

# Robust Control for Discrete-Time T-S Fuzzy Singular Systems\*

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**Abstract** This paper deals with the robust admissibility and state feedback stabilization problems for discrete-time T-S fuzzy singular systems with norm-bounded uncertainties. By introducing a new approximation technique, the initial membership functions are conveniently expressed in piecewise-linear functions with the consideration of the approximation errors. By utilizing the piecewise-linear membership functions, the fuzzy weighting-based Lyapunov function and the use of auxiliary matrices, the admissibility of the systems is determined by examining the conditions at some sample points. The conditions can be reduced into the normal parallel distributed compensation ones by choosing special values of some slack matrices. Furthermore, the authors design the robust state feedback controller to guarantee the closed-loop system to be admissible. Two examples are provided to illustrate the advantage and effectiveness of the proposed method.

**Keywords** Admissible, discrete-time singular systems, piecewise-linear membership functions, state feedback, T-S fuzzy models.

## 1 Introduction

Most complex physical plants and industrial processes can be modeled as nonlinear systems which are difficult to analysis and synthesis<sup>[1–5]</sup>. T-S fuzzy model<sup>[1]</sup> can successfully approximate a wide class of nonlinear systems and attracts considerable attention in recent years<sup>[6–11]</sup>. The quadratic Lyapunov method is popular to obtain the stability and stabilization conditions via a set of linear matrix inequalities (LMIs)<sup>[12–17]</sup>. However, this method may lead to conservatism because a single positive definite matrix is required in the Lyapunov function

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for all rules. Scholars have made great efforts on the aspect of reducing the conservatism of the stability criteria. Recently, many results have been reported in terms of all kinds of methods. For continuous-time systems, a fuzzy Lyapunov function-based approach<sup>[18]</sup>, a fuzzy weighting-dependent approach<sup>[19]</sup>, and a fuzzy Lyapunov function combined with a line-integral function<sup>[20, 21]</sup> are used for analysis and design. Other work tries to exploit the characteristics of the membership functions. A membership function dependent method is proposed in [22]. The imperfect premise matching method<sup>[23]</sup> and piecewise-linear membership function method<sup>[24]</sup> are given and extended to the tracking control, sampled-data output feedback control for continuous systems<sup>[25–27]</sup>. For discrete-time systems, a piecewise Lyapunov function method<sup>[28]</sup>, a Kronecker-product approach<sup>[29]</sup> are given. In the fuzzy controller design, the controller shares the same membership functions so that the implementation cost is increased. The membership functions or the fuzzy controller rules are not necessarily the same, which can reduce the complexity of the control systems. However, it makes the controller design more complicated. In [23, 25, 26], the local or global information of membership functions was employed to relax the stability criteria.

The singular system is used to describe many types of complex systems, such as biological systems, robotic systems, or chemical systems<sup>[30–32]</sup>. A review of the latest literatures, more interests are concentrated on the admissibility and robust control of singular systems<sup>[33]</sup>. In [34, 35], the authors have studied the  $H_\infty$  control problems via dynamic feedback controller. The methods in [36] and [37] give the bounded real lemma to deal with the controller design. In [38], the dissipative control and filtering are studied. A sufficient and necessary condition of  $H_\infty$  control<sup>[29]</sup> is put forward for discrete-time singular systems. In [39, 40], fuzzy singular models are introduced, and the robust stability are studied. The  $H_\infty$  filter design for fuzzy discrete-time singular systems are studied in [41]. The output feedback control for nonlinear discrete-time systems is investigated in [42]. The sliding mode control<sup>[43]</sup> and finite-time control via output feedback<sup>[44]</sup> are studied recently. From this, we can find that many achievements in the research of singular fuzzy systems have been acquired. However, they are based on the quadratic Lyapunov function method and rather conservative. In addition, there are less results on discrete-time systems. This motivates us to do this work.

In this paper, the problems of admissibility and fuzzy control problems for uncertain discrete-time singular systems are investigated. The membership functions and fuzzy rules of the systems and the fuzzy controllers are not necessarily the same which is much helpful to practical application. New sufficient conditions for the admissibility of the considered systems is derived which can be expressed by LMIs, and the conditions are extended to design a fuzzy controller for the closed-loop systems. Comparing with the existing achievements, the obtained results have the following contributions.

- By introducing a new approximation technique, the initial membership functions are expressed in piecewise-linear functions. The approximation errors are reduced.
- By using the piecewise-linear membership functions, the fuzzy weighting-based Lyapunov function and the use of auxiliary matrices, the admissibility and stabilization conditions

are less conservative.

## 2 Problem Formulation and Preliminaries

Consider the following T-S fuzzy discrete-time singular system:

$$Ex(k + 1) = \sum_{i=1}^s h_i(\theta(k))(A_i + \Delta A_i(k))x(k) + B_i u(k), \tag{1}$$

where  $i \in \mathfrak{R} := \{1, 2, \dots, s\}$ ,  $s$  is the number of IF-THEN rules,  $\theta(k) = [\theta_1(k) \ \theta_2(k) \ \dots \ \theta_s(k)]$  are the premise variables.  $h_i(\theta(k))$  are the normalized membership functions. Hence, for all  $k$ ,  $h_i(\theta(k)) \geq 0$ ,  $i = 1, 2, \dots, s$ ,  $\sum_{j=1}^s h_j(\theta(k)) = 1$ .  $x(k) \in \mathbb{R}^n$  is the state vector of the system, and  $u(k) \in \mathbb{R}^p$  is the control input.

The matrix  $E$  is known. We assume that  $\text{rank}(E) = r < n$ .  $A_i$ , and  $B_i$ ,  $i = 1, 2, \dots, s$ , are known matrices.  $\Delta A_i(k)$  is the unknown matrix representing time-varying norm-bounded parameter uncertainties, and is assumed to be

$$\Delta A_i(k) = M_i F_i(k) N_i, \quad i = 1, 2, \dots, s, \tag{2}$$

where  $M_i$  and  $N_i$  are known real constant matrices and  $F_i(\cdot) : \mathbb{N} \rightarrow \mathbb{R}^{l_1 \times l_2}$  are unknown real and possibly time-varying matrices satisfying

$$F_i(k)^T F_i(k) \leq I, \quad \forall k. \tag{3}$$

The uncertainties  $\Delta A_i(k)$  is admissible if Equations (2) and (3) hold.

**Assumption 2.1** Suppose that the membership functions  $h_i(\theta(t))$  satisfies

$$|h_i(\theta(k + 1)) - h_i(\theta(k))| \leq \gamma_i, \quad i = 1, 2, \dots, s, \tag{4}$$

where  $\gamma_i \geq 0$ , and the range of  $\theta(t)$  is known.

**Remark 2.1** For the membership functions satisfies  $0 \leq h_i(\theta(t)) \leq 1$ , the condition in Assumption 2.1 is not loss of generality in real-world processes.

For the singular system:

$$Ex(k + 1) = Ax(k), \tag{5}$$

the following definition will be adopted.

