SHORT RESEARCH AND DISCUSSION ARTICLE

Incineration disposal of organic waste bio‑residue via a deep dewatering process using refuse incineration bottom ash: moisture transfer and low calorifc value improvement

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Abstract

Bio-residue is a by-product from organic waste anaerobic digestion process with high moisture, high organic matter, low calorifc value and poor biological stability, and may be incinerated after deep dewatering. The moisture existence forms of bio-residue were clarifed frstly, fnding that adsorbed water, capillary water and bound water occupied 75.61%, 23.81% and 0.58%, respectively. Furthermore, refuse incineration bottom ash was used as a typical deep dewatering reagent, when compared with calcium oxide (CaO), refuse incineration fly ash and iron powder–potassium persulfate (Fe(0)-K₂S₂O₈). Results showed that the addition of bottom ash powder could decrease the bio-residue's moisture from 80.0% to 37.9% at the optimal dosage of 2.0%, and corresponding low calorific value reached 10.5 MJ/kg at the $10th$ d. It was suggested that $ZnCl₂$ and $ZnSO₄$ present in bottom ash powder could react with moisture in bio-residue, forming hydrates of inorganic salt and breaking the polyacrylamide colloid, and lead to the release of adsorbed water in the bio-residue.

Keywords Anaerobic digestion · Organic residue · Moisture forms · Moisture release · Incineration waste · Dewatering mechanism

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Introduction

Organic solid waste, with a huge quantity around the world, refers to solid waste contains organic components produced by human activities and may include fruit peel, rotten vegetable leaves, eggshells, rice, four, vegetable oil, animal oil, meat and bone, and so on. With the increase in the world population, the generation of organic waste, such as food and kitchen waste, garden waste, crop residue and animal manures, is increased (Singh et al. [2014](#page-12-0); Mata-Alvarez et al. [2000](#page-11-0); Tella et al. [2013](#page-12-1); Wei et al. [2021\)](#page-12-2). Around 30%-40% of municipal solid waste in China consists of organic waste, with an annual quantity of around 110 million and possibly several billion of tons globally (Zhao and Wei [2020\)](#page-12-3), which have caused a worldwide crisis (Arun and Sivashanmugam [2017](#page-11-1); Guo et al. [2021\)](#page-11-2).

The common organic waste treatment and disposal technologies include anaerobic digestion and aerobic composting. Anaerobic digestion is a highly efective technique for the disposal of agricultural residues, organic solid waste, food waste and sludge, and has been widely used as an ideal method for the waste disposal in recent years (Hu et al. [2022\)](#page-11-3). In the anaerobic digestion process, anaerobic

fermentation bacteria, hydrogen-producing acetic acid bacteria and hydrogen-consuming acetic acid bacteria are used to degrade complex organic matter into methane, carbon dioxide and other gases, achieving harmlessness and resource utilization (Yu et al. [2020](#page-12-4)). During anaerobic digestion process, biogas that is rich in methane and carbon dioxide is produced, which could be used as a fuel for combustion in transport or energy production, leaving the bio-residue for treatment further. Most organic substance in organic waste such as sugar, fat and protein has been decomposed and transferred into the biogas slurry, leaving the bio-residue with high moisture, high organic matter, low calorific value and poor biological stability that should be properly treated.

In the current technological process of organic waste anaerobic digestion plant, bio-residue is treated by polyacrylamide (PAM) for dewatering. Polyacrylamide is a water-soluble polymer and commonly used as the thickeners, viscosity modifed reagents or focculant (Li et al. [2020](#page-11-4)). Hundreds of millions of dollars per year on polyacrylamides is spent for the conditioning and dewatering of wastewater sludge. Polyacrylamide is also widely used in many industrial processes such as dewatering of sludge, treatment of wastewater and production of paper. After treated by polyacrylamide, the bio-residue will be disposed of by incineration along with municipal solid waste. However, because of the moisture holding capacity of polyacrylamide, the moisture of organic waste bio-residue can only be decreased to about 80%, which is still not suitable for incineration. Therefore, deep dewatering by certain reagents to reduce the moisture further and improve low calorifc value is necessary before incineration (Šyc et al. [2020;](#page-12-5) Chen et al. [2020;](#page-11-5) Wan et al. [2018\)](#page-12-6).

