

# Comparative Study of Nickel-Iron Composite with Fe<sub>3</sub>O<sub>4</sub> **Nanoparticles for the Adsorption of Chromium from Aqueous Medium**

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**Abstract** Water contamination caused by hexavalent chromium [Cr(VI)] ions has attracted interest since Cr(VI) ions are highly poisonous and carcinogenic, posing major health risks. We report a simple and efficient approach for preparing  $Fe<sub>3</sub>O<sub>4</sub>$  nanoparticles and  $Fe<sub>3</sub>O<sub>4</sub>/NiO$  composite using the chemical co-precipitation method for Cr(VI) removal. The produced magnetic adsorbents could be readily isolated from the solution using an external magnet and were used for Cr(VI) ion adsorption. The adsorbents were characterized by XRD, VSM, FT-IR, FE-SEM, EDX, and BET analyses. The Langmuir type 1 isotherm provided a good representation of the adsorption data when the Langmuir, Freundlich, Temkin, Harkins–Jura, Hasley, and Redlich-Peterson models were utilized to analyze the adsorption isotherm data. The adsorption capacities of  $Fe<sub>3</sub>O<sub>4</sub>$  and  $Fe<sub>3</sub>O<sub>4</sub>/NiO$  composite calculated from the Langmuir type 1 model were 96.15 mg g<sup>-1</sup> and 150 mg g<sup>-1</sup>, respectively. The saturation magnetization of  $Fe<sub>3</sub>O<sub>4</sub>$  and  $Fe<sub>3</sub>O<sub>4</sub>/NiO$ 

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composite was 60.54 emu/g and 11.09 emu/g, respectively. Both adsorbents may be easily and quickly separated from tainted water by an external magnetic feld. According to the fndings, both adsorbents are possibly reusable adsorbents for Cr(VI) adsorption. The main advantage of the material is that, due to its magnetic nature, it is easily separated from the adsorbate and may thus be used efficiently in sorption studies. As a result, this magnetic adsorbent provides a viable solution for the successful management of chromium-containing wastewater.

**Keywords** Fe<sub>3</sub>O<sub>4</sub> nanoparticles  $\cdot$  Cr(VI) adsorption. Desorption of Cr(VI) · Wastewater

### **1 Introduction**

Indeed, the current prosperity of industries has evident positive efects on economic growth, but the release of industrial wastes into water bodies without proper treatment has the potential to wipe out humanity (Eltaweil et al., [2021](#page-19-0)). The typical contaminants, like heavy metal ions and organic dyes, often coexist in polluted water and have signifcant ecological effects on the ecosphere because of their bio-accumulation, non-biodegradability, and environmental persistence (Tang et al., [2021](#page-21-0); Wen et al., [2019\)](#page-21-1).

A severe concern for the environment and human health is heavy metal contamination. Metals are generally non-biodegradable and enter the environment

through a variety of anthropogenic and natural sources. Chromium has recently gained a lot of interest among heavy metals due to its toxicity in the environment (Imran et al., [2020\)](#page-20-0). Long-term exposure to high chromium concentrations increases the risk of diabetes, skin disease, respiratory illness, and gastrointestinal disease. The most common oxidation states of chromium in nature are Cr(III) and Cr(VI) (Manoj et al., [2021](#page-20-1); Rahman & Singh, [2019](#page-20-2); Teklay, [2016](#page-21-2)). Many scientists are interested in Cr(VI) since it is a common carcinogen that results in negatively charged compounds with great environmental mobility (Yao et al., [2020;](#page-21-3) Zou et al., [2021\)](#page-21-4). As a result, removing Cr(VI) from aqueous solutions before releasing them into the environment becomes essential (Pourmortazavi et al., [2019](#page-20-3); Shekhawat et al., [2022\)](#page-21-5).

Various techniques, including ion exchange, ultrafltration, coagulation, electrodeposition, reverse osmosis, chemical precipitation, and solvent extraction, have been developed by researchers to eliminate hexavalent chromium ions from wastewater. However, these methods have signifcant disadvantages and are not completely suitable for Cr(VI) adsorption. Owing to its flexibility, low cost, high efficiency, and simple operation, adsorption technology is recognized as the best technique among these (Pavithra et al., [2021](#page-20-4)).

A solid material that permits liquid or gaseous molecules to adhere to its surface is known as an adsorbent. The adsorbent surface's chemical and physical characteristics, in addition to the soluble compounds' qualities, determine the adsorbent's performance. A good adsorbent material should have both a minimal volume and a wide surface area. High mechanical strength, chemical and thermal stability, high porosity, and small pore diameter—which result in more exposed surface area and, consequently, appropriate surface chemistry that leads to high adsorption capacity—must be among the other characteristics. To suit the needs of the application, adsorptive materials can be designed as pellets, rods, moldings, or monoliths. Adsorbents made of a variety of materials have been employed for a wide range of purposes, including desiccants, water treatment, separation, catalysis, and indicators (Abegunde et al., [2020;](#page-19-1) Younas et al., [2021\)](#page-21-6).

