

Prospects in straw disintegration for biogas production

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Abstract The pretreatment methods for enhancing biogas production from oat straw under study include hot maceration, steam explosion, and pressure shockwaves. The micropore area (9, 55, and 64 m² g⁻¹) inhibitor formations (0, 15, and 0 mL L⁻¹) as well as the overall methane yields (67, 179, and 255 CH₄ VS t⁻¹) were robustly analyzed. It was confirmed that the operating conditions of the steam explosion must be precisely tailored to the substrate. Furthermore, it was beneficial to prepend the hot maceration before the steam explosion and the pressure shockwaves. The second alternative may give increased methane yields (246 in comparison to 273 CH₄ VS t⁻¹); however, the application of pressure shockwaves still faces limitations for deployment on a commercial scale.

Keywords Hot maceration · Steam explosion · Pressure shockwaves · Oat straw · Phytomass · Disintegration

Introduction

So far, there was only a negligible shift from purpose-grown phytomass (e.g., maize silage) to waste phytomass (e.g., straw) regarding biogas production. Based on its chemical composition, straw could also be a perfect source for

biochemical processes. However, various costly pretreatment procedures (physical, chemical, and biological, as well as their various combinations) are necessary for its smooth utilization (Taherzadeh and Karimi 2008). The reason lies in the natural resistance of plant cell walls to microbial and enzymatic deconstruction, collectively known as “biomass recalcitrance” (Himmel 2008). Unfortunately, the recalcitrance lignocellulose ballast also inhibits the digestion of readily fermentable compounds through their inclusion (Wachendorf et al. 2009). There are low methane yields (Amon et al. 2007; Shiralipour and Smith 1984), low conversion efficiencies (Herrmann et al. 2007; Prochnow et al. 2005; Röss et al. 1998), and high retention times in the fermentor (Lemmer and Oechsner 2001; Noike et al. 1985). Several studies have shown a good correlation between the pore volume or population (accessible surface area for cellulase) and the enzymatic digestibility of lignocellulosic materials. The effect of this area may correlate with crystallinity, lignin protection, hemicellulose presentation, or all three factors (Taherzadeh and Karimi 2008).

It was hypothesized that focusing on the anaerobic fermentation of straw in order to reduce the negative agronomic and environmental aspects of the purpose-grown phytomass (Herrmann 2012) would be beneficial. The hypothesis was continued by an assumption that the micropore area (Brunauer et al. 1938) may serve as a supporting reference method for measuring the level of phytomass disintegration. The oat straw was the tested substrate, and hot maceration and steam explosion were the disintegration methods compared in a commercial scale. In addition, the promising technology of shockwaves generated by high-

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voltage discharges was taken into account, although its development for commercial use is not yet completed.

Materials and methods

Substrate

Medium-early oat variety with short straw called “Atego” with origin in varieties of Gramena and Auron was sown (450 seeds m^{-2}) on 23 March 2011 in Dub (Czech Republic). The fertilization was carried out using the following soil properties to achieve the requirements (75 kg N, 60 kg P_2O_5 , and 85 kg N ha^{-1}) recommended by the breeder (SELGEN a.s., Czech Republic): loamy soil, pH 5.8, 109.4 mg P, and 168 mg K kg^{-1} . The harvest was done at full maturity (3.7 t seeds and 2 t straw in fresh weight per hectare) on August 19. Raked straw was pelleted into 6-mm rolls ($970.5 \pm 23 \text{ kg } m^{-3}$, $88.5 \pm 0.2 \%$ volatile solids (VS), $30 \pm 2.1 \%$ acidic-detergent fiber, $17.6 \pm 0.4 \%$ acidic-detergent lignin, $14.935 \pm 0.092 \text{ MJ } kg^{-1}$, labile pool 1 of carbon $28.1 \pm 3.6 \%$, and labile pool 2 of carbon 23.5 ± 3 , all $n=12$; $P < 0.05$) using JGE 120 (PCC Ltd., Czech Republic) and stocked in plastic fabric bags.