To study the deep dewatering of bio-residue, it is necessary to research its moisture types. It is generally considered that the moisture in organic waste may be categorized into four types, i.e., free water, adsorbed water or surface water, interstitial water or capillary water, and cell water or bound water, as done for sewage sludge (Tsang and Vesilind [1990](#page-12-7)), and can be measured by thermal gravity–diferential thermal analysis (TG–DTA) (Katsiris and Kouzeli-Katsiri [1987](#page-11-6); Willard et al. [1988](#page-12-8)) and thermal drying method (Smollen [1986\)](#page-12-9). Moisture content is the key factor infuencing the performance of sludge incineration, including combustion completeness, energy recovery and pollutant emission (Xiao et al. [2015](#page-12-10)). Before mechanical dehydration of municipal sludge, some pretreatments are usually used to strengthen its dehydration property. The main pretreatment methods include chemical conditioning (Mahmood and Elliott [2007](#page-11-7); Novak [2006](#page-11-8)), hydrothermal treatment (Neyens and Baeyens [2003](#page-11-9); Jomaa et al. [2003](#page-11-10)) and ultrasound treatment (Dewil et al. [2006](#page-11-11); Bien et al. [1997](#page-11-12)).

There are many reagents that can be used for deep dewatering. Calcium oxide, a conventional dewatering reagent, is usually applied into municipal sludge for strengthening the process of dehydration and raising the thermal drying efficiency. General speaking, drying the sludge with 80% moisture content by adding CaO (sludge: $CaO = 10:3$, w/w) can raise the drying rate by 20%, compared with sludge only. Persulfate is also used as oxidant for strengthening dehydration of sewage sludge. Persulfate salt is stable under the ordinary condition. However, under the condition of heating, irradiation with light and transition metal ions (Fe²⁺, Cu²⁺, Ag^+ , Mn²⁺), persulfate can be activated and produces SO₄and ·OH. Under the ordinary temperature and pH 3.0–8.5, persulfate is used to treat sludge activated by Fe^{2+} , and the dehydration performance of organic waste and sludge can be thus improved (Zhen et al. [2012\)](#page-12-11).

Bottom ash is a by-product from municipal solid waste incineration (Wiles [1995\)](#page-12-12), mainly composed of slag, black and nonferrous metals, ceramic chips, glass and other noncombustible organic matter (Zhu et al. [2020\)](#page-12-13). Although the presence of heavy metals confnes the use of bottom ash in further applications, some of it is used in applications such as road subbase material, aggregate in concrete, clay brick and pavement, but most are currently landflled (Loginova et al. [2021;](#page-11-13) Zhu et al. [2019](#page-12-14)). The incineration bottom ash of sludge was used with CPAM (cationic polyacrylamide) to dewater the sludge, and the result showed that its effect of dehydration was better than any single reagent (Ning et al. [2013](#page-11-14)). The efects of CaO, coal ash, diatomite, sodium dodecyl sulfate and municipal solid waste incineration fy ash on dehydration of sludge were compared, and it was found that the dehydration efect of CaO was the best and next were coal ash, diatomite, sodium dodecyl sulfate and municipal solid waste incineration fy ash, respectively (Zhu et al. [2012\)](#page-12-15).

The purpose of this study was to research the deep dewatering of organic waste bio-residue for the improvement of low calorifc value, which was convenient for incineration. The moisture form of bio-residue was studied by thermal drying, vacuum fltration and thermal gravity analysis. The efects of CaO, Fe(0)- $K_2S_2O_8$, bottom ash and fly ash powder on deep dewatering of bio-residue were compared, and diferent dosages of bottom ash powder's infuence on deep dewatering of bio-residue were analyzed in detail, combining with XPS analysis of bottom ash powder. Finally, the bio-residue treated with bottom ash powder was observed under the electron microscope after drying, for making the mechanism of deep dewatering clear. Meanwhile, economic analysis was given for estimating reagents' benefts.

Materials and methods

Materials

The original bio-residue is in slurry and sent to the treatment process after treated by polyacrylamide. The bio-residue used in this study, which was black and smelly, was collected from the end centrifugal dehydrator of bio-residue treatment process line in an organic waste anaerobic digestion plant in *Shanghai, China*. The characteristics of original bio-residue treated by polyacrylamide are shown in Table [1.](#page-2-0) It can be seen that the moisture content of bio-residue was about 78.4% and the organic matter content of dried bioresidue was about 42.0%, with predominant elements C and O of 20.4% and 29.5%, respectively. The low calorifc value of dried bio-residue was 13.32 MJ/kg, much higher than that required for incineration, and was increased much after drying.