Metal-contaminated wastewater is frequently treated using a variety of porous adsorbents, including activated carbon, natural clay, chitosan composite, nanoparticle and polymer-based adsorbents, magnetic adsorbents, etc. (Abbas & Hussain, [2016](#page-19-2); Abbas et al., [2015](#page-19-3); Arora et al., [2019;](#page-19-4) Kobielska et al., [2018;](#page-20-5) Lodhi et al., [2019](#page-20-6); Soni et al., [2020a](#page-21-7); Wang et al., [2023](#page-21-8); Yan et al., [2020\)](#page-21-9).

Several studies have been carried out to investigate the usage of magnetic adsorbents as a safe, efective, and low-cost material for separating these suspended adsorbents in wastewater. The variation in the response of magnetic substances to outside magnetic felds is associated with a variety of characteristics, since certain substances are much more magnetic than others. Magnetic nanoparticles (MNPs) have recently been identifed as outstanding adsorbents for the elimination of heavy metals. However, magnetism is not the only consideration for their application. When compared to other materials, their exceptional surface charge and redox activity properties are signifcant reasons for their qualifcation.

 $Fe<sub>3</sub>O<sub>4</sub>$  nanoparticles have gained interest as a type of magnetic nanoparticle due to their unique magnetic characteristics and ease of preparation. But  $Fe<sub>3</sub>O<sub>4</sub>$  nanoparticles are prone to agglomerate and lose their magnetic characteristics, which decreases the efficiency of removal. Significant attempts have been made to modify  $Fe<sub>3</sub>O<sub>4</sub>$  nanoparticles using physicochemical approaches in order to overcome these drawbacks, retain their magnetic properties, and improve their adsorption performance and specifc stability (Abdullah et al., [2019;](#page-19-5) Mohammadi et al., [2021;](#page-20-7) Sharma et al., [2019;](#page-21-10) Song et al., [2021;](#page-21-11) Zhao et al., [2021\)](#page-21-12).

In this study, we present the use of  $Fe<sub>3</sub>O<sub>4</sub>$  nanoparticles and  $Fe<sub>3</sub>O<sub>4</sub>/NiO$  composite as efficient materials for the elimination of Cr(VI). Parameters afecting the adsorption process, viz., the adsorbent's dose, contact time, pH, initial concentration, temperature efect, and regeneration study, were evaluated to understand the mechanism. The material was examined using BET, XRD, FT-IR, FE-SEM, EDX, and vibrating-sample magnetometer (VSM) analysis in order to determine its chemical composition and surface characteristics. The use of  $Fe<sub>3</sub>O<sub>4</sub>$  nanoparticles and  $Fe<sub>3</sub>O<sub>4</sub>/NiO$  composite as potential adsorbents for Cr(VI) removal was further probed using kinetic and isotherm models. Moreover, the reusability of both adsorbents was examined for up to six cycles.

# **2 Experimental Section and Adsorption Experiment**

### 2.1 Materials

All analytical grade chemicals as well as reagents were purchased from Sigma-Aldrich and utilized immediately without any additional refning. During the synthesis and adsorption studies, iron (II) chloride tetrahydrate, nickel (II) nitrate hexahydrate, iron (III) chloride hexahydrate, sodium hydroxide, and acetone were utilized.  $K_2Cr_2O_7$  was purchased from E. Merck, India. All aqueous solutions for the adsorption studies were prepared using Millipore Milli-Q® ultrapure water. As Cr(VI) has been chosen as the model contaminant in this investigation, solution of Cr(VI) if desired concentrations were prepared and used as adsorbate solution.

### 2.2 Preparation Fe<sub>3</sub>O<sub>4</sub> Nanoparticles

4.75 g of iron (II) chloride tetrahydrate and 9 g of iron (III) chloride hexahydrate salts were added in 100 mL of deionized (DI) water. In this synthesis process, the stoichiometry of  $FeCl<sub>2</sub>·4H<sub>2</sub>O/FeCl<sub>3</sub>·6H<sub>2</sub>O$  was 1:2. The reaction was conducted in a  $N_2$  environment at 80 °C while being vigorously stirred. A 25-mL aliquot of sodium hydroxide solution was dropped into the mixture while it was still being stirred, resulting in a pH of 10 and the production of a black precipitate. The resulting solution was then centrifuged three times with deionized (DI) water and then with acetone. External magnet was used to collect the  $Fe<sub>3</sub>O<sub>4</sub>$  nanoparticles and then it was rinsed with water (Fig. [1](#page-2-0)) (Mohammadi et al., [2021](#page-20-7); Weber & Morris, [1963\)](#page-21-13).