Inoculate

Fresh inoculate was obtained from biogas station Nedvědice 1 (Miroslav Drs farm, Czech Republic). Its detailed analysis, origin, and method of production can be found in Maroušek (2013).

Hot maceration

The hot maceration was performed by the M2 continuous phytomass macerator (Fig. 1, BiomassTechnology a.s., Czech Republic) based on the Krátký et al. (2012) laboratory prototype. The commercial-scale macerator operated at $300 \text{ kg VS } h^{-1}$ (corresponding to 10 % VS). The temperature was in the range of 75 to 95 °C, and the retention time was between 20 and 200 s.

Steam explosion

The steam explosion process was performed by the TTP3 continuous high-pressure horizontal cylindrical reactor (Fig. 1, BiomassTechnology a.s., Czech Republic), ended with the expansion tourniquet (single 0.3-L explosion performed in 0.11–0.09 s) according to Maroušek et al. (2012). The entering substrate had approximately 15 % VS. The high-pressure reactor operated in the pressure range of 1.4–1.8 MPa, while the inner helix allowed gradual changes in the hydraulic retention between 2 and 20 min.

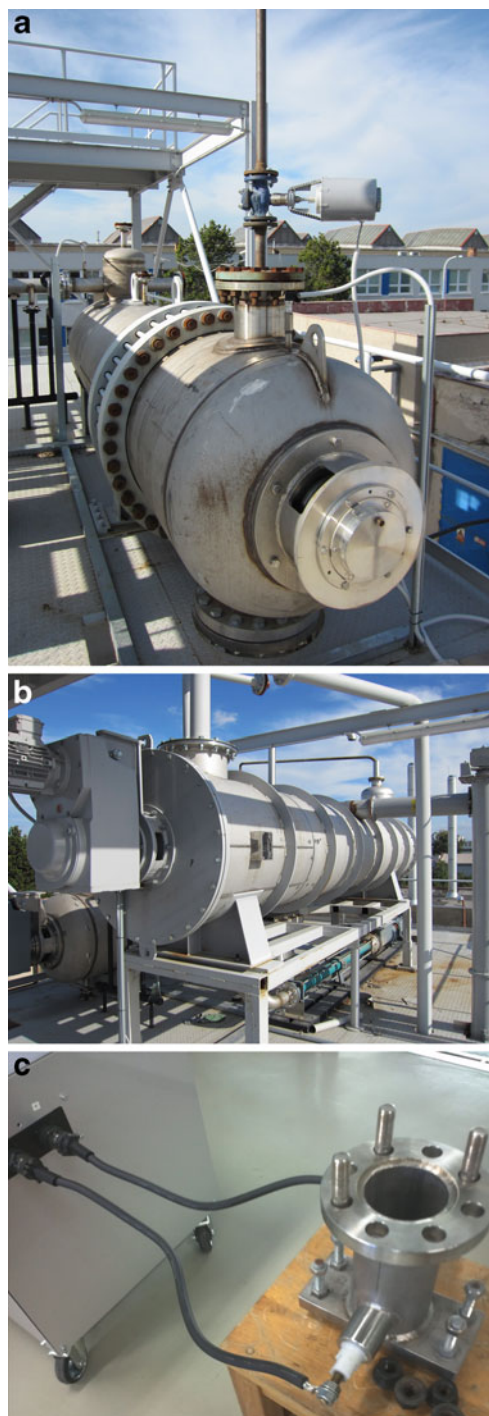


Fig. 1 Hot maceration (a), steam explosion (b), and pressure shockwaves (c)

Shockwave pretreatment

The shockwave pretreatment was performed in prototype number 7 (Higa et al. 2012), which is a lockable, metallic-strengthened vessel (Fig. 1) with a volume of 1 L. The substrate was initially poured into a 200-mL plastic bottle. The bottle was inserted into the vessel filled with distilled

water. Subsequently, the high-voltage generator circuit released several 3.5-kV discharges, resulting in 50- to 60-MPa pressure shockwaves (4.9 kJ , $1,500 \text{ m s}^{-1}$).