The main reagents, including calcium oxide (CaO), iron powder (Fe⁰) and potassium persulfate ($K_2S_2O_8$) were purchased from Aladdin deposits in *Shanghai*, *China*. All reagents were of analytical grade and used without any pretreatment. Bottom ash and fy ash were taken from a municipal solid waste incineration plant and pretreated into powder (60–80 mesh) by the crusher.

Experimental design

Reagents comparison

The pre-experiment for bio-residue's deep dewatering was conducted in 1000-mL plastic containers, and each container contained 500 g of bio-residue. Four experiment groups with 2.0% dosage of diferent dewatering reagents were set for investigating each reagent's dewatering capacity. The bioresidue and reagents were mixed fully, and all the containers were placed in a calm place for 14 days, avoiding disturbed by wind. The treated bio-residue were sampled in two copies every other day, and one copy of the samples was dried in the oven with 101 ℃-105 ℃ until a constant weight is reached, with the weights recorded before and after drying. The other copy of the samples was used for low calorifc value test. For avoiding reagents reacting directly, the iron powder and potassium persulfate were added in order, and their proportions were based on the reaction of Eq. [\(1\)](#page-2-1):

Table 1 Characteristics of bio-residue used in this study

Item	Value		
Moisture	78.40%		
Organic matter content (dry basis)		42.03%	
Low calorific value (wet basis)	0 MJ/kg		
Low calorific value (dry basis)	13.32 MJ/kg		
Element content	N	0.00%	
	C	20.41%	
	H	2.78%	
	S	0.34%	
	∩	29.46%	

$$
\text{Fe}^{0} + 2\text{S}_{2}\text{O}_{8}^{2-} \rightarrow 2\text{SO}_{4}^{2-} + \text{Fe}^{2+} + 2\text{SO}_{4}^{2-} \tag{1}
$$

Bottom ash curing

The detailed curing experiments for bio-residue's deep dewatering by bottom ash powder were conducted on hollowing boards, which would not let the bio-residue leak through the hole. Five experiment groups were set with dosage of 1.0%, 2.0%, 3.0%, 4.0% and 5.0%, respectively. Each hollowing board loaded 100 g bio-residue, which was mixed fully with bottom ash powder, and the treated bio-residues were made into cubes (about $5 \text{ cm} \times 5 \text{ cm} \times 2 \text{ cm}$). Also, all the hollowing boards were placed above a vacant plastic container in a calm place for 14 days, avoiding disturbed by wind. The bio-residue were sampled in two copies every other day, and one copy of the samples was dried in the oven with 101 ℃-105 ℃ until reaching a constant weight, with the weights recorded before and after drying. The other copy of the samples was used for low calorifc value test.

Analytical methods

Most of the moisture content in bio-residue was measured by the oven (DHG-9240A) with 101 ℃-105 ℃. In order to obtain the contents of diferent moisture forms, three steps were conducted: i) thermal drying was used for the measurement of the whole moisture except for bound water. ii) Vacuum fltration was used for the measurement of capillary water. 100 g of bio-residue was compacted in the Büchner funnel in the form of pie. The vacuum pump (SHZ-D(III)) was connected with Büchner funnel and carried on until the vacuum degree of fltration container became zero. iii) Thermal gravity analysis was used for the measurement of bound water.

For evaluating the effect of reagents on bio-residue incineration performance, low calorifc values were tested and analyzed. In this study, 1.0 g samples was taken to the automatic calorimeter (ZDHW-6L) for measurement. In order for comparison, the low calorifc value of original bio-residue treated by polyacrylamide was also tested and analyzed during the bottom ash powder curing experiment.

Organic matter content of bio-residue was measured by weighing method with the muffle furnace $(SX2-5-12Y)$. After treated by bottom ash powder, the bio-residue was dried and observed for its microstructure by electron microscope (Phenom Pro). The X-ray photoelectron spectroscopy (XPS) characterizations of bottom ash and fy ash powder were done with a Kratos AXIS 165 electron spectrometer with monochromatic AlKa radiation at 100 W, and highresolution measurements in S 2p, Cl 2p, K 2p, Ca 2p, O 1 s, F 1 s, Zn 2p and Na 1 s regions were taken. Thermal analysis (TGA-DTG) of bio-residue was recorded on a thermal analysis system (Q600 SDT; TA Instruments, USA) over a temperature range of 25–600 °C with a heating rate of 5 °C/min in an N_2 stream. Elemental analysis of N, C, H, S and O of bio-residue was performed using an elemental analyzer (Vario EL III, Germany).

