CONTAMINATED LAND, ECOLOGICAL ASSESSMENT AND REMEDIATION CONFERENCE SERIES (CLEAR 2012) : ENVIRONMENTAL POLLUTION AND RISK ASSESSMENTS

# Modeling adsorption kinetics of trichloroethylene onto biochars derived from soybean stover and peanut shell wastes

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Received: 23 December 2012 / Accepted: 22 March 2013 / Published online: 23 April 2013 © Springer-Verlag Berlin Heidelberg 2013

Abstract Trichloroethylene (TCE) is one of the most hazardous organic pollutants in groundwater. Biochar produced from agricultural waste materials could serve as a novel carbonaceous adsorbent for removing organic contaminants from aqueous media. Biochars derived from pyrolysis of soybean stover at 300 °C and 700 °C (S-300 and S-700, respectively), and peanut shells at 300 °C and 700 °C (P-300 and P-700, respectively) were utilized as carbonaceous adsorbents to study batch aqueous TCE remediation kinetics. Different rate-based and diffusion-based kinetic models were adopted to understand the TCE adsorption mechanism on biochars. With an equilibrium time of 8-10 h, up to 69 % TCE was removed from water. Biochars produced at 700 °C were more effective than those produced at 300 °C. The P-700 and S-700 had lower molar H/C and O/C versus P-300 and S-300 resulting in high aromaticity and low polarity accompanying with high surface area and high adsorption capacity. The pseudo-second order and intraparticle diffusion models were well fitted to the kinetic data, thereby,

Responsible editor: Philippe Garrigues

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Division of Plant Environmental Research, Gyeongsangnam-do Agricultural Research and Extension Service, Jinju 660-360, South Korea indicating that chemisorption and pore diffusion were the dominating mechanisms of TCE adsorption onto biochars.

**Keywords** Black carbon · Charcoal · Crop residue · Proximate analysis · Slow pyrolysis · Sorption dynamics

## Introduction

Release of chlorinated hydrocarbons is continually threatening the groundwater environment (Yang et al. 2011). Tricholoroethylene (TCE) is a dense non-aqueous phase liquid, which is water soluble substance having 1.1 kg  $m^{-3}$ solubility at 25 °C (Wei and Seo 2010). Because of high density (1,460 kg m<sup>-3</sup>), TCE spills are not easily washable and can percolate down causing severe groundwater contamination (Jo et al. 2010). Therefore, TCE is considered as one of the dangerous and toxic organic contaminants in the groundwater emanating from industries (Erto et al. 2010). The groundwater contamination by TCE has been extensively reported worldwide (Klasson et al. 2009; Wei and Seo 2010). In Korea, TCE is one of the frequently occurring organic contaminants in groundwater nearby industrial and urban areas (Lee and Lee 2004). The groundwater of an industrial complex at Wonju-si has been reported to be contaminated with TCE (Baek and Lee 2011). Approximately 300,000 m<sup>2</sup> of this complex is contaminated with TCE (Yu et al. 2006). Up to 1.52 mg  $L^{-1}$  TCE, which is 51 times higher than the prescribed Korean standard limit of 0.03 mg  $L^{-1}$ , was reported in this area (Yu et al. 2006). Multiple industrial facilities including an asphalt testing laboratory and a molding company have been identified as the major sources of the TCE groundwater contamination (Baek and Lee 2011).

Numerous technologies such as air-stripping, reactive barriers, adsorption, thermal desorption, and biodegradation have been proposed for TCE remediation from contaminated groundwater (Chung et al. 2004; Yang et al. 2007; Klasson et al. 2009; Kim et al. 2012). Among these, adsorption is one of the most certain remediation techniques used to purify TCE contaminated groundwater (Leboda et al. 1997). Carbon materials such as activated carbon (AC)/charcoal, graphitized carbon black, carbon molecular sieves, and carbon nanotubes are most frequently used as effective adsorbents (Leboda et al. 1997; Ahmad et al. 2012a; Alberti et al. 2012). However, the adsorption capacities of these materials are highly dependent on their micro-porous structures and the presence of surface functional groups. Another common consideration to use these carbonaceous adsorbents is the relatively high cost. Many of these adsorbents are derived from wood and coal, and it led to an increase of the application cost. Therefore, various raw materials or wastes, including eggshells, oyster shells, mussel shells, corals, olive stones, coconut husk, and agricultural waste materials, have been used as low cost environment-friendly adsorbents for water remediation (Ioannou and Simitzis 2009; Ok et al. 2011; Park et al. 2011; Ahmad et al. 2012b, c). These materials are either used as a raw form or after physicochemical modifications to enhance their adsorption efficiencies (Ok et al. 2010; Ahmad et al. 2012d; Lee et al. 2013; Pellera et al. 2012). Thermal modification of biomass via pyrolysis and carbonization is gaining much popularity. The biomass-derived black carbon also known as "biochar" is being newly employed to soil for carbon sequestration and soil fertility (Uchimiya et al. 2010; Yu et al. 2010; Awad et al. 2012). Biochar has also been applied to remediate contaminants in water and wastewater (Xu et al. 2012). The use of biochar as an adsorbent is very economical compared to AC (Qui et al. 2009).

