$
(4)

2.2 Initial conditions and boundary conditions

In the present coupled model, initial values of current velocity and surface elevation were calculated using the tidal model. Along closed boundaries, it was assumed that no water would be allowed to flow to the coast; that is, the normal component of the current would be zero. This can be expressed as $\vec{u} \cdot \vec{n} = 0$, where $\vec{u} = (u, v)$ is the current

vector and \vec{n} is the outward unit vector.

The main areas of research for this study were the Bohai Sea and northern Yellow Sea. Suppose that there is a current with a speed of 0.5 m s⁻¹ at the open boundary point (130.9°E, 33.8°N). It will take 24 days for the current to arrive at the LianYunGang tidal station (119.45°E, 34.75°N). However, the simulation time of the typhoon is only three days. In this case, the open boundary conditions of the storm surge are negligible. The present open boundary conditions are therefore determined as sea-surface elevations caused by tides, as follows:

$$\zeta = \sum_{j=1}^{J} f_j H_j \cos\left(\omega_j t + u_j + v_j - g_j\right), \tag{5}$$

where H_i and g_i are the amplitude and phase-lag of the *j*th tidal constituent, respectively; ω_i is angular speed; v_i is the initial phase angle; f_j is the nodal factor; and u_j is the

nodal angle.

2.3 Wind forcing module

Meteorological driving forces that generate storm surges are mainly composed of surface wind stress and pressure gradient forces (Zhang et al., 2007; Chen et al., 2012). It is therefore critical for tropical storm simulations to determine surface wind and pressure fields.

Compared with the impact of a pure tropical storm, that of the background wind field on a storm surge is probably weaker; however, it should not be neglected (Wen et al., 2008; Tang et al., 2013). According to Wen et al. (2008), the synthetic wind field is given by reanalysis surface winds data of the National Centres for Environmental Prediction (NCEP) and by the storm model. The latter (Jelesnianski, 1965) is expressed as follows:

$$\vec{W}_{sm} = \begin{cases} \frac{r}{R+r} \left(V_{ox}\vec{i} + V_{oy}\vec{j} \right) + W_{R} \frac{1}{r} \left(\frac{r}{R} \right)^{\frac{3}{2}} \left(A\vec{i} + B\vec{j} \right), 0 < r \le R, \\ \frac{R}{R+r} \left(V_{ox}\vec{i} + V_{oy}\vec{j} \right) + W_{R} \frac{1}{r} \left(\frac{R}{r} \right)^{\frac{1}{2}} \left(A\vec{i} + B\vec{j} \right), \ r > R, \end{cases}$$
(6)

where *i* and *j* are eastward and northward unit vectors, respectively; V_{ox} and V_{oy} are the components of moving velocity of the storm centre; *r* is the distance between the grid and storm centres; \vec{W}_{sm} is the wind speed at radius *r*; and *R* is the radius of the maximum wind speed W_R .

$$A = -\left[\left(x - x_{c}\right)\sin\theta + \left(y - y_{c}\right)\cos\theta\right],\tag{7}$$

$$B = \left[\left(x - x_c \right) \cos \theta - \left(y - y_c \right) \sin \theta \right], \tag{8}$$

where (x, y) and (x_c, y_c) are the centre coordinates of the grid and storm, respectively; the inflow angle θ is taken as

$$\theta = \begin{cases} 20^{\circ}, & r \le R, \\ 15^{\circ}, & r > R. \end{cases}$$
(9)

We then overlaid this storm model onto the background wind field (NCEP) using a weight coefficient *e* and obtaining a synthetic wind field \vec{W}_{sy} (Wen et al., 2008):

$$\vec{W}_{\rm sy} = \vec{W}_{\rm sm} \left(1 - e \right) + e \vec{W}_{\rm ncep} , \qquad (10)$$

where \vec{W}_{ncep} is the NCEP wind field. The letter *e* is a weight coefficient determined as $e = \frac{(r/nR)^4}{1 + (r/nR)^4}$ (*n* is

usually taken to be 9 or 10). The coefficient e varies with the distance between the grid centre and storm centre. It ensures that the storm model is adopted in the vicinity of the tropical storm, but that the NCEP wind field is used away from the storm centre. Meanwhile, it also ensures a smooth transition between the two wind fields.

The pressure field for the tropical storm (Jelesnianski, 1965) is determined as follows:

$$P_{a} = \begin{cases} P_{0} + \frac{1}{4} \left(P_{\infty} - P_{0} \right) \left(\frac{r}{R} \right)^{3}, & r \leq R, \\ P_{\infty} - \frac{3}{4} \left(P_{\infty} - P_{0} \right) \left(\frac{R}{r} \right), & r > R, \end{cases}$$
(11)

where P_a is the sea surface pressure at r; P_0 is the pressure at the storm centre; and P_{∞} is ambient pressure and is here assumed to be equal to 1020 hPa.

