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Simulation of polycyclic aromatic hydrocarbon remobilization in typical active regions of river system under hydrodynamic conditions

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Abstract

Purpose In an aquatic environment, hydrodynamic condition is a ubiquitous natural process, and the contaminated sediments will act as a potential pollution source once they are remobilized into the overlying water. In this study, remobilization behavior of polycyclic aromatic hydrocarbons (PAHs) under simulated hydrodynamic conditions was studied. Additionally, an adjusted prediction model with addictive consideration of surface properties was developed to exhibit the distribution of PAHs in hydrodynamic system.

Materials and methods An improved syntonic turbulencesimulation device (TSD) was used to simulate hydrodynamic conditions. Two sediments from the Yellow River Delta (YRD) and the intersection of Yangtze and Hanjiang River (YHR), respectively, were used to represent variations in organic carbon contents and sediment surface characteristics. Five PAHs including acenaphthene (Ace), fluorine (Flu), phenanthrene (Phe), fluoranthene (Fla), and pyrene (Pyr) were selected as the target compounds in this study.

Results and discussion ∑PAH concentrations in particles on volume normalization increased 74.1% and 18.5% for the YRD and YHR samples, respectively, and the same increasing trend was observed for individual PAHs. On mass weight basis, ∑PAHs were observed to decrease for both the YRD (from $2,039.5$ to 1,149.7 ngg^{-1}) and YHR (4,222.7 ngg^{-1} to 2,914.2 ngg⁻¹) samples. Interestingly, concerning the different

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heights of the TSD, the YRD-associated PAHs showed an opposite behavior comparing with the YHR-bound PAHs. Conclusions The remobilization of less contaminated, larger-size particles was found to skew the PAH concentration downward, which resulted in the opposite PAH behaviors of the YRD and YHR samples. The distribution of PAHs between solid and liquid phases was affected by both organic carbon contents and surface areas of the remobilized sediments.

Keywords Hydrodynamic conditions. Polycyclic aromatic hydrocarbons · Prediction model · Remobilization . Turbulence-simulation device

1 Introduction

Polycyclic aromatic hydrocarbons (PAHs), originated mainly from incomplete combustion of fossil fuels and biomass, are ubiquitous throughout the environment such as air, water, soil, sediments, plants, and animals (Lee et al. [2005](#page-7-0); Niu et al. [2007;](#page-7-0) Stout et al. [2004;](#page-7-0) Troisi and Borjesson [2005;](#page-7-0) Wang et al. [2010](#page-7-0)). Due to their toxic effects on organisms, some of the PAHs have been studied widely all over the world (Chen et al. [2001](#page-6-0); Kim and Weber [2005;](#page-7-0) Long and Niu [2007](#page-7-0); Niu et al. [2003](#page-7-0), [2004](#page-7-0); Niu and Yu [2004](#page-7-0); Wang et al. [2007](#page-7-0), [2009b](#page-7-0)). As one of the major sinks of PAH contamination, aquatic environmental system has received much attention for PAH investigations (Tao et al. [2003;](#page-7-0) Wang et al. [2009c\)](#page-7-0). Owing to their high hydrophobicity, PAHs have a great tendency to associate with particulate materials and finally deposit in underlying sediments (Chiou et al. [1998](#page-6-0); Tolosa et al. [2004](#page-7-0)). Consequently, sediments act as an important sink for these hydrophobic compounds (Colombo et al. [2006](#page-6-0); Urban et al. [2010\)](#page-7-0). In the aquatic

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environment, hydrodynamic condition is a ubiquitous natural process especially for the active regions of river system such as estuary areas and river intersections. Once remobilized into the overlying water under hydrodynamic conditions, the contaminated sediments will act as a potential contamination source to the water column (Feng et al. [2007b;](#page-7-0) Latimer et al. [1999;](#page-7-0) Smit et al. [2010](#page-7-0); van der Heijden and Jonker [2009\)](#page-7-0).

