RESEARCH ARTICLE

Synthesis of novel epichlorohydrin cross‑linked β‑cyclodextrin functionalized with reduced graphene oxide composite adsorbent for treatment of phenolic wastewater

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Abstract

A novel composite consisting reduced graphene oxide–functionalized beta-cyclodextrin epichlorohydrin polymer (RGOβCD-ECH) was synthesized for the treatment of phenolic wastewater. Batch study of phenolic pollutants (2,4-dichlorophenol, 2-chlorophenol, and phenol) was analyzed using the synthesized composite as an adsorbent from an aqueous solution. The optimized parameters were temperature 25 °C, adsorption time 60 min, solution pH 7, and dosage 0.25 g/L. The isotherm data were more suitably ftted by the Langmuir isotherm model. The maximum uptake for 2,4-dichlorophenol, phenol, and 2-chlorophenol was 702.853, 659.475, and 674.155 mg/g, respectively, at 25 ± 1 °C. The kinetic data for all the phenolic pollutants follow the pseudo-second-order model, and the rate was controlled by flm difusion. Thermodynamic data revealed that the process of removing phenolic pollutants is spontaneous and endothermic. The composite can be used up to fve cycles with a small reduction in the removal. Adsorption performance of the synthesized composite for synthetic industrial effluents shows that up to 78% removal occurred in 60 min adsorption time. Based on the remarkably rapid adsorption and high adsorption capacity, the synthesized composite can be considered an efficient adsorbent for treating phenolic pollutants from wastewater.

Keywords Epichlorohydrin · Beta-cyclodextrin · Adsorption · Langmuir · Endothermic · Wastewater

Introduction

Water pollution from anthropogenic activities and industrial operations has become a global problem due to the possible long-term hazard to human health and ecosystems. In recent times, there has been increased apprehension among scientists and researchers around the world concerning the efects of wildlife, aquatic, and human exposure to hazardous pollutants in the water system. Phenolic pollutants have been considered as the primary pollutants in surface water and groundwater due to their high toxicity, poor natural biodegradability, high oxygen demand, and long-term ecological

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damages (Zhu et al. [2007\)](#page-16-0). The US Environmental Protection Agency (USEPA) has listed phenolic pollutants as priority pollutants due to their bio-recalcitrant, acute toxicity nature and toxic efects on animals and human beings and stick in the aquatic environment over a very long period (Li et al. [2013](#page-15-0)). The phenolic compounds regularly enter the water bodies from domestic, agricultural, and industrial activities. Phenolic compounds like phenols and chlorophenols have been categorized as toxic phenolic pollutants.

Chlorophenols are formed by the reaction of phenols with disinfecting chlorine (Núñez-Gaytán et al. [2010](#page-15-1)). The chlorophenols like 2,4-dichlorophenol (2,4–DCP) and 2-chlorophenol (2–CP) are known as primary pollutants. These pollutants are used in paper, dyes, petrochemicals, antioxidants, plastics, wood preservatives, waste incineration, and pesticides (Jing et al. [2021\)](#page-14-0). In addition, it is produced as by-products during the chlorination disinfection of drinking water as well as bleaching of pulp with chlorine. Due to the presence of chlorine groups in 2-CP and 2,4-DCP, even at low concentrations, it is very hazardous in nature in water bodies (Badu Latip et al. [2021](#page-14-1)). Phenolic pollutants

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possess hazardous health efects, which are both acute and chronic. Human exposure to phenol results in the irritation of the mucous membranes, eyes, and skin and afects the kidney, liver, digestive tract, lungs, and central nervous system (Anku et al. [2017](#page-14-2); Nakhjiri et al. [2021\)](#page-15-2). Even at trace concentration, its presence in surface water and groundwater causes severe health efects. Hence, there is a growing concern over the traces of phenolic levels detected in surface water and groundwater. Long-term exposure can lead to coma, tremors, muscle weakness, and irregular breathing. Chronic effects due to phenol exposure can be the dark coloration of the urine, vertigo, weight loss, anorexia, salivation, and diarrhea (Magdy et al. [2018](#page-15-3)). The allowable concentration of phenol in the surface water is less than 0.001 mg/L, and for groundwater, it is 0.0019–0.01 mg/L, according to USEPA (Kazemi et al. [2014\)](#page-14-3). Therefore, costeffective, efficient, and quick treatment methods are required to remove the phenolic contaminant from the wastewater before releasing it into the natural water body.