**Definition 2.2** (see [45]) The pair  $(E, A)$  is said to be regular if  $\det(zE - A)$  is not identically zero. It is said to be causal if  $\deg(\det(zE - A)) = \text{rank}(E)$ . It is said to be stable if for any scalar  $\varepsilon > 0$ , there exists a scalar  $\delta(\varepsilon) > 0$  such that the solution  $x(k)$  to the system (5) satisfies  $\|x(k)\| \leq \varepsilon$  for any  $k \geq 0$ , moreover  $\lim_{k \rightarrow \infty} x(k) = 0$ .

System (5) is said to be admissible if it is regular, causal and stable.

Moreover, for the pair  $(E, \sum_{i=1}^s h_i(\theta(k))(A_i + \Delta A_i(k)))$ , appropriate invertible matrices  $G$  and  $H$  can be chosen, and we have

$$\begin{aligned} \bar{E} &:= GEH = \begin{bmatrix} I_r & 0 \\ 0 & 0 \end{bmatrix}, \\ \bar{A} &= G \sum_{i=1}^s (A_i + \Delta A_i(k))H = \begin{bmatrix} A_{11} & A_{12} \\ A_{21} & A_{22} \end{bmatrix}, \\ \bar{A}_i &= GA_iH = \begin{bmatrix} A_{i11} & A_{i12} \\ A_{i21} & A_{i22} \end{bmatrix}, \\ \Delta \bar{A}_i(k) &= G\Delta A_i(k)H, \quad \bar{M}_i = GM_i, \quad \bar{N}_i = N_iH, \end{aligned} \tag{6}$$

where  $A_{i11} \in R^{r \times r}$ . It is stated in [37] that the system (1) with  $u(k) = 0$  is admissible if and only if  $\det(A_{22}) \neq 0$  and  $A_{11} - A_{12}A_{22}^{-1}A_{21}$  is stable.

The aim of this paper is to design a  $c$ -rule state feedback controller

$$u(k) = \sum_{j=1}^c \eta_j(\bar{\theta}(k))K_j(\bar{\theta}(k))x(k), \tag{7}$$

where  $\eta_j(\bar{\theta}(k))$  is the membership function which also satisfies Assumptions 2.1–2.2.  $\bar{\theta}(k)$  is a function which can different from  $\theta(k)$ .  $K_j(\bar{\theta}(k)) \in R^{p \times n}$  are the controller gains, and  $\eta_j(\bar{\theta}(k))$  satisfies  $\eta_j(\bar{\theta}(k)) \geq 0$  and  $\sum_{j=1}^c \eta_j(\bar{\theta}(k)) = 1$ , such that the following closed-loop system

$$Ex(k+1) = \sum_{i=1}^s \sum_{j=1}^c h_i(\theta(k))\eta_j(\bar{\theta}(k))(A_i + \Delta A_i(k) + B_iK_j)x(k) \tag{8}$$

is admissible.

Next, we will give several useful lemmas to end this section.

**Lemma 2.3** (see [46]) (*Schur’s complement*) For symmetric matrix  $S = \begin{bmatrix} A & B \\ B^T & D \end{bmatrix}$ , the following inequalities are equivalent:

- i)  $S > 0$ ,
- ii)  $A > 0, D - B^T A^{-1} B > 0$ ,
- iii)  $D > 0, A - B D^{-1} B^T > 0$ .

**Lemma 2.4** Let  $M, N$ , and  $F(k)$  be real matrices of appropriate dimensions with  $F(k)^T F(k) \leq I$ . Then, we have

$$MF(k)N + N^T F(k)^T M^T \leq MUM^T + N^T U^{-1} N, \tag{9}$$

where  $U$  is an arbitrary invertible matrix.

**Lemma 2.5** (see [45]) *Let  $\Phi = \begin{bmatrix} \Phi_{11} & \Phi_{12} \\ \Phi_{21} & \Phi_{22} \end{bmatrix}$ , where  $\Phi_{11}$ ,  $\Phi_{12}$ ,  $\Phi_{21}$  and  $\Phi_{22}$  are any real matrices with appropriate dimensions such that  $\Phi_{22}$  is invertible and  $\Phi + \Phi^T < 0$ , we have*

$$\Phi_{11} + \Phi_{11}^T - \Phi_{12} \Phi_{22}^{-1} \Phi_{21} - \Phi_{21}^T \Phi_{22}^{-T} \Phi_{12}^T < 0. \tag{10}$$

**Lemma 2.6** (see [47]) *Consider the following inequality in the variable  $U$ :*

$$BUC + (BUC)^T + \Phi < 0, \tag{11}$$

which has a solution  $U$  if and only if

$$N_B \Phi N_B^T < 0 \quad \text{and} \quad N_C^T \Phi N_C < 0, \tag{12}$$

where  $N_B$  and  $N_C$  are bases of the null spaces of  $B$  and  $C$ , respectively.

### 3 Main Results

#### 3.1 Piecewise-Linear Membership Functions

Similar to the method in [24], we use the PLMF to facilitate the stability analysis. Let us consider the membership functions depending on the function of  $\theta(k)$ , as defined in Assumption 2.1, and the range of the function  $\theta(k)$  is known as  $[a, b]$ . By choosing suitable points in the range of the function  $\theta(k)$ , the membership functions  $h_i(\theta(k))$ ,  $i = 1, 2, \dots, s$  are divided into several pieces. Then, by the following optimization, the PLMF  $\bar{h}_i(\theta(k))$ ,  $i = 1, 2, \dots, s$ , can be found.

$$\begin{aligned} \min_{\{\alpha_i^{\{j\}}, \beta_i^{\{j\}}\}} & \sup_{\theta(k)} (| h_i(\theta(k)) - \bar{h}_i(\theta(k)) |) \\ \text{s.t.} & \bar{h}_i(\theta(k)) = \alpha_i^{\{j\}} \theta(k) + \beta_i^{\{j\}}, \quad \theta(k) \in [\theta^{\{j-1\}} \ \theta^{\{j\}}], \quad j = 2, 3, \dots, t, \\ & 0 \leq \bar{h}_i(\theta(k)) \leq 1, \quad \text{for all } \theta(k), \end{aligned}$$

where  $\theta^{\{j\}}$ ,  $j = 1, 2, \dots, t$  are the piecewise points of  $h_i(\theta(k))$ , and  $\alpha_i^{\{j\}} \theta(k) + \beta_i^{\{j\}}$  is the PLMF.

Nevertheless, the optimization is nonlinear and can not be solved directly. Instead, we use a practical optimal approach to obtain a solution. It contains four steps (see Figure 1 for example):

- Choosing the intersection abscissas of the endpoints of PLFM  $\theta^{\{1\}}$ ,  $\theta^{\{2\}}$ ,  $\dots$ ,  $\theta^{\{t\}}$ . The grades of membership functions are denoted as  $h_i^{\{1\}}$ ,  $h_i^{\{2\}}$ ,  $\dots$ ,  $h_i^{\{t\}}$ .
- Choosing the points on the membership functions. The inflection points, extremal points, and boundary points are normally required. Drawing the tangent lines of membership curves through the chosen points.
- Finding the endpoints of the piecewise liner membership functions in each region.
  - Calculating the intersection ordinates of tangent lines  $h_i^{\{j\}'}$ ,  $h_i^{\{j\}''}$  associated with each intersection abscissas of the endpoints.

