

# Metal oxide-coated anodes in wastewater treatment

Anantha N. Subba Rao ·  
Venkatesha T. Venkatarangaiah

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**Abstract** Electrochemical oxidation is an effective wastewater treatment method. Metal oxide-coated substrates are commonly used as anodes in this process. This article compiles the developments in the fabrication, application, and performance of metal oxide anodes in wastewater treatment. It summarizes the preparative methods and mechanism of oxidation of organics on the metal oxide anodes. The discussion is focused on the application of SnO<sub>2</sub>, PbO<sub>2</sub>, IrO<sub>2</sub>, and RuO<sub>2</sub> metal oxide anodes and their effectiveness in wastewater treatment process.

**Keywords** Dimensionally stable anodes · Dopant · Incineration · Electrochemical oxidation · Electrocatalytic activity · Dip coating · Sol-gel

## Abbreviations

AO7	Azo dye acid orange 7
AOX	Adsorbable organohalogen
ALD	Atomic layer deposition
BDD	Boron-doped diamond
COD	Chemical oxygen demand
DCP	Dichlorophenol
DSA	Dimensionally stable anode
OA	Oxalic acid
OER	Oxygen evolution reaction
PFBA	Perfluorobutanoic acid
PFCA	Perfluorocarboxylic acid
PFDA	Perfluorodecanoic acid
PFHpA	Perfluoroheptanoic acid
PFHxA	Perfluorohexanoic acid
PFPA	Perfluoropentanoic acid
PFNA	Perfluorononanoic acid
PFOA	Perfluorooctanoic acid

RB-4	Reactive Blue 4
RO-16	Reactive Orange 16
SCE	Standard calomel electrode
SEM	Scanning electron microscopy
TOC	Total organic content
XPS	X-ray photoelectron spectroscopy

## Introduction

Dyes, toxic organic molecules, inorganic salts, adsorbable organohalogen (AOX), aromatic pesticide residues, drugs, and surfactants are the major components of wastewater released from textile, leather, pulp and paper, printing, photograph, cosmetic, pharmaceutical, and food industries (Fornazari et al. 2012; Zaviska et al. 2009). The environmental concern has led to stringent rules and it is mandatory to treat the wastewater before disposing into natural water streams. Chemical, physicochemical, biological/enzymatic, advanced oxidation processes, and electrochemical methods are commonly employed in wastewater treatment (Brungs et al. 1996; Cheng-chun and Jia-fa 2007; Guinea et al. 2009; Hou et al. 2009; Martínez-Huitle and Brillas 2009; Rosales et al. 2009). In the past few years, “electrochemical method” has drawn much attention. It is economical and easy to construct and operate. More importantly, electrodes serve as immobilized active surfaces for the oxidation of organics (Fornazari et al. 2012). In addition, unlike chemical methods, electrochemical method does not necessitate the addition of chemical reagents. However, the addition of electrolyte is inevitable if the wastewater sample is not sufficiently conducting. In many cases, the electrolyte is deliberately added to enhance the degradation process. The added electrolyte strongly influences the efficiency of the process. In exploiting this method as a powerful tool in wastewater treatment, the key part of the electrolytic system—“electrode”—acquires utmost importance.

On oxidation, the organic contaminant undergoes complete oxidation to CO<sub>2</sub> and H<sub>2</sub>O (combustion) or results in the

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A. N. Subba Rao · V. T. Venkatarangaiah (✉)  
Department of P.G. Studies and Research in Chemistry,  
School of Chemical Sciences, Kuvempu University,  
Shankaraghatta 577451, Karnataka, India  
e-mail: drtvenkatesha@yahoo.co.uk

formation of simpler fragments (conversion) (Comninellis 1994). On the other hand, reduction of organics cannot completely lower the chemical oxygen demand (COD) of the wastewater sample, but only leads to poor decontamination (Martínez-Huitle and Brillas 2009). Electrooxidation favors the effective removal of organics over electro-reduction.

Anode is the oxidation site in any electrolytic system. Long service life, large surface area, wide operating potential window between hydrogen and oxygen evolution reaction (OER) overpotentials, high catalytic activity, physically stable, resistant to corrosion, cheap, and easy to fabricate are the prerequisite properties intended to be fulfilled by the anodes employed in electrochemical wastewater treatment.

The anode materials like stainless steel, glassy carbon, Ti/RuO<sub>2</sub>, Ti/Pt-Ir, activated carbon fibers, MnO<sub>2</sub>, Pt carbon black, porous carbon and reticulated vitreous carbon, and electrodes made of lead, iron, and graphite usually undergo deformation during electrolysis (Martínez-Huitle and Ferro 2006; Rodgers et al. 1999). Beer introduced the titanium substrate-based RuO<sub>2</sub> and TiO<sub>2</sub>-coated electrode, referred as dimensionally stable anodes (DSA<sup>®</sup>s) which possessed high catalytic activity and stability (Beer 1980; Chandler et al. 1997). Figure 1 is the flow chart showing the development of DSA<sup>®</sup> and DSA<sup>®</sup>-type metal oxide electrodes (Chandler et al. 1997; Chen et al. 2001, 2002; Klamklang et al. 2012; Nikolić et al. 2012; Panić and Nikolić 2007; Trasatti 2000). The DSAs are good conductors, exhibit high catalytic activity, dimensionally stable, and contribute towards energy savings (see Table 1). They exhibit extended operating life of 8–9 years, without deformation, and their durability has been established in many fields (Chandler et al. 1997; Chen et al. 2002).

The metal oxide electrodes with stability comparable with DSA tempted several research teams to investigate their performance in the electrochemical wastewater treatment. The metal oxide electrodes prepared by Comninellis and Vercesi (RuO<sub>2</sub>, IrO<sub>2</sub>, TiO<sub>2</sub>, ZrO<sub>2</sub>, and Ta<sub>2</sub>O<sub>5</sub>) over Ta substrate exhibited high oxygen evolution overpotential. But, due to high cost of Ta, the other metal Ti was selected as the substrate, and ever since, Ti has been the favorite substrate for the fabrication of metal oxide-coated anodes. Titanium is a cheap “self-healing” substrate which anodically generates a layer of TiO<sub>2</sub> and protects itself against corrosion (Beer 1980). Moreover, the water quality is not affected by the dissolution of Ti in low concentrations (Niu et al. 2012). Ti/tin dioxide (SnO<sub>2</sub>), Ti/lead dioxide (PbO<sub>2</sub>), and platinum group metal oxide coated on valve metals (Ti, Zr, Ta, Nb, Hf, W) (DSA<sup>®</sup>s) are the exhaustively studied metal oxide electrodes.

Numerous combinations of these modified metal oxides have been fabricated and tested for their stability, catalytic activity, and ability to incinerate the organics. The ultimate goal is to fabricate an electrode which satisfies the prerequisite properties of the anode. Though few research teams have been successful in fabricating the electrodes with excellent catalytic

activity and stability, the search for the best recipe still continues! This review outlines the developments in the preparation, properties, and application of metal oxide-coated anodes in the electrochemical wastewater treatment.

### Fabrication of metal oxide anodes

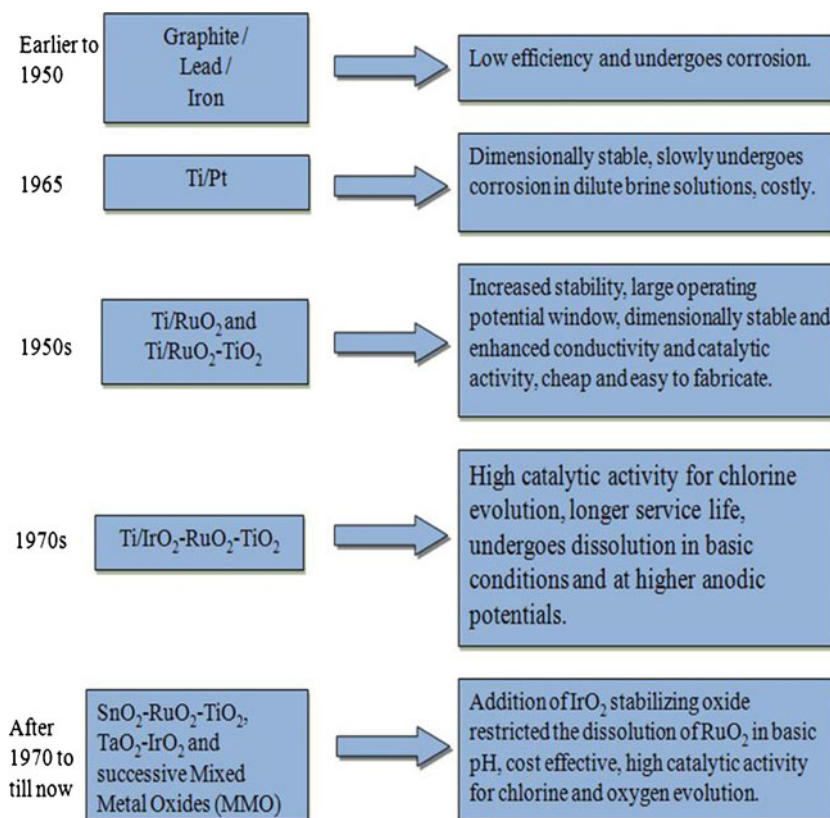
The metal oxide anodes are cheap and easy to fabricate (Gaber et al. 2012; Klamklang et al. 2012; Kusmierek et al. 2011; Yang et al. 2009). Designing and fabricating an electrode of desired composition and characteristics is a challenging task. Thin film metal oxide coatings are prepared by solution phase and gas phase chemical methods. The solution phase method involves dip coating, spin coating, painting, spray pyrolysis, and sol-gel techniques, which employ a precursor solution (Perednis and Gauckler 2005). The gas phase methods are chemical vapor deposition (CVD) and atomic layer deposition (ALD) (Perednis and Gauckler 2005). Electrochemical method (electrochemical anodization and electrochemical deposition) is also widely utilized in the preparation of metal oxide-coated electrode.

A precursor solution is generally prepared by dissolving stoichiometric quantities of metal salts in a solvent or mixture of solvents. The resultant solution is applied on the surface of a substrate using suitable coating techniques [*dip coating* (Watts et al. 2008; Yang et al. 2009), *spin coating* (Fierro and Comninellis 2010), or *painting* (del Río et al. 2009)]. The spin coating technique gives uniform coat on flat substrates. For uneven substrates, dip coating or painting is preferred. The process of coating and drying is repeated until a desired thickness of the coat is obtained. Finally, the coated substrate is annealed to obtain superior morphological characteristics and wear resistance (Comninellis and Vercesi 1991). Thermal decomposition method was adopted in the fabrication of Ti/SnO<sub>2</sub>-Sb<sub>2</sub>O<sub>3</sub> (Yang et al. 2009), Ti/TiO<sub>2</sub>-RuO<sub>2</sub> (Kusmierek et al. 2011; Fachinotti et al. 2007), and Ti/SnO<sub>2</sub>-Pt-antimony (Sb) (del Río et al. 2009) electrodes.

*Spray pyrolysis* is an aerosol process. It is relatively simple and cost effective (Lipp and Pletcher 1997; Perednis and Gauckler 2005; Vicent et al. 1998; Yusta et al. 1997). It involves the atomization of precursor and conversion of these droplets into solid particles by heating. The nature of the deposit obtained on the substrate is dependent on the transformations undergone by the droplets. The temperature gradient between the spraying nozzle and the substrate, the carrier gas and precursor solution flow velocity, and shape and nature of the substrate influence the transformations undergone by the droplets (Correa-Lozano et al. 1996a, 1997). Correa-Lozano et al. (1996a) prepared Ti/SnO<sub>2</sub>-Sb<sub>2</sub>O<sub>5</sub> electrode using spray pyrolysis technique and have thoroughly studied its characteristics (Correa-Lozano et al. 1996b, 1997).