Various conventional techniques have been used for the treatment of phenolic pollutants from wastewater, like solvent extraction (Poonguzhali et al. [2021\)](#page-15-4), chemical oxidation (Hadi et al. [2021](#page-14-4)), wet oxidation (Lal and Garg [2015](#page-15-5)), photocatalytic degradation (Landete et al. [2021\)](#page-15-6), electrochemical coagulation (Olya and Pirkarami [2013](#page-15-7)), biological degradation (Hedbavna et al. [2016\)](#page-14-5), ion exchange (Camacho et al. [2021\)](#page-14-6), and adsorption (Feng et al. [2021;](#page-14-7) Gupta and Garg [2015](#page-14-8)). However, most of the methods have limited application due to their high cost, the longer time required to attain higher efficiency, and the production of unnecessary secondary pollutants. It is now well documented that adsorption is a promising method for wastewater treatment, as it has many advantages over other methods like high removal efficiency, cost-efectiveness, operational simplicity, design simplicity, insensitivity to toxic pollutants, application fexibility, and non-toxic end products (Xiang et al. [2021](#page-16-1)). Barring all this advantages, the adsorption process has some limitations, such as expensive adsorbent materials, difficulty in separation of pollutants from the spent adsorbents, and the deposition of spent adsorbents (Moosavi et al. [2020](#page-15-8)). Considering all the advantages and disadvantages of adsorption process, the selection of efficient adsorbents for the treatment of phenolic pollutants is of great importance. The characteristics of an efficient adsorbent are the accumulation of large quantities of pollutants on its surface, high surface area, excellent reproducibility, and fast and high desorption property and chemical stability (Efome et al. [2018](#page-14-9)). In an enormous number of studies, various adsorbents like metal oxides (Wang et al. [2018\)](#page-16-2), agricultural by-products (Khenniche and Benissad-Aissani [2010\)](#page-15-9), carbon nanotubes (Lee et al. [2018](#page-15-10)), activated carbon, graphene (Sahoo et al. [2020\)](#page-16-3), and graphitic carbon nitride (Chegeni et al. [2019\)](#page-14-10) have been explored for the efective removal of toxic environmental pollutants. Recently, researchers have been giving much attention to synthesizing graphene-based composite adsorbents, as it will beneft various precursor materials into one adsorbent. In recent years, the application of bio-conducting polymeric composite adsorbents has gained much emphasis because of its low cost, presence of various functional groups, wide availability, and outstanding adsorption performance.

In the last decade, graphene, the new member of the carbon family, has displayed remarkable performance in wastewater treatment. It has extraordinary properties such as fast adsorption rate, abundant functional groups, good chemical stability, high surface area $(2630 \text{ m}^2/\text{g})$, and high adsorption capacity (Rout et al. [2019\)](#page-16-4). However, the derivatives of graphene-like reduced graphene oxide (RGO) and graphene oxide (GO) are strongly bonded to water molecules through hydrogen and ionic bonds because of the functional groups (epoxy, hydroxyl, and carboxyl) present on the surface (Rout and Jena [2021](#page-15-11)). However, GO and RGO have specifc problems like susceptibility to aggregation, surface area reduction, easy loss, low dispersion in solution, and difficulty in separation from treated waste-water (Nekouei and Nekouei [2017\)](#page-15-12). Due to these specific problems, it has become a research hotspot in recent times. To overcome this, RGO is functionalized with a cross-linker (beta-cyclodextrin polymer), which attracts more attention in water treatment process.

Beta-cyclodextrin (βCD, $C_{42}H_{70}O_{35}$) is a truncated coneshaped structure having seven D-glucopyranose units linked by an α-1,4-glycosidic bond (Ragavan and Rastogi [2017](#page-15-13)). It has a water-loving cavity on the external surface and a hydrophobic cavity in the center, which allows to form a host–guest inclusion complex with organic and inorganic molecules (Xu et al. [2020](#page-16-5)). Due to stable chemical structure, non-toxicity, high biodegradability, good biocompatibility, simplicity of obtainment, and porous structure, it becomes a suitable adsorbent for the adsorption of organic pollutants. However, it is a water-soluble material; as a result, its application is limited in water treatment. To overcome it, the polymerization of βCD is done with a cross-linker to make it a water-insoluble polymer. Epichlorohydrin (ECH) is chosen as a suitable cross-linker for synthesizing the insoluble polymer because of its low cost, non-toxic, and easy synthesis approach (Heydari et al. [2018\)](#page-14-11).

Recently, various research activities have emphasized the synthesis of βCD and graphene-based composites for treating phenolic compounds by adsorption technique (Gholami-Bonabi et al. [2020](#page-14-12); Gong et al. [2016](#page-14-13); Liu et al. [2020](#page-15-14); Wang et al. [2021](#page-16-6)). Inspired by the above research in this work, efforts have been made to synthesize RGOβCD-ECH composite as an excellent and low-cost adsorbent for treatment of phenol, 2-CP, and 2,4-DCP from an aqueous solution in a batch study. The physicochemical properties of these three pollutants are listed in the supporting material in Table S1. The physicochemical properties of the prepared composite were subsequently characterized using SEM, XRD, and FTIR. In addition, the effect of pH, contact time, phenolic pollutant concentration, adsorbent dosage, and temperature on the extent of adsorption of phenolic pollutants from water has been investigated. Finally, the kinetic models, isotherm models, thermodynamic parameters, desorption/regeneration, and plausible mechanism for phenolic pollutants adsorption have also been studied.

Materials and methods

Chemicals used

All materials and chemicals, which were used in this experimental section, are mentioned in supporting material section S1.

Synthesis of GO and RGO

In the modified Hummers method, $NaNO₃$ is replaced by H_3PO_4 and the synthesis of GO follows both oxidation and exfoliation (Smith et al. [2019](#page-16-7)). In a 1-L beaker, H_3PO_4 (30 ml) and H_2SO_4 (270 ml) were poured in ratio (1:9) and stirred for 15 min. To the above-prepared acidic solution, add 5 g of graphite powder and stir for 45 min. After that, $KMnO₄$ (15 g) was added slowly because of the exothermic nature of the reaction and, to maintain the temperature below 5 °C, ice bath was used. A dark green solution appeared after 6 h of vigorous stirring and then add 250 mL of DIW to the solution dropwise. Again, it was put in an ice bath to control the exothermic reaction temperature. After 15 min, add 150 mL of DIW into the solution, and the color of the solution changes to dark brown. After that, H_2O_2 (9 mL) was added to the solution and the color changed to yellowish brown. The solution was centrifuged at 8000 rpm to remove the unwanted extracts and continually bathed with DIW to make the pH of the solution 7. After that, the suspensions were put in an oven at 70 °C for 12 h to obtain the graphene oxide (GO) powder.