Analytical methods

The elemental soil analysis was conducted externally (ÚKZÚZ S.p.A., Czech Republic). The VS was determined by OV400 oven (Mettler GmbH, Germany) and a LH 06/13 muffle furnace (Fisher Scientific Ltd., Czech Republic) according to the method developed by the U.S. Environmental Protection Agency. The amounts of acidic-detergent fiber and acidic-detergent lignin were determined using the Fibertec 1020(M6) fiber analyzer (FOSS Ltd., Denmark). The heat values were analyzed using auto-calculating bomb calorimeter (CA-4AJ, Shimadzu). The proportions of carbon pools were determined by the acid hydrolysis (H_2SO_4) approach according to Rovira and Vallejo (2002) modified by Shirato and Yokozawa (2006), using the automatic high-sensitivity N/C analyzer (NC-90A, Shimadzu). The pH and temperature were measured using the CyberScan 600 multi-meter (Chromservis Ltd., Czech Republic). The methane yields were qualitatively and quantitatively analyzed as described in Maroušek et al. (2012) and converted to $0 \text{ }^\circ\text{C}$ at $101,325 \text{ Pa}$. Analyses on formic and levulinic acid, hydroxymethylfurfural, and furfural acid were conducted using the 5890 Series II Gas Chromatograph (Hewlett Packard, USA) equipped with a flame ionization detector ($300 \text{ }^\circ\text{C}$) and a DBwax column ($30 \text{ mm} \times 0.25 \text{ mm} \times 0.25 \text{ }\mu\text{m}$). The gas chromatograph settings were as follows: Helium was used as the carrier gas at a flow rate of $40 \text{ }\mu\text{L s}^{-1}$, temperature was set to $50 \text{ }^\circ\text{C}$, the flow rate of nitrogen was 30 mL min^{-1} , the injector used was in split mode, and the injector port temperature was at $250 \text{ }^\circ\text{C}$ (all J&W Scientific Inc., Folsom, CA, USA). The gas chromatograph oven temperature was programmed in the following manner: the temperature was held steady at $50 \text{ }^\circ\text{C}$ for 2 min, increased at a rate of $10 \text{ }^\circ\text{C min}^{-1}$ for 20 min, and then held at $250 \text{ }^\circ\text{C}$ for 8 min. The micropore area was detected using the technique of helium gas adsorption using a TriStar 3000 surface area analyzer (Micromeritics Ltd., Tokyo, Japan) after 24 h of degassing at $200 \text{ }^\circ\text{C}$ and 1 h of degassing at $300 \text{ }^\circ\text{C}$.

Results and discussion

Analysis on the micropore area ($\text{m}^2 \text{ g}^{-1}$) regarding the hot maceration pretreatment is shown in Fig. 2a. The data always analyzed 90 trials using polynomial function, while the lowest sum of squared absolute error (SSAE $2.6\text{E}-19$) reached and lowest root mean squared error (root mean square deviation (RMSE) $7.5\text{E}-17$) were the main fitting

