



Improved reduction efficiency, cycling performance, and removal rate of hexavalent chromium by adding water-soluble salts

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Abstract

Recently, the reaction speed and cycle performance of hexavalent chromium reduction over microsized zero-valent iron (ZVI) with an Fe⁰ core and iron oxide (FeO_x) shell structure have been improved by activating the Fe⁰-core electrons through electromagnetic coupling between Fe⁰-core electrons and charges (hexavalent chromium in solution, double-charge layers of the ZVI/solution interface). Herein, the abovementioned electromagnetic coupling was greatly increased by adding salt (CH₃COONa, NaCl, NaNO₃, and Na₂SO₄) in the hexavalent chromium solution to increase the charge response. Adding salt greatly improved the reaction speed and cycle performance of hexavalent chromium reduction. It took 8 min to reduce hexavalent chromium with CH₃COONa to below the discharge standard of wastewater in the first cycle and 20 min after reducing for 20 cycles. The best apparent rate of constant value (0.416 (min)⁻¹) is nearly four times larger than those without salts. X-ray diffraction and X-ray photoelectron spectroscopy revealed the production of amorphous iron oxide shell with salt. The salt improves the hexavalent chromium reduction speed and cycle performance and impedes the Fe⁰-core-electron transfer via the produced Fe₂O₃, resulting in existence of an optimized salt dosage. This work aims to provide an effective route for enhancing the removal efficiency and cycle performance of heavy-metal-ion reduction via Fe⁰. And this work also proposes a novel viewpoint that adding salt in waste water would increase the electromagnetic coupling between the charges in solution and Fe⁰-core electrons which could finally activate the redox reaction.

Keywords Microsized zero-valent iron (Fe⁰ MZVI) · Enhanced electromagnetic coupling · Hexavalent chromium reduction · Removal efficiency · Cycle performance

Introduction

Nowadays, human activities have caused increased pollution, especially industrial pollution arising from effluents coming from industries such as leather manufacturing, metal processing, and electroplating (Chen et al. 2014; Bhaumik et al. 2012; Nguyen et al. 2021). Among the heavy metals found in industrial wastewater, chromium (VI) (hexavalent chromium) is one of the most toxic and dangerous (Banerjee et al. 2017). Hexavalent chromium is extensively used in industry with the most common sources coming from chrome plating, leather tanning and textiles (Saha et al.

2011; Saha and Orvig 2010). Hexavalent chromium exists as Cr₂O₇²⁻ in acidic conditions or CrO₄²⁻ in neutral or alkaline conditions (Liu et al. 2003; Ambika and Nambi 2016). Thus, hexavalent chromium can be very mobile in the ecological environment (Liu et al. 2003). A highly soluble metal in water, hexavalent chromium may excessively accumulate, which may eventually lead to cancer in humans (Cheung and Gu 2003; Singh et al. 2015). Thus, hexavalent chromium has been classified as a B-grade carcinogen by the U.S. Environmental Protection Agency (Chen et al. 2014). Hence, it is crucial to find a way to safely remove hexavalent chromium from the ecological environment.

Meanwhile, chromium (III) (trivalent chromium), another primary form of Cr existing in solution, is far less toxic. Moreover, it is an essential element in humans (Liu et al. 2010). Hence, a feasible way to remove hexavalent chromium species is to reduce them to trivalent chromium to lessen the toxicity and subsequently remove them from solution (Nguyen et al. 2021; Cheung and Gu 2003; Zhu et al.

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2018). Recently, zero-valent iron (Fe^0 , ZVI) has been used to reduce hexavalent chromium owing to its strong reducibility and nontoxicity (Ambika and Nambi 2016; Guo et al. 2017). However, the efficiency needs to be further improved and its cost needs to be lowered for application.