The procedure for reduced graphene oxide synthesis is as follows: frst, the GO suspension was prepared by the addition of GO powder (1.25 g) with DIW (250 mL) and stirred for 15 min. After that, the pH was adjusted to 10 by adding HCl and NaOH solution as and when required. After that into the above solution, the reducing agent $N_2H_4·H_2O$ (5 mL) was added at 65 °C and stirred for 4 h for the complete reduction. Then, the synthesized product was centrifuged and placed in an oven at 70 °C for 12 h to fnd RGO powder.

Synthesis of cross‑linked beta‑cyclodextrin epichlorohydrin polymer

The synthesis of beta-cyclodextrin epichlorohydrin (βCD-ECH) polymer occurred using ECH as a cross-linker (Gong et al. [2016](#page-14-13)). First in a beaker, add 20 mL of 50% w/w NaOH solution and β CD (10 g) was completely mixed with it and was continuously stirred for 3 h at 25° C. ECH (6 mL) was added and stirred at 400 rpm for 40 min. Then, to stop the reaction, 15 mL acetone was added and decantation process was used to remove the excess acetone. Then, the residue was put in an oven at 50 °C for 12 h. As the above crosslinking reaction occurred in basic conditions to neutralize it, 20 mL of 6 N HCL was added. For moisture evaporation, the solution was placed at 60° C in a dryer, and to form a white precipitate, 44 mL of ethanol was added to the solution. By decantation operation, the white precipitate was separated and put in an oven at 60 °C.

Synthesis of RGO‑βCD‑ECH composite

The synthesis procedure follows frst in a 1-L beaker, add 500 mL DIW, and then RGO (125 mg) was mixed by sonication. To the above solution, $βCD-ECH$ (2 g) was added and a homogeneous solution is formed after 30 min of stirring. Then, 5 mL of NH_4 OH was added and sonicated for 60 min. Finally, a black suspension was produced, and it was constantly washed with DIW and then put in a hot air oven at 60° C for drying.

Instrumentation

The various instruments, which are used, for the characterization of synthesized material are described in supplementary material section S2.

Batch adsorption experiments

The batch experiments were executed in a thermostatic shaker with 180-RPM speed. A total of 12.5 mg of RGOβCD-ECH composite was added to 50 mL of phenolic pollutant solution (100, 150, 200, 250, and 300 mg/L) under the optimized parameter conditions. The various adsorption parameters like $pH = 2-10$, temperature = 15–40 °C, adsorption time= $0-150$ min, dosage= $5-20$ mg, and initial concentration $=(100-300 \text{ mg/L})$ were varied to find out the optimal condition for higher adsorption. HCl or NaOH solution (0.05 mol/L) was used to adjust the phenolic pollutant pH as and when required. The remaining concentrations of BPA, 2-CP, phenol, and 2,4-DCP were determined using a UV–VIS spectrophotometer (Shimazu UV-3150 Japan) at the wavelengths of 270, 275, and 284 nm, respectively. The reusability of the RGO-βCD-ECH composite was explored via consecutive adsorption/desorption cycles. The uptake capacity at equilibrium (q_e) was evaluated according to the following formula:

$$
q_e = \frac{(C_o - C_e) \times V}{m_s} \tag{1}
$$

where *V* is the volume of the solution (mL), C_e and C_o (mg/L) are the equilibrium and initial phenolic pollutant concentration, and m_s (mg) is the amount of adsorbent. The removal rate was evaluated according to the following formula:

$$
\%R = \frac{(C_o - C_t)}{C_o} \times 100\tag{2}
$$

Experiment with simulated effluent

As the real wastewater contains various organic and inorganic pollutants, a lab-made simulated effluent, which has similar characteristics to the textile industry and petroleum refneries industry, was used to study the efectiveness of the composite. The simulated industrial effluents consist of phenolic compounds with high salt concentrations. The composition of the simulated effluent used is as follows: phenol (100 mg/L), 2-chlorophenol (100 mg/L), 2-naphthol (20 mg/L), bisphenol A (30 mg/L), 2-nitrophenol (15 mg/L), hydroquinone (15 mg/L), potassium phosphate (30 mg/L), sodium chloride (40 mg/L), 2,4-dichlorophenol (100 mg/L), and sodium carbonate (40 mg/L). The pH of the simulated effluent was recorded as 8.2, and by adding 0.01 N HCl solution, the pH of the solution was reduced to 7. After that, 12.5 mg of RGO-βCD-ECH composite was added to the 50 mL of synthetic solution, and then, the above solution was put in a thermostatic shaker for 60 min at 30 °C. A UV–VIS spectrometer was used to measure the absorption spectra of the simulated effluent in the range of 200 to 700 nm before and after adsorption treatment. The removal percentage was calculated using the area under the absorption band.