The *sol-gel* method is also widely used in the fabrication of metal oxide anodes (Attia et al. 2002; Brinker et al. 1991;

**Fig. 1** Flow chart of development of DSA® and DSA®-type metal oxide electrodes



Choi et al. 2007; Panić et al. 2003a, b, 2010; Lu et al. 2010; Ozer et al. 1995). In this method, the microstructure of the coating depends on pH and viscosity (Ozer et al. 1995). Generally, the precursor salts are hydrolyzed by dispersing them in an appropriate media and vigorously stirred for certain ageing time. The formation of solid phase particles of the sol from hydrolyzed precursor is dependent on ageing time. Electrodes prepared at different ageing time differ in their electrochemical behavior (Panić et al. 2003a).

A uniform metal oxide coating of desired thickness can be achieved by *electrochemical* method by adjusting its operating conditions. In electrochemical anodization, a pretreated metal substrate is anodized in a suitable electrolytic bath. A layer of metal oxide coat is generated on the surface of the anodized metal. In electrochemical deposition, precursor salts

are dissolved in the electrolytic bath, which are electrodeposited on the substrate. The electrochemical method is advantageous in achieving effective doping and a uniform metal oxide coat on the substrate. Electrochemical method was adopted in the preparation of the following electrodes: Ti/SnO<sub>2</sub>-Sb<sub>2</sub>O<sub>3</sub>-Nb<sub>2</sub>O<sub>5</sub>/PbO<sub>2</sub> (Yang et al. 2009), Er-chitosan-F-PbO<sub>2</sub> (Wang et al. 2010b), C/PbO<sub>2</sub>, Pb + Sn/PbO<sub>2</sub>-SnO<sub>2</sub>, Pb/PbO<sub>2</sub> (Gaber et al. 2012), Ti/PbO<sub>2</sub> (Panizza and Cerisola 2008), Ti/SnO<sub>2</sub>-Sb<sub>2</sub>O<sub>3</sub>/PbO<sub>2</sub> (Liu and Liu 2008), Pb/PbO<sub>2</sub> (Martínez-Huitle et al. 2008), and Ti/SnO<sub>2</sub>-Sb/PbO<sub>2</sub>-Ce (Niu et al. 2012).

The gas phase techniques are also well known, but they require sophisticated instruments and are relatively costly. In CVD, generally the reactant (precursors) gases are pumped into the reaction chamber maintained at optimum temperature and pressure, where these reactive gases adsorb and react with the substrate to form a thin film. Metal organic chemical vapor deposition utilizes organometallic compounds as precursors (Amjoud et al. 1998; Duverneuil et al. 2002; Devilliers et al. 2003). The ALD technique is closely related to CVD, but the factor which distinguishes it from CVD is that the precursors are led on to the substrate alternately, one at a time (Riihelä et al. 1996). Using CVD, thin films with high uniformity can be reproduced. However, it involves complex processes, high temperature, and toxic gases. Few teams have used gas phase methods for the preparation of thin film metal oxide-coated electrodes (Watts et al. 2008; Yusta et al. 1997; Amjoud et al. 1998; Duverneuil et al. 2002). However, the earlier studies

**Table 1** Performance data of different anode materials used in chlor-alkali industry

Anode material	Chlorine overpotential (mV)	Weight loss from anode <sup>a</sup>
Graphite	≈400	2–3 kg/tonne Cl <sub>2</sub>
Platinum	≈200	0.4–0.8 g/tonne Cl <sub>2</sub>
RuO <sub>2</sub> -TiO <sub>2</sub>	≈50	<0.03 g/tonne Cl <sub>2</sub>

Adapted from the Chandler et al. (1997)

<sup>a</sup> Reaction conditions are as follows: 25 % brine at 363 K; current density, 3 kA m<sup>-2</sup>

revealed that in majority of the cases, solution method was preferred for the preparation of metal oxide electrodes. The conditions used in the fabrication of different metal oxide-coated electrodes by solution method are presented in Table 2.

### Mechanism of electrochemical oxidation of organics on metal oxide anodes

Figure 2 displays various electrochemical methods used for wastewater treatment. The electroflocculation and electrocoagulation methods produce large amount of sludge, whereas such problem is not encountered in the case of electrooxidation (Mao et al. 2008). The organics in the wastewater are converted into simple molecules and/or completely incinerated to CO<sub>2</sub> and H<sub>2</sub>O by electrochemical oxidation (Comninellis 1994). The morphology and composition of the metal oxide coating, nature of the contaminating organic molecule, and wastewater matrix influence the mechanism of oxidation of organics and hence the products (Martínez-Huitle and Ferro 2006).

#### Mechanism of oxidation

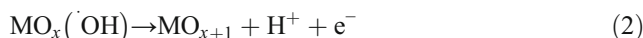
Oxidation of organics proceeds as follows:

- By direct electron exchange with the anode (direct oxidation)

- By the active species during electrolysis (indirect oxidation)

The direct exchange of electrons between the anode material and the organic molecule at the electrode solution interface is referred as “direct oxidation.” This reaction is viable at potentials well below the oxygen evolution overpotential. But the anode surface gradually undergoes passivation due to adsorption of organic molecules (Panizza and Cerisola 2009).

A theoretical model for the mechanism of oxidation of organics on metal oxide anodes was proposed by Comninellis (1994), and it has been accepted by the scientific community. During electrolysis, hydroxyl (<sup>•</sup>OH) radicals are generated on the anode surface by water discharge at high anodic potentials (Panizza and Cerisola 2009; Watts et al. 2008). These <sup>•</sup>OH radicals adsorb physically (Eq. 1) or chemically (Eq. 2) on the metal oxide anode (MO<sub>x</sub>).

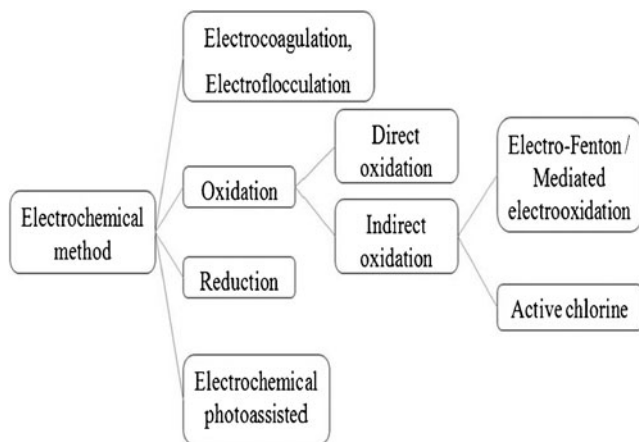


As a result of strong interaction between hydroxyl radical (<sup>•</sup>OH) with the anode metal and availability of a higher oxidation state for the anode metal leads to the formation of MO<sub>x+1</sub> (Martínez-Huitle and Ferro 2006).

**Table 2** Fabrication of metal oxide-coated anodes

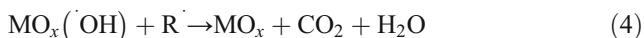
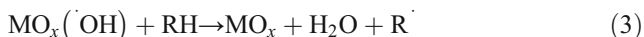
Electrode	Precursors	Solvent and coating technique	Annealing temperature (°C)	Reference
Ti/SnO <sub>2</sub> -Sb <sub>2</sub> O <sub>3</sub>	SnCl <sub>4</sub> ·5H <sub>2</sub> O + Sb <sub>2</sub> O <sub>3</sub>	Isopropanol + conc. HCl, dip coating	480	Yang et al. (2009)
Al/Sb <sub>2</sub> O <sub>5</sub>	SbCl <sub>3</sub> (1.753 g)	Isopropanol + conc. HCl (10:0.5), painting	550	Soni and Ruparelia (2012)
Fe/SnO <sub>2</sub> -Sb <sub>2</sub> O <sub>5</sub>	SnCl <sub>4</sub> ·5H <sub>2</sub> O + SbCl <sub>3</sub> (1.227 g + 0.342 g)	Isopropanol + conc. HCl (10: 0.5), painting	550	
Ti/SnO <sub>2</sub> -Sb	SnCl <sub>4</sub> ·5H <sub>2</sub> O + SbCl <sub>3</sub> Sb/(Sn + Sb)=2.9 to 20 %	Isopropanol + conc. HCl, painting	450	Mao et al. (2008)
Ti/SnO <sub>2</sub> + Sb <sub>2</sub> O <sub>5</sub>	SnCl <sub>4</sub> ·5H <sub>2</sub> O + SbCl <sub>3</sub> SnCl <sub>4</sub> ·5H <sub>2</sub> O/SbCl <sub>3</sub> =20:1 %	Isopropanol + conc. HCl, dip coating	500	Watts et al. (2008)
Ti/SnO <sub>2</sub> + Sb <sub>2</sub> O <sub>5</sub>	SnCl <sub>4</sub> ·5H <sub>2</sub> O + SbCl <sub>3</sub>	92 % isopropanol + 8 % HCl, dip coating	500	Jiang-tao et al. (2007)
Ti/SnO <sub>2</sub> -Pt-Sb	SnCl <sub>4</sub> ·5H <sub>2</sub> O + SbCl <sub>3</sub> + 2PtCl <sub>6</sub> ·6H <sub>2</sub> O Sn/Sb/Pt=10:1:0.252	Ethanol + conc. HCl, painting	600	del Río et al. (2009)
Ti/SnO <sub>2</sub> -Sb	SnCl <sub>4</sub> ·5H <sub>2</sub> O + SbCl <sub>3</sub>	Ethanol, painting	550	Costa et al. (2010)
Ti/SnO <sub>2</sub> -Sb-Ir	SnCl <sub>4</sub> ·5H <sub>2</sub> O + SbCl <sub>3</sub> + IrCl <sub>3</sub> ·xH <sub>2</sub> O Sn/Ir=9:1	Ethanol, painting	550	
Ti/SnO <sub>2</sub> -Sb <sub>2</sub> O <sub>3</sub>	SnCl <sub>4</sub> ·5H <sub>2</sub> O + SbCl <sub>3</sub> (8.5+5 g)	<i>n</i> -Butanol + HCl (40+10 mL), painting	500	Wang et al. (2010a)
Ti/SnO <sub>2</sub> -Sb-La	SnCl <sub>4</sub> ·5H <sub>2</sub> O + SbCl <sub>3</sub> Sn/Sb/La=100/6/2	Citric acid (CA) + ethylene glycol (5 mL) + ethanol (30 mL). Molar ratio of metal/CA/ethylene glycol=1:3:3, painting	550	Xu et al. (2012)
Ti/SnO <sub>2</sub> -Sb-Ru	SnCl <sub>4</sub> ·5H <sub>2</sub> O + SbCl <sub>3</sub> Sn/Sb/Ru=100/6/2		550	
Ti/SnO <sub>2</sub> -Sb	SnCl <sub>4</sub> ·5H <sub>2</sub> O + SbCl <sub>3</sub> Sn/Sb=100/6		550	





**Fig. 2** Electrochemical methods. Adapted from Martínez-Huitle and Brillas (2009)

Electrodes which can undergo such interaction are referred as “active” (carbon, graphite, IrO<sub>2</sub>, RuO<sub>2</sub>, platinum) (Panizza and Cerisola 2009). “Non-active” anodes (SnO<sub>2</sub>, PbO<sub>2</sub>, or boron-doped diamond (BDD)) only act as inert electron sink for the removal of electrons from organics, without providing any adsorptive site (Comninellis 1994; Ozer et al. 1995). Chemisorbed oxygen in MO<sub>x+1</sub>/MO<sub>x</sub> couple acts as an active site for the selective oxidation of organics (Eq. 5), whereas physisorbed ·OH radicals completely incinerate the organics into CO<sub>2</sub> and H<sub>2</sub>O (Eqs. 3 and 4) (Comninellis 1994).



The oxygen evolution reaction (Eqs. 6 and 7) always competes with the oxidation reaction of organics.