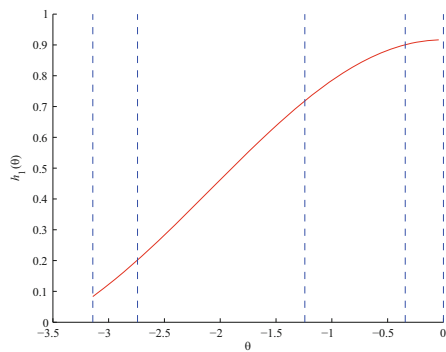
– By  $\bar{h}_i^{\{j\}'} = (h_i^{\{j\}} + (h_i^{\{j\}'} + h_i^{\{j\}''})/2)/2$ , and  $\bar{h}_i^{\{j\}} = \frac{\bar{h}_i^{\{j\}'}}{\sum_{i=1}^s \bar{h}_i^{\{j\}'}}$ , the endpoints are obtained as  $(\theta^{\{j\}}, \bar{h}_i^{\{j\}})$ ,  $j = 1, 2, \dots, t$ .

- Connecting the endpoints in a piecewise line.

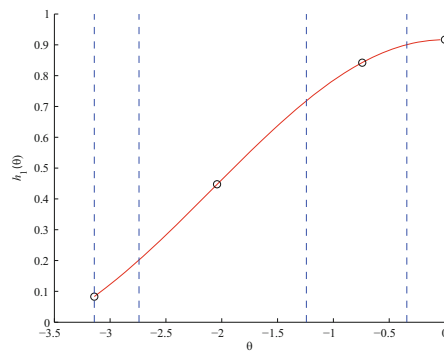
The PLMFs can be extended to approximate higher dimensional membership functions  $h\eta_{ij}(\theta(k), \bar{\theta}(k)) = h_i(\theta(k))\eta_j(\bar{\theta}(k))$ . The PLFM is defined as

$$\bar{h}\eta_{ij}(\theta(k), \bar{\theta}(k)) = \sum_{l=1}^2 \sum_{\iota=1}^2 v_\iota(\theta(k))v_\iota(\bar{\theta}(k))\bar{h}_i^{\{l\}}\bar{\eta}_j^{\{\iota\}}, \tag{13}$$

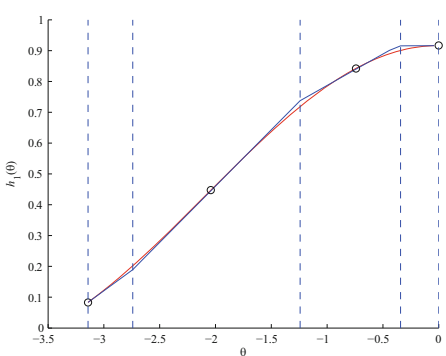
where  $\sum_{\iota=1}^2 v_\iota(\bar{\theta}(k)) = 1$ ,  $v_1(\bar{\theta}(k)) = \frac{\bar{\theta}_{\max} - \bar{\theta}(k)}{\bar{\theta}_{\max} - \bar{\theta}_{\min}}$ , and  $v_2(\bar{\theta}(k)) = 1 - v_1(\bar{\theta}(k))$ . Outside this range, both  $v_1$  and  $v_2$  have to be set to 0.  $\bar{\theta}_{\max}$  and  $\bar{\theta}_{\min}$  denote the minimum and maximum values of  $\bar{\theta}(k)$  in the corresponding region, respectively, and  $\bar{\eta}_j^{\{1\}}$  and  $\bar{\eta}_j^{\{2\}}$  are the corresponding endpoints of PLMFs of  $\eta_j(\bar{\theta}(k))$ .



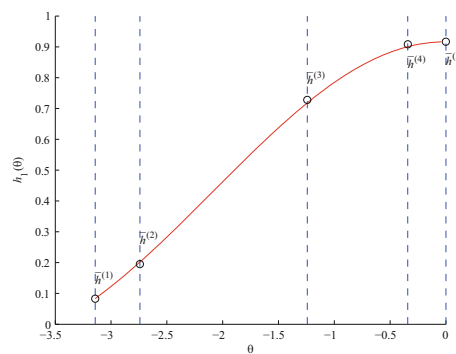
(a) Choosing the intersection abscissas of the endpoints



(b) Choosing the points



(c) Drawing the tangent lines of membership curve

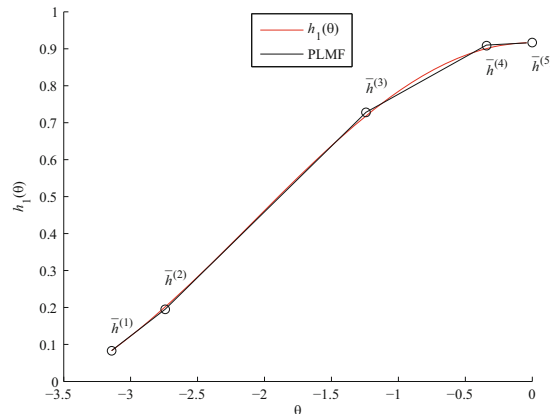


(d) Finding the endpoints of PLFM

**Figure 1** The steps to find a PLFM  $\bar{h}(f)$

**Remark 3.1** The PLMF method is effective to deal with the membership functions which are deterministic, and satisfy Assumption 2.1. Otherwise, the above method is inapplicable.

**Remark 3.2** The PLMF obtained by the the practical optimal approach is more close to the real membership function than the method in [24]. Take the case of the function in Figures 1–2, the maximum value of  $|h(\theta(k)) - \bar{h}(\theta(k))|$  is 0.0132 by using the practical optimal approach. If we adopt the method in [24], the maximum value is 0.0227.