Results and discussion

Characterization of RGO‑βCD‑ECH composite

SEM analysis

The surface properties and morphology of the synthesized RGO-βCD-ECH composite are studied using FESEM microscopy at diferent magnifcations. It is observed from Fig. [1a](#page-4-0) that in GO, the sheets stuck together because of the oxygen-containing functional groups, rough surfaces, wrinkles are present, heterogeneous surface structures, and thin sheets (Rout and Jena [2021](#page-15-11)). The FESEM image of RGO (Fig. [1b](#page-4-0)) shows the wrinkled paper-like structure, corrugated surface, less aggregate, and irregular structure (Rout and Jena [2022a,](#page-15-15) [b\)](#page-16-8). This change in surface properties in RGO is because of the elimination of oxygenated functional groups from GO. It can be seen from Fig. [1c](#page-4-0) that βCD-ECH polymer consists of numerous βCD units in its structure and the surface is smooth, porous in nature, has irregular solid particles, and regularly shaped, which might be due to the presence of cross-linked polymer networks. Also, these morphological properties of βCD-ECH polymer confrm that nanopore structure is not the main adsorption mechanism (Huang et al. [2018\)](#page-14-14). After introducing RGO, the composite (Fig. $1d$) retains the original shape and size of βCD-ECH polymer, suggesting the wellhomogenized well-distributed nanolayers of RGO in the composite. Also, on the surface of the composite, many wrinkles are present and the surface is rough, indicating that βCD-ECH polymer is completely deposited onto the RGO surface.

FTIR analysis

FTIR spectra obtain the surface functional groups and chemical structural information. From our previous work, it has been observed that in GO, peaks are at 3448/cm for –OH stretching of absorbed water molecules, 1030/cm for C–O vibration, 1643 /cm for C = O, 1217 /cm for C–O–C vibration, and C–OH vibration at 1390/cm, which confrmed the oxidation of graphite fakes to synthesize GO (Faniyi et al. [2019\)](#page-14-15). In FTIR spectra of RGO, the peak at 1560/cm is for $O = C-O$ from carboxylate, $C-O-C$ vibration at $1217/cm$, $C = C$ vibration at $2342/cm$, and there is no hydroxyl peak around 3300–3400/cm that suggests the successful synthesis of RGO (Rout and Jena [2022a](#page-15-15)). In Fig. [2a](#page-5-0), it is observed that in $βCD-ECH$ polymer, lower absorption peaks are observed at 707, 756, 857, and 943/ cm confrms the existence of ring vibration. The peak at 3450, 1380, 1655, and 1033/cm belongs to –OH hydroxyl group vibration, C –OH vibration, $C = O$ carbonyl stretching, and C–O epoxide group vibration. In the FTIR spectra of the RGO-BCD-ECH composite, all the peaks of polymer and RGO are present, confrming that on the RGO surface, βCD-ECH polymers are efectively accumulated. Due to the hydrogen bonding formation between βCD-ECH and RGO, the –OH group is shifted to a lower wavenumber value (3440/cm) in the composite. In addition, the appearance of the bending vibrations of N–H for composite at 1124/cm testifes the successful introduction of amine groups in the composite.

Fig. 1 FESEM image of **a** GO, **b** RGO, **c** βCD-ECH polymer and **d** RGO-βCD-ECH composite

XRD patterns

The XRD pattern of RGO-βCD-ECH composite is shown in Fig. [2b.](#page-5-0) In the XRD spectra of graphite powder, a sharp peak is obtained at a 2θ value of 26.62° with d-spacing 0.33 nm (Hidayah et al. [2017](#page-14-16)). Our previous work observed that after the introduction of oxygen functionalities, the graphitic peak shifts towards left having 2*θ* to a value of 12.12°; having (001) plane for GO and d-spacing of 0.82 nm confrms the synthesis of GO (Rout and Jena [2022a\)](#page-15-15). For RGO, a sharp peak is observed around 2*θ* value 28.68° having d-spacing 0.34 nm and (002) plane. One common peak could be seen at 41.7° (100) for both RGO and GO, which could occur due to some manganese in the synthesized GO (Rout and Jena [2022a](#page-15-15)). Two broad peaks are observed at 2*θ* values of 36.72° and 53.4° in the βCD-ECH polymer (Fig. [2b](#page-5-0)) corresponding to (022) and (202) plane, which is due to the amorphous nature of the polymer (Huang et al. [2015\)](#page-14-17). In the RGO-βCD-ECH composite XRD spectra, three characteristic peaks are observed at 2*θ* of 29.68°, 36.72°, and 53.4°, corresponding to (002), (022), and (202) plane. These peaks confrmed the successful synthesis of RGO-βCD-ECH composite.

N2 adsorption/desorption isotherm

The textural characteristics of the RGO-βCD-ECH composite are measured by using N_2 adsorption/desorption technique. The results (Fig. [2c](#page-5-0)) displayed a type-III isotherm with type H_4 hysteresis loop associated with the co-existence of both mesoporous and microporous

Fig. 2 a FTIR spectra, **b** XRD pattern, **c** N2 adsorption/desorption isotherm, and **d** BJH pore size distribution of RGO-βCD-ECH composite

networks. The specific surface area (SSA) of the RGO- β CD-ECH composite is 35.21 m²/g which is lower than RGO (461.247 m²/g) and higher than β CD-ECH polymer $(12.207 \text{ m}^2/\text{g})$. The Barrett–Joyner–Halenda (BJH) plot (Fig. [2d\)](#page-5-0) shows that sharp peaks are formed between 2.86 and 18.65 nm indicating that the synthesized RGO-βCD-ECH composite is mesoporous in nature. The pore volume of the synthesized composite is $0.085 \text{ cm}^3/\text{g}$, whereas the mean pore diameter is 2.98 nm. After adsorption treatment, the SSA of the used RGO-βCD-ECH composite is reduced to 30.15 m^2/g as some of the active sites are filled with pollutants and some pore structures collapse.