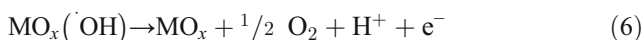


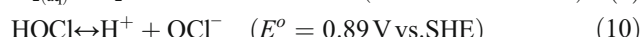
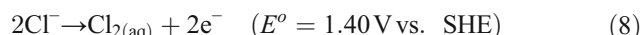
Figure 3 is the schematic diagram of electrochemical oxidation of organics on metal oxide anodes.

#### Oxidation by electrochemically generated oxidants

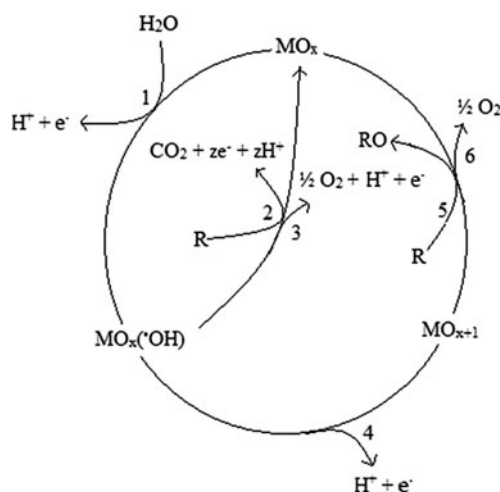
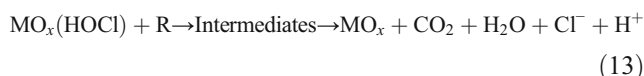
On electrolysis, species generated by the discharge of water (hydroxyl radical, hydrogen peroxide, ozone) react with themselves or with the electrolytes to produce active oxidants. These oxidants are utilized in the oxidation of organics and this type of oxidation is referred as “indirect oxidation” (Jüttner et al. 2000;

Li et al. 2009; Martínez-Huitle and Ferro 2006; Panizza et al. 2000; Scialdone 2009; Scialdone et al. 2009b; Simond et al. 1997b; Zhao et al. 2003). Mediated electrooxidation involves metal ions with high oxidation potential. In this method, oxidants are electrochemically generated in a closed cycle and can completely incinerate the organics (Jüttner et al. 2000).

Different electrolytes could be found in any industrial effluent. Chloride salts are most common. It is observed that the presence of chloride (Cl<sup>-</sup>) ions in the wastewater increases the organic removal efficiency (Comninellis 1994; Scialdone et al. 2009b). Electrochemically generated active chlorine species efficiently oxidize the organics as per Eqs. 8–11 (Jüttner et al. 2000; Martínez-Huitle and Ferro 2006; Panizza et al. 2000; Scialdone et al. 2009b).



The equilibrium in Eq. 10 is pH dependent. HOCl predominates in the pH range 3–8 and ClO<sup>-</sup> predominates above pH 8 (Fornazari et al. 2012; Malpass et al. 2012). Hence, oxidation of organics by HOCl is favorable at near neutral pH (Fornazari et al. 2012; Malpass et al. 2012). The Cl<sub>2</sub>/Cl<sup>-</sup> and HOCl/Cl<sub>2</sub> couples also oxidize the organics completely (Fornazari et al. 2012; Song et al. 2010b). The electrochemical reactions at the anode surface involving chloride ions are given in Eqs. 12 and 13 (Scialdone et al. 2009b):



**Fig. 3** Electrochemical oxidation of organics on metal oxide MO<sub>x</sub> anode. 1 Water discharge. 2 Combustion of R (organic molecule). 3 and 6 O<sub>2</sub> evolution. 4 Higher oxide formation. 5 conversion of R to RO. Adapted from Comninellis (1994) and Simond et al. (1997a).

$\text{MO}_x(\text{HOCl})$  mediates unselective oxidation and thereby provides substantial total organic carbon (TOC) removal (Fornazari et al. 2012). However, the presence of chloride ions is associated with the following disadvantages: the formation of AOX (Malpass et al. 2012; Sakalis et al. 2007) and the generation of  $\text{ClO}^-$ . AOXs are toxic and recalcitrant to degradation, and  $\text{ClO}^-$  reduces the service life of the metal oxide anode (Costa et al. 2010). Several other electrolytes like  $\text{ClO}_4^-$ ,  $\text{NO}_3^-$ ,  $\text{PO}_4^{2-}$ ,  $\text{SO}_4^{2-}$ ,  $\text{CO}_3^{2-}$ , and  $\text{Br}^-$  were tested for electrochemical degradation process (Fornazari et al. 2012; Gaber et al. 2012). But the degradation efficiency in presence of  $\text{Cl}^-$  ions was found to be better than that achieved in the presence of these electrolytes. The peroxodisulfate is a powerful oxidizing agent and as effective as hydroxyl radical (Malpass et al. 2012). Excellent degradation of organics is possible in presence of sulfate ions, provided that the electrode and the wastewater environment matrix favors the formation of sulfate radical or peroxodisulfate ion (Martínez-Huitle et al. 2008; Martínez-Huitle et al. 2008; Brillas et al. 2009). However, the COD/TOC removal not only depends on the electrode and electrolytes, but also on the organic molecule itself (Marugán et al. 2007).

### Factors influencing the anode performance

The performance of an electrode is rated in terms of its ability to incinerate the organics with minimum consumption of energy and time. The nature of the electrode, applied current density, duration of electrolysis, supporting electrolyte, pH, temperature, and cell geometry significantly contribute to the efficiency and energy consumption of the electrochemical oxidation process. The nature of the electrode is dependent on its fabrication technique, composition, and structure.

#### Fabrication technique

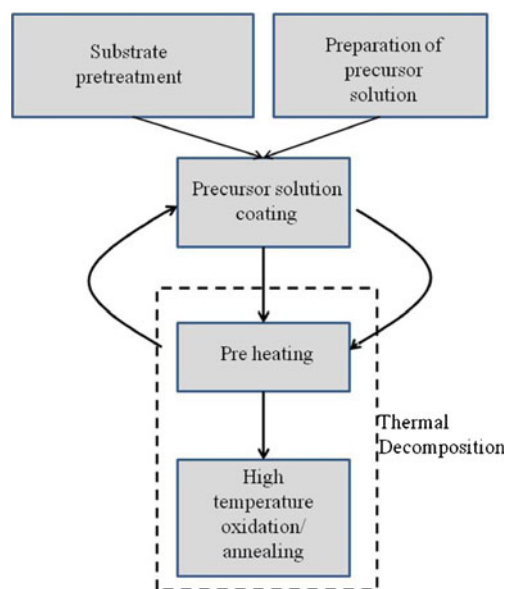
Both physical (surface morphology, metal oxide film thickness, composition, dimension, microstructure) (Wang et al. 2009) and chemical (availability of higher oxidation state, its affinity towards hydroxyl radicals, stability in different pH, active species generated in presence of different electrolytes, and wear-tear) properties of an anode influence its ability to oxidize the organics (electrochemical activity) or to generate active oxidants (electrocatalytic activity). The fabrication technique can modulate both the chemical and physical nature of the coating and hence its electrocatalytic and electrochemical activities.

Proper substrate pretreatment is the key to produce a strong adhesion of metal oxide coating on the surface of the substrate (Beer 1980). The solvents used in the precursor solution, dopant and its content, coating technique, dip withdrawal rate, and annealing temperature are crucial factors which contribute

in altering the characteristics of an anode. The schematic representation of the steps involved in the fabrication of metal oxide anodes by thermal decomposition is shown Fig. 4 (Comminellis and Guohua 2010).

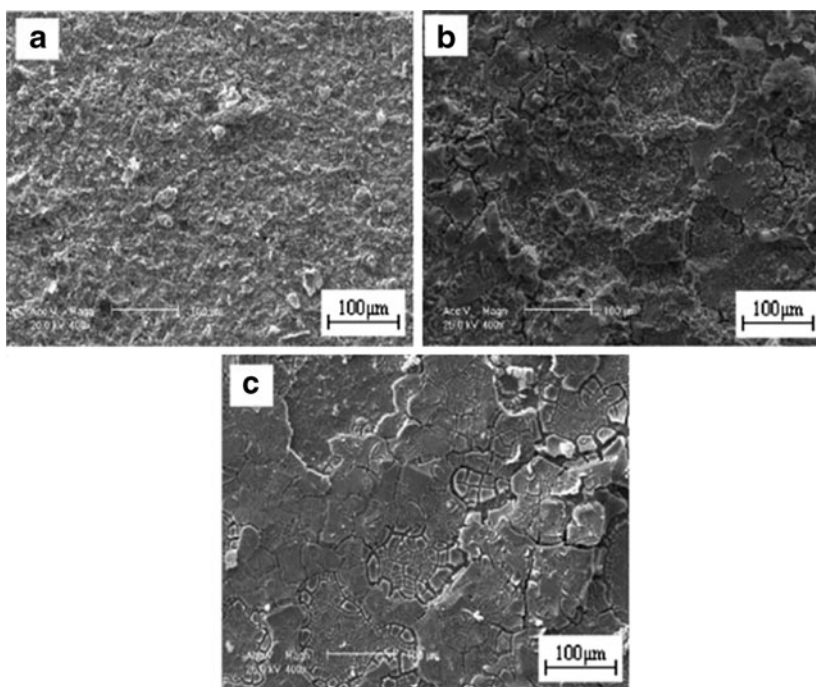
The solvents used in the preparation of precursor solution play a role of great consequence in altering the morphology and hence the characteristics associated with the morphology (exposure of catalytic and adsorptive sites, porosity, and effective surface area) of the metal oxide coating. The difference in the thermal expansion coefficient of the base metal and the coating leads to the formation of cracks in the coating and results in typical cracked mud coating (Jiang-tao et al. 2007; Wang et al. 2009). Cracked mud coating gradually undergoes erosion. The adsorption capacity is favored by the irregular electrode surface. But it involves undesired strong adsorption of hydroxyl radicals as well. Weak interaction between the electrode surface and hydroxyl radicals increases electrochemical activity of the electrode towards the oxidation of organics, whereas strong interaction results in oxygen evolution (Costa et al. 2010; Kapalka et al. 2008). The efficiency of the process decreases with oxygen evolution.

Three different precursor solutions prepared in ethanol, *n*-butanol and a polymeric precursor were used in the fabrication of  $\text{SnO}_2 + \text{Sb}_2\text{O}_3$  interlayer by thermal decomposition (Wang et al. 2009). The scanning electron microscopy (SEM) images in Fig. 5 clearly reveal the morphological differences in the oxide interlayer obtained from these precursor solutions. The oxide interlayer from the polymeric precursor assisted the structural alignment and produced more agglomerated coating, whereas alcoholic precursors produced typical cracked mud coating.



**Fig. 4** Schematic diagram of steps involved in the fabrication of metal oxide electrodes by thermal decomposition technique. Adapted from Comminellis and Guohua (2010)

**Fig. 5** SEM micrographics of SnO<sub>2</sub> + Sb<sub>2</sub>O<sub>3</sub> coatings prepared with different precursor solvents: **a** polymeric precursor, **b** ethanol, and **c** *n*-butanol. Reprinted from Wang et al. (2009). Copyright 2008 Elsevier



The nature of the precursor solution can significantly affect the host metal and dopant content in the coating. It was found that viscous precursor solutions aid in the formation of agglomerated uniform coating and accumulation of the dopant on the surface of the coating, whereas alcoholic precursor solutions lead to cracked mud coating. Precursor solution prepared in isopropanol and sol–gel was used in the fabrication of Sb–SnO<sub>2</sub>/Ti electrode by thermal decomposition. The Sn/Sb content in the coating was found to be higher than in the alcoholic precursor solution (Wang et al. 2010a; He and Mho 2004). On the contrary, the Sb content was found to be higher in the coating than in the solution when sol–gel method was adopted (Wang et al. 2006).