Results and discussion

Moisture existence forms in bio‑residue

The vacuum fltration experiments were conducted in triplicate, and the results are shown in Table [2](#page-3-0). The weight of moisture removed by fltration was about 20 g, which cannot be removed easily by gravity. Drawing on the experience of sludge's moisture form, the capillary water in sludge could be removed by negative pressure (vacuum flter). Therefore, this part of moisture in bio-residue was identifed as capillary water.

For analyzing the moisture form in bio-residue, thermogravimetric analysis of dried bio-residue was conducted, and the result is shown in Fig. [1](#page-3-1). When the temperature reached 306.96 °C, the $\frac{dw}{dT}$ reached the maximum value and the dried bio-residue started to burn. The dewatering happened between 162.90 ℃ and 213.74 ℃, and the weight loss was about 3.16% of bio-residue (dry basis). According to the

Table 2 Vacuum fltration experiment results (Unit: g)

No	Initial weight	Weight of water removed by filtration (w_1)	Weight loss of w_1/w_2 drying (w_2)	$(\%)$
	100.0	20.5	84.3	24.32
\mathcal{L}	100.0	19.3	85.1	22.68
\mathcal{E}	100.0	20.6	84.3	24.44

moisture content of bio-residue (wet basis), the weight loss between 162.90 ℃ and 213.74 ℃ was about 0.58% of the whole moisture in bio-residue. This part of moisture could not be removed by low-temperature thermal drying, which was identifed as bound water. Bio-residue, coming from digested organic waste, was diferent from municipal sludge. Due to the utilization of polyacrylamide for dewatering, it can adsorb moisture and form colloid, which makes a large amount of moisture stored in the polyacrylamide colloid as adsorbed water. Therefore, the moisture in bio-residue could be classifed into adsorbed water, capillary water and bound water, which occupied 75.61%, 23.81% and 0.58%, respectively.

Dewatering capacity of diferent reagents

In bio-residue, the moisture was classifed into adsorbed water, capillary water and bound water, which occupied 75.61%, 23.81% and 0.58%, respectively. Among these moisture types, adsorbed water had the largest proportion, which was the most possible moisture to be dewatered. The content of bound water was small, which could be ignored in practical engineering. The adsorbed water and capillary water were the main impediments for bio-residue's dewatering and were removed hardly before treated by reagents.

The variations of moisture content and low calorifc value with diferent dewatering reagents at the dosage of 2.0% were conducted. Figure $2(a)$ shows that at the dosage of 2.0%, the moisture content decreased over the curing time. At the $4th$ d, the moisture contents of four groups with CaO, bottom ash powder, fly ash powder and Fe(0)- $K_2S_2O_8$ were 69.17%, 61.34%, 72.00% and 65.39%, respectively, and bottom ash powder's excellent dewatering capacity was justifed. After 8-day curing, the moisture content of four groups decreased sharply and reached 67.94% (CaO), 66.20% (bottom ash powder), 71.50% (fly ash powder) and 68.84% $(Fe(0)-S_2O_8^{2-})$ at the 8th d, respectively. Taking CaO group

Fig. 2 Moisture content variation (**a**) and low calorifc value (**b**) of bio-residue with the 2.0% dosage of CaO (Co), bottom ash (Ba), fy ash (Fa) and Fe(0)- $K_2S_2O_8$ (Ip)

as example, the moisture content of bio-residue decreased from 78.4% to 43.3% after 14-day treatment. The moisture loss was about 40.34 g, accounting for 51.5% of the whole moisture. According to the moisture proportion and characteristics of bio-residue, the dewatering treatment mainly removed the adsorbed water in bio-residue.