criteria for all of the multi-parameter plots provided. The plot shows that there are no interacting effects between operating temperature and micropore area. In addition, it was observed that after a short delay in the macerator, the micropore area spiked, but subsequently, this speculated rise diminished. However, in comparison to manifestations of other pretreatment methods discussed below, the overall increase on the micropore area was relatively small (roughly from 2 to $9 \text{ m}^2 \text{ g}^{-1}$). It is assumed that the plot solely reflects how the substrate loses its outer pellet form which may interfere with the analyses conducted. Figure 2b describes the change in micropore area regarding the steam explosion pretreatment. Approximation (SSAE $1.9\text{E}-4$, RMSE $1.7\text{E}-3$) of these data shows that both operating conditions (hydraulic retention time and operating pressure) greatly affect the micropore area. The hydraulic retention times in the high-pressure reactor shorter than approximately 7 min affect the increase on the micropore area less substantially, independent of the operating pressure. There likely exists a minimum amount of time necessary for the hot steam to penetrate deeper into the internal structures of lignocellulosic fibers to be more effectively exposed to the rapid pressure changes in the following expansion tourniquet. Similar manifestations may be seen in Fig. 2c, which describes the dynamics (SSAE $9.4\text{E}-5$, RMSE $3.7\text{E}-7$) of the pressure shockwaves. It appears that the first couple of shockwaves is absorbed by the substrate to lose its pellet form. The observations show that larger amounts of water in the pretreated substrate make the micropore expand easier. Once the water is almost incompressible, this phenomenon may be explained by better pressure shockwave transmissions into the inner structure of the substrate, resulting in deeper warping of the plant cells. This assumption is supported by the peaks which are being discreetly formed in the area where higher amounts of shockwaves meet the larger amounts of water (bottom right contours), respectively, in opposite conditions (smaller amounts of water and less pressure shockwaves, up left). Based on these observations, in the next trials, the hot maceration (100 s , $95 \text{ }^\circ\text{C}$) was preceding the steam explosion (Fig. 2d, SSAE $5.7\text{E}-9$, RMSE $4.6\text{E}-4$) and the pressure shockwaves (Fig. 2e, SSAE $8.4\text{E}-5$, RMSE $3.7\text{E}-7$). Both figures show that the obstacles connected with the external form of the substrate were reduced. Admittedly, Richter et al. (2009) achieved methane yields of $397\text{--}426 \text{ CH}_4 \text{ VS t}^{-1}$. The scope of their experiments is different as they used similar techniques on a grass silage which does not have recalcitrance-like properties as straw. In relation to the energy requirements (can be looked up in referred papers and manufacturer's manuals), this discovery could be of great economic significance. Further verification on how the increase on the micropore area