Antimony is the most commonly used dopant in the preparation of SnO<sub>2</sub> electrodes and it is the hydroxyl radical generation site (Jiang-tao et al. 2007). Hence, its accumulation on the surface of the coating is recommended. Variation in the Sb content considerably influences the morphology of the coating.

The electrocatalytic activity can be enhanced by minimizing the interlayer thickness and maximizing the outer active surface area by choosing the right combination of techniques in the preparation of metal oxide electrodes (Yeo et al. 2010). Different preparative methods were used in combination by Yeo et al. (2010) to obtain a compact layer of metal oxide coat. They prepared Ti/Pb(E)/PbO<sub>2</sub>(T,E) (E-electrodeposition, T-thermal decomposition) electrode by electrodepositing a layer of Pb on Ti, followed by coating a layer of PbO by thermal decomposition. The PbO was then electrooxidized to PbO<sub>2</sub>. This electrode acquired large surface area and roughness. The relative roughness factor of this electrode was found to be 8.98, where the arbitrary roughness factor of Ti/Pb(E)/PbO<sub>2</sub>

(E) electrode was set as unity. Watts et al. (2008) found that the dopant content, coating technique, and the annealing temperature are the major factors which contribute significantly in controlling the characteristics of a metal oxide coat. The effect of number of layers of the coating and dip withdrawal rate on the performance of the electrode in eliminating the organics was found to be very feeble.

#### Interfacial layer or undercoat

The oxygen which evolved at the anode surface creeps through the metal oxide coating and passivates the substrate metal. This is eliminated by the inclusion of an interfacial layer connecting the active metal oxide coating and the substrate. The chemical stability, resistance against corrosion, and service life of the anode are enhanced by the insertion of an interlayer (Kong et al. 2012). An undercoat of stable metal oxide is applied on a substrate and then an outer active layer is overlaid. It is represented as substrate/interlayer/active surface layer as shown in Fig. 6. The interlayer supports the active metal oxide layer to adhere strongly onto the substrate and helps in guarding the stability and enhancing the electrocatalytic activity of the electrode. It is important for the interlayer to be highly conducting and itself does not undergo passivation. The constituent metals of the interlayer should satisfy



**Fig. 6** Representation of multilayer metal oxide-coated substrate

the Hume-Rothery limit (15 %) between their ionic radii, so that a solid solution between the three layers is possible.

The direct deposition of  $\text{PbO}_2$  on Ti substrate by electro-deposition leads to the formation of a passive layer of  $\text{TiO}_2$  (Yang et al. 2009). This can be avoided by depositing an interlayer on Ti substrate. The interlayer acts as a barrier against such passivation of the substrate by avoiding the diffusion of oxygen. For the interlayer in Ti/solid solution interlayer/ $\text{PbO}_2$  electrode, the metals chosen by Kong et al. (2012) were such that the ratios of their corresponding ionic radii (Sn/Sb, Ru/Ti, Ir/Ta) were below the Hume-Rothery limit. Figure 7 is the SEM images of the interlayer surfaces  $\text{SnO}_2\text{-Sb}_2\text{O}_5$ ,  $\text{RuO}_2\text{-TiO}_2$ , and  $\text{IrO}_2\text{-Ta}_2\text{O}_5$  (Kong et al. 2012). The ionic radii ratio of the metals in the interlayer to  $\text{Ti}^{4+}$  obtained from the oxidation of Ti substrate also lays within the limit; hence, excellent binding was obtained between the interlayer and the substrate. Similarly, the interlayer and the electrodeposited  $\text{PbO}_2$ -active layer formed a continuous solid solution, except in the case of  $\text{RuO}_2\text{-TiO}_2$  interlayer, which provided only partial solid solution with the  $\text{PbO}_2$  due to large difference in the ionic radii of  $\text{Ti}^{4+}$  and  $\text{Pb}^{4+}$ . The interlayer enhanced the orientation of the crystal structure of the electrodeposited  $\text{PbO}_2$ .  $\text{Ti/IrO}_2\text{-Ta}_2\text{O}_5/\text{PbO}_2$  electrode coating showed high catalytic activity for oxygen evolution. The inclusion of  $\text{IrO}_2\text{-Ta}_2\text{O}_5$  interlayer in  $\text{Ti/PbO}_2$  electrode increased its service life from 11 to 672 h as determined by the accelerated lifetime test in 1 M  $\text{H}_2\text{SO}_4$  under galvanostatic

condition ( $4 \text{ A cm}^{-2}$ ).  $\text{RuO}_2\text{-TiO}_2$  and  $\text{SnO}_2\text{-Sb}_2\text{O}_5$  interlayers showed intermediate enhancement in service life of 207 and 58 h, respectively. The interlayer effectively eliminated the passivation of Ti substrate and enhanced the performance of the anode towards oxidation of organics. Similar results were obtained from the electrodes with interlayers of different composition (see Tables 2, 3, and 4).

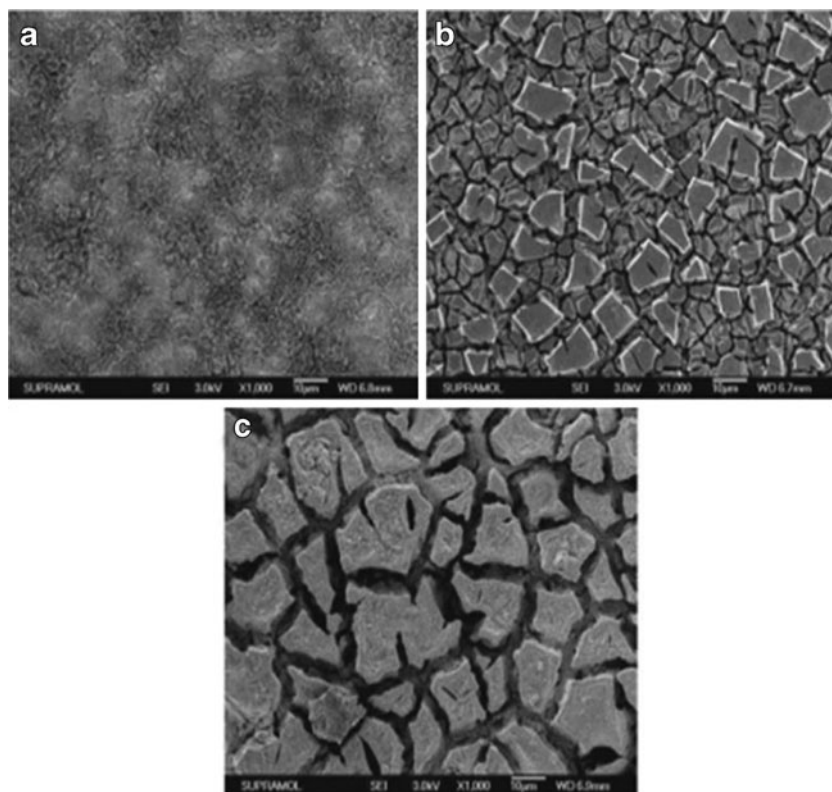
### Metal oxides in wastewater treatment

Several mixed metal oxide electrodes have been used in the electrochemical wastewater treatment. Nevertheless, it is found from the literature that majority of these are the derivatives of four metal oxides,  $\text{SnO}_2$ ,  $\text{PbO}_2$ ,  $\text{RuO}_2$ , and  $\text{IrO}_2$ , and hence we limit our discussion to these metal oxide electrodes.

#### $\text{SnO}_2$

Tin oxide is an insulator in its stoichiometric form. The distortions created by the oxygen vacancies make it an n-type and conductive material. Doped  $\text{SnO}_2$  anodes (non-active) show excellent conductivity, high oxygen and chlorine evolution overpotential, electrocatalytic activity for the oxidation of organic compounds, ability to adhere strongly to the base metal, and stability over a large pH range (Correa-Lozano et al. 1997; del Río et al. 2009; Jiang-tao et al. 2007;

**Fig. 7** SEM images of the interlayer surface. **a**  $\text{Ti/SnO}_2\text{-Sb}_2\text{O}_5$ . **b**  $\text{Ti/RuO}_2\text{-TiO}_2$ . **c**  $\text{Ti/IrO}_2\text{-Ta}_2\text{O}_5$ . Reprinted from Kong et al. (2012). Copyright 2012 Springer Science + Business Media B.V.





**Table 3** Performance of different modified SnO<sub>2</sub> anodes and working conditions

Pollutant	Electrode, ASL, ACS	Operating conditions	% COD, TOC removal, %CE, TEC	Remarks	Reference
Synthetic tannery wastewater	1. Ti/SnO <sub>2</sub> -Sb	SE=0.1 mol L <sup>-1</sup> Na <sub>2</sub> SO <sub>4</sub> , 4 h, <i>j</i> =25	TOC=56.100 %CE=65.000 TEC=0.104	%CE decreased with time Complete electrode Deactivation reached after 4 h	Costa et al. (2010)
	1. Ti/SnO <sub>2</sub> -Sb-Ir	SE=0.1 mol L <sup>-1</sup> Na <sub>2</sub> SO <sub>4</sub> , 4 h, <i>j</i> =25	TOC=2.100 %CE=2.000 TEC=2.547	Ir doping made no enhancement in TOC removal, but stability of the electrode increased	
	1. Ti/SnO <sub>2</sub> -Sb ASL=28.5 ACS=12.0	IC, 500 mg L <sup>-1</sup> (100 mL) SE=0.1 M Na <sub>2</sub> SO <sub>4</sub> , 2.5 h, <i>j</i> =30	COD=60.200 %CE=28.290	ASL test conditions: 1 M H <sub>2</sub> SO <sub>4</sub> , 40 °C, stainless steel cathode, <i>j</i> =2 A cm <sup>-2</sup> . Doping with Ru and La substantially increased the service life, crystallite size, conductivity, and surface charge density of Ti/SnO <sub>2</sub> -Sb	Xu et al. (2012)
Phenol	2. Ti/SnO <sub>2</sub> -Sb-Ru ASL=34.0 ACS=9.7		COD=82.100 %CE=38.630		
	3. Ti/SnO <sub>2</sub> -Sb-La ASL=35.5 ACS=8.6		COD=86.400 %CE=40.650		
	1. Ti/SnO <sub>2</sub>	IC=50 mg L <sup>-1</sup> (100 mL), SE: Na <sub>2</sub> SO <sub>4</sub> , <i>j</i> =10, 20, 30; pH=2 IC=100 mg L <sup>-1</sup> (200 mL), 2 h; SE, 1.4 g L <sup>-1</sup>	–	Electrooxidation at all applied current densities was slow	Martínez-Huitle et al. (2008)
PFOA	1. Ti/SnO <sub>2</sub> -Sb-Bi ASL=0.8 h		PFOA removal ratio=89.8	ASL conditions: <i>j</i> =100 mA cm <sup>-2</sup> , 0.5 M H <sub>2</sub> SO <sub>4</sub> until cell potential reached 5 V from initial value	Zhuo et al. (2011)
	2. Ti/SnO <sub>2</sub> -Sb ASL=0.4 h		PFOA removal ratio=93.3		

*IC* initial concentration of the pollutant, *SE* supporting electrolyte, *j* current density (in milliamperes per square centimeter), %*CE* percentage current efficiency, *TEC* total energy consumed (in kilowatt-hours per cubic meter), *ASL* accelerated service life in hours, *ACS* average crystallite size (in nanometers)