Adsorption study

Efect of solution pH

The effects of solution pH on the adsorption performance of phenolic compound (phenol, 2-CP, 2,4-DCP) using RGO-βCD-ECH composite are studied in the pH range of 2.0–10.0, at 60 min of contact time, and 15 mg of adsorbents, 100 mg/L initial phenolic compound concentration, and at room temperature (25 °C) . The resulting adsorption performance is shown in Fig. [3a](#page-6-0). It is observed

Fig. 3 Efect of **a** pH, **b** adsorbent dosage, **c** Initial concentration and contact time, and **d** temperature on phenolic pollutants removal onto RGOβCD-ECH composite

that at both $pH < 7$ and $pH > 7$, the removal percentage decreases for all the phenolic pollutants. The maximum performances for phenol, 2-CP, and 2,4–DCP are 90.895, 93.452, and 96.745%, respectively, that occur at $pH = 7$. The pK_a values for 2,4-DCP, phenol, and 2-CP are 7.9, 9.9, and 8.8, respectively, suggesting that all phenolic compounds are weak acidic in nature (Raoov et al. [2013](#page-15-16)). Chlorophenols and phenols behave as anions at certain pH values as they are proton donors. At pH values greater than 7, the phenolic compounds became phenolate anion, and the RGO-βCD-ECH composite surface is negative $(pH_{ZPC}= 6.55)$ $(pH_{ZPC}= 6.55)$ $(pH_{ZPC}= 6.55)$ (Rout and Jena [2022a](#page-15-15), b) in charge; both so repel each other as a result, and the adsorption performance decreases. In addition, at pH values greater than 7, the phenolic compounds start deprotonate and form phenolate anion as a result; the hydrogen bond between phenolic compound and adsorbent decrease causes a reduction in performance. At pH values lower than 7, the protonation of the phenolic compound starts and the H^+ ions increases in the solution. As a result, the electrostatic repulsion between protonated phenolic compounds and the H^+ ions increases and causes the depletion of the adsorption process (Zhao et al. [2021](#page-16-9)). Therefore, the pH is set at 7 for further experiments to obtain high adsorption efficiency.

Efect of adsorbent dosage

Another key parameter is the amount of adsorbent as it determines the uptake capacity for a given adsorbate concentration. The efect of composite dosage on adsorption performance is explored in the range of 5–20 mg/50 mL solution at pH of solution 7, 60 min of contact time, 100 mg/L initial phenolic compound concentration, and at room temperature (25 °C). From Fig. $3(b)$ $3(b)$ $3(b)$, it is observed that from 5 mg to 12.5 mg/50 mL, the removal of phenolic pollutants sharply increases and then attains equilibrium on the further increase. This is because as the adsorbent dosage increases, the number of available adsorption sites of the adsorbent increases. Therefore, it results in an increase in more amount of phenolic pollutants on the composite surface. However, the increment of adsorbent dosage above 12.5 mg does not allow any additional improvement in the adsorption performance. This is due to the agglomeration of phenolic pollutants on the RGO-βCD-ECH composite (Srivastava et al. [2016](#page-16-10)). Also, with an increase in dosage, equilibrium starts between unadsorbed molecules in the solution, with the molecules bonded to the adsorbent surface. As a result, the adsorbent surface becomes saturated, and the adsorption of new molecules does not occur, so the adsorption attains equilibrium. Therefore, 12.5 mg/50 mL is the optimum adsorbent dosage for further experiments to obtain high adsorption efficiency with the conditions described above.

Efect of initial phenolic pollutant concentration and adsorption time

Initial concentration of the adsorbate is one of the most important parameters of an adsorption process as it gives an essential driving force, which is required in all mass transfer operations to overcome the resistances between solid and liquid phases (Gholizadeh et al. [2013\)](#page-14-18). The batch experiments were done in the concentration range of 100–300 mg/L of phenol, 2-CP, and 2,4-DCP under optimized parameter conditions at pH of solution 7, adsorption time range of 0–150 min, 12.5 mg/50 mL of adsorbent dosage, and at room temperature (25 °C). The results obtained are illustrated in Fig. [3c](#page-6-0) and [d](#page-6-0). In Fig. [3c,](#page-6-0) it has been observed that, initially, the availability of active adsorption sites are more on the surface of the adsorbent; as a result, it adsorbs more pollutants on their surface, and rapid adsorption occurs. However, with the progress of adsorption time, the active sites of the adsorbent decrease because of the agglomeration of pollutants on the adsorbent surface, so the decline rate of adsorption occurs. As the maximum adsorption occurs at 60 min of contact time for further adsorption experiments, 60 min is chosen as optimum time. Figure $3d$ shows that the $%R$ decreases with an increase in initial concentration because as the initial concentration increases, it increases the mass

transfer driving force; as a result, it overcomes the mass transfer resistance between the adsorbent and adsorbate in the aqueous solution. Therefore, more adsorbate molecules start difusing from the surface to the bulk solution, which causes a reduction in percentage removal.

Efect of temperature

The solution temperature is an essential parameter in an adsorption process, as it describes the thermodynamic state of the adsorption process. The batch adsorption experiments using RGO-βCD-ECH composite are performed from 15 to 40 °C temperature under optimized parameter conditions described above. The temperature efect on the phenolic compound removal is illustrated in Fig. [3e.](#page-6-0) The plot shows that as the temperature increases, the removal percentage also rises, suggesting the adsorption is endothermic in nature. It is observed that in up to 30 °C, the removal rate increases highly, and after that, the removal rate gradually slows down and attains equilibrium. As a result, 30° C is chosen as the optimal temperature for further experiment. This increase in removal percentage is that with an increase in temperature, the phenolic pollutants present in solution start accelerating, leading to enhanced kinetic energy (Jiang et al. [2018\)](#page-14-19). As a result, the transfer rate of phenolic ions accelerated to the surface of the composite, which enhances the adsorption performance. However, with increasing temperature, beyond 30 °C, the attractive forces between the adsorbent surface and phenolic pollutants weakened, reducing the adsorption performance.