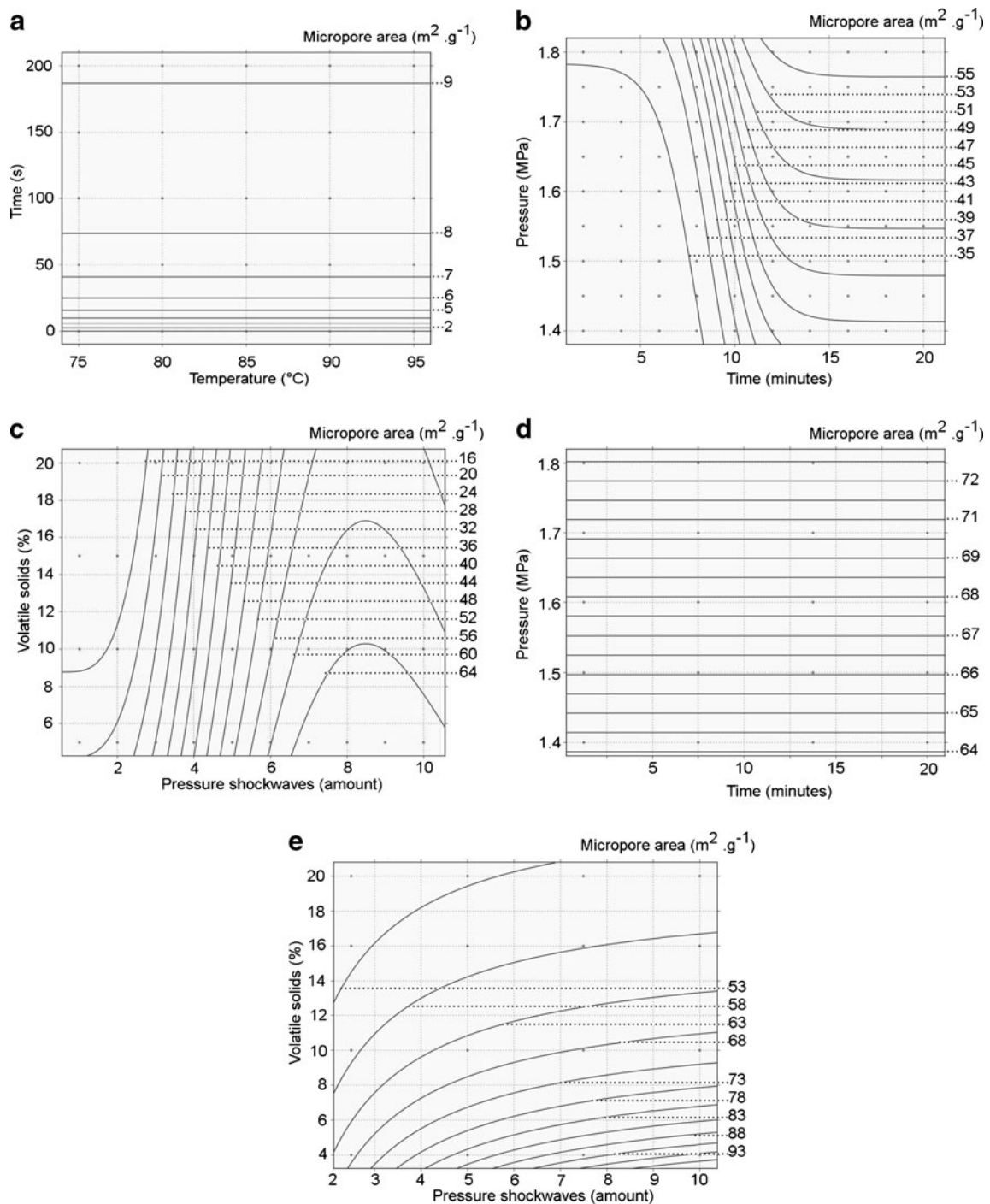


Fig. 2 Manifestation of the micropore area in relation to various process conditions of the hot maceration (a), steam explosion (b), pressure shockwaves (c), hot maceration followed by steam explosion (d), and hot maceration followed by pressure shockwaves (e)

correlates with the methane yields obtained was required. The hot maceration did not show any correlation ($y=1.34X+73.13$, $R^2=0.062$). The best non-linear approximation found (Fig. 3a) gave $R^2=0.108$. This result shows that the hot maceration does not significantly increase the micropore area and the micropore area achieved is not responsible for the methane yields obtained. It can thus

be assumed that the increase in the methane yield was caused by other factors. According to Richter et al. (2009), it is likely the phenomenon of hydrothermal conditioning and mechanical dehydration of the organic matter. A significant correlation was not achieved even in case of steam explosion ($y=0.44X+107$, $R^2=0.092$). However, closer examination of the data approximated by non-linear