$$
Fe^{2+}(aq) + 2Fe^{3+}(aq) + 8OH^{-}(aq) \rightarrow Fe_3O_4(s) + 4H_2O
$$

### 2.3 Preparation of  $Fe<sub>3</sub>O<sub>4</sub>/NiO$  Composite

 $Fe<sub>3</sub>O<sub>4</sub>/NiO$  composite was prepared by the co-precipitation technique. 3.1 g of  $Ni(NO<sub>3</sub>)<sub>2</sub>·6H<sub>2</sub>O$  and 0.31 g of  $Fe<sub>3</sub>O<sub>4</sub>$  nanoparticles were added to 20.0 mL of water. The solution's temperature was then raised to 75 °C using a magnetic stirrer. The second step was adding 20 mL of NaOH to original solution dropwise until a black-green suspension was attained and stirred for 60 min. After 60 min, a powerful magnet was used to remove the composite from the solution. They were then thoroughly washed with acetone and DI water and placed in an oven at 60 °C show in Fig. [2](#page-3-0) (Hassan & Hrdina, [2022](#page-20-8)).

$$
\text{Ni(NO}_3)_2/\text{Fe}_3\text{O}_4 + 2\text{NaOH} \rightarrow \text{Ni(OH)}_2/\text{Fe}_3\text{O}_4 + 2\text{NaNO}_3
$$

### 2.4 Adsorption Experiments

Using the required chromium stock solution, adsorption studies were conducted to assess the tendency of  $Fe<sub>3</sub>O<sub>4</sub>$  nanoparticles and  $Fe<sub>3</sub>O<sub>4</sub>/NiO$  composite for adsorption. In addition, several optimal conditions involving signifcant factors such as pH (4–9), adsorbent dose  $(0.01-0.14 \text{ g/L})$ , contact time  $(5-70 \text{ min})$ , and initial chromium concentration (2–20 mg/L) were



<span id="page-2-0"></span>**Fig. 1** Preparation of  $Fe<sub>3</sub>O<sub>4</sub>$  nanoparticles

<span id="page-3-0"></span>

studied. NaOH and HCl solutions were used to equilibrate the pH. Proceeding adsorption, the remaining chromium concentration was analyzed by AAS. Using Eqs. [\(1](#page-3-1)) and [\(2](#page-3-2)), the adsorption percent and equilibrium absorption of Cr(VI) by  $Fe<sub>3</sub>O<sub>4</sub>$  nanoparticles and  $Fe<sub>3</sub>O<sub>4</sub>/NiO$  composite from aqueous solution were calculated.

% Adsorption = 
$$
\frac{(C_0 - C_e) \times 100}{C_0}
$$
 (1)

Adsorption Capacity
$$
(q_e)
$$
 =  $\frac{(C_0 - C_e) \times V}{m}$  (2)

where  $q_e$  is the adsorption capacity at equilibrium (mg/g),  $C_0$  represents the initial Cr(VI) concentration  $(mg/L)$ ,  $C_e$  is the equilibrium Cr(VI) concentration, *V* is the volume of the solution (L), and *m* is the mass of the adsorbent  $(g)$  (Li et al., [2021](#page-20-9)).

### 2.5 Characterization

XRD of the Fe<sub>3</sub>O<sub>4</sub> nanoparticles and Fe<sub>3</sub>O<sub>4</sub>/NiO composite were recorded on Bruker D8 Discover X-ray difractometer using Cu Kα radiation. For XRD analysis, powdered and degassed samples were directly put on the sample disk of XRD and then exposed to the X-ray source. The XRD pattern was recorded in the 2θ range of 10° and 70°. XRD studies revealed the crystalline character of the adsorbents. By using surface area analyzer (Quantachrome Autosorb iQ surface analyzer),  $N_2$ adsorption–desorption studies were carried out to <span id="page-3-2"></span><span id="page-3-1"></span>characterize their textural properties (pore volume and the BET specifc surface area). For the analysis of surface area, the samples were frst degassed for 3.0 h to remove volatile gases and were then placed in surface area analyzer for  $N_2$  adsorption–desorption. The FTIR spectra were recorded using a Perkin-Elmer FT-IR spectrometer. A spectrum of the adsorbents in the 400–4000  $cm^{-1}$  range to characterize the type of surface functional groups and the nature of chemical bonding. For the functional group analysis, the samples were frst mixed with KBr powder and the sample pellets with KBr were prepared in the form for thin flms using a pelletizer. Then the sample was placed in the FTIR chamber for analysis. A feld emission scanning electron microscope was used to investigate the morphology of  $Fe<sub>3</sub>O<sub>4</sub>$  nanoparticle and  $Fe<sub>3</sub>O<sub>4</sub>/NiO$  composite as well as their elemental composition. FE-SEM equipped with EDX (FE-SEM, MIRA3 TESCAN, and an INCA Energy X-MAX-50) was used to characterize the morphology and chemical composition of the adsorbents used in the study. For FE-SEM analysis, the adsorbents were frst coated on carbon tape present on the sample holder, so as to make them conductive, and then the stub with the sample was placed in the FE-SEM chamber for study. The magnetic characteristics of the adsorbents were determined using a LakeShore 7404 VSM. The magnetic sample is mounted on the sample holder and placed between the electromagnetic poles, generally horizontally, for VSM measurement. At the ambient temperature, the hysteresis loops were measured on the VSM.