Biomass types, pyrolysis and/or carbonization temperature, residence time, and heat transfer rate determine the structural and chemical properties of biochar. Pyrolysis processes induce the pore development in biochar by evaporation of gases, thereby expanding their surface area (Novak et al. 2009). Consequently, the carbon fractions in biochars can be categorized into polyaromatic, elemental, or graphitic structures (Chun et al. 2004). These transitional phase changes would strongly influence biochar function as a carbonaceous adsorbent (Keiluweit et al. 2010). Additionally, biochar efficiency as an adsorbent depends on surface area related to physical and chemical adsorption on the active sites of biochar (Ioannou and Simitzis 2009).

Adsorption kinetics generally describes the time-dependent uptake of an adsorbate by an adsorbent in an aqueous or gaseous phase. Thus, the application of adsorption kinetics is useful in determining the adsorption mechanism. Earlier we have reported the TCE adsorption equilibrium studies on biochars (Ahmad et al. 2012e). In the present investigation, TCE sorption dynamics on biochars derived from soybean stover and peanut shells pyrolyzed at 300 °C and 700 °C are reported. Various rate and diffusion models were used to establish the possible sorption mechanism.

## Materials and methods

Biochars development as adsorbents

Soybean stover and peanut shells were converted into biochars. A detailed description of biochar production and characterization is available elsewhere (Ahmad et al. 2012e). Briefly, soybean stover and peanut shells waste materials were pyrolyzed in a muffle furnace (MF 21 GS, Jeio Tech, Korea) in absence of air. Pyrolysis was carried out at 300 °C and 700 °C with an increment rate of 7 °C per min. The peak temperature of 300 °C or 700 °C was maintained for 3 h to complete the carbonization. The pyrolyzed products were allowed to cool down in the furnace and stored in an air-tight container. Biochars thus produced from soybean stover and peanut shells at 300 °C and 700 °C were designated as S-300, S-700, P-300, and P-700, respectively. A commercially available biochar produced from oak wood (OW) at 400 °C was obtained from Gangwon Charmsoot Company located in Hoengseong-gun, Gangwon province, Korea. A powdered AC was also purchased from Sigma Aldrich Company to compare the results from other adsorbents. All adsorbents used in this study were characterized before adsorption experiment. Structural characteristics of the adsorbents were determined by measuring specific surface area, pore volume, and pore diameter by an adsorption apparatus (Micromeritics, ASAP 2010 v 5.02H, USA). The elemental composition of C, H, and O was determined by an elemental analyzer (Flash EA 1112 series, CE Instruments, UK), and then molar H/C and O/C ratios were calculated from the elemental analysis results.

## Adsorption kinetics experiment

Batch adsorption kinetics experiments were conducted with different biochars and AC to determine the TCE adsorption (Yang et al. 2006). Reagent grade TCE (99 % purity) was purchased from Wako Pure Chemical Industries (Osaka, Japan). The sorbate solution (50 mg L<sup>-1</sup>) was prepared by dissolving TCE in ultrapure water obtained from a water purification system (Arium<sup>®</sup> Pro UV/DI, Sartorius Stedium Biotech, Germany). The water was buffered to pH 7 using 1 mM phosphate buffer (0.5 mM Na<sub>2</sub>HPO<sub>4</sub>·H<sub>2</sub>O and 0.5 mM NaH<sub>2</sub>PO<sub>4</sub>) to reduce the effect of adsorbents on solution pH (Quinlivan et al. 2005). The carbonaceous adsorbents were added to the TCE solution at a rate of 1.0 g L<sup>-1</sup> in Teflon-lined screw caped glass vials. The vials were fully filled without headspace to minimize TCE volatilization loss, and placed on a horizontal shaker set to

50 rpm and 25 °C. Three replicates for each adsorbent and control (without adsorbent) were performed. At specific time intervals of 0.25, 0.5, 0.75, 1.0, 1.5, 2.0, 2.5, 3.0, 4.0, 5.0, 6.0, 8.0, 10.0, 12.0, 16.0, 20.0, 24.0, 32.0, 40.0, and 48.0 h, three vials of each treatment were removed. An aliquot of the solution was filtered through a 0.45-µm pore-size syringe-filter and transferred to a 2-mL amber-colored-glass-vial for TCE analysis. Aqueous phase concentrations of TCE were measured at specific time intervals (*t*), while the uptake of TCE at time t ( $q_t$  in mg g<sup>-1</sup>) was calculated using Eq. (1) (Ok et al. 2007; Salih et al. 2011):

$$q_t = [(C_0 - C_t)v]/m$$
(1)

where  $C_0$  and  $C_t$  are the TCE initial and equilibrium concentrations (in mg L<sup>-1</sup>) at time *t*, *v* is the solution volume (in L), and *m* is the adsorbent dose (in g).