To address the abovementioned problem, in our previous work, tribocatalysis was conducted on wastewater to persistently remove hexavalent chromium by reducing it to trivalent chromium over iron turning (Fe^0) with nearly complete hexavalent chromium removal (removal rate 98%) in 80 min (He et al. 2021). Hexavalent chromium was removed by absorbing on the surface of iron turning and precipitating as Cr_2O_3 and magnetic production such as FeOOH , followed by removal with a magnet. The iron turning was micro-sized which was easy to be removed from the solution. Despite being an environmentally friendly method, the process has unsatisfactory efficiency and cycle performance for application (Liu et al. 2003; Sun et al. 2011; Dalal and Reddy 2019). The residual Fe concentration in the treated solution was only slightly lower than the government standard (0.3 mg/L) (Liu et al. 2003). Thus, the efficiency and cycle performance need to be further improved and the residual Fe concentration should be lowered more.

The employed iron turning is micro-sized zero-valent iron (MZVI) with a ZVI (Fe^0) core and an iron oxide (FeO_x) shell structure. MZVI can be recycled with magnets and also separated during stirring, which can be suitable for large-scale applications. The mechanism of improving the hexavalent chromium-reduction speed and cycle performance by MVZI in our previous work is that the mechanical energy is coupled to the electrons of iron turning by stirring the solution and disturbing the charges (including hexavalent chromium ions in solution and the double-charge layers in the iron/hexavalent chromium solution interface). The motion of charges can produce an induced electromagnetic field, which may activate the electrons in MZVI to overcome the potential barrier produced by the oxide shell more easily, yielding higher hexavalent chromium reduction efficiency and better cycle performance. Based on this mechanism, an innovative way to further enhance the induced electromagnetic field is designed to further promote the reduction speed and cycle performance while reducing the Fe concentration to a much lower level in the treated solution. The charges of ions in solution and double layers on the interface of Fe^0/FeO_x is limited, affording limit variation of the electromagnetic field by stirring. Adding ions in hexavalent chromium solution would increase the ion density and therefore enhance the variation of the electromagnetic field by stirring, and it is expected that there is more electromagnetic field coupling with the electrons in MZVI and therefore more electrons react with hexavalent chromium, yielding an enhanced hexavalent chromium-reduction efficiency.

Herein, sodium salts, namely, CH_3COONa (CNa), NaCl , NaNO_3 , and Na_2SO_4 , were chosen to provide the ions for the hexavalent chromium solution to enhance the variation of the electromagnetic field by stirring the ions in the solution. It has been found that the added sodium salts have led to vastly enhanced hexavalent chromium removal efficiency and greatly improved cycle performance and simultaneous reduction of Fe concentration in the treated solution. In all treating cases of this work, the maximum removal rate of hexavalent chromium can reach to 99.9%, at which the lowest concentration of hexavalent chromium in waste water is much less than the discharge standard required by the government. The reaction equilibrium time (denoted as t_{100}) with salt is 8 min compared to that (80 min) obtained in our previous work. The Fe concentration in the treated solution is also far below the drinking water limit. t_{100} is still 20 min at the 20th cycle.

The reactions between solid and liquid are always related to the variation of electric double layer (EDL) near the solid-liquid interface. In previous work, the effect of adding salt into the waste water is regarded as changing the EDL and the Zeta potential of the waste water—a viewpoint of electrochemistry (Zhang et al. 2019). In this work, the other effect of adding salt into the waste water has been proposed from the viewpoint of the energy conversion: EDL can assist to converse the non-chemical energy (like mechanical energy) near the solid-liquid interface into the chemical energy which could activate the redox reaction through producing electromagnetic induction by changing EDL. And it is pointed that this kind of electromagnetic induction can be increased by adding involving ions in solution, like adding salt in waste water. This is the innovativeness in this work. Also, this work provides an effective route to treat heavy-metal wastewater massively, simply, and environmentally friendly at a low cost.