## **3 Results and Discussion**

#### 3.1 BET Surface Area

The  $N_2$  gas adsorption–desorption isotherm was observed in the relative pressures  $(p/p_0)$  values to estimate the surface area and porosity values of the synthesized adsorbents. BET sorptometry was performed to study the pore volume, average pore size, and surface area of the material. The  $N_2$  adsorption–desorption curves for the  $Fe<sub>3</sub>O<sub>4</sub>$  nanoparticles and  $Fe<sub>3</sub>O<sub>4</sub>/NiO$  composite are depicted in Fig. [3,](#page-4-0) and their characteristic parameters are listed in Table [1.](#page-4-1) Furthermore, this figure shows that  $Fe<sub>3</sub>O<sub>4</sub>$ nanoparticles and  $Fe<sub>3</sub>O<sub>4</sub>/NiO$  composites follow the IUPAC type (IV) isotherm. In other words, it denotes a structure with the mesoporous nature of the adsorbents (Koohi et al., [2021](#page-20-10); Mohammadi et al., [2021\)](#page-20-7). The surface area of synthesized  $Fe<sub>3</sub>O<sub>4</sub>$ nanoparticles and  $Fe<sub>3</sub>O<sub>4</sub>/NiO$  composites is equivalent to 110.7 m<sup>2</sup> g<sup>-1</sup> and 163.9 m<sup>2</sup> g<sup>-1</sup>, respectively. The Langmuir surface area and total pore volume of  $Fe<sub>3</sub>O<sub>4</sub>$  nanoparticles and  $Fe<sub>3</sub>O<sub>4</sub>/NiO$  composites were 171.9 m<sup>2</sup> g<sup>-1</sup>, 287.4 m<sup>2</sup> g<sup>-1</sup>, and 0.484 cm<sup>3</sup> g<sup>-1</sup>, 0.327 cm<sup>3</sup> g<sup>-1</sup>, respectively. The average pore size of the  $Fe<sub>3</sub>O<sub>4</sub>$  nanoparticles and  $Fe<sub>3</sub>O<sub>4</sub>/NiO$ composite was 87.42 Å and 39.92 Å, respectively.

<span id="page-4-1"></span>**Table 1** Surface parameters of  $Fe<sub>3</sub>O<sub>4</sub>$  nanoparticle and  $Fe<sub>3</sub>O<sub>4</sub>$ NiO composite before Cr(VI) adsorption

Parameters	Fe <sub>3</sub> O <sub>4</sub>	Fe <sub>3</sub> O <sub>4</sub> /NiO
Specific surface area $(m^2/g)$	110.7	163.9
Langmuir surface area $(m^2/g)$	171.9	287.4
Average pore size $(\AA)$	87.42	39.92
Total pore volume $(cc/g)$	0.484	0.327

As a result, the higher the surface area, the greater will be the adsorption capacity.

### 3.2 Fourier Transform Infrared Spectroscopy

For understanding the nature of chemical bonding and the kinds of surface functionalities, the adsorbents used in this study were examined by FT-IR. The FT-IR spectra of  $Fe<sub>3</sub>O<sub>4</sub>$  nanoparticles and Cr(VI)loaded  $Fe<sub>3</sub>O<sub>4</sub>$  nanoparticles are demonstrated in Fig. [4](#page-5-0)a. Likewise, the FT-IR spectra of the  $Fe<sub>3</sub>O<sub>4</sub>/$ NiO composite before and after the adsorption process are demonstrated in Fig. [4b](#page-5-0).

The distinctive peaks of nanoparticles are visible in the FT-IR spectra of  $Fe<sub>3</sub>O<sub>4</sub>$  nanoparticles. The tensile vibrations of the Fe–O and Ni–O bonds were measured between 500 and 650  $cm^{-1}$ . This band is



<span id="page-4-0"></span>**Fig. 3**  $N_2$  sorption isotherm of **a** Fe<sub>3</sub>O<sub>4</sub> nanoparticle, **b** Fe<sub>3</sub>O<sub>4</sub>/NiO composite



<span id="page-5-0"></span>**Fig. 4** FTIR spectra of **a** Fe<sub>2</sub>O<sub>4</sub> nanoparticles and **b** Fe<sub>2</sub>O<sub>4</sub>/NiO composite (before and after Cr(VI) adsorption)

very sharp and has strong intensity, indicating the crystallinity of the sample.

The broad bands around 3401 cm<sup>-1</sup> and 1626 cm<sup>-1</sup> were due to the O–H stretching vibration of surfaceadsorbed water molecules. The bands located around 1386 cm−1 and 1076 cm−1 were attributed to the asymmetric and symmetric stretching vibrations of COO− (Fig. [4](#page-5-0)a). The O–H stretching vibration of surface-adsorbed water molecules is responsible for the broad band around 3491  $cm^{-1}$  (Fig. [4b](#page-5-0)) (Chaki et al., [2015;](#page-19-6) Mahdavi & Amini, [2016](#page-20-11); Munkaila et al., [2021;](#page-20-12) Nodehi et al., [2022](#page-20-13); Shi et al., [2020\)](#page-21-14).