**Figure 2** Membership function of  $h(f)$  and PLFM  $\bar{h}(f)$

By the PLMF in (13), and noted that

$$\sum_{i=1}^s \sum_{j=1}^c (h_i(\theta(k))\eta_j(\bar{\theta}(k)) - \bar{h}\eta_{ij}(\theta(k), \bar{\theta}(k)))T = 0 \tag{14}$$

holds for any symmetric matrix  $T$ . The condition

$$x^T \Omega x = x^T \sum_{i=1}^s \sum_{j=1}^c h_i(\theta(k))\eta_j(\bar{\theta}(k))\Omega_{ij} x < 0 \tag{15}$$

can be transformed as follows.

$$\begin{aligned} & x^T \sum_{i=1}^s \sum_{j=1}^c h_i(\theta(k))\eta_j(\bar{\theta}(k))\Omega_{ij} x \\ &= x^T \sum_{i=1}^s \sum_{j=1}^c (\bar{h}\eta_{ij}(\theta(k), \bar{\theta}(k))\Omega_{ij} + (h_i(\theta(k))\eta_j(\bar{\theta}(k)) - \bar{h}\eta_{ij}(\theta(k), \bar{\theta}(k)))(\Omega_{ij} + T) \\ & \quad + (\delta_{ij} - \delta_{ij})(\Omega_{ij} + T)) x \\ &= x^T \Theta x + x^T \sum_{i=1}^s \sum_{j=1}^c (h_i(\theta(k))\eta_j(\bar{\theta}(k)) - \bar{h}\eta_{ij}(\theta(k), \bar{\theta}(k)) - \delta_{ij})(\Omega_{ij} + T)x, \end{aligned}$$

where  $\Theta = \sum_{i=1}^s \sum_{j=1}^c (\bar{h}\eta_{ij}(\theta(k), \bar{\theta}(k)) + \delta_{ij})\Omega_{ij} + \delta_{ij}T = \sum_{l=1}^2 \sum_{l=1}^2 \nu_l(\theta(k))v_l(\bar{\theta}(k))\Phi_{ll}$ , and  $\Phi_{ll} = \sum_{i=1}^s \sum_{j=1}^c (\bar{h}_i^{\{l\}}\bar{\eta}_j^{\{l\}} + \delta_{ij})\Omega_{ij} + \delta_{ij}T$ . Thus, we have the following lemma.

**Lemma 3.3** *The inequality (15) holds, if there exists symmetric matrix  $T$ , such that*

$$\begin{aligned} &\Omega_{ij} + T < 0, \\ &\sum_{i=1}^s \sum_{j=1}^c (\bar{h}_i^{\{l\}} \bar{\eta}_j^{\{l\}} + \delta_{ij}) \Omega_{ij} + \delta_{ij} T < 0, \\ &h_i(\theta(k)) \eta_j(\bar{\theta}(k)) - \bar{h}_{i,j}(\theta(k), \bar{\theta}(k)) - \delta_{ij} > 0, \text{ for all } l, \iota. \end{aligned} \tag{16}$$

**3.2 Admissibility and Stabilization**

In this subsection, a new admissibility condition for the system (1) with  $u(k) = 0$  is derived and the controller synthesis is addressed. For simplicity, in the rest of this section, we will consider the equivalent transformation of the system (1) and the closed-loop system (8) as

$$\bar{E}\bar{x}(k+1) = \sum_{i=1}^s h_i(\theta(k)) (\bar{A}_i + \Delta\bar{A}_i(k)) \bar{x}(k) + \bar{B}_i u(k) \tag{17}$$

$$= \sum_{i=1}^s \sum_{j=1}^c h_i(\theta(k)) \eta_j(\bar{\theta}(k)) (\bar{A}_i + \Delta\bar{A}_i(k) + \bar{B}_i \bar{K}_j) \bar{x}(k), \tag{18}$$

respectively, where  $\bar{x}(k) = H^{-1}x(k)$ ,  $\bar{B}_i = GB_i$ , and  $\bar{K}_j = K_jH$ . For the system (17) with  $u(k) = 0$ , the following admissible condition is proposed.

**Theorem 3.4** *System (17) with  $u(k) = 0$  under Assumption 2.1 is admissible, if there exist symmetric matrices  $P_i > 0, U_i > 0, i = 1, 2, \dots, s, T, X$ , matrices  $Q, R, S$  such that*

$$\begin{aligned} &P_i - X \geq 0, \\ &\begin{bmatrix} \Omega_i + T & * \\ \Pi_{1i} & -U_i \end{bmatrix} < 0, \quad i = 1, 2, \dots, s, \\ &\begin{bmatrix} \sum_{i=1}^s (\bar{h}_i^{\{l\}} + \delta_i) \Omega_i + \delta_i T & * \\ \Pi_2 & \Pi_3 \end{bmatrix} < 0, \quad \text{for all } l \end{aligned} \tag{19}$$

hold, where  $h_i(\theta(k)) - \bar{h}_i(\theta(k)) - \delta_i \geq 0$ , and

$$\begin{aligned} \Omega_i &= \begin{bmatrix} -\frac{1}{2}Q - \frac{1}{2}Q^T & * & * \\ A_i^T [Q \ R]^T & \Pi_{22i} & * \\ P_i - \frac{1}{2}Q - Q^T + \sum_{j=1}^s \gamma_j (P_j - X) [Q \ R] A_i - Q - Q^T \end{bmatrix}, \\ \Pi_{22i} &= A_i^T \begin{bmatrix} 0 & 0 \\ 0 & S \end{bmatrix}^T + \begin{bmatrix} 0 & 0 \\ 0 & S \end{bmatrix} A_i - \begin{bmatrix} P_i & 0 \\ 0 & 0 \end{bmatrix} + N_i^T U_i N_i, \\ \Pi_{1i} &= \left( [Q \ R] M_i \right)^T \left( \begin{bmatrix} 0 & 0 \\ 0 & S \end{bmatrix} M_i \right)^T \left( [Q \ R] M_i \right)^T, \\ \Pi_2 &= [(\bar{h}_1^{\{l\}} + \delta_1) \Pi_{11}^T, (\bar{h}_2^{\{l\}} + \delta_2) \Pi_{12}^T, \dots, (\bar{h}_s^{\{l\}} + \delta_s) \Pi_{1s}^T]^T, \quad \Pi_3 = -\text{diag}\{U_1, U_2, \dots, U_s\}. \end{aligned}$$



*Proof* By Lemma 2.4 and Equations (2)–(3), we obtain

$$\begin{aligned} & \begin{bmatrix} 0 \\ \Delta A_i(k)^T \\ 0 \end{bmatrix} \begin{bmatrix} [Q \ R]^T \begin{bmatrix} 0 \ 0 \\ 0 \ S \end{bmatrix}^T \\ [Q \ R]^T \end{bmatrix} + \begin{bmatrix} [Q \ R] \\ \begin{bmatrix} 0 \ 0 \\ 0 \ S \end{bmatrix} \\ [Q \ R] \end{bmatrix} \begin{bmatrix} 0 \ \Delta A_i(k) \ 0 \end{bmatrix} \\ & \leq \begin{bmatrix} 0 \\ N_i^T \\ 0 \end{bmatrix} U_i [0 \ N_i \ 0] + \begin{bmatrix} [Q \ R] \\ \begin{bmatrix} 0 \ 0 \\ 0 \ S \end{bmatrix} \\ [Q \ R] \end{bmatrix} M_i U_i^{-1} M_i^T \begin{bmatrix} [Q \ R]^T \begin{bmatrix} 0 \ 0 \\ 0 \ S \end{bmatrix}^T \\ [Q \ R]^T \end{bmatrix}, \end{aligned} \tag{20}$$

where  $U_i > 0$ . By (20) and Schur’s complement, (19) gives

$$\begin{aligned} & P_i - X \geq 0, \\ & \bar{\Omega}_i + \bar{T} < 0, \quad i = 1, 2, \dots, s, \\ & \sum_{l=1}^s (\bar{h}_i^{(l)} + \delta_i) \bar{\Omega}_i + \delta_i \bar{T} < 0, \quad \text{for all } l, \end{aligned} \tag{21}$$