Experiments

Materials

Iron turning, AR, was purchased from Tianjin Kermel Chemical Reagent Company, China. Potassium dichromate ($\text{K}_2\text{Cr}_2\text{O}_7$), (AR, Chengdu Keshi Chemical Reagent Company, China) was used to prepare the hexavalent chromium solution. Sodium acetate anhydrous (CH_3COONa , AR, Tianjin Zhiyuan Chemical Reagent Co., Ltd.), sodium chloride (NaCl , AR, Tianjin Zhiyuan Chemical Reagent Co., Ltd.), sodium nitrate (NaNO_3 , AR, Guangzhou Chemical Reagent Factory), and sodium sulfate anhydrous (Na_2SO_4 , AR, Tianjin Zhiyuan Chemical Reagent Co., Ltd.) were used as the assisted salts during experiments. Table 1 lists the various

Table 1 Different dosages of assisted salts

Designation for salts concentration	Dosage (mmol)	Salt/Cr (molar ratio)
Lv1	0.122	31.66
Lv2	0.61	158.44
Lv3	1.122	291.41
Lv4	1.8	467.53
Lv5	2.438	633.25
Lv6	3	779.22

dosages of salts used, labeled Lv1-Lv6, according to the rank of the amounts.

Characterization

X-ray diffraction (XRD, Bruker D8 Advance, Germany) using a Cu target (40 kV, 40 mA) within 2θ from 10 to 80° and X-ray photoelectron spectroscopy using a Thermo Scientific K-Alpha XPS system (XPS, Thermo Fisher Scientific, USA) were used to analyze the phases and surface elements of iron turning and sediments.

Measurement of the removal rate of hexavalent chromium with assisted salts in the dark

Removal experiments were conducted using a mechanical stirrer (JJ-1A, Changzhou Chunqiu Electronic Instrument Co. Ltd., China) at a rotation speed of 360 rpm. In order to meet higher effluent discharge standard, wastewater with

low concentration (2mg/L) is used as simulated contaminant which is more difficult to be removed. K₂Cr₂O₇ was used to prepare 2 mg/L hexavalent chromium as simulated wastewater. During the experiments, ~1 g of iron turning and various amounts of different assisted salts (Lv1-Lv6, one kind each experiment) were put into 100 mL hexavalent chromium solution and 2 mL of solution was taken out at a certain time interval to test the hexavalent chromium concentration in the rest solution using a UV-vis spectrophotometer (UV-2600 Shimadzu, Japan) via the 1,5-diphenylcarbazide colorimetric method (Velegraki et al. 2018) analyzed at 540 nm. Cr and Fe concentrations in the treated solution were measured using an inductive-coupled plasma emission spectrometer (ICP, SPECTRO ARCOS MV, Germany). The pH values were measured using a conductivity meter (DDSJ-308F, Shanghai INESA Scientific Instrument Co., Ltd.).

Results and discussion

Improved hexavalent chromium-reduction speed and cycle performance by MZVI with sodium salt

Figure 1 (a)-(d) displays the hexavalent chromium removal rates using MZVI with different amounts of CH₃COONa, NaCl, NaNO₃, and Na₂SO₄, respectively. The removal rates in all cases finally reached 99.9%, and the t₁₀₀ values varied with the added salt types and dosages, among which the shortest times were 8, 8, 8, and 7 min and the longest times were 12, 14, 14, and 14 min for CH₃COONa, NaCl, NaNO₃, and Na₂SO₄, respectively. Bioremediation is also a useful method for hexavalent chromium removal. Previous works

Fig. 1. Hexavalent chromium removal rate vs time curves. Treatment by microsized zero-valent iron (MZVI) with different dosages of (a) CH₃COONa, (b) NaCl, (c) NaNO₃, and (d) Na₂SO₄