3. Numerical procedure

3.1 Model configuration

The coupled tide-surge model used in this study covered an area of the Bohai Sea, Yellow Sea, and East China Sea. The open boundaries were set along the first island chains and the Taiwan Strait. At this location, tides are provided by eight principal constituents (M2, S2, K1, O1, N2, K2, P1, Q1). The numerical model domain extends from 117.5°E to 131.5°E and from 24°N to 41°N; bathymetry data was obtained from E-TOP-5. The spherical grid has a resolution of 1/12th of a degree, that is, 5'×5'. The time step was set to 60 s.

The model was able to compute three water levels: the tide level without the effect of meteorological forcing (denoted by tidal model); a pure storm surge without regard to tidal impact (denoted by storm surge model); and total water level, considering tidal and meteorological forcing (denoted by coupled tide-surge model). In order to investigate the effects of tide-surge interactions on storm surge elevations, the model was run three times for each storm event (Zhang et al., 2007). During the first run, we calculated total water level with tidal and meteorological forcing. During the second run, we only simulated the tidal level using the tidal model. By subtracting the tidal level from the total water level, we obtained a storm surge elevation time series with the coupling effect of tide-surges. During the third run, we simulated the pure storm surge level using the storm surge model. When the pure storm surge elevation was subtracted from the storm surge elevation with coupling effects, we were able to obtain the water level caused by tide-surge interactions.

3.2 Case description

In the Bohai Sea, Yellow Sea, and East China Sea, the tide regularly rises and falls day after day. Typhoons occur, usually resulting from low-pressure systems, and can lead to a sharp rise or fall in seawater level, that is, storm surges. If these are combined with astronomical tides, abnormal increases or decreases in water level may occur, referred to as storm tides (Kong, 2014). Specifically, flooding and ebbing tidal phases can affect the height and arrival time of peak surges (Sinha et al., 2008).

In this paper, we explore the influences of tide-surge interactions on storm surge elevations during Typhoon 7203 at several tidal stations. Figure 1 shows the track of Typhoon 7203 (from 25–28th July, 1972) and the locations of tidal stations. Typhoon data was available at six-hourly intervals.

A tide has steady high and low water elevations, but storm surge elevations are relevant to typhoon intensity and landing time. The interaction between tides and storm surges differs at different landing times. Different tide-surge interactions can thus cause differences in computational scenarios.

For the purpose of exploring the impacts of tide-surge interactions on storm surge elevations, we assumed that Typhoon 7203 arrived at 12 different times, with all other conditions remaining constant; that is, there were 12 independent cases for analysis. Specific processes were determined as per the following steps. Suppose that the start time of the first numerical experiment (hereafter, E1) was 08:00 AM on 25th July, 1972; that is, the typhoon arrived at this time. In the second numerical experiment (hereafter, E2), the start time was 10:00 AM on 25th July, 1972. The arrival time of the typhoon in E2 was two hours later than in E1. In other words, there was a two-hour lag between the two contiguous experiments; in this way, 12 cases were simulated. For all cases, background wind fields were taken from NCEP reanalysis surface winds data, spanning the period from 08:00 AM on 25th July to 08:00 AM on 28th July, 1972. Typhoon and pressure data were from Typhoon 7203. Each experiment lasted 72 h and was consistent with the time length of Typhoon 7203. In addition, 12 tidal levels were also simulated using the tidal model.

4. Results and discussion

4.1 Tides

When the tidal potential and open boundary terms are removed from eqs. (2), (3) and (5), the coupled tide-surge model is reduced to the storm surge model of Fan et al. (2011). The latter authors conducted verification of computed water surface elevation representing the Typhoon 7203induced storm surge, based on field data at different tidal stations; model results showed that the numerical simulations of the storm surge were reasonable.

When the pressure term and wind stress term are removed from eqs. (2) and (3), the coupled tide-surge model is reduced to the tidal model of Lu et al. (2006). In the tidal



Figure 1 Asterisks denote tidal stations, solid lines represent the track of Typhoon 7203, and red circles indicate the typhoon time series.

model, the computing area, spherical resolution, and time step are the same as those of the coupled tide-surge model. Initial values of sea surface elevation and horizontal velocities were set to zero. The tidal model is driven by tidal potential and open boundary conditions. Tidal potential was calculated as per Fang et al. (1999), and the sea surface elevation on the open boundary condition was provided by eq. (5). The model start point was 27th April, 1972 and it ran for 90 days, with the possibility of harmonic analysis calculations for simulated results over the latter 60 days of the simulation. Table 1 lists absolute mean differences in amplitude and phase-lag of sea surface elevation between simulated results and observations at the 489 points of TOPEX/ Poseidon (T/P) tracks (as shown in Figure 2) for the four principal constituents M2, S2, K1, and O1. Their cotidal charts are shown in Figure 3, respectively.

4.2 Simulation and analysis of 12 storm surge elevations

By running the coupled tide-surge model, total water levels for each of the 12 cases were simulated. Similarly, astronomical tide levels were also calculated using the tidal model. Subtracting tide levels from total water levels allowed us to obtain a storm surge elevation time series with tide-surge coupling effects. Table 2 lists extreme values of the 12 storm surge elevations at 10 tidal stations during Typhoon 7203. Table 3 lists the maximum differences between the 12 extreme values for each tidal station.