Adsorption isotherms

The adsorption equilibrium study between the solute and solvent at a constant temperature could be analyzed by the isotherm study (Desta [2013\)](#page-14-20). It is also crucial to the optimal utilization of the adsorbent. The equilibrium data of the phenolic pollutant adsorption using RGO-βCD-ECH composite are examined using Temkin, Langmuir, and Freundlich models. The surface of the adsorbent is energetically homogeneous, and the adsorption process is driven in a ratio of 1:1, where one molecule of adsorbate is bound to one binding site only (Langmuir [1918](#page-15-17)). Freundlich isotherm assumes that heterogeneous adsorption occurs in the process, where the adsorption sites are diverse and the binding sites are not saturated (Prabhakar et al. [2011\)](#page-15-18). The assumption for the Temkin model is for all the molecules; adsorption heat decreases linearly rather than exponentially with an increase in amount of adsorbent. The non-linear form models could be expressed as follows (Rout and Jena [2022b\)](#page-16-8):

$$
q_e = \frac{q_m K_{\rm L} C_e}{1 + K_{\rm L} C_e} \tag{3}
$$

$$
q_e = k_{\rm F} C_e^{1/nF} \tag{4}
$$

$$
q_e = \frac{RT}{b_T} \ln(A_T C_e) \tag{5}
$$

where q_m is the theoretical maximum uptake capacity of phenolic pollutant (mg/g), A_T is the binding energy (L/mg), q_e is the uptake capacity at equilibrium (mg/g), K_L (L/mg) is the affinity constant, b_T (J/mol) is the heat of adsorption,

n and K_F (mg/g)(L/mg)^{1/*n*} are Freundlich constants, and *T* (K) is the temperature. The non-linear plot of the above model is displayed in Fig. [4a.](#page-8-0) Based on non-linear regression, the parameters are calculated and documented in Table [1.](#page-9-0) It is observed that for all the phenolic pollutant, the regression coefficient (R^2) and adjusted regression coefficient (R^2_{adj}) both are maximum for the Langmuir model. This confrmation indicates that the above adsorption process is monolayer adsorption. Accordingly, the q_{max} values found from the Langmuir model are 702.853, 674.155, and 659.475 mg/g, respectively, for the 2,4-DCP, 2-CP, and phenol, respectively, which are higher than that of other

Fig. 4 a Non-linear isotherm model, **b** Non-linear kinetic model, **c** intraparticle difusion model, and **d** Boyd kinetic plot for the adsorption of phenolic pollutants adsorption using RGO-βCD-ECH composite

Table 1 Langmuir, Freundlich, and Temkin isotherm parameters obtained from non-linear regression

Adsorbate	Langmuir				Freundlich				Temkin			
	q_m (mg/g)	k_L (L/mg)	R^2	$R_{\rm adi}^2$	k_F (mg/g)(L/mg) ^{1/n}	1/n	R^2	$R_{\rm adi}^2$	b_T (J/mol)	$A_T(L/mg)$	R^2	$R_{\rm adj}^2$
Phenol	659.475	0.086	0.985	0.981	218.797	0.216	0.944	0.932	22.372	2.868	0.986	0.982
$2-CP$	674.155	0.168	0.981	0.975	280.036	0.176	0.951	0.943	26.485	5.094	0.978	0.978
$2.4-DCP$	702.853	0.304	0.998	0.992	326.272	0.158	0.937	0.928	28.321	8.542	0.972	0.974

Table 2 Comparison of the adsorption capacities of diferent adsorbents for removal of phenolic pollutants from literature

Bold texts represent the results of this present study

adsorbents reported in the literature (Table [2](#page-9-1)) as compared to the amount of RGO-βCD-ECH composite.

data obtained from the contact time study to know the adsorption mechanism. Their equations are respectively given as follows:

$$
q_t = q_e (1 - \exp^{-k_1 t})
$$
\n(6)

$$
q_t = \frac{k_2 q_e^2 t}{1 + k_2 q_e t} \tag{7}
$$

$$
q_t = \frac{1}{\beta} \ln(1 + \alpha \beta t) \tag{8}
$$

$$
q_t = k_{id}t^{1/2} + C_i
$$
 (9)

where k_2 (g/mg min) is the rate constant of PSO, k_1 (/min) is the rate constants of PFO models, C_i is the boundary layer

Adsorption kinetic study

For any adsorption process, the mechanism involves three difusion steps: (i) from the bulk solution, transport of the adsorbate occurs towards the flm covering the adsorbent, (ii) difusing into the adsorbent surface from the adsorbent flm, and (iii) entering into the internal sites of the adsorbent and then attachment to the active sites of adsorbent (Rudzinski and Plazinski [2009\)](#page-16-11). In this context, the kinetic models such as intraparticle difusion (IPD), Elovich, pseudo-second-order (PSO), and pseudo-frst-order (PFO) are widely used to interpret the experimental adsorption

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Table 3 Parameters obtained from non-linear regression of PFO, PSO, and Elovich kinetic models for phenolic pollutant adsorption onto RGO-βCD-ECH composite