After Cr(VI) adsorption, there is a minor shift in the band centered at  $549 \text{ cm}^{-1}$ , corresponding to the Fe–O bonds, which changes to  $547 \text{ cm}^{-1}$ , suggesting the formation of Fe–O–Cr on the magnetite surface. Peak values in  $Fe<sub>3</sub>O<sub>4</sub>$  and  $Fe<sub>3</sub>O<sub>4</sub>/NiO$  composites showed signifcant changes in Table [2](#page-5-1).

# 3.3 X-ray Difraction

To understand more about the chemical and physical composition of the magnetic particles, X-ray difraction (XRD) is a highly valuable technique. Figure [5](#page-6-0) represents the XRD pattern of  $Fe<sub>3</sub>O<sub>4</sub>$  nanoparticle and  $Fe<sub>3</sub>O<sub>4</sub>/NiO$  composite. The crystalline phase of  $Fe<sub>3</sub>O<sub>4</sub>$ nanoparticle and  $Fe<sub>3</sub>O<sub>4</sub>/NiO$  composite was analyzed by XRD.

<span id="page-5-1"></span>



<span id="page-6-0"></span>**Fig. 5** XRD spectra for **a** Fe<sub>3</sub>O<sub>4</sub> nanoparticle and **b** Fe<sub>3</sub>O<sub>4</sub>/NiO composite (before and after Cr(VI) adsorption)

It was notable that  $Fe<sub>3</sub>O<sub>4</sub>$  nanoparticles showed XRD pattern with diffraction peaks at  $2\theta = 30.1^{\circ}$ , 35.5°, 43.2°, 53.6°, 57.3°, and 62.7° relative to the difractions of (220), (311), (400), (422), (511), and (440) crystal faces of  $Fe<sub>3</sub>O<sub>4</sub>$  (Mohammadi et al., [2021\)](#page-20-7). The peaks at 2θ=30.1°, 33.03°, 35.5°, 38.38°, 43.23°, 51.8°, 57.2°, 59.09°, 62.7°, 75°, and 79.4° are associated with  $Fe<sub>3</sub>O<sub>4</sub>/NiO$  composite. The crystal plane of NiO is (1 1 1), (2 0 0), (2 2 0), (2 2 2), and (4 0 0) (Ashan et al., [2018](#page-19-7); Koohi et al., [2021;](#page-20-10) Mahdavi & Amini, [2016](#page-20-11)). The crystallite size of produced  $Fe<sub>3</sub>O<sub>4</sub>$ -NPs can be estimated using the Debye–Scherrer equation, which demonstrates a link between X-ray difraction peak broadening and crystallite size. The Debye–Scherrer equation is presented as follows:

$$
d = \frac{k\lambda}{\beta_{hkl}cos\theta_{hkl}}
$$

The equation for manufactured Fe3O4 NPs for (hkl) phase is as follows: *d* is the crystallite size, *k* is the Scherrer constant (0.9),  $\lambda$  is the X-ray wavelength of radiation for Cu Kα  $(0.154 \text{ nm})$ , βhkl is the full-width at half maximum (FWHM) at (hkl) peak in radian, and θ hkl is the difraction angle for the (hkl) phase. The crystallite size of synthesized  $Fe<sub>3</sub>O<sub>4</sub>$ NPs was determined to be 6.25 nm using an equation based on the full-width at half maximum of the Fe<sub>3</sub>O<sub>4</sub> (311) diffraction peak at  $2\theta$  = 35.35°. Based on the X-ray diffraction pattern, the produced  $Fe<sub>3</sub>O<sub>4</sub>$  NPs were determined to be high purity crystalline, with no impurity peak detected.

### 3.4 FE-SEM Analysis

The morphology of  $Fe<sub>3</sub>O<sub>4</sub>$  nanoparticles and  $Fe<sub>3</sub>O<sub>4</sub>$ / NiO composite was investigated using FE-SEM, and the elemental composition was determined using EDX. SEM and EDX images of both are displayed in Fig. [6.](#page-8-0) The spherical-shaped particles with agglomeration were observed in synthesized  $Fe<sub>3</sub>O<sub>4</sub>$  nanoparticles (Fig. [6a](#page-8-0)). In Fig. [6b](#page-8-0), the synthesized composite particles are distributed relatively uniformly. Also, the particles are strongly clumped together. The inserted figure shows the porosity in the  $Fe<sub>3</sub>O<sub>4</sub>/NiO$ composite. Figure [6](#page-8-0)c and d depict the corresponding EDX spectra, which show the elemental composition of Fe<sub>3</sub>O<sub>4</sub> nanoparticles and Fe<sub>3</sub>O<sub>4</sub>/NiO composites (Mohammadi et al., [2021](#page-20-7); Nodehi et al., [2022\)](#page-20-13).