#### Kinetic models

Various kinetic models were used to investigate the sorption mechanism of TCE adsorption on carbonaceous adsorbents. The linear form of first order kinetic equation can be expressed as (Almaroai et al. 2012):

$$\ln q_t = \ln q_0 - k_1 t \tag{2}$$

where  $q_t$  and  $q_0$  are the amounts of TCE adsorbed at time *t* and 0 min, while  $k_1$  is the rate constant for the first order reaction.

The linear form of second order kinetics is (Almaroai et al. 2012):

$$1/q_t = 1/q_0 - k_2 t \tag{3}$$

where  $k_2$  is the second order rate constant.

The pseudo-first order equation is generally expressed as (Wong et al. 2004):

$$\ln(q_e - q_t) = \ln q_e - k_1' t \tag{4}$$

where  $q_e$  is the sorption capacity at equilibrium (in mg g<sup>-1</sup>) and  $k_1'$  is the rate constant for a pseudo-first order reaction.

The pseudo-second order kinetics equation is expressed as (Plazinski et al. 2009):

$$t/q_t = 1/k_2 q_e^2 + (1/q_e)t.$$
(5)

where  $k_2'$  is the rate constant for a pseudo-second order reaction. Initial sorption rate (*h*, in mg g<sup>-1</sup> min<sup>-1</sup>) can be calculated from the intercept of Eq. (5).

The Elovich equation can be expressed as (Almaroai et al. 2012):

$$q_t = 1/\beta \ln(\alpha\beta) + (1/\beta) \ln t \tag{6}$$

where  $\alpha$  is the initial sorption rate (in mg g<sup>-1</sup> min<sup>-1</sup>) and  $\beta$  is the sorption constant.

The power function equation can also be used to describe the adsorption kinetics as follows (Almaroai et al. 2012):

$$\ln q_t = \ln b + k_f(\ln t) \tag{7}$$

where  $k_f$  is the rate coefficient value (in mg g<sup>-1</sup> min<sup>-1</sup>) and *b* is the rate constant.

The intraparticle diffusion model equation can be expressed as (Almaroai et al. 2012):

$$q_t = c + k_{id}t^{0.5} \tag{8}$$

where  $k_{id}$  is the apparent diffusion rate constant (in [mg g<sup>-1</sup>]<sup>-0.5</sup>) and *c* is the diffusion constant.

The goodness of fit for the models was evaluated by comparing the coefficient of determination  $(r^2)$  and standard error of estimates (*SEE*) values. The SEE values were calculated using Eq. (9) (Mohammad and Maya 2011):

$$SEE = \sqrt{\left(\Sigma q_{\exp} - \Sigma q_{calc}\right)^2 / (n-2)}$$
(9)

where  $q_{exp}$  and  $q_{calc}$  are the experimental and model calculated sorption capacities (in mg g<sup>-1</sup>), and *n* is the number of observations.

## Analytical methods

Biochars and AC were characterized for various structural and elemental characteristics, and details were reported elsewhere (Ahmad et al. 2012e). In summary, the traditional N<sub>2</sub> gas adsorption technique was used to determine the surface area using a gas sorption analyzer (NOVA-1200, Quantachrome Corp., USA). The isotherms were obtained by plotting the N<sub>2</sub> adsorbed per gram of sample versus the relative vapor pressure  $(P/P_0)$  of N<sub>2</sub> ranging from 0.02 to 0.2. The surface area was calculated by fitting the data to the Brunauer-Emmett-Teller (BET) equation, and total pore volume was estimated from N<sub>2</sub> adsorption at  $P/P_o \sim 0.5$ (Park and Komarneni 1998). Surface morphological microstructures of the carbonaceous adsorbents were determined using a field emission scanning electron microscope (FE-SEM) equipped with energy dispersive spectroscopy (SU8000, Hitachi, Japan). SEM images were obtained from a 50-µm area of sample placed on a double-sided platinum coated tape. An elemental analyzer (EA1110, CE Instruments, Italy) was used to determine the elemental composition (C, H, N, S, and O) of adsorbents. The sample was combusted at 1,014 °C and electrical output signals proportional to the amount of eluted gas were generated by a thermo conductivity detector (TCD).

A high performance liquid chromatograph (HPLC, SCL-10A, Shimadzu, Japan) equipped with an auto-sampler (SIL-10AD, Shimadzu, Japan) and UV-VIS detector (SPD-10A, Shimadzu, Japan) was used to analyze the aqueous TCE concentration. A reverse-phase Sunfire C18 column (Waters, USA; 4.6 mm×250 mm) was employed in a column oven (CTO-10AS, Shimadzu, Japan). The mobile phase was a mixture of 85:15 v/v acetonitrile and water. The eluent was pumped isocratically at the rate of 1.0 mL min<sup>-1</sup>. A 10-µL aliquot of the sample solution was injected onto the column heated at 40 °C and the absorbance was measured at 214 nm.