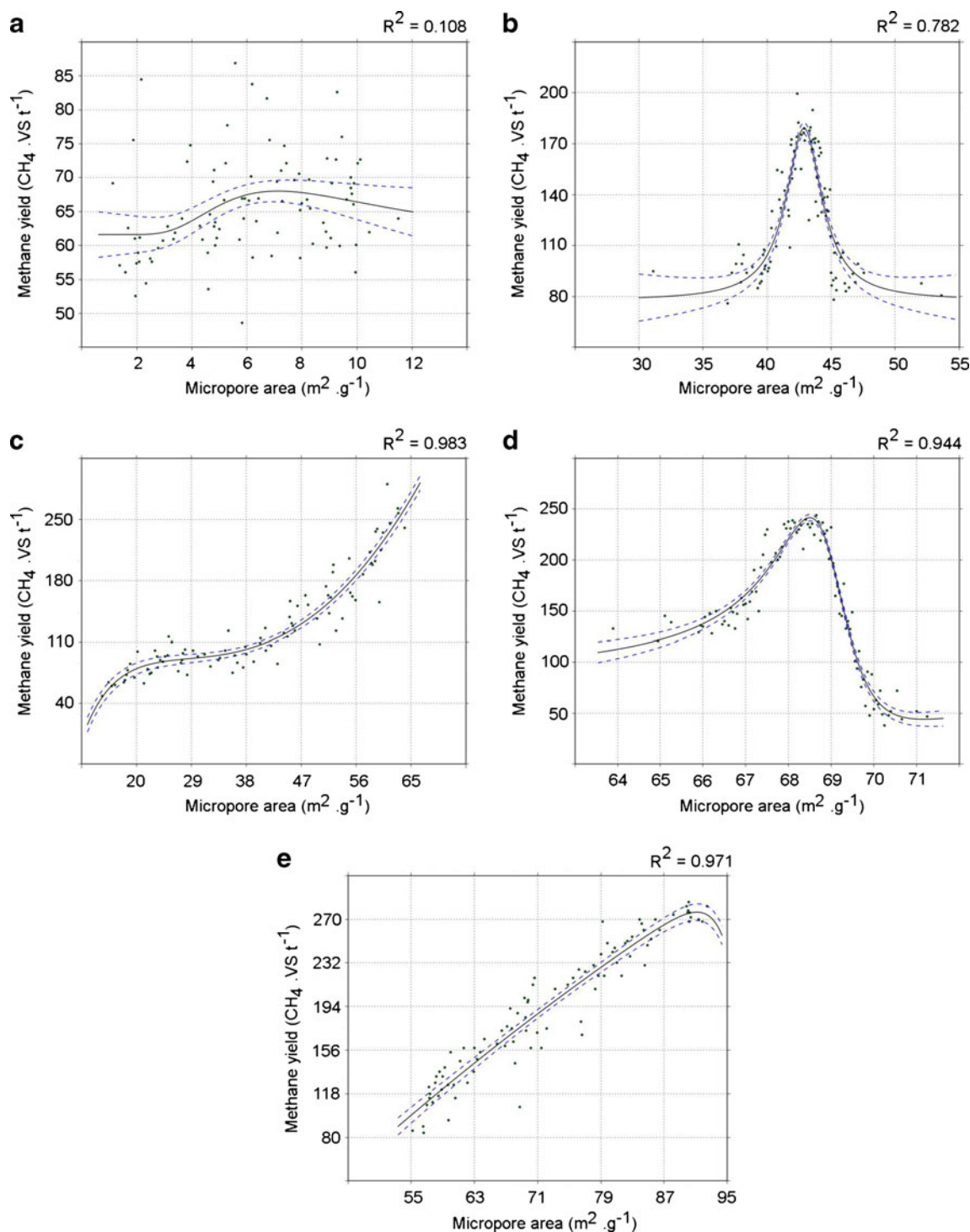


Fig. 3 Correlation of the micropore area and the methane yields achieved. **a–e** as in Fig. 2. The *dashed line* indicates the 95 % confidence intervals

function (Fig. 3b, $R^2=0.782$) allows us to speculate that the data may be divided into two groups which, under certain assumptions, may correlate linearly. According to Palmqvist and Hahn-Hägerdal (2000), this phenomena may be caused by a wide range of compounds which

are inhibitory to microorganisms (mostly furan derivatives). Analyses of the main representatives of this group as well as other possible causes of the decrease of the methane yield are discussed later. Pretreatment by pressure shockwave showed positive correlations

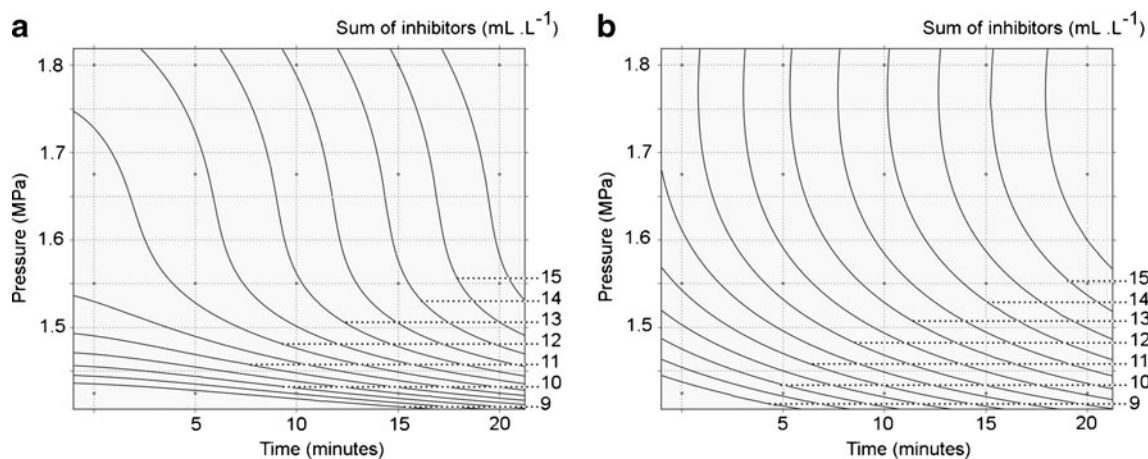


Fig. 4 Formic and levulinic acid, hydroxymethylfurfural, and furfural expressed as a sum of inhibitors in relation to the operating conditions of the high-pressure reactor, where **a** stands for steam explosion and **b** for hot maceration followed by steam explosion