After CaO was mixed with bio-residue, which reacted with moisture in bio-residue, the calcium hydroxide $(Ca(OH₂)$ was generated. Both CaO and Ca(OH)₂ started to absorb carbon dioxide in the air over time, as shown in Eq. [\(2](#page-4-1)) and [\(3](#page-4-2)). Therefore, the weight loss can only refect a part of dewatering efect.

$$
CaO + CO2 = CaCO3
$$
 (2)

$$
Ca(OH)2 + CO2 = CaCO3 + H2O
$$
 (3)

According to the XPS analysis, the fy ash powder used in pre-experiment mainly contained $Na₃PO₄$, $Na₂SO₄$ and $CaSO₄$, which could react with water by forming $Na_3PO_4·12H_2O$, $Na_2SO_4·10H_2O$ and $CaSO_4·2H_2O$. These reactions are exothermic, shown as Eq. $(4)-(6)$ $(4)-(6)$ $(4)-(6)$, and could help the evaporation of moisture. Although the fly ash powder was conducive to the release of moisture, most of which the existence form was bound water in the hydrates of inorganic salts and could not be dewatered by volatilization easily. The low calorifc value of treated bio-residue was afected by the existence of hydrates, which was consistent with the results of low calorific value test.

$$
CaSO4 + 2H2O = CaSO4 \cdot 2H2O
$$
 (4)

$$
Na_3PO_4 + 12H_2O = Na_3PO_4 \cdot 12H_2O
$$
 (5)

$$
Na_2SO_4 + 10H_2O = Na_2SO_4 \cdot 10H_2O
$$
 (6)

The dewatering effect of $Fe(0)$ - $K_2S_2O_8$ ranged between the bottom ash powder and CaO. Persulfate is a strong and non-selective oxidant with a high redox potential of 2.01 V. It can be efectively activated by initiators including heat, UV light or transition metals (Me^{n+}) to generate sulfate free radicals (SO_4^-) which has an even higher redox potential estimated to be 2.60 V. Some of the reaction during activation of $S_2O_8^{2-}$ may be expressed as Eq. [\(7](#page-4-5))-([10\)](#page-4-6) (Yan et al. [2011](#page-12-16); Oh et al. [2009](#page-11-15), [2010;](#page-12-17) Zhen et al. [2012](#page-12-11)).

$$
S_2O_8^{2-} + 2e^- \to 2SO_4^{2-} E^0 = 2.01 V
$$
 (7)

$$
S_2O_8^{2-} + \text{heat}/UV \rightarrow 2SO_4^{-}.
$$
 (8)

$$
S_2O_8^{2-} + Me^{n+} \to Me^{(n+1)+} + SO_4^{-} \cdot + SO_4^{2-} \tag{9}
$$

$$
SO_4^- \t + e^- \t + SO_4^{2-} E^0 = 2.60 V
$$
 (10)

Similar to fly ash powder, the dewatering capacity of bottom ash powder could be explained preliminarily that some inorganic salts in the bottom ash powder could react with moisture in bio-residue and achieve the transfer of moisture from bio-residue to inorganic salts. These reactions are exothermic, which can help the evaporation of moisture. However, diferent from CaO, bottom ash powder has little efect on low calorifc value. Meanwhile, the inorganic salts in fy ash powder could bind more moisture than bottom ash powder, afecting its evaporation. The results suggested that bottom ash powder was a preferred dewatering reagent, and more mechanisms will be analyzed in detailed experiments.

The low calorifc value is associated with moisture and organic contents. Figure $2(b)$ shows that the low calorific value was related to moisture content and dewatering reagents greatly. With the decrease in the moisture, the low calorific value increased. At the $4th$ d, the low calorific values of bio-residue with CaO, bottom ash powder, fy ash powder and Fe(0)-K₂S₂O₈ were 1872 kJ/kg, 1424 kJ/kg, 1066 kJ/ kg and 976 kJ/kg, respectively. After treated for 8 days, the low calorific values increased gently, and at the 14th d, the low calorifc values of bio-residue with CaO, bottom ash powder, fly ash powder and $Fe(0)-K_2S_2O_8$ were 9697 kJ/kg, 10,544 kJ/kg, 10,163 kJ/kg and 10,873 kJ/kg, respectively. Although the low calorifc value had a positive correlation with dosage at the $8th$ d, it was mainly affected by the moisture content, due to the dewatering efect of CaO. With the increase in the dosage, the dewatering efect got better in the middle phase of treatment.

Dewatering capacity of bottom ash with diferent dosages

The detailed curing experiments for bio-residue's deep dewatering by bottom ash powder with diferent dosages were conducted, and the variations of moisture content and low calorifc value are shown in Fig. [3.](#page-6-0) During the curing experiments, there was no leakage of moisture.