## Statistical analysis

Mean values of three replicates from each batch experiment were used as input into the kinetic models to calculate various model parameters. Linear regression fittings were employed.

#### **Results and discussion**

#### Properties of carbonaceous adsorbents

Table 1 shows the physicochemical properties of AC, OW, and developed biochars (i.e., S-300, P-300, S-700, and P-700). Relatively high surface area was obtained for S-700  $(420.33 \text{ m}^2 \text{ g}^{-1})$  and P-700  $(448.23 \text{ m}^2 \text{ g}^{-1})$  versus S-300  $(5.61 \text{ m}^2 \text{ g}^{-1})$  and P-300  $(3.14 \text{ m}^2 \text{ g}^{-1})$ , showing the pyrolysis temperature effect. Generally, the increased surface area at high pyrolysis temperature is related to the development of micropores in biochars due to the removal of volatile materials (Lee et al. 2010). Biochars produced at 700 °C are characterized by the pore volume of 0.19 and 0.20 cm<sup>3</sup> g<sup>-1</sup> for S-700 and P-700, respectively. The pore diameters were 1.09 and 1.12 nm for S-700 and P-700 biochars, respectively. Furthermore, the micropores development in S-700 and P-700 is also apparent in their SEM images (Fig. 1). The highest surface area of 1,110 m<sup>2</sup> g<sup>-1</sup> accounted for AC may be due to the additional activation processes generally applied after feedstock carbonization during the AC synthesis. The OW biochar had a medium range surface area of 270.76 m<sup>2</sup> g<sup>-1</sup>, resulting from its pyrolysis at 400 °C.

Total C, H, and O contents in all adsorbents ranged from 68.27-90.85 %, 0.90-4.29 %, and 8.24-25.89 %, respectively. The total C contents were higher in S-700 (81.98 %) and P-700 (83.76 %) as compared to S-300 (68.81 %) and P-300 (68.27 %), indicating a higher degree of carbonization at a higher temperature. Contrarily, the H and O contents were lower in S-700 (1.27 % and 15.45 %, respectively) and P-700 (1.75 % and 13.34 %, respectively) than S-300 (4.29 % and 24.99 %) and P-300 (3.85 % and 25.89 %, respectively). Removal of O at high pyrolysis temperature may result in increasing hydrophobicity or decreasing polarity. Li et al. (2002) reported that the removal of O at high pyrolysis temperature makes the carbon surface more basic due to the acidic functional groups removal, thereby, inducing these carbons less polar. The molar ratios of H/C and O/C were calculated as indicators of aromaticity and polarity of the biochars and AC, respectively (Uchimiya et al. 2010). Lower ratios of H/C and O/C in S-700 (0.19 and 0.14, respectively), P-700 (0.25 and 0.12, respectively), OW (0.16 and 0.08, respectively), and AC (0.12 and 0.07, respectively) than S-300 and P300 indicated high aromaticity and low polarity. Chun et al. (2004) has reported increase in aromaticity and decrease in polarity at high pyrolysis temperatures in the chars derived from wheat residues. The structural characteristics and elemental compositions of biochars revealed that the pyrolysis temperature had a strong influence on biochar properties. Moreover, surface area and total C contents of the biochars increased with rise in pyrolysis temperature during feedstock combustion. Removal of O and H at high temperature resulted in biochars having high aromaticity and low polarity. These results imply that the specific properties of biochars may influence their adsorptive behavior towards organic contaminants remediation including TCE.

#### TCE sorption dynamics

TCE sorption dynamics on various biochars with time are shown in Fig. 2. Rapid TCE adsorption was observed within

Sample	S-300	S-700	P-300	P-700	OW	AC					
Structural characteristics											
Surface area $(m^2 g^{-1})$	5.61	420.33	3.14	448.23	270.76	1110					
Pore volume (cm <sup>3</sup> g <sup><math>-1</math></sup> )	_	0.19	-	0.20	0.12	0.64					
Pore diameter (nm)	_	1.09	_	1.12	1.10	1.44					
Elemental composition (wt%)											
С	68.81	81.98	68.27	83.76	88.71	90.85					
Н	4.29	1.27	3.85	1.75	1.21	0.90					
0	24.99	15.45	25.89	13.34	9.72	8.24					
Molar H/C	0.74	0.19	0.67	0.25	0.16	0.12					
Molar O/C	0.27	0.14	0.29	0.12	0.08	0.07					

Table 1Selected physicochemical properties of biocharsderived from soybean stover(S-300 and S-700) and peanutshells (P-300 and P-700),commercial oak biochar (OW),and activated carbon (AC)(Extended result of Ahmad et al.(2012e))

Fig. 1 Scanning electron micrographs of a biochar derived from soybean stover at 700 °C, S-700, b biochar derived from peanut shell at 700 °C, P-700, c commercial oak biochar, OW, and d activated carbon, AC