Investigations on the remobilization and behavior of contaminants under hydrodynamic conditions have been an issue for several years (Alkhatib and Weigand [2002](#page-6-0); de Vicente et al. [2010](#page-6-0); Hedman et al. [2009](#page-7-0); Latimer et al. [1999;](#page-7-0) Rockne et al. [2002](#page-7-0); van der Heijden and Jonker [2009](#page-7-0)). However, the contaminant changes during the remobilization process have not been clearly understood. In remobilization events, the contaminants might be sorbed to the resuspended material and removed from water column, however, they might also be released to the aqueous phase, and their availability in solution was therefore increased (de Vicente et al. [2010\)](#page-6-0). Moreover, previous studies revealed that variations of dissolved PAHs in the overlying water were not uniform on account of different sediment compositions and complicated phase changes (Latimer et al. [1999;](#page-7-0) Yang et al. [2008\)](#page-7-0). Thus, further investigations of the contaminant distribution in response to the hydrodynamic conditions are needed to provide a better understanding of their remobilization behavior.

Although the factors affecting the behavior of contaminants during remobilization events have been studied by some researchers, few prediction models for describing the contaminant distribution in hydrodynamic system have been developed. So far, organic matter normalized partition coefficient (K_{OC}) was commonly used for estimating the PAH distribution between solid and liquid phases. Wang et al. [\(2009a\)](#page-7-0) investigated the role of grain size in the remobilization of phenanthrene (Phe), and attributed the influence of grain size to the effect of organic carbon content in sediments. Accordingly, a sorption dynamic model was built based on the linear isotherm expression. Similarly, the affecting mechanism of PAH distribution between the dissolved and particulate phases is also considered to be mainly due to the linear partition into organic carbon by other researchers. Prediction models were accordingly developed, and the differences between measured and predicted values were supposed to be due to the presence of other active sorbents in sediment (Feng et al. [2007b;](#page-7-0) Latimer et al. [1999\)](#page-7-0). However, as sediment is a multi-component mixture, its sorption mechanisms cannot be distinctly determined by a single partition hypothesis (van der Heijden and Jonker [2009](#page-7-0); Wang et al. [2008](#page-7-0)). In addition, under hydrodynamic conditions, particle collisions occurring during remobilization altered the size and surface areas of the suspended solid (DePinto et al. [1994](#page-6-0)).

Thus, further work is needed to develop a regulating prediction model by giving consideration to the surface properties of remobilized sediments.

The aim of the present study was to investigate the distribution of PAHs between the solid and liquid phases in response to the turbulence energy and remobilized sediment characteristics under hydrodynamic conditions. By applying an improved syntonic turbulence-simulation device (TSD), two sediments from different active regions of river system were remobilized under two different turbulence energies. In addition, a prediction model for describing the PAH distribution in hydrodynamic system was developed from the view of hydrodynamic conditions.

2 Materials and methods

2.1 Sample collection

Two active regions of river system were chosen as sediment sample collection sites. One is located at the land–ocean interaction region of the Yellow River Delta (YRD), and the other one is at the intersection of the Yangtze River and Hanjiang River (YHR). Top 10-cm surface sediments were taken using a Van Veen stainless steel grab sampler (Eijkelamp, Netherlands). After collection, the samples were passed through a 500-μm mesh sieve to remove macrofauna. The sediments were covered with sampling water and kept at 4°C in the dark prior to tests.

2.2 Chemicals

Acenaphthene (Ace), fluorine (Flu), phenanthrene (Phe), fluoranthene (Fla), and pyrene (Pyr) were selected as the target PAHs in this study. The working standard solutions were prepared by diluting appropriate volumes of the standard mixture (PAH-Mix 9, 100 ng μL^{-1} in acetonitrile, Germany) with methanol. The background water was composed of 1-mM CaCl₂ and some of 100-mgL⁻¹ NaN₃ in order to make the aquatic environment condition close to natural freshwater. All solutions were prepared using distilled water that was passed through a MilliQ UV-plus water purification system (Millipore, Bedford, MA, USA) with a specific resistivity of 18.2 M Ω cm.

2.3 Hydrodynamic experiments

An improved syntonic turbulence-simulation device (TSD) was employed for simulating the natural aquatic environment and performing hydrodynamic experiments. The TSD was described elsewhere (Wang et al. [2009a](#page-7-0)). Briefly, the improved TSD consists of a vertical acrylic cylinder $(\Phi = 25$ cm, $h=60$ cm) and a set of oscillating vibratory

grids driven by a variable speed motor which controlled the turbulence energy. As the turbulated particles distributed relatively evenly under high turbulence energies in the TSD, weaker hydrodynamic conditions were used in this study to provide insight into the sediment properties in each layer affecting the PAH behavior. The perforated grids were driven by variable speed motor with 70 and 100 rpm, which was mentioned as low energy (L energy) and high energy (H energy), respectively.