Figure $3(a-1)$ $3(a-1)$ shows the dewatering performance of bioresidue without reagents. In the frst 6 days of curing, the bio-residue's moisture content descended slowly, and its low calorifc value maintained about 2.0 MJ/kg. With the decrease in the moisture content, the low calorifc value was increased obviously. After 14-day treatment, the moisture content declined to about 30% and corresponding low calorifc value raised to about 10.0 MJ/kg, which was suitable for incineration without afecting the operation of incineration plant. Combined with the dried bio-residue's combustion low calorific value (13.3 MJ/kg), the fitting curve of bioresidue' moisture content and low calorifc value is given, as shown in Fig. [3\(a-2\)](#page-6-0), which ftted *Boltzmann equation* and its image was like S-shaped curve. When the moisture content was over 45%, the low calorifc value raised fast with the decrease in the moisture content. With the moisture content going down to 45%, the low calorifc value raised slowly and reached a stable value when the moisture came to about 30%, over 10.0 MJ/kg.

Figure $3(b - f)$ $3(b - f)$ confirms that bottom ash powder contributed to the deep dewatering of bio-residue in detail. After 10-day curing, bio-residue's moisture content decreased to about 40% and its low calorific value raised to over 8.0 MJ/kg. When the dosage of bottom ash powder was 2.0%, the final dewatering efficiency after 14 days was better than that of 1.0%, and its low calorific value maintained stably over 10.0 MJ/kg from the 10^{th} d. When the dosage of bottom ash was 3.0%, the dewatering rate was accelerated as shown in Fig. $3(d-1)$. Compared with the dosage of 1.0% and 2.0%, the final low calorific value declined because the bottom ash powder had no calorific value. With the increase in the bottom ash powder dosage, low calorific value decreased at the same moisture content. The high dosage could promote the deep dewatering of bio-residue, but affect the final low calorific value more obviously. The fitting function is shown as Eq. ([11](#page-5-0)) and their specific parameters of different dosages are shown in Table [3.](#page-8-0)

$$
Q = \Delta Q + \frac{Q_0}{1 + e^{\frac{w - \omega}{k}}}
$$
\n(11)

where Q , ΔQ , Q_0 – low calorific value, kJ/kg.

w – moisture content, %

In Eq. ([11\)](#page-5-0), ω represents the critical point of *Boltzmann equation*. When the value of moisture content was bigger than ω, low calorifc value was relatively low, and raised fast with the decrease in the moisture content. With the value of moisture content getting smaller than ω, low calorifc value raised slowly and reached a stable value gradually. The sum of ΔQ and Q_0 represents the theoretical maximum low calorifc value. Table [3](#page-8-0) easily shows that with the increase in the bottom ash powder dosage, the theoretical maximum low calorifc value declined gradually.

With the increase in the bottom ash powder dosage, the low calorific value at the $14th$ d was declined, illustrating that bottom ash powder will affect incineration of bio-residue. When the dosage of bottom ash powder was 2.0%, the moisture of bio-residue could be decreased to about 50% and the corresponding low calorifc value reached 10.79 MJ/ kg at the $10th$ d from the original 0 MJ/kg. Based on the above experiment, 2.0% dosage of bottom ash powder addition indicated an excellent efect on deep dewatering of bio-residue.

Decoupling of moisture in bio‑residue

Chemical composition of bottom ash powder

Figure $4(a)$ shows the survey of XPS spectra for bottom ash powder, which exhibited S, Cl, C, K, Ca, O, F, Zn and Na signals. Figure [4](#page-9-0)([b-i\)](#page-9-0) compiles the high-resolution surface spectra of S, Cl, K, Ca, O, F, Zn and Na recorded on bottom ash powder sample.

The high-resolution surface spectra of S included four peaks with binding energy of 169.5 eV, 170.7 eV, 169.1 eV and 170.3 eV. The binding energy of 169.5 eV and 170.7 eV represented S 2p3/2 peak and S 2p1/2 peak in $ZnSO₄$, and the binding energy of 169.1 eV and 170.3 eV

Fig. 3 Moisture content and low calorifc value variation of bio-residue treated with diferent dosages of bottom ash powder (a, b, c, d, e and f represent the dosages of 0%, 1.0%, 2.0%, 3.0%, 4.0% and 5.0%; (**a-1**), (**b-1**), (**c-1**), (**d-1**), (**e-1**) and (**f-1**) represent the moisture con-

tent and low calorifc value variations of bio-residue; and (**a-2**), (**b-2**), (**c-2**), (**d-2**), (**e-2**) and (**f-2**) represent the ftting relation law of bioresidue' moisture content and low calorifc value)