1 h of contact time. Specifically, S-300, S-700, P-300, and P-700 removed 39 %, 43 %, 36 %, and 51 % TCE, respectively. This was followed by a slow removal phase resulting in 48 %, 60 %, 50 %, and 68 % maximum TCE removal, respectively, after 8 h of contact time. In the case of AC, rapid adsorption occurred within 0.25 h of contact time, removing 81 % TCE, followed by a short slow phase of 1.5 h, causing a maximum 87 % TCE removal. However, the application of OW followed only the slow phase TCE adsorption completing in 20 h with a maximum removal of



Fig. 2 TCE adsorption kinetics on biochars derived from soybean stover (S-300 and S-700) and peanut shells (P-300 and P-700), commercial oak biochar (OW) and activated carbon (AC). (Initial TCE concentration, 50 mg  $L^{-1}$ ; adsorbent dose, 1 g  $L^{-1}$ )

46 %. The general two-phase adsorption, consisting predominantly of a rapid phase and a relatively slow phase, is a commonly observed phenomenon (Saeed et al. 2005; Pellera et al. 2012), and can be explained by the abundant availability of active sites in biochars, which then become progressively saturated with time. The equilibrium time for S-300, S-700, P-300, and P-700 was 8–10 h, whereas OW required 20–24 h. On the other hand, the equilibrium time for AC was only 1.5–2 h. At equilibrium, the maximum TCE adsorption by various biochars followed the order: P-700>S-700>P-300>OW≥S-300. However, AC showed high adsorption of TCE (43.52 mg g<sup>-1</sup>) than biochars at equilibrium, which may be attributed to its high surface area (1,110 m<sup>2</sup> g<sup>-1</sup>).

It is noteworthy that the biochars produced at 700 °C were more effective in TCE adsorption than those produced at 300 °C, thereby, indicating the temperature effect on their adsorption capacities. Pyrolysis temperature significantly affected the structural and elemental properties of biochars (Table 1). Specifically, the greater increases of the surface area for S-700 (420.33 m<sup>2</sup> g<sup>-1</sup>) and P-700 (448.23 m<sup>2</sup> g<sup>-1</sup>) compared to S-300 (5.61 m<sup>2</sup> g<sup>-1</sup>) and P-300 (3.14 m<sup>2</sup> g<sup>-1</sup>), resulting from high pyrolysis temperature, enhanced their TCE adsorption efficiency. TCE adsorption on OW  $(22.65 \text{ mg g}^{-1})$  was surprisingly low, in spite of its high surface area (270.8 m<sup>2</sup> g<sup>-1</sup>) versus S-300 and P-300. This may be due to the competitive effect of TCE with acetate in the OW (Erto et al. 2010) because wood vinegar (acetic acid) is being produced as a by-product of OW manufacture. Erto et al. (2010) emphasized that TCE adsorption capacity

onto carbonaceous adsorbents is greatly lowered by the presence of ethyl acetate because of its competitive effect with TCE. Recently, Spokas et al. (2011) qualitatively analyzed volatile organic compounds in a variety of biochars, and reported the presence of 52 % methyl acetate content in the wood biochars. Sorption of volatile organic compounds such as acetates produced during pyrolysis or from direct contact with liquor (vinegar) onto the OW may cause the active sites to be occupied, consequently resulting in lowering the TCE adsorption compared to other biochars.

#### Adsorption mechanism

**Table 2** Kinetic models and their mathematical expressions

used to fit the data

Sorption process is mainly controlled by the sorbate to sorbent transport, film diffusion through the boundary layer, intraparticle diffusion of ions or molecules, and chemisorption (Alberti et al. 2012). The greatest confrontation offered by one of these stages becomes the rate-limiting step of the sorption process (Alberti et al. 2012). Kinetic studies were performed to investigate the chemical reaction rates and sorption mechanisms for biochars and AC, having heterogeneous reactive sites. To investigate the sorption mechanism, the experimental data were fitted to various kinetic models listed in Table 2 and discussed under kinetic model.

The models were evaluated based on  $r^2$  and *SEE* values as given in Table 3. The  $r^2$  value is the most reliable and widely used error function to determine the best fit kinetic model (Kumar et al. 2008). According to the  $r^2$  values, kinetic data had a good fit with a pseudo-second order model followed by the intraparticle diffusion model for all adsorbents (Fig. 3). The kinetic parameters obtained from various models are summarized in Table 4.