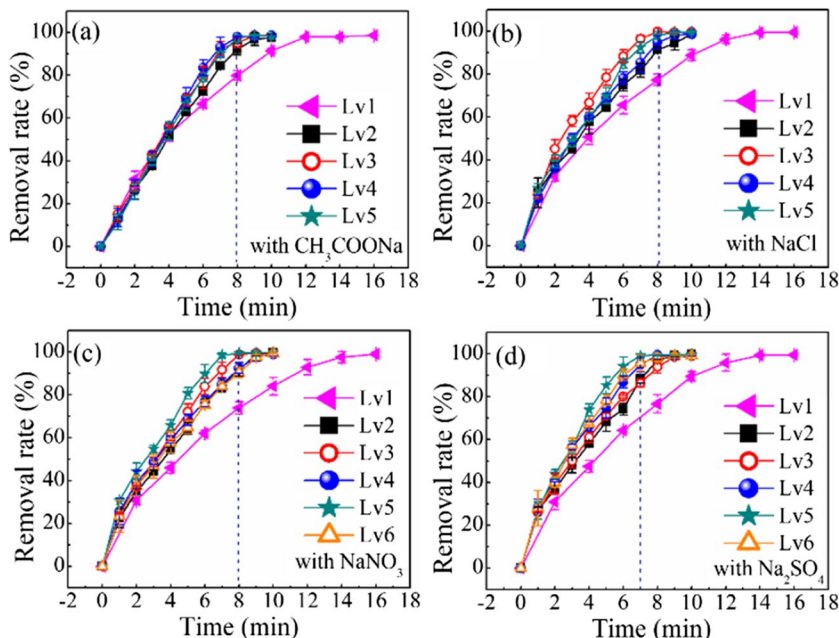


Table 2 k values fitted and calculated by pseudo-first-order model based on Fig. 1.

Designation for salts concentration	k_{CNa} (min) ⁻¹	k_{NaCl} (min) ⁻¹	k_{NaNO_3} (min) ⁻¹	$k_{\text{Na}_2\text{SO}_4}$ (min) ⁻¹
Lv1	0.198	0.191	0.164	0.171
Lv2	0.202	0.196	0.211	0.232
Lv3	0.246	0.325	0.265	0.231
Lv4	0.266	0.242	0.235	0.301
Lv5	0.213	0.244	0.322	0.416
Lv6	-	-	0.199	0.319

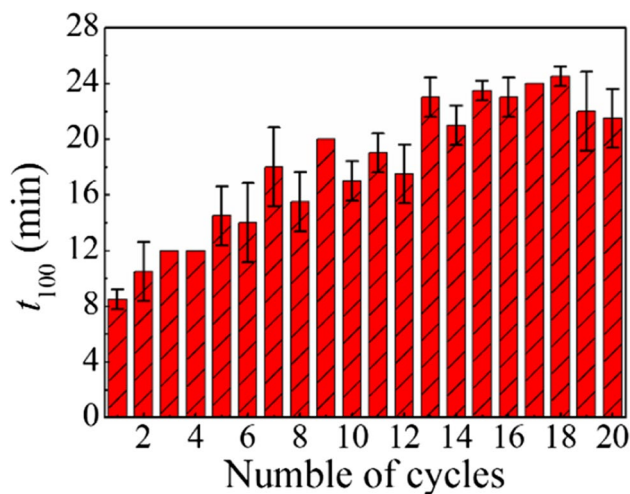
Table 3 The Cr and Fe concentration after treatment assisted by CH₃COONa.

Designation for CH ₃ COONa concentration	Cr (mg/L)	Fe (mg/L)
Lv1	0.016	0.13
Lv2	0.038	0.17
Lv3	0.012	0.08
Lv4	< 0.00130	0.094
Lv5	0.0025	0.0047
Effluent Discharge Standard	0.05	0.3

have demonstrated good performances in removing hexavalent chromium by bioremediation in high concentration (Saha et al. 2013a; Saha and Saha 2014; Saha et al. 2013b). This study aims to further process the low-concentration hexavalent-chromium waste water, i.e., the post processing hexavalent-chromium waste water, to meet the high emission standard.