As can be seen from Table 3, the maximum difference between the 12 extreme storm surge elevation values, of up

Table 1Absolute mean differences in amplitude and phase-lag of seasurface elevation between simulated results and observations at T/P pointsfor the four principal constituents M2, S2, K1, and O1

Tides	Amplitude (cm)	Phase-lag
M2	3.2	4.6°
S2	3.3	4.0°
K1	3.7	4.5°
01	3.6	4.4°



Figure 2 Dots denote the position of T/P observation points.

Exp —		Tidal stations									
	DL	YK	HLD	QHD	LK	YT	RS	QD	SJS	LYG	
E1	101	168	158	163	119	130	-91	-97	-123	-147	
E2	103	158	161	156	115	126	-94	-98	-125	-149	
E3	101	139	154	142	116	131	-82	-93	-115	-127	
E4	101	121	135	148	118	130	-78	-90	-110	-120	
E5	94	117	122	150	109	129	-80	-92	-124	-147	
E6	93	133	133	146	114	125	-84	-104	-128	-152	
E7	97	162	148	145	115	123	-87	-96	-122	-145	
E8	105	175	161	159	114	126	-93	-98	-118	-130	
E9	103	171	170	162	119	132	-83	-87	-104	-111	
E10	100	155	170	150	118	130	-73	-87	-103	-113	
E11	103	137	150	161	109	127	-77	-95	-124	-143	
E12	99	145	142	170	109	128	-79	-107	-128	-151	

 Table 2
 Extreme values (cm) of 12 storm surge elevations at 10 tidal stations during Typhoon 7203 ^{a)}

a) Acronyms DL, YK, HLD, QHD, LK, YT, RS, QD, SJS, and LYG refer to the 10 tidal station (Dalian, Yingkou, Huludao, Qinhuangdao, Longkou, Yantai, Rushan, Qingdao, Shijiusuo, and Lianyungang).



Figure 3 Model-produced cotidal charts for M2, S2, K1 and O1 constituents. Phase-lag (in deg); amplitude (in m) in [0.1, 3.0] m, with an interval of 0.2 m for the M2 constituent, 0.1 m for S2 constituent and 0.05 m for K1 and O1 constituents.

to 58 cm, was observed at Yingkou tidal station. Maximum differences for rising water were largest at Yingkou and Huludao, and at Shijiusuo and Lianyungang for falling water. Figure 4 shows extreme values of the 12 storm surge elevations at these four selected tidal stations, based on numerical simulation results.

In order to better understand the influences of tide-surge

interactions on storm surge elevations, Figure 5 shows storm surge elevations with tide-surge coupling effects at four selected tidal stations. It can be noted that interactions between astronomical tides and storm surges at different landing times can lead to differences in storm surge elevations. The differences between the 12 storm surge elevations at each tidal station are very apparent, demonstrating

Table 3	Maximum differences	(cm)	between 1	12 extreme	values at	10 tidal	stations du	ring T	yphoon	7203 ^{a)}
		· /						<u> </u>	~ .	

Tidal stations	DL	YK	HLD	QHD	LK	YT	RS	QD	SJS	LYG
Maximum difference	12	58	48	28	10	9	21	20	25	41

a) Acronyms DL, YK, HLD, QHD, LK, YT, RS, QD, SJS, and LYG refer to the 10 tidal stations (DaLian, Yingkou, Huludao, Qinhuangdao, Longkou, Yantai, Rushan, Qingdao, Shijiusuo, and Lianyungang).



Figure 4 Extreme values (cm) of 12 storm surge elevations at Yingkou tidal station (a), Huludao tidal station (b), shijiusuo tidal station (c) and Lianyungang tidal station (d).



Figure 5 Storm surge elevations for the 12 cases at Yingkou tidal station (a), Huludao tidal station (b), shijiusuo tidal station (c) and Lianyungang tidal station (d).

the effects of tide-surge interactions, which must be considered in the prediction of storm surge elevations.

5. Conclusions

A coupled tide-surge model was developed in this study and applied to the Bohai Sea, Yellow Sea, and East China Sea. The model had a resolution of 1/12th of a degree. Storm surges and astronomical tides were simultaneously included in the numerical model. The tide was computed with open boundary conditions and tidal potential. Wind stress was provided by a synthetic wind field. Storm surge elevations, with coupled effects of tide-surge, were investigated in coastal regions.

To explore the effects of tide-surge interactions on storm surges, total water levels and tide levels for 12 cases were simulated, assuming that Typhoon 7203 arrived at 12 different times. The storm surge elevation, that is, the difference between total water level and tide level, was calculated for each tidal station. Numerical simulation results indicated that the maximum differences between the 12 extreme storm surge elevation values were 58 and 48 cm at YingKou and HuLuDao tidal stations, respectively. At ShiJiuSuo and LianYunGang tidal stations, the largest differences for falling water values were 25 and 41 cm, respectively. The impacts of tide-surge interactions must therefore be taken into account in prediction of storm surge elevations.

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