The pseudo-second order kinetic model has been successfully applied and the rate constant  $(k_2')$ , the adsorption capacity  $(q_e)$ , and the initial adsorption rate (h) were determined simultaneously (Ho and Ofomaja 2006). The rate

constant is a time-scaling factor in determining the time required to reach an equilibrium-state. High rate constant indicates a short time and vice versa (Plazinski et al. 2009). The  $k_2$  'values obtained from pseudo-second order model for different adsorbents ranged from  $0.250 \times 10^{-3}$  to  $5.409 \times$  $10^{-3}$  g mg<sup>-1</sup> min<sup>-1</sup>. The  $k_2'$  values follow the order: AC>S-300>P-300>S-700>P-700>OW. The high  $k_2$  values obtained for AC, S-300, and P-300 indicated the enhanced mobility of TCE, which reached the solid surfaces in a short time interval. This finding agrees with the corresponding hvalues of the adsorbents, suggesting a high initial sorption rate. The  $q_a$  values calculated from the kinetic model ranged from 21.38 to 45.01 mg  $g^{-1}$  for different adsorbents. This follows the order: AC>P-700>S-700>P-300>S-300>OW. The high  $q_e$  values for P-700 (37.00 mg g<sup>-1</sup>) and S-700  $(29.38 \text{ mg g}^{-1})$  could be attributed to their surface area imparted at high pyrolysis temperature versus P-300  $(24.30 \text{ mg g}^{-1})$  and S-300  $(21.94 \text{ mg g}^{-1})$ . The positive linear relationship between surface area and equilibrium sorption capacities ( $r^2=0.877$ ) is shown in Fig. 4. Maximum capacity of equilibrium sorption (45.01 mg  $g^{-1}$ ) was obtained for AC due to its higher surface area than other biochars. The best fit of adsorption kinetics data was obtained with the pseudo-second order model suggesting the chemisorption to be the rate-limiting step, i.e., the rate of direct adsorption controls the overall sorption kinetics for all carbonaceous adsorbents (Plazinski et al. 2009). These findings are in agreement with the results published recently for the Cu(II) adsorption on biochars (Pellera et al. 2012).

In the kinetics analysis, TCE sorption on carbonaceous adsorbents may also involve intraparticle diffusion through macro- (>50 nm), meso- (2–50 nm), and micro- (<2 nm) pores, which could be the rate-determining step of the sorption process. Among diffusion-driven kinetics, the intraparticle diffusion model had a good fit (relatively high  $r^2$  values) with the experimental data. The intraparticle diffusion rate constant

Model	Mathematical expression	Plot	Parameters
First order	$ln q_t = ln q_0 - k_1 t$	$ln q_t$ vs $t$	$k_1 =$ slope
Second order	$1/q_t = 1/q_0 - k_2 t$	$1/q_t$ vs t	$k_2 = slope$
Pseudo-first order	$ln (q_e - q_t) = ln q_e - k_1't$	$ln (q_e - q_t)$ vs t	$k_1' = slope$
Pseudo-second order	$t/q_t = 1/k_2' {q_e}^2 + (1/q_e) t$	$t/q_t$ vs $t$	$q_e$ = intercept $k_2'$ = slope <sup>2</sup> /intercept $q_e$ = 1/slope h = 1/intercept
Elovich	$q_t = 1/\beta \ln (\alpha\beta) + (1/\beta) \ln t$	$q_t$ vs $ln t$	a = slope
			$\beta = \text{intercept}$
Power function	$ln q_t = ln b + k_f (ln t)$	ln qt vs ln t	$k_f = slope$
			b=intercept
Intraparticle diffusion	$q_t = c + k_{id} t^{0.5}$	$q_t vs t^{0.5}$	$k_{id}$ = slope
			c = intercept

**Table 3** Coefficients of determination ( $r^2$ ) and standard errors of estimate (SEE) for kinetic models used to model TCE kinetic data onto biochars derived from soybean stover (S-300 and S-700) and peanut shells (P-300 and P-700), commercial oak biochar (OW), and activated carbon (AC)

Adsorbent	First order		Second order		Pseudo-first order		Pseudo-second order		Elovich		Power function		Intraparticle diffusion	
	$r^2$	SEE	$r^2$	SEE	$r^2$	SEE	$r^2$	SEE	$r^2$	SEE	$r^2$	SEE	$r^2$	SEE
S-300	0.485	0.070	0.478	0.004	0.481	0.202	0.985	1.078	0.464	1.430	0.478	0.071	0.495	1.388
S-700	0.788	0.080	0.705	0.004	0.816	0.076	0.982	0.711	0.878	1.355	0.899	0.055	0.892	1.279
P-300	0.726	0.098	0.647	0.006	0.679	0.130	0.974	0.820	0.816	1.381	0.834	0.077	0.819	1.466
P-700	0.894	0.049	0.868	0.002	0.963	0.058	0.993	0.520	0.861	1.518	0.881	0.051	0.948	1.007
OW	0.674	0.303	0.463	0.051	0.763	0.194	0.916	5.225	0.856	1.977	0.874	0.207	0.908	1.581
AC	0.676	0.055	0.655	0.002	0.894	0.219	0.999	0.023	0.877	1.300	0.866	0.035	0.794	1.687

 $(k_{id})$  was relatively high for AC (1.339 mg g<sup>-1</sup> min<sup>-0.5</sup>), S-700 (0.618 mg g<sup>-1</sup> min<sup>-0.5</sup>), P-700 (0.575 mg g<sup>-1</sup> min<sup>-0.5</sup>), and P-300 (0.599 mg g<sup>-1</sup> min<sup>-0.5</sup>), showing high adsorption rates.