**Table 4** Performance of different modified PbO<sub>2</sub> anodes and working conditions

Pollutant	Electrode	Operating conditions	% COD and TOC removal, %CE, TEC	Remarks	Reference
Phenol	Ti/PbO <sub>2</sub>			OER=1.8–2.0 V	Kapalka et al. (2008)
	1. Ti/SnO <sub>2</sub> -Sb <sub>2</sub> O <sub>3</sub> -Nb <sub>2</sub> O <sub>5</sub> /PbO <sub>2</sub> AGS 6 μm	IC=0.5 g L <sup>-1</sup> (50 mL); SE=Na <sub>2</sub> SO <sub>4</sub> (7.5 g L <sup>-1</sup> )	COD=78.6	OER=1.8 V (vs SCE), condition=7.4 g L <sup>-1</sup> Na <sub>2</sub> SO <sub>4</sub> , pH 7. No metal dissolution occurred	Yang et al. (2009)
		120 min, <i>j</i> =20, SE: NaCl (21.3 g L <sup>-1</sup> )	COD=97.2	The addition of chloride ions evidently enhanced the COD removal due to the generation of active chlorine species	
Phenol	1. Ti/SnO <sub>2</sub> + Sb <sub>2</sub> O <sub>3</sub> /PbO <sub>2</sub> ASL=29.5	IC=200 mg L <sup>-1</sup> (80 mL), 3 h SE, Na <sub>2</sub> SO <sub>4</sub> , <i>j</i> =15	COD=59.3, instantaneous %CE=45	ASL test conditions: 1 M H <sub>2</sub> SO <sub>4</sub> , 60 °C, Cu cathode, <i>j</i> =4 A cm <sup>-2</sup> , until cell potential reached 5 V from initial value.	Wang et al. (2009)
	2. Ti/SnO <sub>2</sub> + Sb <sub>2</sub> O <sub>3</sub> /MnO <sub>x</sub> ASL=39.2		COD=45.7, instantaneous %CE<20	Electrochemical activity for the oxidation of phenol is in the order 1 > 2 > 3. The solvent used in the preparation of precursor solution affected the service life of the electrodes	
	3. Ti/SnO <sub>2</sub> + Sb <sub>2</sub> O <sub>3</sub> /RuO <sub>2</sub> + PbO <sub>2</sub> ASL=8.4		COD=37.9, instantaneous %CE<20		
Real wastewater sample containing Reactive Yellow 160	1. Pb + Sn/PbO <sub>2</sub> + SnO <sub>2</sub>	IC=100 mg L <sup>-1</sup> , SE: NaCl (4 g L <sup>-1</sup> ), pH=7.13, <i>j</i> =50 380 min	COD=100	The effect of NaCl, KCl, CaCl <sub>2</sub> , Na <sub>2</sub> CO <sub>3</sub> , NaF, Na <sub>3</sub> PO <sub>4</sub> , and Na <sub>2</sub> SO <sub>4</sub> supporting electrolytes was investigated. Best results were obtained in presence of chloride ions	Gaber et al. (2012)
Alphazurine dye	2. C/PbO <sub>2</sub>	300 min			
	3. Pb/PbO <sub>2</sub>	400 min			
	1. Pb/PbO <sub>2</sub>	IC=500 mg L <sup>-1</sup> , SE: Na <sub>2</sub> SO <sub>4</sub> ; <i>j</i> =30 and 60 180 mL, 20 °C 2 h, <i>j</i> =10	COD=90, %CE=24, TEC=124	Consumed high energy for the complete incineration of the dye. OER=1.8 V (vs SCE)	Nava et al. (2008)
2,4-Dichlorophenol (2,4-DCP)	1. Ti/SnO <sub>2</sub> -Sb <sub>2</sub> O <sub>3</sub> /F-PbO <sub>2</sub> AGS=5 μm		COD=71	All 3 electrodes showed good stability against deterioration and passivation. Er doping reduced the grain size and enhanced the degradation and mineralization of 2,4-DCP in the order 3 > 2 > 1	Wang et al. (2010b)
	2. Ti/SnO <sub>2</sub> -Sb <sub>2</sub> O <sub>3</sub> /Er-F-PbO <sub>2</sub>		COD=88, TOC=44	Mineralization rate increased with the flow rate. Performance of PbO <sub>2</sub> was compared with BDD. PbO <sub>2</sub> consumed same energy as BDD, but the rate of mineralization was slow	Panizza and Cerisola (2008)
	3. Ti/SnO <sub>2</sub> -Sb <sub>2</sub> O <sub>3</sub> /Er-chitosan-F-PbO <sub>2</sub>		COD=95, TOC=53	OER determined in 0.5 M H <sub>2</sub> SO <sub>4</sub> solution. 1. OER=1.6 V (vs SCE), <i>k</i> =0.0738/min; 2. OER=1.75 V (vs SCE), <i>k</i> =0.0988/min, highest electrocatalytic activity, porous, compact, and smallest crystallite size. 3. OER 1.55 V (vs SCE),	Liu and Liu (2008)
Methyl Red	1. Ti/PbO <sub>2</sub>	IC=100 mg L <sup>-1</sup> ; current=0.5; FR=240 L h <sup>-1</sup> (varied from 100 to 240 L h <sup>-1</sup> )	COD=90, %CE-decreased with increasing <i>j</i> . TEC=48		
<i>o</i> -Nitrophenol (k-pseudo-first-order rate constant for the oxidation of <i>o</i> -nitrophenol)	1. Ti/β-PbO <sub>2</sub> ACS=27.929	IC=50 mg L <sup>-1</sup> (300 mL), SE: Na <sub>2</sub> SO <sub>4</sub> + NaCl, <i>j</i> =30	COD=77.8, %CE=28.14		
	2. Ti/Bi-PbO <sub>2</sub> ACS=17.491		COD=87, %CE=31.49		
	3. Ti/Co-PbO <sub>2</sub> ACS=27.057		COD=75.9, %CE=27.47		

Table 4 (continued)

Pollutant	Electrode	Operating conditions	% COD and TOC removal, %CE, TEC	Remarks	Reference
	1. Ti/Bi-Co-PbO <sub>2</sub> ACS- 19.467		COD=83.3, %CE=30.15	$k=0.0716/\text{min}$ , crystalline size decreased on doping. 4. OER 1.70 V (vs SCE), $k=0.0411/\text{min}$ . Bi is more effective as dopant than Co. It increased the stability of undoped PbO <sub>2</sub> anode	Martinez-Huitle et al. (2008)
Methamidiphos (O,S-dimethyl phosphoramidothioate) (MMD)	1. Pb/PbO <sub>2</sub>	IC=50 mg L <sup>-1</sup> (100 mL), SE: Na <sub>2</sub> SO <sub>4</sub> , $j=30$	TOC=85 %	Eighty-five percent mineralization was achieved under $j=10$ and 20 mA cm <sup>-2</sup> . COD removal efficiency reached maximum at $j k=30$ , pH=2	
Reactive Orange 16	1. Ti-Pt/ $\beta$ -PbO <sub>2</sub>	IC=85 mg L <sup>-1</sup> in 0.1 M Na <sub>2</sub> SO <sub>4</sub> , FR=7 L min <sup>-1</sup> , SE=50 mM NaCl, $j=50$		NaCl addition improved the performance by 90 %; 85 % mineralization was achieved with 2.0 A h L <sup>-1</sup> charge supply. CE=16.7 % with 1.0 A h L <sup>-1</sup> charge supply	Andrade et al. (2009)
4-Chloro-3-methylphenol (CMP)	1. Ti/SnO <sub>2</sub> -Sb/PbO <sub>2</sub> ASL- 175	IC=0.70 mM (80 mL); SE=0.25 M Na <sub>2</sub> SO <sub>4</sub> , $j=10$	49 (TOC) instantaneous %CE-initial=20 (for 1 h)	ASL conditions: $j=1.2$ A cm <sup>-2</sup> , 9 M H <sub>2</sub> SO <sub>4</sub> , 90 °C until cell potential reached 5 V from initial value. Addition of NaCl significantly increased the CMP removal. %CE decreased with time	Song et al. (2010a)
Car wash wastewater	1. Ti/PbO <sub>2</sub>	FR=300 L h <sup>-1</sup> 10 h, $j=10$	COD=97 (at 25 °C), COD=99 (at 40 °C), $j=3$ , A TEC=770	Temperature variation made small influence on COD removal. Small increase in COD removal with flow rate. TEC for BDD=375 kWh m <sup>-3</sup>	Panizza and Cerisola (2010)
Methyl green	1. Ti/PbO <sub>2</sub>	IC=300 mg L <sup>-1</sup> 0.5 M H <sub>2</sub> SO <sub>4</sub> , $j=10-40$	TOC=40 (25 °C), 60 (40 °C), 82 (60 °C); PCE=70, TEC=0.289 ( $j=10$ ) 1.637 ( $j=40$ )	Color removal rate increased with temperature and applied current density	Carvalho et al. (2011)
Sulfamethoxazole (SMX)	1. Ti/SnO <sub>2</sub> -Sb/Ce-PbO <sub>2</sub>	IC=100 mg L <sup>-1</sup> , pH 3, distance between electrodes=3 mm, $j=5-10$	99 % SMX removal	Time required was 32.9–23.0 min, and energy consumed was 26.3–46.3 Wh L <sup>-1</sup>	Lin et al. (2013b)
PFBA	1. Ti/SnO <sub>2</sub> -Sb/PbO <sub>2</sub> -Ce	IC=100 mg L <sup>-1</sup> , SE=10 mM L <sup>-1</sup> NaClO <sub>4</sub> 90 min, $j=20$	TOC=15.6±1.8 TOC=29.1±2.3 TOC=65.9±3.1 TOC=89.4±3.8 TOC=91.7±3.6	The dissolution of Pb was well within the drinking water ordinance limit. Complete mineralization of PFCA claimed to be possible on this electrode	Niu et al. (2012)

IC initial concentration of the pollutant, SE supporting electrolyte, j current density (in milliamperes per square centimeter), FR electrolyte flow rate in case of recirculation batch systems, \*PCE percentage current efficiency, TEC total energy consumed (in kilowatt-hours per cubic meter), ACS average grain size (in nanometer), AGS average crystallite size, PFHxA perfluorhexanoic acid, PFHpA perfluoroheptanoic acid

Lipp and Pletcher 1997; Vicent et al. 1998; Xu et al. 2012; Yusta et al. 1997). The deviation in the native defects, nature, and effect of doping into the crystal lattice influences the activity of  $\text{SnO}_2$ . The oxygen vacant sites are responsible for the conductivity of  $\text{SnO}_2$  and also the availability of these vacant sites determines the ratio of  $\text{MO}_{x+1}$  and  $\text{MO}(\cdot\text{OH})$  on the anode surface. If the crystal defect increases with the formation of more of oxygen vacant sites, the formation of  $\text{MO}_{x+1}$  is favored. The physically adsorbed hydroxyl radical reacts chemically to fill the vacant sites of the crystal lattice to form  $\text{MO}_{x+1}$ .  $\text{MO}_{x+1}$  favors only the conversion of organics into oxidized intermediates, whereas  $\text{MO}(\cdot\text{OH})$  completely incinerates the organics into  $\text{CO}_2$  and  $\text{H}_2\text{O}$  (Feng et al. 2008). The electrocatalytic activity of  $\text{Ti}/\text{SnO}_2$  electrode is higher than that of  $\text{PbO}_2$  and  $\text{RuO}_2/\text{IrO}_2$  electrodes (Radjenovic et al. 2011; Mao et al. 2008). Moreover, it is comparatively cheaper than the noble metal oxide electrodes and easy to fabricate (Mao et al. 2008).

The empty electron orbitals available on the *f*-block elements can be used as channels for electron transaction from the substrates, if doped into metal oxide coating (Fenga and Li 2003). Electrocatalytic activity of the electrodes for the oxidation of organics markedly improves on doping (Fenga and Li 2003). The dopant and its molar ratio with the host metal oxide influence the physicochemical properties of the electrode. Among the various dopants (B, Bi, Ce, F, Fe, Gd, Ir, La, Ni, Pt, Ru, and Sb) used to enhance the characteristics of the  $\text{SnO}_2$ , Sb has shown remarkable impact (Jiang-tao et al. 2007; Costa et al. 2010). Sn and Sb ionic radii satisfy the Hume-Rothery limit, and hence, a homogeneous solid solution between the two metals is possible. A list of modified  $\text{SnO}_2$  electrodes and conditions used in their fabrication is given in Table 2.