Fig. 3 (continued)

represented S 2p3/2 peak and S 2p1/2 peak in K_2SO_4 . The high-resolution surface spectra of Cl included four peaks. The binding energy of 198.5 eV and 200.1 eV represented Cl 2p3/2 peak and Cl 2p1/2 peak in NaCl, and the binding energy of 198.8 eV and 200.4 eV represented Cl 2p3/2 peak and Cl 2p1/2 peak in $ZnCl_2$. Two peaks were visible

Table 3 Moisture content and low calorifc value's ftting function and specifc parameters with diferent dosages of bottom ash powder

Dosage	General Equation	Parameters			
		ΔQ	Q_0	ω	k
0%	$\frac{Q_0}{1+e^{\frac{w-\omega}{k}}}$ $Q = \Delta Q +$	1186	11,850	45	9
1.0%		2151	8663	50	5
2.0%		2552	8270	54	1
3.0%		2512	7401	46	3
4.0%		-1400	10,719	62	8
5.0%		2331	7442	49	3

in the spectra of K 2p with the binding energy of 296.2 eV and 293.5 eV, which belonged to K 2p1/2 peak and K 2p3/2 peak in K_2SO_4 . The high-resolution surface spectra of Ca included two peaks with binding energy of 351.1 eV and 347.5 eV, which represented Ca 2p1/2 peak and Ca 2p3/2 peak in $CaCO₃$. The high-resolution surface spectra of F 1 s included only one peak with binding energy of 685.1 eV, which represented ZnF_2 . The high-resolution surface spectra of Zn 2p included six peaks. The binding energy of 1023.0 eV and 1046.0 eV represented Zn 2p3/2 peak and Zn $2p1/2$ peak in $ZnSO_4$, the binding energy of 1021.9 eV and 1044.9 eV represented Zn 2p3/2 peak and Zn 2p1/2 peak in $ZnCl₂$, and the binding energy of 1022.2 eV and 1045.2 eV represented Zn 2p3/2 peak and Zn 2p1/2 peak in ZnF_2 . The high-resolution surface spectra of Na 1 s included only one peak with a binding energy of 1072.3 eV, which represented NaCl. The results confrmed that the bottom ash powder mainly contained NaCl, K_2SO_4 , CaCO₃, $ZnSO_4$, ZnF_2 and $ZnCl_2$.

Dewatering mechanism

The dewatering mechanism was analyzed, combined with XPS analysis of the bottom ash powder. $ZnCl₂$ in bottom ash powder can react with moisture in bio-residue and achieve the transfer of moisture from bio-residue to $ZnCl₂$, and the reaction is shown as Eq. [\(12](#page-8-1)).

$$
ZnCl2 + H2O = Zn(OH)Cl + HCl
$$
 (12)

 $ZnSO₄$ can also react with moisture by forming $ZnSO₄·7H₂O$ and this reaction is exothermic, which can help the evaporation of moisture. The reaction is shown as Eq. [\(13](#page-8-2)). The bottom ash powder can react with moisture in bio-residue and realize the dewatering efficiently, and different from fy ash, the amount of moisture that bottom ash powder can react with was relatively limited, infuencing low calorifc value slightly.

$$
ZnSO4 + 7H2O = ZnSO4 \cdot 7H2O
$$
 (13)

Figure [5](#page-10-0) shows the microstructure of treated bio-residue under the electron microscope, with the decoupling mechanism of moisture. Figure $5(a)$ $5(a)$ $5(a)$ shows that after treated by polyacrylamide, the bio-residue was packed by polyacrylamide colloid and presented a steric reticular structure. After treated by bottom ash powder further, the packed polyacrylamide colloid began to spalling and the strip fber structure could be observed clearly. This appearance got more obvious with the increase in the bottom ash powder's dosage, which is shown in Fig. $5(b-f)$.