**Fig. 3** Linear regression fittings of **a** pseudo-second order and **b** intraparticle diffusion models for TCE adsorption kinetics on biochars derived from soybean stover (S-300 and S-700) and peanut shells (P-300 and P-700), commercial biochar (OW) and activated carbon (AC)

The boundary layer thickness (c) ranged from 2.65 to 31.37. Regarding the boundary layer effect, the low c values for OW (2.65) indicated less resistance to mass transfer, thus causing an increase in the mobility of TCE towards carbonaceous adsorbent (Kannan and Sundaram 2001; Hameed and El-Khaiary 2008). The macro- and meso-porous structures of the adsorbents (Fig. 1), especially in the cases of OW, S-700, and P-700 biochars, may have resulted in greater diffusion of TCE within adsorbent particles. In the batch type kinetics experiment, the intraparticle diffusion has been reported to be the rate-limiting step by El-Ashtoukhy et al. (2008).

The relation between adsorbate mass per unit adsorbent mass can also be described by the power function equation (Witek-Krowiak et al. 2011). The values of  $r^2$  and *SEE* calculated in the power function model ranged from 0.834 to 0.899 and 0.035 to 0.207, respectively, for various adsorbents except S-300. The rate coefficient ( $k_{ff}$ ) values were high for OW (0.373 mg g<sup>-1</sup> min<sup>-1</sup>), S-700 (0.148 mg g<sup>-1</sup> min<sup>-1</sup>), and P-300 (0.162 mg g<sup>-1</sup> min<sup>-1</sup>), indicating an increase in TCE adsorption on these adsorbents with time.

The Elovich kinetic model, which was originally applied to describe the gas adsorption phenomenon, is now widely used to explain the aqueous contaminants sorption by assuming strong heterogeneity of sorbent surface (Plazinski et al. 2009). The experimental data had a good fit with the Elovich model as indicated by  $r^2$  values of 0.816–0.878 except S-300. The initial adsorption rate ( $\alpha$ ) for various carbonaceous adsorbents was in the order: AC (4.397 mg g<sup>-1</sup> min<sup>-1</sup>)>OW (3.627 mg g<sup>-1</sup> min<sup>-1</sup>)>P-700 (3.384 mg g<sup>-1</sup> min<sup>-1</sup>)> S-700 (3.269 mg g<sup>-1</sup> min<sup>-1</sup>)>P-300(2.934 mg g<sup>-1</sup> min<sup>-1</sup>)> S-300 (1.140 mg g<sup>-1</sup> min<sup>-1</sup>), indicating relatively high adsorption on biochars produced at 700 °C. This also implies the predominance of TCE chemical sorption on these materials assuming a multilayer sorption, with each layer exhibiting different activation energies for chemisorption (Alberti et al. 2012).

Except for P-700, the first, second, and pseudo-first order rate kinetics could not adequately describe the experimental data as apparent from the  $r^2$  values of <0.8 (Table 3).

Table 4 Parameters obtained from kinetic models used for TCE sorption dynamics modeling onto biochars derived from soybean stover (S-300 and S-700) and peanut shells (P-300 and P-700), commercial oak biochar (OW), and activated carbon (AC)

Adsorbent	First order	Second order	Pseudo-first	order	Pseudo-second order			Elovich		Power function		Intraparticle diffusion	
	$k_1$	<i>k</i> <sub>2</sub>	<i>k</i> <sub>1</sub> ′	$q_e$	<i>k</i> <sub>2</sub> ′	$q_e$	h	α	β	k <sub>f</sub>	b	k <sub>id</sub>	С
S-300	$0.355 \times 10^{-3}$	$1.788 \times 10^{-5}$	$1.085 \times 10^{-3}$	0.577	$2.903 \times 10^{-3}$	21.94	1.398	1.140	13.94	0.058	2.684	0.204	16.83
S-700	$1.010 \times 10^{-3}$	$4.466 \times 10^{-5}$	$1.331 \times 10^{-3}$	1.063	$1.141 \times 10^{-3}$	29.38	0.985	3.269	6.859	0.148	2.413	0.618	15.40
P-300	$1.323 \times 10^{-3}$	$7.138 \times 10^{-5}$	$1.878 \times 10^{-3}$	0.960	$1.633 \times 10^{-3}$	24.30	0.964	2.934	5.487	0.162	2.186	0.599	12.35
P-700	$0.606 \times 10^{-3}$	$2.036 \times 10^{-5}$	$1.332 \times 10^{-3}$	1.130	$0.779 \times 10^{-3}$	37.00	1.066	3.384	12.43	0.115	2.794	0.575	21.28
OW	$1.179 \times 10^{-3}$	$12.73 \times 10^{-5}$	$0.941 \times 10^{-3}$	1.305	$0.250 \times 10^{-3}$	21.38	0.114	3.627	-7.949	0.373	0.339	0.514	2.65
AC	$2.378 \times 10^{-3}$	$6.093 \times 10^{-5}$	$19.12 \times 10^{-3}$	1.200	$5.409 \times 10^{-3}$	45.01	10.96	4.397	24.01	0.113	3.274	1.339	31.37

Overall, the pseudo-second order, Elovich, and intraparticle diffusion models adequately described the experimental data, thereby, indicating chemisorption and intraparticle diffusion to be the dominant mechanisms in the TCE adsorption on various carbonaceous adsorbents.