The content of the dopant has a critical role to play in directing the microcrystalline structure, morphology, electrocatalytic activity, and capability of generation of hydroxyl radicals and hence the oxidation of organics.  $\text{Ti}/\text{SnO}_2$ -Sb electrode possesses high OER potential which varies with the composition of Sn/Sb ratio. For the electrodes prepared with varying concentrations of Sb, OER showed potential greater than 1.9 V (vs standard calomel electrode (SCE)) in all the cases and it increased with an increase in Sb content (Mao et al. 2008). The highest catalytic activity was found with 8 mol % [ $\text{SnO}_2$ -Sb(0.08)] and generated high concentration of oxidants.

The competition between the oxidation reaction and the OER resulted in low efficiency of  $\text{Ru}_{0.7}\text{Ir}_{0.3}\text{O}_2$  anode to degrade  $\beta$ -blocker metoprolol and led to the persistence of halogenated derivatives, whereas on  $\text{SnO}_2$ -Sb electrode, the production of hydroxyl radical was sufficient enough to degrade the metoprolol into simpler intermediates (Radjenovic et al. 2011).

Jiang-tao et al. (2007) doped  $\text{SnO}_2$  with 5, 10, and 15 % of Sb and used these electrodes in the electrooxidation of 4-

chlorophenol. The oxygen evolution potential for  $\text{Ti}/\text{Sb}-\text{SnO}_2$  with 5 % Sb electrode skipped from 1.5 V (without Sb) to 1.65 V. The oxidizable species in this potential window are oxidized directly on the anode surface. COD removal (48.9 %) of 4-chlorophenol with 15 % current efficiency was obtained on 5 % Sb-doped electrode, whereas for 0, 10, and 15 %, Sb dopant the COD removal was 36.4, 44.8, and 26.6 %, respectively. However, it has also been reported in both cases (Mao et al. 2008; Jiang-tao et al. 2007) that effective and homogeneous distribution of Sb diminished with an increase in Sb content. This was attributed to the difference in the thermal expansion coefficients. This effect is not so strong at lower Sb contents, but at higher content of Sb, the variation in the surface morphology is clearly noticeable. On using high content of dopant, the electrode follows conversion mechanism, due to selective oxidation by the chemisorbed oxygen, as discussed earlier (Kong et al. 2012). At low content of dopant (Sb centers are sites for hydroxyl radical generation), physisorbed hydroxyl radicals are involved in the oxidation leading to complete combustion of the organics. The inhomogeneous distribution of Sb reduces the catalytic activity, and the base metal gets exposed to the electrolytic bath solution leading to its passivation. The dopant not only influences the morphology of the oxide coating, but also controls the mechanism of oxidation of organics on the anode surface. Hence, it is important to choose the right dopant and monitor its content very carefully during the fabrication of an electrode.

Gd (2 mol %)-doped  $\text{SnO}_2$ -Sb possesses low oxygen vacancies in the crystal lattice of  $\text{SnO}_2$  than undoped  $\text{SnO}_2$ -Sb (Feng et al. 2008). Lower oxygen vacancies enhance the production of hydroxyl radicals on the surface of the electrode and hence the oxidizing ability. Gd covered the electrode surface with an increase in its content and reduced the availability of Sb (Feng et al. 2008). It is worth noting that not only the dopant, but also its content substantially influences the performance of an electrode.

Other dopants like La and Ru are also advantageous in modifying the characteristics of an electrode. On doping  $\text{SnO}_2$ -Sb with La and Ru, distortion effects led to the hindrance in the crystal growth and the crystallite size was reduced (Xu et al. 2012). The smaller crystallite size not only increases the surface area, but also increases the number of active sites on the surface of the anode. XPS measurements of this electrode revealed two different oxygen 1s peaks, one with lower binding energy (BE) component of 530.08–530.36 eV (assigned to lattice oxygen  $\text{O}_{\text{lat}}$ ) incorporated into  $\text{SnO}_2$  lattice and the other higher BE component of 531.86–531.89 eV (assigned to adsorbed oxygen  $\text{O}_{\text{ads}}$ ) is of the weakly bonded oxygen species. The adsorbed oxygen is very reactive towards the oxidation of organics. The  $\text{O}_{\text{ads}}$  content on the surface of  $\text{Ti}/\text{SnO}_2$ -Sb-La was found to be the highest (41.78 %), followed by  $\text{Ti}/\text{SnO}_2$ -Sb-Ru (39.42 %) and  $\text{Ti}/\text{SnO}_2$ -Sb (29.13 %) electrodes. Evidently, the addition of La



and Ru as dopants substantially enhanced the performance of the Ti/SnO<sub>2</sub>-Sb electrode in terms of COD removal and current efficiency (see Table 3).

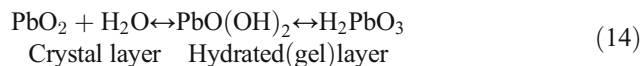
Zhuo et al. (2011) reported that the service of Ti/SnO<sub>2</sub>-Sb electrode doubled on doping with Bi. The degradation of perfluorooctanoic acid (PFOA) was successfully achieved (~90 %) on both Ti/SnO<sub>2</sub>-Sb and Ti/SnO<sub>2</sub>-Sb-Bi. Liu et al. (2013) have recently shown that the OER potential for the carbon nanotube (CNTs) coated with SnO<sub>2</sub> nanoparticles is higher than that of bulk SnO<sub>2</sub>. A comparison was made between SnO<sub>2</sub> (TO-CNT), SnO<sub>2</sub>-Sb (ATO-CNT), and SnO<sub>2</sub>-Bi nanoparticle-coated CNT (BTO-CNT) for the electrochemical filtration of oxalate. SnO<sub>2</sub>-Bi/CNT showed 1.5 to 3.5 times greater current efficiency and 4 to 5 times lesser energy consumption as compared to bare CNT for the electrooxidative filtration of ethanol, methanol, formaldehyde, and formate. Also, BTO-CNT showed higher OER potential and TOC removal as compared to ATO-CNT, suggesting that Bi can be an alternative for Sb. However, Lin et al. (2013a) reported that the Ti/SnO<sub>2</sub>-Sb-Ce electrode yielded lower perfluorocarboxylic acid (PFCA) (perfluorononanoic acid (PFNA) and perfluorodecanoic acid (PFDA)) removal and observed secondary products of Sb due to the dissolution.

Modifications in the composition of SnO<sub>2</sub> electrode fabrication and investigation of their performance in the wastewater treatment are summarized in Table 3. The conditions used in the electrochemical wastewater treatment process, maximum COD/TOC removal achieved, and percent current efficiency have been summarized in this table. As mentioned earlier, the extent of degradation of an organic molecule is dependent on its chemical nature, structure, and stability. The data in Table 3 is helpful in selecting a particular electrode for the degradation of different organic pollutant and vice versa.

### PbO<sub>2</sub>

Generally, there are two kinds of PbO<sub>2</sub>. Orthorhombic α-PbO<sub>2</sub> (brown color) and tetragonal β-PbO<sub>2</sub> (black color), where β-PbO<sub>2</sub> is a disordered close packed structure, possessing comparatively higher conductivity and higher overpotential for oxygen evolution are highly preferred (Abaci et al. 2005; Aquino et al. 2010; Gaber et al. 2012; Li et al. 2011; Yang et al. 2009; Zhoua and He 2008). β-PbO<sub>2</sub> is a non-active anode, highly conducting, chemically inert, cheaper than noble metals, and possesses high oxygen evolution overpotential and high catalytic activity for the production of oxidants. Direct oxidation of organics on the surface of PbO<sub>2</sub> anode is allowed (Fenga and Li 2003; Liu and Liu 2008; Yang et al. 2009). Thermal decomposition, electrodeposition (both in acidic and alkali media), and electrooxidation (anodization) are the techniques commonly employed in the fabrication of PbO<sub>2</sub> electrodes (Fenga and Li 2003; Liu and Liu 2008; Martínez-Huitle et al. 2008; Niu et al. 2012; Panizza and

Cerisola 2008; Panizza and Cerisola 2009; Sala and Gutiérrez-Bouzán 2012; Soloman et al. 2009; Yang et al. 2009). Liu et al. (2009) have been able to fabricate both kinds of PbO<sub>2</sub> coat on Ti substrate. Pavlov (1992) carried out detailed work on the PbO<sub>2</sub> electrodes and proposed a complex mechanism of formation of hydroxyl radicals on the surface of lead dioxide anodes. A gel-crystal system was suggested which follows the equilibrium shown below (Liu et al. 2009; Pavlov 1992):



Precisely, according to Pavlov, in the gel zone, the hydrated PbO<sub>2</sub> forms linear polymer chains which allow the electron hopping from one Pb<sup>4+</sup> ion to the other along the chain and from one polymer chain to the other, which accounts for its conductivity. The crystal zone is made up of PbO<sub>2</sub> and allows electrical conductivity. There exists certain number of active centers on the surface of the PbO<sub>2</sub> crystal layer. The hydroxide ions in the solution give out the electrons to these active centers which lead to the formation of hydroxyl radicals and create a weak interactive bond with the active centers. These hydroxyl radicals are utilized in the oxidation of organics (Liu et al. 2009).

PbO<sub>2</sub> as itself has been used in the electrochemical treatment of wastewater and also in its doped form. On adding suitable dopant, PbO<sub>2</sub> exhibits exceptional electrochemical properties. Ni, Bi, Co, Er, and Ce are the most commonly used dopants (Yang et al. 2009; Liu and Liu 2008; Liu et al. 2009; Niu et al. 2012; Wang et al. 2010b). Niobium-doped PbO<sub>2</sub> has showed excellent hydrophilicity and conductivity due to the improvement in its microcrystal structure (Yang et al. 2009). It has also been reported that doping roughened the thin film surface and increased the effective surface area for the generation of hydroxyl radicals (Yang et al. 2009). The effect of bismuth and cobalt as dopants in the fabrication of PbO<sub>2</sub> by electrodeposition was studied by Liu et al. (2009) and Liu and Liu (2008). This electrode was used in the degradation of nitrophenols. The addition of bismuth into the PbO<sub>2</sub> matrix remarkably decreased the crystallite size of the deposit and improved its electrocatalytic activity. Out of Ti/β-PbO<sub>2</sub>, Ti/Bi-PbO<sub>2</sub>, Ti/Co-PbO<sub>2</sub>, Ti/Bi-Co-PbO<sub>2</sub> electrodes, the morphology of Ti/Bi-PbO<sub>2</sub> was found to be compact and porous with small crystallite size. This was attributed to the variations caused by the formation of Bi<sub>2</sub>O<sub>5</sub> in the nucleation and crystal growth of the film (Liu and Liu 2008; Liu et al. 2009). In addition, this anode showed the highest oxygen evolution overpotential of 1.75 V (vs. SCE) and stability. Ti/Bi-PbO<sub>2</sub> and Ti/Bi-Co-PbO<sub>2</sub> favored the generation of hydrogen peroxide and hypochlorite ion. In contrast, no effect on the PbO<sub>2</sub> crystallite size was found by doping cobalt. Ti/Bi-PbO<sub>2</sub> showed the highest electrocatalytic activity

for the generation of  $\cdot\text{OH}$ . Obviously, the COD removal was maximum in the case of Ti/Bi-PbO<sub>2</sub>. Though Ti/Bi-Co-PbO<sub>2</sub> exhibited smallest removal rates, its current efficiency was higher than Ti/ $\beta$ -PbO<sub>2</sub> and Ti/Co-PbO<sub>2</sub>. Thus, Bi doping into the PbO<sub>2</sub> matrix dramatically improves its characteristics, but Co doping does not make any such differences.