Table 2 lists the k values of the removal rate–time curves. The k values were obtained through fitting and calculating according to the pseudo-first-order model (Sun et al. 2015). From Table 2, all k values were larger than 0.08 (min)⁻¹ which obtained without assisted salt reported in our previous work (He et al. 2021). In addition, the best k values of CH₃COONa, NaCl, NaNO₃, and Na₂SO₄ are 0.266 (min)⁻¹ at Lv4, 0.325 (min)⁻¹ at Lv3, 0.322 (min)⁻¹ at Lv5, and 0.416 (min)⁻¹ at Lv5, respectively. The best k (0.416 (min)⁻¹) is nearly four times larger than that without salt reported in our previous work (He et al. 2021). It can be concluded that different salts possessed different optimum dosages during the removal process. In other words, both salt type and dosage are factors that can influence the removal efficiency.

To examine if the treated wastewater meets the effluent discharge standard, the Cr and Fe concentrations in the solution after treatment assisted by CH₃COONa with Lv1 to Lv5 dosages were measured using ICP. As shown in Table 3, the Cr and Fe concentrations in the solution after treatment were far below the drinking water limit (0.05 and 0.3 mg/L, respectively) (Liu et al. 2003) and those of our previous work (0.0499 and 0.277 mg/L) (He et al. 2021) in all cases. Hence,

**Fig. 2** Cycle performance of hexavalent chromium reduction with assisted CH₃COONa at Lv4 at 25 °C

the hexavalent chromium removal rate could be regarded as 100% after the treatment in the cases mentioned. Moreover, at Lv4, the lowest hexavalent chromium concentration was obtained in the solution after treatment.

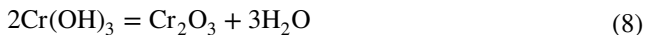
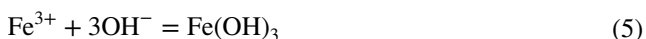
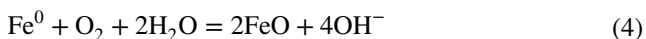
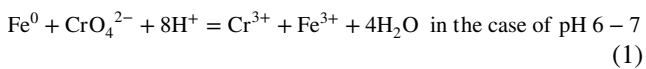
Considering the 100% removal rate of Cr and low Fe concentration in the treated solution, CH₃COONa with an Lv4 dosage was chosen in the next cycling experiments at room temperature (25°C). Figure S1(a) shows the “removal rate vs time” curves in 20 cycles in case of CH₃COONa at Lv4 dosage. The “removal rate vs time” curves in 5 circles without CH₃COONa obtained in our previous work (He et al. 2021) are also given in Fig. S1(b) as comparison. In order to clearly show the cycle performance, a column diagram presenting “ t_{100} -cycle number” relations was drawn based on Fig. S1(a) and shown in Fig. 2. Figure 2 illustrates that increasing the cycles took a longer time to thoroughly remove hexavalent chromium. However, the t_{100} -s varied with cycles with the nonmonotonic law, which can possibly be attributed to the irregular drop of compounds forming on the surface of iron turning during the treatment. Nevertheless, the t_{100} of the 20th cycle was 20 min and the longest one was 24 min at the 18th cycle, both far more quickly than those in our previous work (He et al. 2021). In summary, the

assisted salts can greatly enhance the cycle performance of hexavalent chromium reduction over MZVI.

Chemical reaction route in assisted salt

To investigate the possible chemical reaction route of hexavalent chromium reduction over MZVI with sodium salt, XRD and XPS were conducted to measure the characteristics of MZVI at every stage and sediment collected from the solution after treatment with CNa, an example of sodium salt (He et al. 2021). The phases, element, and chemical bonds of the surface on MZVI and the collected sediment are shown in Figs. S2 and S3. Analysis of the Figs. revealed that there were Fe^0 , FeO , and amorphous Fe_2O_3 on the MZVI surface after CNa treatment. Moreover, the following materials existed in the sediments after hexavalent chromium reduction with CNa based on the reducing content order: $\text{FeOOH} > \text{Fe}^0 > \text{FeO} > \text{Cr}_2\text{O}_3$. The added sodium salt triggered a corrosion reaction of MZVI, yielding more amorphous Fe_2O_3 on the MZVI surface.

From Figs. S2 and S3, the possible mechanism at pH 6–7 involved in the removal treatment is given below (Ambika and Nambi 2016; He et al. 2021).