where

$$\begin{aligned} \bar{\Omega}_i &= \begin{bmatrix} -\frac{1}{2}Q - \frac{1}{2}Q^T & * & * \\ (A_i + \Delta A_i(k))^T [Q \ R]^T & \bar{\Pi}_{22i} & * \\ P_i - \frac{1}{2}Q - Q^T + \sum_{j=1}^s \gamma_j (P_j - X) \begin{bmatrix} Q \ R \end{bmatrix} (A_i + \Delta A_i(k)) - Q - Q^T \end{bmatrix}, \\ \bar{\Pi}_{22i} &= (A_i + \Delta A_i(k))^T \begin{bmatrix} 0 \ 0 \\ 0 \ S \end{bmatrix}^T + \begin{bmatrix} 0 \ 0 \\ 0 \ S \end{bmatrix} (A_i + \Delta A_i(k)) - \begin{bmatrix} P_i \ 0 \\ 0 \ 0 \end{bmatrix}. \end{aligned}$$

By Lemma 3.3 and the condition (21), we have

$$\sum_{i=1}^s h_i(\theta(k)) \bar{\Omega}_i := \bar{\Omega} < 0, \tag{22}$$

where

$$\begin{aligned} \bar{\Omega} &= \begin{bmatrix} -\frac{1}{2}Q - \frac{1}{2}Q^T & * & * \\ \bar{A}^T [Q \ R]^T & \bar{\Pi}_{22} & * \\ \bar{P}_k - \frac{1}{2}Q - Q^T \begin{bmatrix} Q \ R \end{bmatrix} \bar{A} - Q - Q^T \end{bmatrix}, \\ \bar{P}_k &= P_k + \sum_{j=1}^s \gamma_j (P_j - X), \quad \bar{\Pi}_{22} = \bar{A}^T \begin{bmatrix} 0 \ 0 \\ 0 \ S \end{bmatrix}^T + \begin{bmatrix} 0 \ 0 \\ 0 \ S \end{bmatrix} \bar{A} - \begin{bmatrix} P_k \ 0 \\ 0 \ 0 \end{bmatrix}, \end{aligned}$$

$\bar{A}$  is defined in (6), and  $\mathbf{P}_k = \sum_{i=1}^s h_i(\theta(k))P_i$ .

Next, we will decompose (22) by (6) and obtain

$$\tilde{\Omega} < 0, \quad (23)$$

where

$$\tilde{\Omega} = \begin{bmatrix} -\frac{1}{2}Q - \frac{1}{2}Q^T & * & * & * \\ A_{11}^T Q^T + A_{21}^T R^T & -\mathbf{P}_k & A_{21}^T S^T & * \\ A_{12}^T Q^T + A_{22}^T R^T & SA_{21} & A_{22}^T S^T + SA_{22} & * \\ \bar{\mathbf{P}}_k - \frac{1}{2}Q - Q^T & QA_{11} + RA_{21} & QA_{12} + RA_{22} & -Q - Q^T \end{bmatrix}.$$

Left and right-multiplying (23) by  $\begin{bmatrix} I_r & & & \\ & I_r & & \\ & & I_r & \\ & & & I_{n-r} \end{bmatrix}$  and its transpose, we obtain that

$$W + W^T < 0, \quad (24)$$

where

$$W = \begin{bmatrix} -\frac{1}{2}Q & 0 & 0 & 0 \\ A_{11}^T Q^T + A_{21}^T R^T - \frac{1}{2}\mathbf{P}_k & A_{11}^T Q^T + A_{21}^T R^T & A_{21}^T S^T & \\ \bar{\mathbf{P}}_k - \frac{1}{2}Q - Q^T & 0 & -Q & 0 \\ A_{12}^T Q^T + A_{22}^T R^T & 0 & A_{12}^T Q^T + A_{22}^T R^T & A_{22}^T S^T \end{bmatrix},$$

which implies that  $A_{22}^T S^T + SA_{22} < 0$ . Therefore, the system (17) with  $u(k) = 0$  is regular, and causal.

Applying Lemma 2.5 to (24), we obtain that

$$\begin{bmatrix} -\frac{1}{2}Q - \frac{1}{2}Q^T & * & * \\ \hat{A}^T Q^T & -\mathbf{P}_k & * \\ \bar{\mathbf{P}}_k - \frac{1}{2}Q - Q^T & Q\hat{A} & -Q - Q^T \end{bmatrix} < 0, \quad (25)$$

where  $\hat{A} = A_{11} - A_{12}A_{22}^{-1}A_{21}$ . Noted that Equation (25) can be rewritten as

$$\Xi + \xi^T Q^T \psi + \psi^T Q \xi < 0, \quad (26)$$

where  $\Xi = \begin{bmatrix} & & \bar{\mathbf{P}}_k \\ \bar{\mathbf{P}}_k & -\mathbf{P}_k & \end{bmatrix}$ ,  $\psi = [I_r \ 0 \ I_r]^T$ , and  $\xi = [-\frac{1}{2}I_r \ \hat{A} \ -I_r]$ . By Lemma 2.6, (26) is equivalent to

$$\Upsilon \psi^T \Xi \Upsilon \psi \quad \text{and} \quad \Upsilon_\xi^T \Xi \Upsilon_\xi < 0, \quad (27)$$

where

$$\Upsilon \psi = \begin{bmatrix} 0 & -I_r \\ I_r & 0 \\ 0 & I_r \end{bmatrix}, \quad \Upsilon_\xi = \begin{bmatrix} I_r & 0 \\ 0 & I_r \\ -\frac{1}{2}I_r & \hat{A} \end{bmatrix},$$

which can be rewritten as

$$\begin{bmatrix} -\mathbf{P}_k & \\ & -2\overline{\mathbf{P}}_k \end{bmatrix} < 0, \quad \begin{bmatrix} -\overline{\mathbf{P}}_k & \overline{\mathbf{P}}_k \widehat{\mathbf{A}}^T \\ \widehat{\mathbf{A}} \overline{\mathbf{P}}_k & -\mathbf{P}_k \end{bmatrix} < 0. \tag{28}$$