The decoupling mechanism of moisture in bio-residue is shown in Fig. $5(g)$ $5(g)$ $5(g)$. The decomposition of polyacrylamide colloid was related to the addition of bottom ash powder. As analyzed by XPS, the bottom ash powder mainly contained NaCl, K_2SO_4 , CaCO₃, ZnSO₄, ZnF₂ and ZnCl₂. After adding bottom ash powder, the bio-residue treated by PAM was bound up and adhered with bottom ash powder. These inorganic salts in bottom ash powder were electrolyte, which could accelerate the hydrolysis and destruction of polyacrylamide colloid with the moisture itself contained frstly. After the polyacrylamide colloid was broken, the moisture in colloid was exposed and began to release into the air by evaporation. Furthermore, it could be observed that when the dosage of bottom ash powder was over 2.0%, the spalling degrees of polyacrylamide colloid were similar, which meant 2.0% dosage of bottom ash powder was enough for the hydrolysis and destruction of polyacrylamide colloid, indirectly proving that 2.0% dosage of bottom ash powder has the best effect on deep dewatering of bio-residue.

Economic analysis of reagents

The conventional dewatering reagents include CaO and Fe(0)-K₂S₂O₈. Take the treatment with 2% dosage as example, different reagents' 10-day dewatering efficiencies are shown in Table [4.](#page-11-16) CaO had the best 10-day dewatering efficiency among four reagents, followed by bottom ash powder, about 21.84%. Fe(0)- $K_2S_2O_8$ has the worst 10-day dewatering efficiency among four reagents, followed by fly ash powder, about 17.08%. According to the cost of reagents and their dewatering efficiencies, the dewatering capacity cost can be calculated and the results are also shown in Table [4](#page-11-16).

Compared with bottom ash and fy ash powder from municipal solid waste incineration plant, the dewatering capacity cost of CaO and Fe(0)- $K_2S_2O_8$ reagents were higher. Although they had a certain dewatering efficiency, the high costs restricted their application in deep dewatering of bio-residue. On the one hand, although the dewatering efficiency of fly ash powder was close to bottom ash powder, fy ash powder had greater impact on low calorifc value of treated bio-residue, which was not convenient for the operation of incineration plant. As a consequence, municipal solid waste incineration (MSWI) fy ash categorized as

Fig. 4 X-ray photoelectron spectroscopy survey spectra of bottom ash powder (**a**) and high-resolution surface spectra of elements in bottom ash powder (**b**-**i**) (note: (**b**) S 2p, (**c**) Cl 2p, (**d**) K 2p, (**e**) Ca 2p, (**f**) O 1 s, (**g**) F 1 s, (**h**) Zn 2p, (**i**) Na 1 s)

Added bottom ash

After treatment by bottom ash (g)

Fig. 5 Electron microscope observation of bio-residue treated by PAM and further treated with diferent dosages of bottom ash powder $(a - bio-residue treated by PAM; $b - 1.0\%$ dosage; $c - 2.0\%$ dosage,$

treated bio-residues

 $d - 3.0\%$ dosage; $e - 4.0\%$ dosage; $f - 5.0\%$ dosage) and decoupling mechanism of moisture (**g**)

a hazardous material must be managed and regulated more scientifcally and efectively, which is not suitable for deep dewatering of treated bio-residue (Li et al. [2018](#page-11-17)). On the other hand, due to the source from municipal solid waste incineration plant, bottom ash has characteristics of huge yield and harmless. As estimated, the incineration of one-ton solid waste generates approximately 250-300 kg of bottom ash (Tan et al. [2022](#page-12-18)). Therefore, bottom ash powder is the best reagent for organic waste bio-residue's deep dewatering.

Table 4 Comparison between cost and dewatering efficiency of reagents $(6.7 \text{ CNY} = 1 \text{ US}\$$ in June 2022)

Conclusion

Organic waste bio-residue should be deep dewatered before incineration. The moisture existence forms of bio-residue were clarifed as adsorbed water, capillary water and bound water, which occupied 75.61%, 23.81% and 0.58%, respectively. Furthermore, refuse incineration bottom ash powder was used as a typical deep dewatering reagent, when compared with CaO, refuse incineration fy ash powder and Fe(0)-K₂S₂O₈. Results showed that the addition of bottom ash powder could decrease the bio-residue's moisture from 80.0% to 37.9% at the optimal dosage of 2.0%, and corresponding low calorifc value reached 10.5 MJ/kg at the 10^{th} d. The ZnCl₂ and ZnSO₄ present in bottom ash powder could react with moisture in bio-residue to form hydrates of inorganic salt and break polyacrylamide colloid, realizing the release of adsorbed water in bio-residue via water evaporation accelerated by exothermic process.

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Declarations

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Consent for publication Not applicable.

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Bottom ash powder 21.84 50–80 5–7

Fly ash powder 17.08

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