Mechanism

As stated in the Introduction, sodium salt increases the charges involved in electromagnetic field induction by stirring. Therefore, the electromagnetic field coupling with the electrons in MZVI increases, along with the electrons participating in hexavalent chromium reduction.

Figure 3 displays the comparison of hexavalent chromium-removal rates among different cases. In the figure, the removal rates are nearly the same both in the cases that

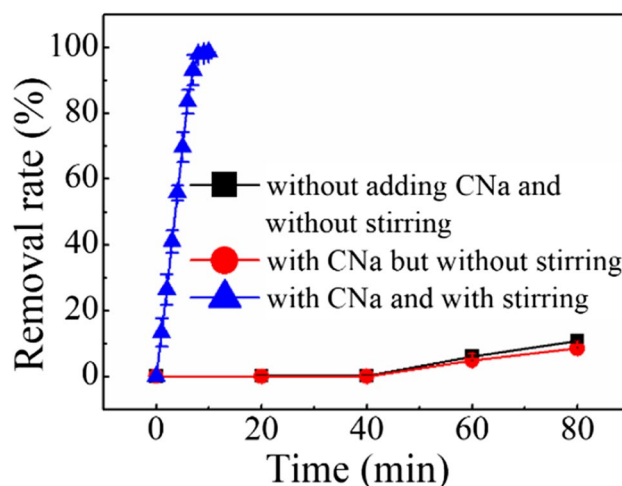


Fig. 3 Comparison of hexavalent chromium-removal rates among the cases: without adding CNa and without stirring (■), with CNa but without stirring (●), with CNa and stirring (▲)

without stirring. It means that applying no stirring has no effect on the hexavalent chromium-reduction speed with CNa, which is almost the same as that without CNa. In another word, stirring plays a significant role in the process.

Figure 4 (a) and (b) illustrate the mechanism increasing the induced electromagnetic field by adding salt in wastewater when stirring. The effect of the added salt could be contributed by cations (Fig. 4 (a)) such as Na^+ and anions (Fig. 4 (b)) such as Cl^- and NO_3^- . Figure 4 illustrates the top view of the hexavalent chromium reduction system, which includes a container holding wastewater, MZVI (schematically shown by a black square in Fig. 4), and a stir bar. Without stirring, Na^+ and anions maintain a static state and no induced electromagnetic field is produced. Hence, no effect from the added salt is observed (Fig. 3). Applying rotation, as shown in Figs. 4 (a) and (b), both cations and anions rotate along with the rotation of the solution. Suppose that the solution rotates in a clockwise manner (Fig. 4 (a)), the cations will produce a current in the direction of rotation, producing a magnetic field with a direction perpendicular to the top view plane and inward (with the symbol \times), determined using the right-hand screw rule. Under this magnetic field, an additional Lorentz force will be applied on the electrons in the MZVI core in the direction of pulling the electrons out of MZVI. The Lorentz force pushes the electrons in MZVI to go over the potential barrier near the interface of Fe^0/FeO_x to the outside of the MZVI, as shown in Fig. 5, increasing the number of electrons reacting with hexavalent chromium in the solution. These electrons will enhance the removal efficiency.

Likewise, the anions in the solution would produce a Lorentz force on the electrons in Fe^0 , pulling those electrons out of the MZVI (Fig. 4 (b)). Although the direction of the

Fig. 4. Mechanism of increasing the induced electromagnetic field with stirring the added salt: **(a)** the effect from cations; **(b)** the effect from anions. F represents the Lorentz force in MZVI, v refers to the speed of solution, \times means that the direction of the induced electromagnetic field is perpendicular to the paper plane and inward, and \bullet means that the direction of the induced electromagnetic field is perpendicular to the paper plane and outward