By Schur’s complement, (28) is equivalent to

$$\widehat{\mathbf{A}}^T \left( \mathbf{P}_k + \sum_{j=1}^s \gamma_j (\mathbf{P}_j - X) \right) \widehat{\mathbf{A}} - \mathbf{P}_k < 0, \tag{29}$$

where  $\mathbf{P}_k > 0$ , and  $\mathbf{P}_k + \sum_{j=1}^s \gamma_j (\mathbf{P}_j - X) > 0$ . Now by Assumption 2.1, and noted that  $\sum_{j=1}^s (h_j(\theta(k+1)) - h_j(\theta(k)))X = 0$ , we obtain that

$$\begin{aligned} \mathbf{P}_{k+1} &:= \sum_{i=1}^s h_i(\theta(k+1))P_i \\ &= \sum_{i=1}^s h_i(\theta(k))P_i + \sum_{j=1}^s (h_j(\theta(k+1)) - h_j(\theta(k)))P_j \\ &\leq \mathbf{P}_k + \sum_{j=1}^s \gamma_j (\mathbf{P}_j - X) \\ &= \overline{\mathbf{P}}_k, \end{aligned} \tag{30}$$

where  $P_j - X > 0$ , for  $j = 1, 2, \dots, s$ . Thus, (29) implies that

$$\widehat{\mathbf{A}}^T \mathbf{P}_{k+1} \widehat{\mathbf{A}} - \mathbf{P}_k < 0, \tag{31}$$

which ensures the stability of the system. Taken together, the conditions in Theorem 3.4 can guarantee the admissibility of the system (17) with  $u(k) = 0$ . ■

**Remark 3.5** The PFMB system, with the membership functions satisfying  $h_i(\theta(k)) - \overline{h}_i(\theta(k)) - \delta_i \geq 0$  for all  $i$ , is guaranteed to be admissible. It is easy to see that the value of  $\delta_i$  is greatly related to the value of  $\max_{\theta(k)} |h_i(\theta(k)) - \overline{h}_i(\theta(k))|$ . By the practical optimal approach, the value of  $\max_{\theta(k)} |h_i(\theta(k)) - \overline{h}_i(\theta(k))|$  can be effectively reduced. Thus, larger values of  $\delta_i$  can be obtained by the practical optimal approach which can reduce the conservatism of the conditions.

**Remark 3.6** For the conditions (19) in Theorem 3.4, the admissible condition  $\sum_{i=1}^s h_i(\theta(k)) \overline{\Omega}_i < 0$  can be achieved if it satisfied for all values of PLMFs in sample points. Therefore, an infinite number of LMIs can be solved by the finite ones with the PLMFs. Furthermore, If  $T = 0$  in Theorem 3.4, the conditions reduce to the common PDC cases as in the following corollarys.

**Corollary 3.7** *The discrete-time T-S fuzzy singular system (17) with  $u(k) = 0$  under Assumption 2.1 is admissible, if there exist symmetric matrices  $P_i > 0, U_i > 0, i = 1, 2, \dots, s$ ,*

$X$ , matrices  $Q, R, S$ , such that

$$\begin{aligned}
 &P_i - X \geq 0, \\
 &\begin{bmatrix} \Omega_i & * \\ \Pi_{1i} & -U_i \end{bmatrix} < 0, \quad i = 1, 2, \dots, s
 \end{aligned} \tag{32}$$

hold, where  $\Omega_i$ , and  $\Pi_{1i}$  are defined in Theorem 3.4.

**Corollary 3.8** System (17) with  $u(k) = 0$  under Assumption 2.1 is admissible, if there exist symmetric matrices  $P > 0, U_i > 0, i = 1, 2, \dots, s$ , matrices  $Q, X$ , matrices  $R, S$ , such that

$$\begin{bmatrix} \tilde{\Omega}_i & * \\ \tilde{\Pi}_{1i} & -U_i \end{bmatrix} < 0, \quad i = 1, 2, \dots, s \tag{33}$$

hold, where

$$\begin{aligned}
 \tilde{\Omega}_i &= \begin{bmatrix} -\frac{1}{2}Q - \frac{1}{2}Q^T & * & * \\ A_i^T [Q \ R]^T & \tilde{\Pi}_{22i} & * \\ P - \frac{1}{2}Q - Q^T & [Q \ R]A_i & -Q - Q^T \end{bmatrix}, \\
 \tilde{\Pi}_{22i} &= A_i^T \begin{bmatrix} 0 & 0 \\ 0 & S \end{bmatrix}^T + \begin{bmatrix} 0 & 0 \\ 0 & S \end{bmatrix} A_i - \begin{bmatrix} P & 0 \\ 0 & 0 \end{bmatrix} + N_i^T U_i N_i,
 \end{aligned}$$

$\Pi_{1i}$  is defined in Theorem 3.4.

**Remark 3.9** If  $T = 0$  in Theorem 3.4, the conditions in (19) reduce to the conditions in (32) of Corollary 3.7. Thus, Corollary 3.7 is a special case of Theorem 3.4. A fuzzy weighting-based Lyapunov function is used in Theorem 3.4 and Corollary 3.7. Its applicability relies on  $|h_i(\theta(k + 1)) - h_i(\theta(k))|$ . Thus, the conditions in Theorem 3.4 and Corollary 3.7 are less conservative than that in Corollary 3.8. This is because the LMIs in (32) reduce to (33) by setting  $P_i = P, i = 1, 2, \dots, s$ , and  $X = P$ . If the number of subsystem is set by  $s = 1$ , it reduces to the method in [37] for linear discrete-time singular systems.

Next, we will further deal with the state feedback stabilization problem for Systems (18) and the following theorem is obtained.

**Theorem 3.10** System (18) under Assumption 2.1 is admissible, if there exist matrices  $P_i > 0, U_i > 0, Y_i, Q, R, S, X, T, i = 1, 2, \dots, s$ , such that

$$\begin{aligned}
 &P_i - X \geq 0, \\
 &\begin{bmatrix} \Phi_{ij} + T & * \\ \hat{\Pi}_{1i} & -U_i \end{bmatrix} < 0, \quad i = 1, 2, \dots, s, \quad j = 1, 2, \dots, c, \\
 &\begin{bmatrix} \sum_{i=1}^s \sum_{j=1}^c (\bar{h}_i^{\{l\}} \bar{\eta}_j^{\{\iota\}} + \delta_{ij}) \Phi_{ij} + \delta_{ij} T & * \\ & \hat{\Pi}_2 & & \hat{\Pi}_3 \end{bmatrix} < 0, \\
 &\text{for all } l, \iota,
 \end{aligned} \tag{34}$$

hold, where  $h_i(\theta(k))\eta_j(\bar{\theta}(k)) - \overline{h}\eta_j(\theta(k), \bar{\theta}(k)) - \delta_{ij} \geq 0$ , and