For dynamic testing, about 20 L of background water and appropriate amount of sediments (100 g for the YHA sediment and 150 g for the YRD sediment, respectively) were added to the cylinder and kept static for 48 h. The cylinder was positioned to the TSD unit, and the perforated grid was performed with the vertical amplitude of 3.2 cm, ranging between 5.0 and 8.2 cm above the sediment surface. After a 24-h process of oscillating turbulence, 1 L of samples was collected from the top, middle, and bottom sample ports on the device, respectively. After being centrifuged at 5,000 rpm for 20 min, the sediments were air-dried, and their physicochemical characteristics were analyzed.

By using a Liquid TOC analyzer (Elementar, Germany), total organic carbon content (f_{oc}) of each sediment sample was determined. Moreover, N₂-surface area (S_A) was measured by ASAP2010 (Micromerities, America).

2.4 Analytical methods

In order to evaluate the behavior of PAHs under hydrodynamic conditions, samples of different phases were measured for quantifying the PAH content. Filtered water samples were extracted with dichloromethane. The aqueous extracts were then reduced to a volume of 1–2 mL, subject to a solvent exchange to methanol, concentrated to 1.0 mL by the rotary evaporator prior to HPLC analysis. The suspended particulate matter (SPM) samples separated by precombusted glass fiber filters (0.45 μm effective pore sizes, Beijing Shenghe Membrane Science and Technology Co., China) were freeze-dried until constant weights were maintained. SPM samples as well as sediments were mixed with 30-mL hexane/acetone mixture (1:1, v/v) and left to settle overnight. The advanced PAH quantifying analysis was as demonstrated in our previous study (Wang et al. [2008\)](#page-7-0).

2.5 Quality control

Before the onset of the extraction and analysis program, PAH standard mixture was spiked with water and solid samples for the recovery experiments. The spiked samples were extracted, purified, and analyzed in the same way as normal samples. The results of recovery for the five PAHs were more than 60%. The relative standard deviations of

the mass balance determination experiments were less than 10%. Blank experimental results displayed that the effect of both device wall sorption and PAH volatilization was less than 3.2%. Under analytical condition, detection limits for the five PAHs ranged from 0.87 to 7.12 ngL⁻¹ for water samples and from 0.34 to 3.06 ngg⁻¹ for solid samples.

3 Results and discussion

3.1 PAH sequestration correlated with sediment characteristics

3.1.1 Mass-normalized PAH sequestration

The variations of PAH concentrations in remobilized particle for YRD and YHR on mass basis are exhibited in Fig. 1. As the turbulence energy increases, ∑PAH concentrations normalized by mass weight were observed to decrease for both the YRD (from 2,039.5 to 1,149.7 ngg^{-1}) and YHR $(4,222.7 \text{ ngg}^{-1} \text{ to } 2,914.2 \text{ ngg}^{-1})$ samples. This concentration trend was also found for individual PAHs (Table [1\)](#page-3-0). This phenomenon is considered to be attributed to the turbulence of larger size sediments at higher turbulence energy. In the previous study, the median diameters of sediments under designed dynamic conditions in the simulation device were found to increase dramatically with the increase of turbulent energy, from 5.1 to 17.3 μm at different turbulence energies (Wang et al. [2009a](#page-7-0)). Accordingly, the size of particles was larger under higher turbulence energy compared with the situation under lower turbulence energy. Many studies have investigated that the grain size distribution acts as an important variable which correlated well with the quantity of PAHs (Ahrens and Depree [2004;](#page-6-0) Lee et al. [2005](#page-7-0); Wang et al. [2001](#page-7-0)). Larger size sediment fractions were often

Fig. 1 Mass loading PAHs on remobilized particles normalized to dry weight

Table 1 Average mass loading of individual PAHs on remobilized sediments under different turbulence energies $(\text{ngg}^{-1}, \text{dw})$

observed to contain relatively low PAH concentrations (Wang et al. [2009a\)](#page-7-0). The less contaminated, larger size sediment fractions are considered to skew the compound concentration downward and dilute the contaminants. The similar results have been observed for PAHs and PCBs by other researchers during resuspension events (Feng et al. [2007b](#page-7-0); Latimer et al. [1999](#page-7-0)).