### 3.5 Magnetization

To evaluate the adsorbents' magnetic properties, VSM tests was utilized (Ashan et al., [2018](#page-19-7)). Magnetization curves were utilized to examine the magnetic properties of the magnetic materials under investigation. Figure [7](#page-9-0) illustrates the magnetization curves of Fe<sub>3</sub>O<sub>4</sub> nanoparticles, Fe<sub>3</sub>O<sub>4</sub>/NiO, and Fe<sub>3</sub>O<sub>4</sub>/NiO-Cr(VI) composites. The saturation magnetization





<span id="page-8-0"></span> $\blacktriangleleft$  **Fig.** 6 FESEM image of **a** Fe<sub>3</sub>O<sub>4</sub> nanoparticles, **b** Fe<sub>3</sub>O<sub>4</sub>/NiO composite, and EDX image of  $\mathbf{c}$  Fe<sub>3</sub>O<sub>4</sub> nanoparticles, **d** Fe<sub>3</sub>O<sub>4</sub>/ NiO composite, **e** Fe<sub>3</sub>O<sub>4</sub> nanoparticles after absorption Cr, **f** Fe3O4/NiO composite after absorption Cr

of the Fe<sub>3</sub>O<sub>4</sub> nanoparticle and Fe<sub>3</sub>O<sub>4</sub>/NiO composite was 60.54 emu/g and 11.09 emu/g, respectively, though, even at this saturation magnetization value, a magnetic field is sufficient to separate the adsorbent from the aqueous medium (Mahmoudi & Behnajady, [2018\)](#page-20-14). The existence of a non-magnetic shell reduces the magnetization of the  $Fe<sub>3</sub>O<sub>4</sub>/NiO$  composite. The shell's interaction with  $Fe<sub>3</sub>O<sub>4</sub>$  nanoparticle surface locks of the surface spins, lowering magnetic torque in the  $Fe<sub>3</sub>O<sub>4</sub>/NiO$  composite. Because lowering the size of the particle leads to an increase in the proportion of surface atoms, even minor irregularities in the surface layers have a significant impact on nanoparticle magnetic saturation (Nodehi et al., [2022](#page-20-13)).

## 3.6 Zeta Sizer

The particle size distribution of  $Fe<sub>3</sub>O<sub>4</sub>$  nanoparticles was analyzed using zeta sizer. The particle size distribution nanoparticles was found to be 180.7 nm.

Zeta potential further confrmed the successful fabrication of  $Fe<sub>3</sub>O<sub>4</sub>$  nanoparticles. The zeta potential of Fe<sub>3</sub>O<sub>4</sub> nanoparticles was  $-22.7$  eV show in Fig. [8](#page-9-1).

# 3.7 Study of Kinetics of Adsorption of Cr(VI) on to the Adsorbents,  $Fe<sub>3</sub>O<sub>4</sub>$  Nanoparticle, and  $Fe<sub>3</sub>O<sub>4</sub>$ / NiO Composite

Adsorption kinetics explains how the material's chemical and physical characteristics afect the reaction's rate and pathways. Using the pseudo-frst-order (PFO) and pseudo-second-order (PSO) models, the kinetics of adsorption were explained.

Adsorption in a solid–liquid system was described using the PFO kinetic model. According to this model, one metal ion is adsorbed per sorption site on the adsorbent's surface (Suo et al., [2019](#page-21-15)). PFO is represented by

$$
\ln(q_e - q_t) = \ln q_e - k_1 \times t \tag{3}
$$

where  $k_1$  (min<sup>-1</sup>) is the PFO sorption rate constant.

The kinetic plot for PFO for Cr(VI) adsorption was obtained by plotting  $ln(q_e - q_t)$  against *t*. The rate constant and equilibrium adsorption capacity were calculated using the slope and intercept (Fig. [9](#page-10-0)a).

In accordance with the PSO model, one metal ion is adsorbed onto two sorption sites on the adsorbent's surface. This model has been utilized to investigate the kinetics of chemisorption from liquid solutions (Almomani & Bhosale, [2021](#page-19-8); Bin-Dahman & Saleh, [2024\)](#page-19-9). PSO is represented as

$$
t/q_t = 1/(k_2 \times q_e^2) + t/q_e
$$
 (4)

where  $k_2$  (g mg<sup>-1</sup> min<sup>-1</sup>) is the PSO rate constant. The graph displayed between  $t/q_t$  and  $t$  in Fig. [9](#page-10-0)b produces a straight line, and the slope and intercept may be used to get the values of  $q_e$  and  $k_2$ , respectively (Khare et al., [2018](#page-20-15)).

The  $k_1$  of PFO was found to be 0.073 and 0.115 min<sup>-1</sup> for Fe<sub>3</sub>O<sub>4</sub> nanoparticles and Fe<sub>3</sub>O<sub>4</sub>/NiO composite, respectively. While the  $k_2$  of PSO was determined to be 0.00102 and 0.0013 g mg<sup>-1</sup> min<sup>-1</sup> for  $Fe<sub>3</sub>O<sub>4</sub>$  nanoparticles and  $Fe<sub>3</sub>O<sub>4</sub>/NiO$  composite, respectively.