$$\begin{aligned} \Phi_{ij} &= \begin{bmatrix} -\frac{1}{2}Q - \frac{1}{2}Q^T & * & * \\ A_i[Q \ R]^T + B_iY_j[I_r \ 0] & \widehat{\Pi}_{22ij} & * \\ P_i - \frac{1}{2}Q - Q^T + \sum_{m=1}^s \gamma_m(P_m - X) [Q \ R] A_i^T + [I_r \ 0]^T Y_j^T B_i^T - Q - Q^T \end{bmatrix}, \\ \widehat{\Pi}_{22ij} &= A_i \begin{bmatrix} 0 & 0 \\ 0 & S \end{bmatrix}^T + B_i Y_j \begin{bmatrix} 0 & 0 \\ 0 & I_{n-r} \end{bmatrix} + \begin{bmatrix} 0 & 0 \\ 0 & S \end{bmatrix} A_i^T + \begin{bmatrix} 0 & 0 \\ 0 & I_{n-r} \end{bmatrix} Y_j^T B_i^T - \begin{bmatrix} P_i & 0 \\ 0 & 0 \end{bmatrix} + M_i U_i M_i^T, \\ \widehat{\Pi}_{1i} &= \begin{bmatrix} [Q \ R]^T N_i, & \begin{bmatrix} 0 & 0 \\ 0 & S \end{bmatrix}^T N_i, [Q \ R]^T N_i \end{bmatrix}, \\ \widehat{\Pi}_2 &= \left[ \sum_{j=1}^c (\overline{h}_1^{\{l\}} \overline{\eta}_j^{\{l\}} + \delta_{1j}) \widehat{\Pi}_{11}^T, \sum_{j=1}^c (\overline{h}_2^{\{l\}} \overline{\eta}_j^{\{l\}} + \delta_{2j}) \widehat{\Pi}_{12}^T, \dots, \sum_{j=1}^c (\overline{h}_s^{\{l\}} \overline{\eta}_j^{\{l\}} + \delta_{sj}) \widehat{\Pi}_{1s}^T \right]^T, \\ \widehat{\Pi}_3 &= -\text{diag}\{U_1, U_2, \dots, U_s\}. \end{aligned}$$

If it is the case, the controller gain can be solved by  $K_i = Y_i \begin{bmatrix} Q^{-1} & -Q^{-1}RS^{-1} \\ 0 & S^{-1} \end{bmatrix}^T H^{-1}$ .

*Proof* Replacing  $A_i^T$  into  $A_i + B_i K_j$ , and letting  $Y_j = K_j \begin{bmatrix} Q & R \\ 0 & S \end{bmatrix}^T$ . Using the similar procedure as the proof in Theorem 3.4, this theorem can be proved easily. ■

### 4 Numerical Examples

**Example 4.1** Consider the system (1) with the parameters<sup>[29]</sup>

$$E = \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix}, \quad A_1 = \begin{bmatrix} 0.3 & 0.1 \\ a & 0.9 \end{bmatrix}, \quad A_2 = \begin{bmatrix} 0.9 & 0.5 \\ a & 0.5 \end{bmatrix},$$

where  $a \in (-\infty, 0]$ .

The system is stable in the region  $a \in [\alpha, 0]$  where  $\alpha (< 0)$  is the undetermined parameter. Now we will determine the minimum value  $\alpha_{\min}$  of  $\alpha$ . By Corollary 3.8, the value of  $\alpha_{\min}$  is  $-0.3773$  which is equal to the case of  $g = 0, d = 0$  or  $d = 1$ , and  $m = 1$  in [29]. Set  $\gamma_1 = \gamma_2 = 0.2$  in Corollary 3.7, the minimum value of  $\alpha$  is obtained as  $-0.7325$ , which is better than the case of  $m = 1$  in [29]. The Lyapunov matrices are

$$P_1 = \begin{bmatrix} 30.5925 & 8.5995 \\ 8.5995 & 87.8845 \end{bmatrix}, \quad P_2 = \begin{bmatrix} 43.9164 & -15.1394 \\ -15.1394 & 62.6322 \end{bmatrix}.$$

If  $\gamma_1 = \gamma_2 = 0.1$  in Corollary 3.7, we can obtain that  $\alpha_{\min} = -0.8752$ , which is better than all the cases in Table 1 of [29]. In this case, the Lyapunov matrices are

$$P_1 = \begin{bmatrix} 51.9476 & 21.3634 \\ 21.3634 & 175.1358 \end{bmatrix}, \quad P_2 = \begin{bmatrix} 72.7435 & -25.4349 \\ -25.4349 & 127.6076 \end{bmatrix}.$$

**Example 4.2** Consider the truck-trailer model<sup>[48]</sup> in this simulation.

$$\begin{aligned} x_1(k + 1) &= x_1(k) + v \cdot t/l \cdot u(k), \\ x_2(k) &= x_1(k) - x_3(k), \\ x_3(k + 1) &= x_3(k) + v \cdot t/L \cdot \sin(x_2(k)), \\ x_4(k + 1) &= x_4(k) + v \cdot t \cdot \cos(x_2(k)) \sin[\{x_3(k + 1) + x_3(k)\}/2], \\ x_5(k + 1) &= x_5(k) + v \cdot t \cdot \cos(x_2(k)) \cos[\{x_3(k + 1) + x_3(k)\}/2]. \end{aligned}$$

$l$  is the length of truck,  $L$  is the length of trailer,  $t$  is sampling time, and  $v$  is the constant speed of backing up. In this note,  $l = 2.8$  m,  $L = 5.5$  m,  $v = -1.0$  m/s, and  $t = 2.0$  s.

Let  $\theta(k) = x_3(k) + v \cdot t/2L \cdot x_2(k)$ , and assume  $-179.997^\circ < \theta(k) < 179.997^\circ$ , the membership functions are defined as follows:

$$h_1(\theta(k)) = \begin{cases} \frac{\sin(\theta(k)) + 0.1\theta(k)}{1.2\theta(k)}, & \text{if } \theta(k) \neq 0, \\ 0.9167, & \text{if } \theta(k) = 0, \end{cases}$$

$$h_2(\theta(k)) = 1 - h_1(\theta(k)).$$

The T-S fuzzy model that represents the nonlinear system is as follows:

- Plant Rule 1 : If  $\theta(k)$  is  $h_1$   
Then  $Ex(k + 1) = A_1x(k) + Bu(k)$ ,
- Plant Rule 2 : If  $\theta(k)$  is  $h_2$   
Then  $Ex(k + 1) = A_2x(k) + Bu(k)$ ,

where

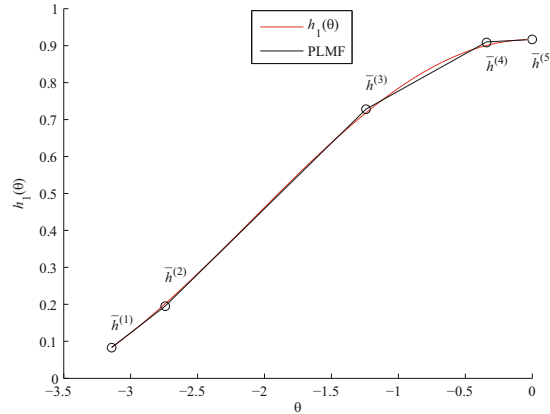
$$E = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}, \quad A_1 = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 1 & -1 & -1 & 0 \\ 0 & v \cdot t/L & 1 & 0 \\ 0 & 1.1v^2 \cdot t^2/(2L) & 1.1v \cdot t & 1 \end{bmatrix},$$

$$A_2 = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 1 & -1 & -1 & 0 \\ 0 & v \cdot t/L & 1 & 0 \\ 0 & -0.1 \cdot v^2 \cdot t^2/(2L) & -0.1 \cdot v \cdot t & 1 \end{bmatrix},$$

$B = [v \cdot t/l \ 0 \ 0 \ 0]^T$ ,  $M = [0 \ 0 \ 0.3v \cdot t/L \ 0]^T$ , and  $N = [0 \ 1 \ 0 \ 0]$ .