The second explanation for this phenomenon was the redistribution of PAHs to water column. As the turbulence energy increased, the particle aggregation was intensified which could be implied by the result of surface area analysis for the remobilized sediments in Table 2. The loss of adsorption sites on particles results in the transfer of contaminants from particle flocs to water phase which contributes to the decreasing of contaminant on particles under higher turbulence energy (Alkhatib and Weigand [2002\)](#page-6-0).

3.1.2 Volume-normalized PAH sequestration

Total suspended solids (TSS) for each TSD run were measured and were found to increase with the increasing turbulence energy (see Table 2). As the height changed from bottom to top, TSS values were observed to decrease for both YHR and YRD samples. This phenomenon indicates that the hydrodynamic condition plays an important role in the distribution of sediment concentration in the aquatic environment.

On the basis of TSS and mass loading PAH values, volume-normalized concentrations of PAHs were calculated and observed to generally increase with the increasing of turbulent energy (Fig. [2](#page-4-0)). On average, the ∑PAH concentration increased from 456.0 ngL⁻¹ at lower turbulent energy to 793.9 ngL⁻¹ at higher energy for YRD samples. In the case of YHR solids, the corresponding ∑PAH

concentration increased from 1,164.1 to 1,378.9 ngL^{-1} . Referring to individual PAHs, the same trend was observed (see Fig. [2\)](#page-4-0). Concentrations of YRD-associated PAHs increased as much as 38.9% to 85.8%, and the YHR samples showed less increase, from 8.4% to 59.3%. These results corresponded to the variation of TSS amount under different turbulence energies for different sediments (see Table 2). YRD samples exhibited a relatively greater response to the turbulence energy, and it showed more significant TSS increase than the YHR samples. Moreover, according to the results of PAH concentration, the turbulence events were found to remobilize significant amounts of PAHs into the water column, implying that the water quality criteria could be exceeded as the result of turbulence although they may be under the safety standard in static condition. Accordingly, sediment remobilization could cause periodic exposure of aquatic organisms with PAHs and results in subsequent adverse effects. Other researchers have also noted that the turbulence condition could act as a potential pollution source to water column (Alkhatib and Castor [2000;](#page-6-0) Feng et al. [2007b](#page-7-0); Martino et al. [2002;](#page-7-0) Saulnier and Mucci [2000](#page-7-0)).

Lower-aqueous solubility (S_W) PAHs (i.e., Phe, Fla, and Pyr) were found to be dominant components on the remobilized particles under both low and high turbulent energies. Phe, Fla, and Pyr accounted for more than 80% of the ∑PAH concentration, which was supposed to be on account of the common distribution of four-ring PAH fractions in the Yellow River Delta (Yang et al. [2009](#page-7-0)) and the intersection of Yangtze and Hanjiang River (Feng et al. [2007a\)](#page-6-0). The similar phenomenon was also observed by Feng et al. ([2007b](#page-7-0)) who investigated the resuspension event for sediments from the intersection of Yangtze and Hanjiang River by using a particle entrainment simulator.

Fig. 2 The concentration profiles on a volume normalized basis for PAHs versus applied shear during the study

Comparing the PAH concentrations at different heights (top, middle, and bottom), the YRD-associated PAHs showed a decreasing trend from the top to bottom layer in the TSD. However, the PAHs combined on YHR showed an opposite trend. According to the TSS values in Table [2,](#page-3-0) it can be seen that the TSS amounts at bottom layers were higher than the top layers. Accordingly, the PAH concentrations in the particles at the bottom should be greater. For the YRD samples, the increase in the amount of TSS at the bottom layer was not so large (see Table [2](#page-3-0)). Based on the textual considerations, the YRD particles had a greater proportion of larger size sediment than the YHR (median diameter, $d_{50, YRD}$ =46.8 μm; $d_{50, YHR}$ =28.1 μm), and these particles for YRD at the bottom of TSD skewed the concentration downward, additionally, it improved the results in Section [3.1.1.](#page-2-0)

3.2 Solid–water phase relationships

The dissolved fraction of PAHs in overlying water showed a decreasing trend as the turbulence energy increased for both YRD (from 6.66 to 5.84 μ gL⁻¹ on average) and YHR (from 5.82 to 4.81 $\mu g L^{-1}$ on average) samples. With regard to individual PAHs, Ace and Flu were observed to maintain relatively constant with the increasing turbulence energy. However, relatively lower- S_W PAHs (i.e., Phe, Fla, and Pyr) presented a decreasing trend during the remobilization experiments. ∑PAHs in liquid phase is in accordance with the mass loading of ∑PAHs, as the result of dominant PAHs of Phe, Fla, and Pyr accounting for most of the PAH composition.