Similar influence of doping was observed when Er was used as dopant. The Er doping into F-PbO<sub>2</sub> improved the electrocatalytic activity and produced compact coating with decreased crystallite size. Wang et al. (2010b) prepared erbium-doped chitosan-F-PbO<sub>2</sub> electrode and compared it with the electrode without Er doping and without chitosan for the degradation of 2,4-dichlorophenol (2,4-DCP). Maximum 2,4-DCP removal was achieved on the electrode obtained from 10 mM Er electroplating solution. The order of 2,4-DCP removal on different electrodes was found to be Ti/SnO<sub>2</sub>-Sb<sub>2</sub>O<sub>3</sub>/Er-chitosan-F-PbO<sub>2</sub> > Ti/SnO<sub>2</sub>-Sb<sub>2</sub>O<sub>3</sub>/Er-F-PbO<sub>2</sub> > Ti/SnO<sub>2</sub>-Sb<sub>2</sub>O<sub>3</sub>/F-PbO<sub>2</sub>.

PbO<sub>2</sub> was electrodeposited on Ti/SnO<sub>2</sub>-Sb(0.08) (8 mol % of Sb) interlayer using different concentrations of NaF in the electrodeposition bath solution (Mao et al. 2008). The NaF concentration not only affected the stability of PbO<sub>2</sub>, but also the morphology of the PbO<sub>2</sub> deposit. Without the addition of NaF, the PbO<sub>2</sub> coat obtained consisted irregular crystallite size and shape with dents of varying sizes on the surface. As the concentration of NaF increased, a more compact coat of PbO<sub>2</sub> was obtained. Only 55 % color removal of the substrate AO7 was achieved on PbO<sub>2</sub>-F (0.75) electrode, whereas PbO<sub>2</sub>-F (0) showed 94 % removal for the same time period. This was attributed to more compact and uniform deposition which resulted with the inclusion of NaF. The higher color removal in case of PbO<sub>2</sub>-F (0.75) electrode is due to the rough surface area which facilitated the adsorption of dye. With 0.1 g L<sup>-1</sup> of NaF (PbO<sub>2</sub>-F (0.1)), the PbO<sub>2</sub> coat obtained was most stable to anodic dissolution in 1 M HOCl<sub>4</sub> (Mao et al. 2008).  $\beta$ -PbO<sub>2</sub> coated on Ti with SnO<sub>2</sub>-Sb<sub>2</sub>O<sub>3</sub>-Nb<sub>2</sub>O<sub>5</sub> interlayer showed higher electrochemical activity than Ti/RuO<sub>2</sub> and Ti/Sb-Sn-RuO<sub>2</sub> anodes for the degradation of phenol. The interlayer enhanced the surface area, electrocatalytic activity, conductivity, and hence the efficiency. Evidently, the removal efficiency increased from 78.6 % (Na<sub>2</sub>SO<sub>4</sub>) to 97.2 % on adding 21.3 g L<sup>-1</sup> of NaCl.

Niu et al. (2012) reported that the toxic PFCAs like perfluorobutanoic acid (PFBA), PFPA, PFHxA, PFHpA, and PFOA, which are recently driving attention as serious contaminants in various environmental matrices, can be successfully mineralized by electrochemical method using Ce-doped porous nanocrystalline PbO<sub>2</sub> film electrode (Ti/SnO<sub>2</sub>-Sb/PbO<sub>2</sub>-Ce). The same electrode provided excellent mineralization of PFNA, PFDA, and sulfamethoxazole as reported by Lin et al. (2013a, b) under mild conditions.

The dissolution of PbO<sub>2</sub> in strong basic conditions and on specific anodic polarization limits its usage in wastewater

treatment (Carvalho et al. 2011; Niu et al. 2012). However, by adopting suitable fabrication technique, the wear resistance of PbO<sub>2</sub> can be conditioned (Carvalho et al. 2011) and possible release of Pb<sup>2+</sup> in acidic conditions can be avoided by the application of suitable anodic current (Niu et al. 2012). Unlike SnO<sub>2</sub>, passivation of surface due to the formation of hydroxides is avoided by the continuous production of hydroxyl radicals on the surface of PbO<sub>2</sub> and offers high charge transfer. Table 4 summarizes the comparison between the various modified PbO<sub>2</sub> anodes and conditions used in the electrochemical wastewater treatment process.

#### Ruthenium oxide and iridium oxide

RuO<sub>2</sub>- and IrO<sub>2</sub>-based anodes are active anodes, known for their electrocatalytic activity for oxygen and chlorine evolution. IrO<sub>2</sub> is one of the cheapest dimensionally stable anodes and shows low chlorine and oxygen evolution overpotential used in the generation of active chlorine species (Zaviska et al. 2009). Both IrO<sub>2</sub>- and RuO<sub>2</sub>-coated Ti anodes undergo dissolution in basic medium on anodization (Li et al. 2009). Ti/RuO<sub>2</sub> undergoes corrosion during electrolysis on prolonged usage (Papastefanakis et al. 2010). However, the service life of RuO<sub>2</sub> enhances on doping with Ir (Chandler et al. 1997; Chen et al. 2001, 2002; Duby 1993; Nikolić et al. 2012). The electrochemical properties of iridium (Ti<sub>0.6</sub>Ir<sub>0.4</sub>O<sub>2</sub>/Ti) and ruthenium (Ti<sub>0.6</sub>Ru<sub>0.4</sub>O<sub>2</sub>/Ti) oxide anodes, prepared by sol-gel method, were investigated by Panić et al. (2003a, b, 2007, 2010). They found that the iridium oxide shows enhanced catalytic activity for both oxygen and chlorine evolution and stability against corrosion as compared to ruthenium oxide (Panić et al. 2003a, b, 2007, 2010). These electrodes provide only small range of operating potential within hydrogen and oxygen evolution reactions. It is difficult to realize the direct oxidation of variety of organics on these anodes within this potential range. Hence, practical relevance of these anodes in the wastewater treatment on large scale is unacceptable. However, few research teams have successfully degraded the organic pollutants using these anodes.

The low chlorine evolution overpotential on these anodes is advantageous in the production of active chlorine species in wastewater containing chloride ions. The addition of NaCl as supporting electrolyte improves the removal efficiency, indicating that electrochemical treatment using Ti/IrO<sub>2</sub> and Ti/RuO<sub>2</sub> involves both direct and indirect oxidation (Chatzisyseon et al. 2009; Li et al. 2009). Enhancement in the COD removal efficiency was observed due to oxidation mediated by the electrochemically generated oxidants in the presence of chloride ions using Ti/RuO<sub>2</sub> anode in olive mill wastewater treatment (Papastefanakis et al. 2010). The degradation process involved the formation of intermediates followed by further oxidation to CO<sub>2</sub> and water.

**Table 5** Performance of different modified RuO<sub>2</sub> and IrO<sub>2</sub> anodes and working conditions

Pollutant	Electrode	Operating conditions	% COD and TOC removal, %CE, TEC	Remarks	Reference
Phenol-formaldehyde	IrO <sub>2</sub> -Ta <sub>2</sub> O <sub>5</sub> 1. Ti/Ru <sub>0.3</sub> Ti <sub>0.7</sub> O <sub>2</sub>	Phenol-IC=0.425 mmol L <sup>-1</sup> , formaldehyde=67.000 mmol L <sup>-1</sup> , SE: NaCl (1.000 mol L <sup>-1</sup> ) pH=5.5, j=40	TOC=68	OER potential=1.5–1.8 V Effect of Na <sub>2</sub> SO <sub>4</sub> and NaNO <sub>3</sub> as supporting electrolytes was investigated. But removal efficiency was found to be highest in the presence of NaCl. Electrode is wear resistant	Kapalka et al. (2008) Fomazari et al. (2012)
				COD=62.7±3.7 (initial in mg L <sup>-1</sup> ), COD=15.7±0.0 (final in mg L <sup>-1</sup> ), TOC=40.6±4.5 (initial in mg L <sup>-1</sup> ), TOC=19.8±0.6 (final in mg L <sup>-1</sup> ), instantaneous %CE=41.3±3.3 COD=27.4 (initial in mg L <sup>-1</sup> ), COD=20.9 (final in mg L <sup>-1</sup> ), instantaneous %CE=5.7	The removal efficiency increased with the chloride concentration and current density, but decreased with the increase in the initial concentration of the dye and flow rate. Trypan blue was most resilient to degradation
Trypan Blue	1. Ti/IrO <sub>2</sub>	IC=50 mg L <sup>-1</sup> , SE=3.42 mM, FR=2 L min <sup>-1</sup> , j=15	COD=35.3 (initial in mg L <sup>-1</sup> ) COD=17.0 (final in mg L <sup>-1</sup> ), instantaneous %CE=16.1		
Acridine		IC=48.6 mg L <sup>-1</sup>	COD=22.2 (initial in mg L <sup>-1</sup> ) COD=2.6 (final in mg L <sup>-1</sup> ), instantaneous %CE=17.2		
Eosin Yellow		IC=51.6 mg L <sup>-1</sup>	TOC=13, COD=18 TOC=14, COD=39	Complete mineralization was achieved with irradiation (wavelength 254 nm) and j=20 mA cm <sup>-2</sup>	Kusmierek et al. (2011)
Reactive blue 81 Reactive Red 2	1. Ti/TiO <sub>2</sub> (70 %)-RuO <sub>2</sub> (30 %)	IC=0.5 g L <sup>-1</sup> (60 mL), 2 h, SE: NaClO <sub>4</sub> (0.1 mol L <sup>-1</sup> ), appl. voltage=0.9 V			
Alphazurine dye	1. Ti/IrO <sub>2</sub>	IC=500 mg L <sup>-1</sup> , SE: Na <sub>2</sub> SO <sub>4</sub> , j=30	COD=60, %CE=3, TEC=254	Oxidation of alphazurine was slow as compared to oxygen evolution reaction (OER=1.3 V vs SCE)	Nava et al. (2008)
Olive mill wastewater	1. Ti/RuO <sub>2</sub>	1 M HClO <sub>4</sub> , 80 °C, 5 h, j=50	COD=52, TOC=38	Charge consumed=28 Ah L <sup>-1</sup> . Addition of 20 mM NaCl enhanced the COD removal by 8 times	Papastefanakis et al. (2010)
Olive mill wastewater	1. Ti/IrO <sub>2</sub>	1 M HClO <sub>4</sub> , 80 °C, j=50	COD=60, total phenolic compound removal=85	COD removal increased with current density. Variation in temperature influenced the removal efficiency. Addition of 5 mM NaCl enhanced the COD removal. Formation of toxic organochlorinated by-products was observed	Chatzisyameon et al. (2009)

Table 5 (continued)