For Cr(VI) ions, the  $R^2$  values obtained from the PSO model were 0.988 and 0.976, while those obtained from the PFO model were 0.876 and 0.805 for Fe<sub>3</sub>O<sub>4</sub> nanoparticles and Fe<sub>3</sub>O<sub>4</sub>/NiO composite, respectively. The best-ftting model for the adsorption process was PSO, according to  $R^2$  analysis. Table [3](#page-10-1) shows the corresponding kinetic parameters. These results also revealed that the as-prepared adsorbents' adsorption kinetics may be adequately explained by the PSO model, indicating that chemical adsorption is the step that determines rate. The observations reveal that adsorption happens via chemical interactions (chemisorption) and the availability of adsorption sites. The Cr(VI) adsorption by  $Fe<sub>3</sub>O<sub>4</sub>$  nanoparticles and  $Fe<sub>3</sub>O<sub>4</sub>/NiO$  composite was thus investigated using a PSO model.

#### 3.8 Adsorption Isotherm

Adsorption isotherm is a key consideration in the development of adsorption systems and is frequently employed for the evaluation of the adsorption capacity (Li et al., [2021\)](#page-20-9). It is also used to describe the interaction between the adsorbate and the adsorbent. The adsorption capacity of  $Fe<sub>3</sub>O<sub>4</sub>$  nanoparticles and



<span id="page-9-0"></span>**Fig. 7** Magnetization curves of the  $Fe<sub>3</sub>O<sub>4</sub>$  nanoparticle,  $Fe<sub>3</sub>O<sub>4</sub>/NiO$  composite, and  $Fe<sub>3</sub>O<sub>4</sub>/NiO$  composite after Cr(VI) adsorption

 $Fe<sub>3</sub>O<sub>4</sub>/NiO$  composite was estimated using isotherm models, including Langmuir, Freundlich, Temkin, Harkins–Jura, Hasley, and Redlich and Peterson (Saraswat et al., [2020](#page-21-16)).

In order to depict monomolecular layer adsorption, the Langmuir isotherm model presupposes that the adsorption takes place on a homogenous surface and that there is no interaction between adsorbate

molecules. Linearized forms of the Langmuir isotherm are represented as

$$
Langmuir type 1 \frac{C_e}{q_e} = \frac{1}{K_L q_m} + \frac{C_e}{q_m}
$$
\n<sup>(5)</sup>

where  $K_L$  is the Langmuir adsorption equilibrium constant.

The parameters were obtained by plotting  $C_e/q_e$ vs  $C_e$ ,  $1/q_e$  vs  $1/C_e$ , and  $q_e$  vs  $q_e/C_e$  (Figs. [10](#page-11-0) and [11\)](#page-12-0) (Raghav & Kumar, [2019](#page-20-16)). The values of  $q<sub>m</sub>$  and other Langmuir parameters are shown in Table [3.](#page-10-1) For Fe<sub>3</sub>O<sub>4</sub> nanoparticles and the Fe<sub>3</sub>O<sub>4</sub>/NiO composite, the  $q_m$  value determined by the Langmuir type 1 isotherm was 96.15 mg  $g^{-1}$  and 150 mg  $g^{-1}$ , respectively. Among the three types of Langmuir isotherms, Langmuir type 1 is best suited for the process of adsorption.

The Freundlich adsorption model presupposes that the surfaces of the adsorbents are heterogeneous and contain sites with various adsorption potentials. Furthermore, it is hypothesized that stronger binding sites are used frst and that binding strength decreases as occupancy rises (Gayathri et al., [2021](#page-19-10)). The linearized form is represented as

$$
\ln q_e = \ln K_F + \frac{1}{n} \ln C_e \tag{6}
$$



<span id="page-9-1"></span>**Fig. 8** a Particle size distribution of Fe<sub>3</sub>O<sub>4</sub> nanoparticles and **b** zeta potential of Fe<sub>3</sub>O<sub>4</sub> nanoparticles



<span id="page-10-0"></span>**Fig. 9 a** PFO and **b** PSO for Fe<sub>3</sub>O<sub>4</sub> nanoparticles and Fe<sub>3</sub>O<sub>4</sub>/NiO composite

where  $K_F$  is the Freundlich constant and *n* is the adsorption intensity, indicating favorable or unfavorable adsorption processes. The parameters were obtained by plotting  $\ln q_e$  vs  $\ln C_e$  (Fig. [12a](#page-13-0)). The Freundlich isotherm becomes linear at  $n=1$  and shows that the adsorption afnities of all the sites on the  $Fe<sub>3</sub>O<sub>4</sub>$  nanoparticles and the  $Fe<sub>3</sub>O<sub>4</sub>/NiO$  composite are equal. Adsorption intensity  $(n>1)$  shows that affinity decreases as adsorption density increases, whereas  $n < 1$  shows poor adsorption. For the Cr(VI) adsorption process, the adsorption intensity (*n*) values were 1.92 and 1.96 for  $Fe<sub>3</sub>O<sub>4</sub>$  nanoparticles and  $Fe<sub>3</sub>O<sub>4</sub>/NiO$ 

<span id="page-10-1"></span>**Table 3** Kinetic parameters of Fe<sub>3</sub>O<sub>4</sub> nanoparticle and Fe<sub>3</sub>O<sub>4</sub>/ NiO composite