The apportioning of PAHs between solid and liquid phases is commonly depicted with the distribution coefficient (K_{d}) :

$$
K_{\rm d} = C_{\rm p}/C_{\rm d} \tag{1}
$$

where C_p is the PAH concentration in the particle phase, μg kg^{-1} ; C_d is the concentration in dissolved phase, $\mu g L^{-1}$. The K_d values for individual PAHs on each height of the TSD were calculated and were found to be positively related to the organic content (f_{oc}) of each particle sample ($R=0.834\sim$ 0.988). Accordingly, the K_d for PAHs in this study was

Fig. 3 Percent difference between predicted and measured K_d values for each PAH during the remobilization event

Fig. 4 The vertical distribution of ∑PAHs on suspended particles under different hydrodynamic conditions

predicted from published K_{OC} values (Karickhoff et al. [1979\)](#page-7-0) together with f_{oc} measured in remobilized particles using Eq. (2):

$$
K_{\rm d} = f_{\rm OC} K_{\rm OC} \tag{2}
$$

According to Eq. (2), the predicted $log K_d$ values for all of measured PAHs were shown in Fig. [3](#page-4-0). The f_{oc} was known to play an important role in the partition of PAHs onto particles. Accordingly, the predicted K_d values for PAHs should compare favorably with the measured coefficients. However, it appeared that for higher- S_W PAHs (i.e., Ace and Flu), the measured amount of PAH was generally greater than the predicted values, especially for the YRD samples which had less f_{oc} . This could be due to the presence of another active sorbent besides organic carbon in the solid samples (Latimer et al. [1999](#page-7-0)). The same phenomenon was also found for Ace and Flu by Feng et al. ([2007b](#page-7-0)), and the result was attributed to the sorption onto mineral surfaces which might be an additional means to elevate the K_d values. Other researchers also attributed the PAH sorption to both organic carbon partition and particle surface area adsorption (Allen-King et al. [2002](#page-6-0); Joo et al. [2008;](#page-7-0) Pignatello et al. [2006;](#page-7-0) Rockne et al. [2002;](#page-7-0) Xing et al. [1996](#page-7-0)). The correlationship between PAH concentrations and S_A for each remobilized particle sample was determined, and the results indicated a relatively high relationship coefficient $(R=0.879 \sim 0.924)$. Accordingly, a sorption model giving consideration to the surface adsorption in addition to the organic carbon partition was employed based on the two-component model developed by Joo et al. ([2008](#page-7-0)) for predicting the distribution coefficient of higher- S_W PAHs:

$$
K_{\rm d} = K_{\rm OC} f_{\rm OC} + (1 - f_{\rm OC}) S_{\rm A} K_{\rm S} \tag{3}
$$

where K_S is the surface area normalized distribution coefficient, Lm−² .

The contributions of both f_{oc} and S_A to the overall sorption of compounds were included in Eq. (3). The K_S is

calculated by using the surface area values based on N_2 adsorption. In general, all of the resulting K_S values for the nonpolar neutral organic compounds were on the order of 10^{-5} Lm⁻² (Joo et al. [2008](#page-7-0)). In this study, $K_S=10^{-5}$ Lm⁻² was used for calculating. S_A was multiplied by 10^3 to meet the unit of m^2 kg⁻¹. With the adjusted model (3), all the differences between the measured and predicted K_d values for Ace and Flu were within 40%, suggesting relatively accurate predictions.