Pollutant	Electrode	Operating conditions	% COD and TOC removal, %CE, TEC	Remarks	Reference
Reactive Red 120	1. Ti/IrO <sub>2</sub> -RuO <sub>2</sub>	120 mL, 1 M HClO <sub>4</sub> , 5 h	TOC=10 (25 °C), TOC=40 (80 °C), Only selective oxidation occurred. COD=43 ( $j=50 \text{ mA cm}^{-2}$ ), COD=32 ( $j=15 \text{ mA cm}^{-2}$ ), instantaneous %CE=13 TOC=100		Panakoulas et al. (2010)
Phenol	1. Ti/IrO <sub>2</sub> -Pt	IC=8 mg L <sup>-1</sup> , SE=0.3 mg L <sup>-1</sup> , NaCl 50 min, $j=10$	TOC=100	OER potential 1.2 V vs SCE. The TOC removal rate increased with current density	Li et al. (2009)
	2. Ti/RuO <sub>2</sub> -Pt	IC=8 mg L <sup>-1</sup> , SE=0.3 g L <sup>-1</sup> , NaCl 30 min, $j=10$	TOC=100	OER potential 1.58 V vs SCE	
Oxalic acid	1. IrO <sub>2</sub> -Ta <sub>2</sub> O <sub>5</sub>	IC=0.1 M, FR=1.2 L min <sup>-1</sup> , 25 °C, $j=17$	COD=91 to 95, instantaneous %CE=62 to 66	The duration for complete mineralization was monitored (778 min). The removal rate increased with flow rate of the sample and applied current density Time elapsed=334 min	Scialdone et al. (2009a)
		IC=0.1 M, FR=0.2 L min <sup>-1</sup> , SE=5 g L <sup>-1</sup> NaCl, 25 °C, $j=39$	COD=>98, instantaneous %CE=71 to 75		
Reactive Blue 4		IC=0.1 M, FR=1.2 L min <sup>-1</sup> , 50 °C, $j=17$	COD=>99, instantaneous %CE=68 to 72	Time elapsed=778 min	
	1. Ti/(RuO <sub>2</sub> ) <sub>0.77</sub> (Ta <sub>2</sub> O <sub>5</sub> ) <sub>0.30</sub>	IC=100 mg L <sup>-1</sup> (50 mL), SE=Na <sub>2</sub> SO <sub>4</sub> , $j=50$	TOC=20 TOC=38, instantaneous %CE=3 to 6 TOC=28 TOC=22 TOC=32 TOC=27	The COD removal increased from 30 to 80 % in the presence of chloride ions. The formation of toxic AOX was observed with all 3 electrodes. Ru and Ta electrode although displayed slowest oxidation rates, the amount of AOX formed was low	da Silva et al. (2011)
	2. Ti/Ru <sub>0.30</sub> Ti <sub>0.70</sub> O <sub>2</sub>			Degradation of brilliant red K-2BP was improved in the presence of NaCl on Ti/RuTiSnMn electrode at lower pH and higher temperatures	Jiancheng et al. (2012)
Reactive Orange 16	1. Ti/(RuO <sub>2</sub> ) <sub>0.70</sub> (Ta <sub>2</sub> O <sub>5</sub> ) <sub>0.30</sub>				
Reactive Brilliant Red K-2BP	2. Ti/Ru <sub>0.30</sub> Ti <sub>0.70</sub> O <sub>2</sub>				
	3. Ti/Ru <sub>0.30</sub> Sn <sub>0.70</sub> O <sub>2</sub>				
	Ti/RuTiIrSnMn oxide	100 mg L <sup>-1</sup> (200 mL), $j=30$ , FR=50 mL min <sup>-1</sup> , SE: NaCl (0.4 g L <sup>-1</sup> )			

IC initial concentration of the pollutant, SE supporting electrolyte, j current density (in milliamperes per square centimeter), FR electrolyte flow rate in case of recirculation batch systems, %CE instantaneous percentage current efficiency, TEC total energy consumed (in kilowatt-hours per cubic meter)



Due to high electrocatalytic activity and stability, IrO<sub>2</sub>-Ta<sub>2</sub>O<sub>5</sub> anode finds wide industrial applications (Scialdone et al. 2009a). IrO<sub>2</sub>-Ta<sub>2</sub>O<sub>5</sub> anode is known for its selective oxidation. It oxidizes the organics into simpler carboxylic acids, particularly oxalic acid (Scialdone et al. 2009a). IrO<sub>2</sub>-Ta<sub>2</sub>O<sub>5</sub> is the suitable electrode for the degradation of OA (Scialdone et al. 2009a; Ferro et al. 2010).

Three different DSA<sup>®</sup>s, Ti/(RuO<sub>2</sub>)<sub>0.70</sub>(Ta<sub>2</sub>O<sub>5</sub>)<sub>0.30</sub>, Ti/Ru<sub>0.30</sub>Ti<sub>0.70</sub>O<sub>2</sub>, and Ti/Ru<sub>0.30</sub>Sn<sub>0.70</sub>O<sub>2</sub>, were used in the degradation of RB-4 and RO-16 (da Silva et al. 2011). The Ti/Ru<sub>0.30</sub>Ti<sub>0.70</sub>O<sub>2</sub> showed the highest current efficiency among these electrodes. Indirect electrochemical oxidation by the active chlorine species generated in presence of NaCl enhanced the COD removal on this electrode. Ti/Ru<sub>0.30</sub>Ti<sub>0.70</sub>O<sub>2</sub> anode showed higher OER potential as compared to the other two. The same electrode was used in the degradation of Reactive Blue 81 and Reactive Red 2 by Kusmierek et al. (2011). Complete mineralization was achieved when the electrochemical degradation was coupled with the UV irradiation. These results indicate that TiO<sub>2</sub>-RuO<sub>2</sub> mixed metal oxide solid solution is effective in the generation of active chlorine species. As these dyes can be successfully mineralized by indirect electrochemical oxidation, Ti/Ru<sub>0.30</sub>Ti<sub>0.70</sub>O<sub>2</sub> anode is suitable for the treatment of wastewater containing these dyes.

Chu et al. (2010) prepared Ti/RuO<sub>2</sub>/IrO<sub>2</sub>/TiO<sub>2</sub> with two compositions: one electrode (#1) with 0.20, 0.85, and 0.40 mg cm<sup>-2</sup> of Ru, Ir and Ti, respectively, whereas the other electrode (#2) composed of 1.10, 1.20, and 0.55 mg cm<sup>-2</sup> of Ru, Ir, and Ti, respectively. The higher oxide loading in case of #2 led to relatively rough surface of the coating. Direct oxidation of 2,4-DCP was observed on this electrode (Chu et al. 2010). Pt doping increases the service life of IrO<sub>2</sub> and RuO<sub>2</sub> anodes and the inability of Pt to produce hydroxyl ions is compensated by the ruthenium and/or iridium oxides (Li et al. 2009).

Table 5 compares different modified RuO<sub>2</sub> and IrO<sub>2</sub> anodes. The conditions used in the electrochemical wastewater treatment process, COD and TOC removal, and current efficiency displayed are useful in comparing the affinity of electrodes for different pollutant molecules.

#### Comparison between main metal oxide anodes

Table 6 reveals that the potential corresponding to the commencement of oxygen evolution reaction on the

anode is related to OER overpotential and adsorption enthalpy of hydroxyl radicals (Kapařka et al. 2008). The ability of the anode to oxidize the organics increases with an increase in OER overpotential. Evidently, IrO<sub>2</sub> and RuO<sub>2</sub> are active anodes with low OER overpotential and are best suited for the production of chlorine and oxygen in chlor-alkali industries and electroorganic synthesis. They provide only partial decontamination with high energy consumption. The OER is highest for SnO<sub>2</sub> anode, and hence, it possesses high electrocatalytic activity for the production of hydroxyl radicals. Therefore, complete incineration of organics is viable. Similarly, OER for PbO<sub>2</sub> is also considerable and it is only slightly less than that of SnO<sub>2</sub>. The only problem encountered in the implementation of these anodes for the wastewater treatment on large scale is their dissolution on electrolysis in severe wastewater matrix. Studies on appropriate modifications in the fabrication technique to enhance their stability are of much importance.

BDD anode recognized as the highly efficient anode for the oxidative degradation of organics in the past few years has acquired a lot of attention. Hydroxyl radical adsorption is very weak on the surface of BDD. The potential window between OER (2.2–2.6 V) and hydrogen evolution reaction is wide (>3 V) (Brillas et al. 2009; Koparal et al. 2007; Martínez-Huitle and Ferro 2006; Panizza and Cerisola 2008). However, BDD fabrication is very expensive as compared to metal oxide anodes. If appropriate modifications of metal oxide anodes to meet the characteristics of BDD and operating conditions are optimized to stretch the performance to the maximum, it only takes a mere part of the cost to achieve the same effectiveness as on BDD.

#### Conclusion

The electrochemical oxidation involving metal oxide electrodes for the abatement of organics in wastewater is an effective tool to keep up the aesthetic and environmental health. Nature of the electrode, pollutant, and operating conditions should coordinate suitably to successfully accomplish the goal of complete elimination of

**Table 6** Oxidation power of the anode material in acid media

Electrode	Oxidation potential/V	Overpotential for oxygen evolution/V
RuO <sub>2</sub> -TiO <sub>2</sub> (DSA-Cl <sub>2</sub> )	1.4–1.7	0.18
IrO <sub>2</sub> -Ta <sub>2</sub> O <sub>5</sub> (DSA-O <sub>2</sub> )	1.5–1.8	0.25
Ti/PbO <sub>2</sub>	1.8–2.0	0.50
Ti/SnO <sub>2</sub> -Sb <sub>2</sub> O <sub>5</sub>	1.9–2.2	0.70

Adapted from Kapařka et al. (2008) and Martínez-Huitle and Andrade (2011). Standard potential for oxygen evolution is 1.23 V vs normal hydrogen electrode

organics. The physical and chemical properties of the electrodes can be tuned by adopting appropriate fabrication technique to serve their purpose.

The structure, size, alignment, and morphology of the coated oxide thin film command the mechanism followed by the electrode. Electrodes with smooth surface interact very weakly with the hydroxyl radicals, and hence, these radicals are available for the oxidation of the organics, whereas on the electrodes with small crystallite size, large and rough surface areas provide sites for the hydroxyl radicals and organic molecules to adsorb strongly. The availability of hydroxyl radicals for the oxidation of organics diminishes on strong adsorption. Furthermore, with an increase in active centers on the surface of the oxide electrode and applied current density, the rate of formation of hydroxyl radicals also increases. Hence, metal oxide electrodes with smooth surface, small crystallite size, and high surface area are more effective. These prerequisite properties can be furnished with the help of suitable alterations made during the fabrication of the electrode. Selection of proper fabrication method, doping agent, interlayer insertion, and composition can bring out the best results.

Indirect oxidation of organics by the electrochemically generated oxidants is also a best method. Chloride is the most favorite electrolyte and  $\text{ClO}_4^-$ ,  $\text{NO}_3^-$ ,  $\text{PO}_4^{2-}$ ,  $\text{SO}_4^{2-}$ ,  $\text{CO}_3^{2-}$ , and  $\text{Br}^-$  are also effective under appropriate optimized operating conditions. Inclusion of chloride ions substantially enhanced the efficiency in color, COD, and TOC removal in many cases due to the formation of  $\text{HOCl}$ ,  $\text{ClO}^-$ , and  $\text{Cl}_2$ . However, the risk of formation of AOX should be considered. Sulfate radicals, peroxydisulfate, peroxydicarbonate, and peroxydiphosphates are also strong oxidants and can be effective under suitable conditions.

Among the three main metal oxide anodes discussed in this review,  $\text{IrO}_2$  and  $\text{RuO}_2$  show lowest OER potential. The oxygen evolution reaction on these electrodes competes with the oxidation reaction of organics. The complete removal of organics using these electrodes is possible only by indirect electrochemical oxidation. However, these electrodes are best suited for  $\text{Cl}_2$  generation and electroorganic synthesis. Both  $\text{SnO}_2$  and  $\text{PbO}_2$  exhibit very good electrochemical activity for the oxidation of organics and electrocatalytic activity for the production of hydroxyl radicals. The service life of  $\text{PbO}_2$  is greater than that of  $\text{SnO}_2$ , and the OER for  $\text{SnO}_2$  is higher than that of  $\text{PbO}_2$ . Metal dissolution is a serious concern in electrochemical treatment process.  $\text{SnO}_2$ -Sb,  $\text{PbO}_2$ ,  $\text{IrO}_2$ , and  $\text{RuO}_2$  electrodes undergo dissolution in basic medium and high anodic potentials. However, modified  $\text{SnO}_2$  and  $\text{PbO}_2$  electrodes show high stability, electrochemical, and electrocatalytic

properties than modified  $\text{IrO}_2$  or  $\text{RuO}_2$  electrodes. The performance of  $\text{SnO}_2$  and  $\text{PbO}_2$  is comparable with the BDD electrode which is recognized as a highly efficient anode for the oxidative degradation of organics. This makes modified  $\text{SnO}_2$  and  $\text{PbO}_2$  electrodes as suitable candidates for the electrochemical wastewater treatment on large scale.

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