Parameters	Phenol		2-Chlorophenol 2,4-Dichlorophenol		
$q_{\rm exp}$ (mg/g)	352.518	376.911	387.929		
Pseudo-first-order					
q_{cal} (mg/g)	345.134	369.247	370.101		
k_1 (/min)	0.069	0.086	0.093		
R^2	0.981	0.982	0.971		
$ARE (\%)$	2.512	2.125	4.238		
RMSE	8.315	7.852	16.237		
Pseudo-second-order					
q_{cal} (mg/g)	354.125	379.584	393.124		
$k_2 \times 10^3$ (g/mg) min)	0.241	0.309	0.394		
R^2	0.995	0.996	0.995		
ARE $(\%)$	1.352	0.709	1.081		
RMSE	4.542	2.489	3.891		

thickness, and k_{id} is the diffusion rate constant. The non-linear plots of Elovich, PFO, and PSO models are shown in Fig. [4b.](#page-8-0) The calculated and experimental values of various kinetic and statistical parameters like R^2 , RMSE, and ARE are also calculated from the non-linear plots and shown in Table [3.](#page-10-0) It is observed that PSO kinetic model is the best-ftted model for this adsorption process, which suggests that chemisorption occurs and it involves the formation of chemical bonds and electron transfer between the adsorbent and pollutant (Zhou et al. [2020\)](#page-16-12).

IPD model

To know the exact difusion mechanism in the adsorption process, the IPD model is used to identify the rate-limiting steps (Eq. [10\)](#page-10-1). Figure [4c](#page-8-0) illustrates the IPD plots of phenol, 2-CP, and 2,4-DCP, and the values of C_i and k_{id} are calculated from the plot and tabulated in supporting material Table S2. Accordingly, if the plot passes the origin, then IPD is the rate-controlling step (Kumar and Jena [2016](#page-15-22)). The result indicates that the plots do not pass through the origin and three stages of straight line, revealing that IPD and some other difusion mechanism afect the adsorption rate. The frst linear part is flm difusion, where adsorbate molecules difuse rapidly into the adsorption sites of the composite because of the availability of higher active sites. In the second part, the adsorbate molecules start difusing into the macropores, mesopore, and micropore of composite from the surface of the adsorbent; in the fnal section, IPD starts to decrease. This study confrmed that the adsorption of phenolic pollutants onto the RGO-βCD-ECH composite is controlled by both flm difusion and intra-particle difusion (Ohemeng-Boahen et al. [2021](#page-15-23)).

Boyd kinetic model

Furthermore, the exact rate-limiting steps of the process could be defned by the Boyd kinetic plot and the equation which are used are given in Eq. (10) (10) (10) (Liu et al. [2014](#page-15-24)).

$$
B_t = -0.4977 - \ln(1 - F) \tag{10}
$$

 $F = q_t/q_0$ represents the fraction of phenolic pollutant and B_t is a mathematical function of *F*. Figure [4d](#page-8-0) shows the B_t vs. *t* plot for different phenol concentrations. It is observed that all the plots have *y*-intercept and linear, suggesting flm difusion as the rate-determining step.

Adsorption thermodynamics study

The experimental data obtained from the adsorption of phenolic pollutants (phenol, 2-CP, and 2,4-DCP) for the thermodynamic analysis on RGO-βCD-ECH composite at diferent temperatures (288, 293, 298, 303, 308, and 313 K) are investigated. The thermodynamics parameters are evaluated by using Eqs. (11) (11) – (13) (Eslek Koyuncu and Okur [2021\)](#page-14-25):

$$
K_d = \rho \frac{q_e}{C_e} \tag{11}
$$

$$
\ln(K_d) = \frac{\Delta S^\circ}{R} - \frac{\Delta H^\circ}{RT} \tag{12}
$$

$$
\Delta G^{\circ} = \Delta H^{\circ} - T\Delta S^{\circ} \tag{13}
$$

where ρ is the solution density (g/L) and K_d is the adsorption coefficient and a dimensionless constant. By plotting Eqs. ([13\)](#page-10-4), it is possible to calculate the values of ΔH° and ΔS° from the Van't Hoff plot (Fig. [5a\)](#page-11-0) and the obtained ΔG° , ΔH° , and ΔS° results are presented in Table [4](#page-11-1). It has been observed that for all the temperatures, the ΔG° values are negative for all the phenolic pollutants, which illustrate the spontaneous process that occurred. The positive value of Δ*H°* confrms the endothermic nature of the process, which is already discussed in the efect of temperature. The positive ΔS° values reflect the adsorbents high affinity toward phenolic pollutants and suggest that the disorder and randomness increased at the solid–liquid interface.

Reusability study

The reusability and stability of adsorbents are the most important parameters in evaluating the performance of an adsorbent as it directly relates to the cost of the adsorbent.