($y=2.15X+22.86$, $R^2=0.951$) between the micropore area and the methane yields. More sensitive approximation of the data by non-linear function (Fig. 3c, $R^2=0.983$) shows that there may be other unidentified factors. In comparison to steam explosion, it does not show that these unidentified factors are dampening the methane production. Quite contrary, the data can be read as the generated pressure shockwaves are a gentle and effective method of increasing the micropore area and methane yields. According to Himmel (2008) and Taherzadeh and Karimi (2008), this phenomena may be explained as follows: The increased micropore area seems to correlate with accelerated enzymatic hydrolysis of the lignocellulose, which subsequently provided more fermentable compounds and higher methane yields. Increase on micropore area achieved by hot maceration followed by steam explosion did not show correlation with the methane yields subsequently obtained (Fig. 3d, $y=-7.14X+645.91$, $R^2=0.123$). In comparison to self-standing steam explosion (Fig. 3b), it can be assumed that the hot maceration followed by steam explosion made the substrate more sensitive to the operating conditions of the high-pressure reactor, resulting in higher yields responsible for a steeper fall in excess of critical operating pressure. The methane yields achieved are exactly in the same range ($250\text{--}300\text{ CH}_4\text{ VS t}^{-1}$) as Dererie et al. (2011). However, their steam explosion was carried out in the presence of lime and dilute acid or followed by enzymatic hydrolysis. On the other hand, the hot maceration followed by pressure shockwaves showed a more significant correlation than the pressure shockwaves itself ($y=2.09X+68.4$, $R^2=0.96$). In addition, sensitive approximation by non-linear function (Fig. 3e, $R^2=0.971$) showed a small reduction of the methane yield regarding the highest micropore area achieved. According to Fan et al. (1980), this phenomena

may be explained by the crystallinity of the remaining cellulose which is the next limiting factor. In order to confirm or refute the assumption about possible inhibitor formations on enzymatic hydrolysis (cellulases), analysis on the main inhibitors (formic and levulinic acid, hydroxymethylfurfural, and furfural) as defined by Palmqvist and Hahn-Hägerdal (2000) was performed. In the case of hot maceration, pressure shockwaves, and hot maceration followed by pressure shockwaves, the amounts of furan derivatives analyzed were under the limit of detection. However, pretreatment of the substrate by steam explosion formed certain quantities of these inhibitors, especially hydroxymethylfurfural (Fig. 4a, b). The data show that the inhibitors were formed mostly in the most severe conditions of the high-pressure reactor. In both cases, the dynamics of the operating pressure and the hydraulic retention are relatively similar in regard to the formation of such inhibitors. Following the previous results regarding the manifestations of the methane yield, it is assumed that the microorganism consortia in the anaerobic fermentation are able to adapt the presence of inhibitors to some extent. After exceeding a certain limit (10.7 ± 2.8 and $10.9\pm 2.5\text{ mL L}^{-1}$, both $P<0.05$), their activity is strongly paralyzed. These observations give rise to the possibility of further work exploring if yields of methane may be further improved by developing specific detoxification methods, optimizing the process of anaerobic fermentation or choosing adapted microorganism.

Conclusion

The self-standing hot maceration does not significantly increase the micropore area or the methane yields. Pretreatment by steam explosion has potential to significantly increase the micropore area and the methane

yields, but the operating conditions must be precisely tailored once inhibitor formations occur. This phenomenon is intensified if the steam explosion is following the hot maceration. The pressure shockwaves are capable of high increases of the micropore area as well as achieving high methane yields without the formations of inhibitors. Admittedly, this technology works so far only in volumes of liters per minute.

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