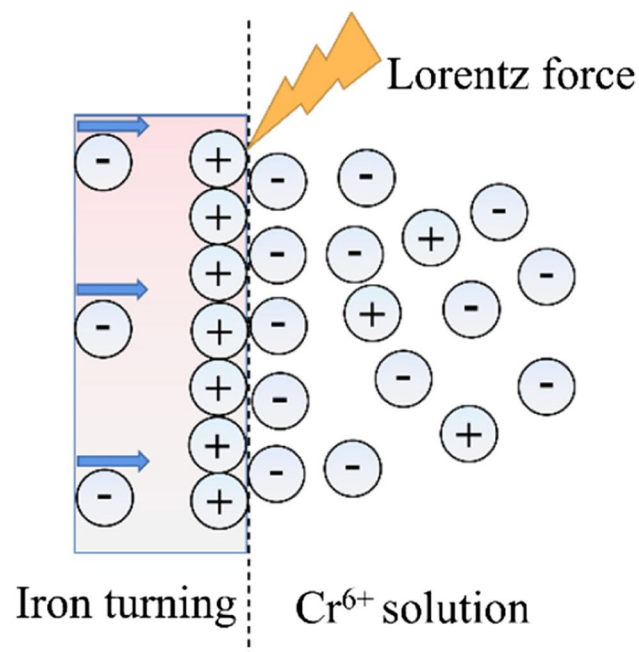
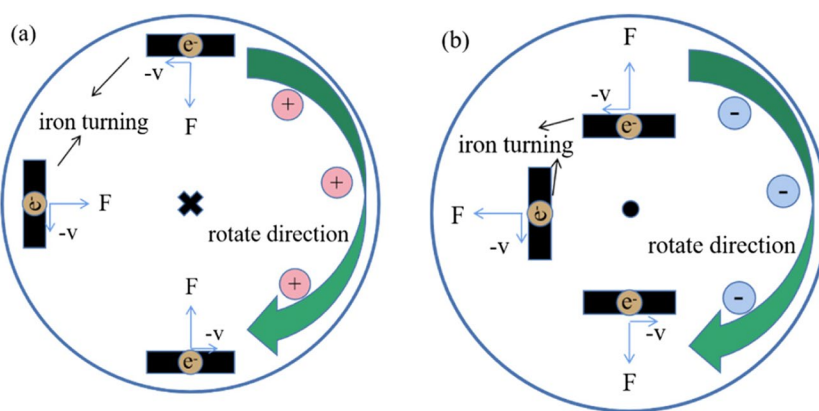


Fig. 5 The migration of electrons inside iron turning pulled by Lorentz force

Lorentz force from the rotated anions is opposite to that from the rotated cations, the ultimate effect of the Lorentz force is to pull the electrons out of MZVI, causing similar effects.

Based on double-charge layer theory, the whole removal process of hexavalent chromium may be summarized. As shown in Fig. 6, at first, hexavalent chromium in the solution may diffuse towards iron turning under the influence of rotation. Then hexavalent chromium may be physically adsorbed on the surface of iron turning. The addition of sodium salts may induce a stronger electromagnetic field generated by stirring the solution, which may attract more electrons inside iron turning to migrate to the outside, and react with hexavalent chromium. And the process of charges transfer was accelerated. Thus, the improved removal performance was achieved. Subsequently, trivalent chromium reduced from

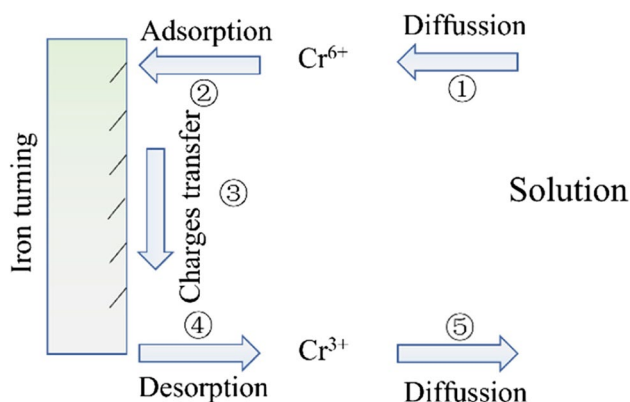


Fig. 6 The removal process of hexavalent chromium

hexavalent chromium may desorb from the surface of iron turning and be removed from solution in the form of sediments. The present of sodium salts may also accelerate the desorption of trivalent chromium, which may also improve the removal performance of hexavalent chromium.