The methods in [29, 39, 49] is infeasible for the above fuzzy model. If the piecewise-linear membership functions are chosen as the method in [24], the controller can not be solved by Theorem 3.10. Now, we use the practical optimal approach to obtain the PLMF of the membership functions. We define the sample points as  $\theta(k) = [-180^\circ, -157.08^\circ, -71.14^\circ, -19.57^\circ, 0^\circ]$ . The

memberships at the sample points are  $h_1(\theta(k)) = [0.0833 \ 0.2017 \ 0.7185 \ 0.9006 \ 0.9164]$ , and  $\bar{h}_1(\theta(k)) = [0.0833 \ 0.1955 \ 0.7281 \ 0.9160 \ 0.9164]$ , respectively. The PLMFs are obtained in Figure 3.



**Figure 3** The PLMF of  $h_1(\theta(k))$

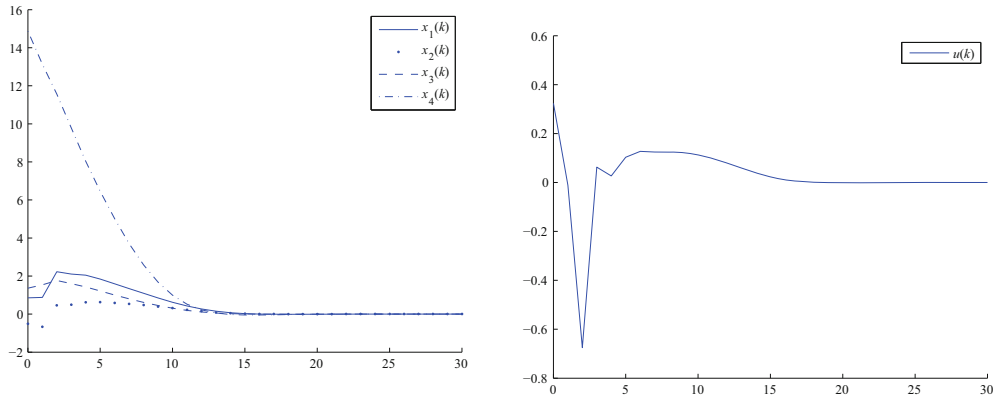
Next, we will design the robust state feedback controller of this system. The membership function of  $\eta_i(\bar{\theta}(k))$  is chosen as  $h_i(\theta(k))$ ,  $i = 1, 2$ . For  $B_1 = B_2 = B$ , the function  $\sum_{i=1}^s \sum_{j=1}^c \bar{h}_i^{\{l\}} \bar{\eta}_j^{\{l\}}$  in Theorem 3.10 reduces to  $\sum_{i=1}^2 \bar{h}_i^{\{l\}}$ , and  $\delta_{ij}$  reduces to  $\delta_i$ . It can be found numerically that  $\delta_1 = -0.0132$ , and  $\delta_2 = -0.0096$  such that  $h_i - \bar{h}_i - \delta_i > 0$ ,  $i = 1, 2$ , are satisfied. Let  $G = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \\ 0 & 1 & 0 & 0 \end{bmatrix}$ , and  $H = G^T$ . If we build the stabilization conditions by Corollaries 3.7–3.8, the conditions are fail to achieve the feasible solutions. Now, we solve the conditions in Theorem 3.10, let  $\gamma_1 = \gamma_2 = 0.1$ , and obtain the state feedback controller gains as

$$K_1 = [1.3650 \ 1.9134 \ -5.4150 \ 0.5162], \quad K_2 = [1.2765 \ 1.5975 \ -3.9488 \ 0.3424].$$

In this case, the Lyapunov matrices are

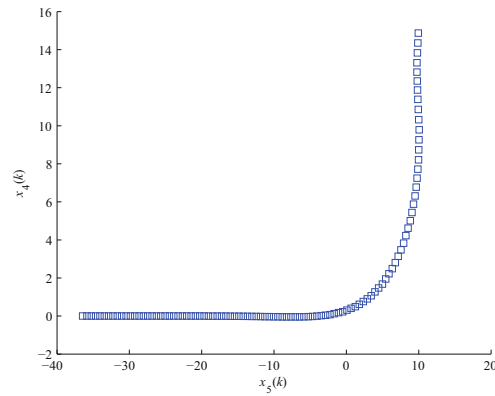
$$P_1 = \begin{bmatrix} 144.0101 & 41.1091 & 22.9274 \\ 41.1091 & 15.7136 & 23.0178 \\ 22.9274 & 23.0178 & 179.8645 \end{bmatrix}, \quad P_2 = \begin{bmatrix} 124.8407 & 37.5273 & 23.0371 \\ 37.5273 & 16.1596 & 23.0315 \\ 23.0371 & 23.0315 & 179.8653 \end{bmatrix},$$

and  $Y_1 = [106.5224 \ 19.8468 \ -0.2968 \ 46.4164]$ ,  $Y_2 = [113.2999 \ 24.6251 \ 0.0249 \ 38.7546]$ ,  $Q = \begin{bmatrix} 88.0224 & 22.8588 & 8.6930 \\ 25.6959 & 10.0781 & 13.9035 \\ 15.3471 & 15.3520 & 119.9053 \end{bmatrix}$ ,  $R = [55.2243 \ 16.8123 \ -0.0036]^T$ ,  $S = 24.2589$ . By the above controller gains, and let  $x(0) = [0.3684 \ -0.9943 \ 1.3627 \ 14.8691 \ 9.9463]^T$ , the control responses are illustrated in Figure 4. Figure 4 (a) shows the state  $x_i(k)$ ,  $i = 1, 2, 3, 4$ , of the closed-loop system, where the admissibility is achieved. Figure 4 (b) shows the input signal of  $u(k)$ , and the position of rear end of trailer is shown in Figure 4 (c).



(a) State response of the closed-loop system

(b) Input signal  $u(k)$



(c) position of rear end of trailer

**Figure 4** Control results of Example 4.2

Therefore, from Figure 4, it is obviously that the discrete T-S fuzzy singular system is admissible.

### 5 Conclusion

The admissibility and robust control problems of discrete-time T-S fuzzy singular systems are studied in this paper. In order to facilitate the analysis, we use a practical optimal approach to obtain a PLMF to approximate the membership function of the control systems. By applying the PLMFs, the fuzzy weighting-based Lyapunov function, and the use of auxiliary matrices, new sufficient conditions with less conservatism for the admissibility of the singular systems are derived. Then, the conditions are extended to check the admissibilization for the closed-loop systems. Numerical examples demonstrate the effectiveness and advantage of the proposed method. Possible research topics in the future study are to further reduce the conservatism produced in the admissible conditions, and to extend the results to nonlinear singular systems with time delay, or singular systems with input and state constraints.



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