Fig. 5 a Van't Hof plot and **b** regeneration study of phenolic pollutants adsorption onto RGO-βCD-ECH composite

The adsorption–desorption experiment is performed with optimal parameter conditions such as pH of solution 7, 60 min of contact time, 12.5 mg/50 mL of RGO-βCD-ECH composite dosage, and 30 °C of temperature for fve consecutive cycles. After adsorption, the exhausted RGOβCD-ECH composites are subject to regeneration by using 0.05 N HNO₃ and 0.1 M NaOH solutions as the combined eluting agents in a thermostatic shaker. After that, the regenerated adsorbents are put in an oven for drying at 60 °C for 12 h. After drying, the adsorbent is again used for the removal of pollutants with predetermined optimal conditions and this is the completion of one cycle. The same procedure follows until the completion of ffth cycle. The percentage removal of phenolic pollutants declines as cycles increase (Fig. [5b](#page-11-0)) due to the reduction of accessible active sites of the RGO-βCD-ECH composite. Furthermore, many chemical reactions occurred on the adsorbent surface after the adsorption of phenolic pollutants, resulting in the collapse in the composite pore structure. The removal percentage of phenolic compound remained at 73.98, 77.45, and 79.85%, respectively, for phenol, 2-CP, and 2,4-DCP after five cycles of regeneration. These results indicate that the synthesized RGO-βCD-ECH composite is cost-efective and can be repeatedly applied for water purifcation.

Adsorption of synthetic wastewater

In industrial effluent, various types of organic and inorganic pollutants are available which is complex in nature. A simulated wastewater is prepared using various phenolic pollutants and inorganic salts to evaluate the adsorption performance of the RGO-βCD-ECH composite. The absorption

Fig. 6 UV–Vis spectra of synthetic effluent before and after adsorption using RGO-βCD-ECH composite

spectra of simulated wastewater before and after treatment are observed by using a UV–VIS spectrophotometer, and the results are shown in Fig. [6.](#page-12-0) The operating conditions for the adsorption experiments are 60 min of contact time, solution pH 7, temperature 30 °C, concentration of phenol 100 mg/L, and 12.5 mg/50 mL of adsorbent dosage. It is observed that after treatment with RGO-βCD-ECH composite, the spectra of simulated wastewater decrease and 56.14% removal percentage is achieved as compared to a single component of phenol (88.12), 2-CP (92.85), and 2,4-DCP (96.15). This decrease in removal percentage compared to the single component occurs, as in the simulated wastewater, various types of pollutants are present. All the pollutants are trying to adsorb on the adsorbent surface during adsorption. As a result, competitions among pollutants occur, resulting in decreased adsorption performance.

Adsorption mechanism

Several literatures reported various mechanisms for the adsorptive removal of phenolic pollutants. Out of these, the three most widely accepted mechanisms are (i) interaction of $\pi-\pi$ electron pairing, (ii) hydrogen bond interactions, and (iii) electron donor–acceptor/electrostatic interaction. The presence of oxygen functional groups of composites at π-electron-rich regions provides complexes with aromatic rings of phenolic compounds. During the adsorption, the π-electron-rich regions of the composite act as a donor, and the phenol rings as acceptors. As a result, the adsorption of phenolic compounds onto the composite is controlled by the dispersive interaction of $\pi-\pi$ electrons (Mojoudi et al. [2019](#page-15-25)). Adsorption on the surface of the composite is due to the formation of H bonds between the hydrogen and oxygen from the adsorbent and phenolic molecules (Dąbrowski et al. [2005\)](#page-14-26). In addition, a host–guest inclusion complex is formed between βCD and phenolic compounds by Van der Waals forces and hydrogen bonds. As a result, more and more phenolic molecules are attracted towards the adsorbent surface, enhancing the adsorption process. As the reaction between phenolic molecules and the composite occurs on the entire surface of the composite, so the adsorbed phenolic molecules are uniformly distributed on the composite. In the adsorption of phenolic pollutants, two diferent electron donor–acceptor interaction occurs. The frst one involves the interaction of carbonyl and hydroxyl groups (electron donor) of composite with the aromatic ring of phenolic compound (electron acceptor). The second one involves the interaction between amine groups (electron donor) of composite with the aromatic ring of phenolic compound (electron acceptor). The interaction between donor and acceptor of the adsorbent and phenolic compounds during the adsorption process depends on the dipole moment of the various functional groups present on the basal plane. The schematic presentation of the adsorption mechanism of phenolic compound is shown in Scheme [1](#page-13-0).

Conclusions

The possible risk to the environment, comprising human health and aquatic resources resulting from the growing industrialization, is a real problem which needs to be addressed to remediation of phenolic compounds before it is released. This work successfully synthesized a novel composite through ECH cross-linked βCD functionalized with RGO through cross-linking reaction. The characterization study confrms the successful synthesis of our prepared composite. The batch adsorption experiments showed 88.12, 92.85, and 96.15% adsorption efficiencies for phenol, 2-CP, and 2,4-DCP, respectively, at an optimum RGO-βCD-ECH composite dosage of 0.25 g/L at pH ∼ 7 at a temperature of (298 K) and time of 60 min. Langmuir model perfectly demonstrates the experimental results and the maximum uptake are 659.475, 674.155, and 702.853 mg/g, respectively, for phenol, 2-chlorophenol, and 2,4-dichlorophenol, respectively. The kinetic data follows the pseudo-secondorder model, which suggests that chemisorption occurs in the adsorption process. The IPD model confrmed that three stages control the adsorption on the RGO-βCD-ECH composite. The thermodynamic study described that the adsorption of phenolic pollutants is an endothermic, favorable, and spontaneous process. In the adsorption study of simulated effluent, the novel adsorbent removes up to 56.14% of phenolic pollutants. These remarkable results concluded that the

Scheme 1 Schematic diagram for proposed phenolic compound removal mechanism.

synthesized RGO-βCD-ECH composite has great application prospect for phenolic contaminated wastewater.

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Author contribution Dibya Ranjan Rout: conceptualization; methodology; data analysis; writing—original draft preparation

Hara Mohan Jena: supervision; conceptualization; investigation; writing—review and editing.

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Declarations

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