Adding sodium salts may thinning the double-charge layer at the interface between iron turning and solution and lead to the decrease of induced electromagnetic field, which may slightly affect the hexavalent chromium reduction. However, this influence may be ignored comparing to the effects caused by the stronger electromagnetic field generated by stirring the solution.

However, the added sodium salt would induce other complicated effects. As stated in the supplementary materials (Figs. S2 and S3), the added sodium salt produced Fe_2O_3 on the MZVI surface owing to the corrosion reaction of MZVI with sodium salt, which would induce more impediment for the electron transferring from the core to the shell surface of MZVI. Meanwhile, the corrosion would change the microstructure on the MZVI surface, accelerating the collapse of the employed MZVI shell. This collapse of the employed MZVI shell benefits the electrons to expose to the hexavalent chromium solution. The synthetic effects of added

sodium salts are complicated. Thus, the improved hexavalent chromium-reduction speed cannot monotonically increase with the amount of added salt, i.e., there is an optimized amount for each salt.

Moreover, the improved hexavalent chromium-reduction efficiency and the collapse of the MZVI shell can account for improved cycle performance. The shorter time when hexavalent chromium is completely removed had led to the less Fe⁰ oxidation, therefore led to less FeO_x to deposit on the surface of MZVI. Meanwhile, the greater collapse of the MZVI shell due to corrosion is good for cycle performance.

Conclusions

This work proposed a novel mechanism to enhance the electromagnetic coupling between the electrons of the core of Fe⁰ and ions in solution by adding sodium salts, namely, CH₃COONa, NaCl, NaNO₃, and Na₂SO₄, in hexavalent chromium solution. The added salts could provide more ions in the hexavalent chromium solution, providing more electromagnetic response and consequently more electromagnetically coupling. It was found that the reaction speed and cycle performance of hexavalent chromium reduction were greatly enhanced with the added salts. The experiments found that t_{100} decreased to 8 min from 80 min and the remaining Fe in the treated solution was far below the drinking water limit compared to that from our previous work. Moreover, the best k (0.416 (min)⁻¹) was nearly four times larger than those without assisted salts in our previous work. Hexavalent chromium was 100% removed in 20 min with CNa even after 20 cycles, resulting mainly from the accelerating hexavalent chromium-reduction speed and accelerating collapse of the MZVI shell owing to the corrosion of MZVI with salt. The synthetic effects of added sodium salts have led to improved hexavalent chromium-reduction speed, which could not be monotonically increased with the amount of added salt, i.e., there was an optimized amount for each salt. This work may provide a very effective route for enhancing the reaction speed and cycle performance of heavy-metal reduction by MZVI.

This work proposes a viewpoint that adding salt in waste water would increase the electromagnetic coupling between the charges in solution and Fe⁰-core electrons which could finally activate the redox reaction. It is of great significance for treating heavy-metal wastewater and completely understanding the effect of EDL on the redox reaction at the solid-liquid interface.

Supplementary Information The online version contains supplementary material available at <https://doi.org/10.1007/s11356-023-30138-y>.

Author contributions All authors contributed to the study conception and design. Material preparation, data collection and analysis were performed by **Junfeng He**. Investigation was performed by **Yuheng Liang**. Resources was performed by **Hao Huang**. Methodology was performed by **Wangjian Zhai**. The first draft of the manuscript was written by **Junfeng He** and the edited draft of the manuscript was written by **Junfeng He** and **Qinyu He**. All authors commented on previous versions of the manuscript. All authors read and approved the final manuscript.

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Data availability All data generated or analyzed during this study are included in this published article.

Declarations

Ethical approval Not applicable.

Consent to publish Not applicable.

Consent to participate Not applicable.

Competing interests The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

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