### Biochar properties and TCE adsorption

The structural characteristics and elemental compositions of biochars influenced TCE removal from water. Particularly in P-700 and S-700, the high surface area and pore volume, and relatively low H/C and O/C molar ratios led to relatively high TCE adsorption. This validated that pyrolysis temperature is a pivotal factor influencing the biochars properties and ultimately affects their adsorption capacities (Chun et al. 2004; Chen et al. 2008). The  $q_e$  value calculated from the pseudo-second order kinetics model was plotted as a function of surface area of the carbonaceous adsorbents (Fig. 4). A linear positive correlation indicated that the adsorbents having high surface area had high adsorption capacity for TCE. Furthermore, the lower H/C and O/C molar ratios of P-700, S-700, and AC (Table 1) imparted high aromaticity and low polarity of these materials, resulting in the TCE removal enhancement. The polarity of carbon surfaces is generally decreased by the removal of acidic functional groups at high temperature (Li et al. 2002), minimizing the chance of water cluster formation on the carbon surfaces, thus increasing the sorption of organic contaminants such as TCE (Karanfil and Dastgheib 2004).

The micro-porous structure of biochars (pore size <2 nm) is another important factor controlling TCE adsorption. The TCE diffusion within carbon particles of biochars was also affirmed from a good fit of the experimental data with the intraparticle diffusion model. Another plausible explanation for the relatively high TCE adsorption on P-700, S-700, and AC may be related to their pore diameters (Table 1). Tri-chloroethylene is a planar molecule having a diameter of 0.56 nm. Thus, it can easily be diffused into the adsorbents pores having a diameter greater than its kinetic diameter. Li et al. (2002) reported that for effective TCE adsorption to take place, a large volume of micropores having ~1.3 to 1.8

times greater diameter than the TCE kinetic diameter are needed in the adsorbents. In the present investigation, P-700 and S-700 were characterized by the pore diameter which is  $\sim$ 2 times greater than TCE kinetic diameter. These findings are in good agreement with findings of Li et al. (2002).

To a lesser extent, feedstock type also influenced the TCE adsorption capacity of biochars. Comparatively, biochars derived from peanut shells were more effective than those derived from soybean stover (Fig. 2). This could probably be due to greater inorganic components in the soybean stover-derived biochars as indicated by higher ash contents (10.41 % to 17.18 %) compared to peanut shell-derived biochars (1.24 % to 8.91 %). Ash minerals can block the organic sorption sites in biochars due to the interaction with inorganic moiety (Zhang et al. 2013).

The efficiency of biochars on TCE adsorption was dependent on surface area, contact time, solute affinity towards adsorbent, number of carbon atoms, and molecular size with respect to adsorbent pore size. The adsorbent properties primarily influenced the TCE removal from water as observed from the analogous behavior of biochars produced at



Fig. 4 Correlation between equilibrium sorption capacities of different biochars calculated from pseudo-second order kinetic equation and surface areas

the same pyrolytic temperature. Therefore, a detailed description of adsorbent properties is required to fully utilize the adsorbent capacity in water and wastewater treatment.

#### Conclusions

In the present investigation, biochars were produced by pyrolyzing soybean stover and peanut shells at 300 °C and 700 °C. The biochars produced at 700 °C were characterized as high surface area, microporosity, aromaticity, and low polarity. High equilibrium sorption capacity was obtained for the biochars produced at a high pyrolysis temperature and commercial AC because of their high surface areas. Furthermore, peanut shell biochar was more effective than biochar produced from soybean stover for TCE adsorption from water. The pseudo-second order and intraparticle diffusion models best fitted the TCE adsorption experimental data obtained for various types of carbonaceous adsorbents. This indicates that chemisorption and pore diffusion were the dominating mechanisms controlling the TCE adsorption. Biochar properties, as affected by the pyrolysis temperature, also influenced their behavior towards TCE adsorption. Overall, biochars derived from agricultural waste materials can be successfully utilized for TCE remediation from water and wastewater, and the specific characteristics of biochar including high surface area, less pore size, high aromaticity and less polarity are recommended for its best performance.

Acknowledgments This study was supported by the Ministry of Environment, Republic of Korea as "The GAIA Project (No. 173-092-010)." Instrumental analysis was supported by the Korea Basic Science Institute, the Environmental Research Institute and the Central Laboratory of Kangwon National University, Korea.

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