3.3 Prediction model

Based on the current results, a prediction model was developed for describing the PAH distribution in hydrodynamic system. Linear isotherm was employed to describe the partition behavior of lower- S_W PAHs (i.e., Phe, Fla, and Pyr), and the adjusted distribution coefficient model was used to depict the sorption behavior of higher- S_W PAHs (i.e., Ace and Flu). Combining the distribution coefficient expression and the law of mass conservation, a prediction model for determining the PAH distribution in the hydrodynamic system was developed and expressed as follows:

$$
K_{\rm d} = K_{\rm OC} f_{\rm OC} + (1 - f_{\rm OC}) S_{\rm A} K_{\rm S} \quad \text{(for Ace and Flu)} \tag{4}
$$

$$
K_{i,j} = K_{\text{OC},j} f_{\text{OC}} \quad \text{(for Phe, Fla, and Pyr)} \tag{5}
$$

$$
q_{i,j} = K_{i,j} C_{e,j} \tag{6}
$$

$$
Q_i = \sum_{j=1}^{5} q_{i,j} S S_i \tag{7}
$$

Fig. 5 The distribution of ∑PAHs in three phases under different hydrodynamic conditions

$$
Q = \sum_{i=1}^{3} \sum_{j=1}^{5} K_{i,j} C_{e,j} S S_i
$$
 (8)

$$
S = N_0 - C_e V - Q \tag{9}
$$

where $K_{\text{OC}, i}$ is the K_{OC} value of *j*-individual PAH; $K_{i,i}$ is the distribution coefficient of sediment with *j*-individual PAH in *i* layer; $C_{e,i}$ stands for equilibrium aqueous-phase *j*individual PAH concentration ($\mu g L^{-1}$); $q_{i,j}$ stands for the amount of j-individual PAH sorbed per unit mass of sediment in *i* layer (μ gkg⁻¹); Q_i is the mass of ∑PAHs in suspended phase in *i* layer (μg); Q is the mass of Σ PAHs in suspended phase (μg); S is the mass of Σ PAHs in sediment phase (μg) ; *V* stands for the water volume in turbulent device (L); and N_0 is the total mass of ∑PAHs in turbulent device (μg).

Based on Eqs. [\(4,](#page-5-0) [5,](#page-5-0) [6,](#page-5-0) [7](#page-5-0), [8](#page-5-0) and 9), the PAH mass loadings in three heights under different turbulence energies were calculated, and the results were compared with the experimental data in Fig. [4.](#page-5-0) In addition, the distribution of PAHs in liquid phase, suspended particles, and sediment phase was obtained and discussed based on the concentration of PAHs in aqueous phase (Fig. [5\)](#page-5-0). The results showed that the predicted values were in good agreement with the experimental data (with the differences from 2.1% to 11.7%) in three phases under different hydrodynamic conditions. The prediction model was validated by PAH behavior acquired with two different hydrodynamic conditions and two sediment samples, and it provided information to predict the distribution of PAHs in hydrodynamic system.

4 Conclusions

Significant amounts of particulate PAHs were introduced into the water column during the remobilization process of sediments. The concentrations of PAHs generally increase with the increasing of turbulent energy, from 456.0 to 793.9 ng L^{-1} for YRD samples and from 1,164.1 to 1,378.9 ngL⁻¹ for YHR samples as the result of increasing suspended solids during the remobilization events. Comparing the PAH concentrations at different heights (top, middle, and bottom) of the TSD, the YRD-associated PAHs showed an opposite behavior to the YHR-bound PAHs due to the textual variation of the two sediments. On the basis of mass weight normalization, ∑PAHs concentrations were observed to decrease for both the YRD (from 2,039.5 to 1,149.7 ngg^{-1}) and YHR (4222.7 ngg^{-1} to 2,914.2 ngg^{-1}) samples. This is attributed to the turbulence of less contaminated, larger size sediments at higher turbulence energy, which skewed the compound concentration down-

ward and dilute the contaminants. Moreover, redistribution of PAHs to water column from the remobilized sediments might also contribute to the decrease of contaminant on particles under higher turbulence energy. The distribution of PAHs between solid and liquid phases showed that, for higher- S_W PAHs (i.e., Ace and Flu), the conventional partition model exhibited generally less amount of PAHs than the measured data, especially for the YRD samples which had less f_{oc} . Accordingly, the model with addictive consideration of surface properties was employed to better describe the sorption behavior of higher- S_W PAHs. Based on this, an adjusted prediction model for describing the distribution of PAHs between solid and liquid phases in hydrodynamic systems were developed, and the prediction values displayed satisfying accordance with experimental data.

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