Adsorbent	Kinetic models	Parameters	Values
Fe <sub>3</sub> O <sub>4</sub>	PFO	$k_1$ (min <sup>-1</sup> )	0.073
		$q_e$ (mg/g)	84.41
		$\mathbb{R}^2$	0.876
	<b>PSO</b>	$k_2$ (g/mg/ min)	0.00102
		$q_e$ (mg/g)	62.81
		$\mathbb{R}^2$	0.988
Fe <sub>3</sub> O <sub>4</sub> /NiO	PFO	$k_1$ (min <sup>-1</sup> )	0.115
		$q_e$ (mg/g)	130.82
		$\mathbf{R}^2$	0.805
	<b>PSO</b>	$k_2$ (g/mg/ min)	0.0013
		$q_e$ (mg/g)	67.20
		$R^2$	0.976

composite which are larger than 1, indicating favorable adsorption. Good adsorption is indicated by the Freundlich isotherm constant value of 1/*n*, which is between 0 and 1. The  $K_F$  and  $1/n$  values were determined to be 140.54 and 0.522 for  $Fe<sub>3</sub>O<sub>4</sub>$  nanoparticles and 179.82 and 0.51 for  $Fe<sub>3</sub>O<sub>4</sub>/NiO$  composite, respectively. The  $R^2$  value of Freundlich model was found to be 0.692 and 0.875 for  $Fe<sub>3</sub>O<sub>4</sub>$  nanoparticles and  $Fe<sub>3</sub>O<sub>4</sub>/NiO$  composite.

According to the Temkin isotherm, the adsorption energy decreases linearly rather than logarithmically. This isotherm is known for describing how adsorbate and adsorbent interact (Azizkhani et al., [2021](#page-19-11)). The isotherm is given by the equation

$$
q_{\rm e} = \frac{RT}{b_T} \ln \left( K_T C_e \right) \tag{7}
$$

$$
q_e = \mathbf{B}_{\mathrm{T}} \ln \left( K_T C_e \right) \tag{8}
$$

where  $B_T = \frac{RT}{b_T}$ 

where  $B_T$  is the heat of adsorption, the Temkin isotherm constant, or  $b_T$ , measures the change in adsorption energy, and  $K<sub>T</sub>$  is the equilibrium binding constant. Figure [12](#page-13-0)b shows the Temkin isotherm, and the values of  $B_T$  were 28.69 and 19.84 J mol<sup>-1</sup> for Fe<sub>3</sub>O<sub>4</sub> nanoparticles and Fe<sub>3</sub>O<sub>4</sub>/ NiO composite, respectively. The values of  $K<sub>T</sub>$  are 0.061 and 0.237 L mg<sup>-1</sup> for Fe<sub>3</sub>O<sub>4</sub> nanoparticles and  $Fe<sub>3</sub>O<sub>4</sub>/NiO$  composite, respectively. The  $R<sup>2</sup>$  value of

<span id="page-11-0"></span>



Temkin model was found to be 0.893 and 0.631 for  $Fe<sub>3</sub>O<sub>4</sub>$  nanoparticles and  $Fe<sub>3</sub>O<sub>4</sub>/NiO$  composite.

According to the Harkins–Jura model, which focuses on multilayer adsorption and the existence of heterogeneous pore distribution on adsorbent surfaces (Khan et al., [2022\)](#page-20-17), this can be defined as

$$
\frac{1}{q_e^2} = \frac{B_{HJ}}{A_{HJ}} - \frac{1}{A_{HJ}} \log (C_e)
$$
\n(9)

where  $B_{\rm HI}$  and  $A_{\rm HI}$  are the Harkins–Jura constant. The slope and intercept of the linear plot based on  $1/q_e^2$ vs  $log(C_e)$  can be used to determine  $B_{\text{HI}}$  and  $A_{\text{HI}}$ . Figure [12](#page-13-0) c shows the Harkins–Jura model for Cr(VI) removal on both adsorbents, and Table [4](#page-14-0) summarizes the required isotherm parameters. The  $R^2$  value of Harkins–Jura model was found to be 0.425 and 0.325 for  $Fe<sub>3</sub>O<sub>4</sub>$  nanoparticles and  $Fe<sub>3</sub>O<sub>4</sub>/NiO$  composite.

Additionally, multilayer adsorption at a comparatively great distance from the surface was assessed

 $\bigcircled{2}$  Springer  $V$  and  $V$  and  $V$  using the Hasley isotherm model (Buema et al., [2021](#page-19-12)). The adsorption isotherm can be written as

$$
\ln q_e = \frac{1}{n_H} ln K_H - \frac{1}{n_H} ln \frac{1}{C_e}
$$
 (10)

where  $K_H$  and  $n_H$  are the Hasley constants, which can be calculated from the slope and the intercept of the linear plot based on  $ln(q_e)$  vs  $ln(1/C_e)$ . Figure [12](#page-13-0) d shows the Hasley isotherm model for Cr(VI) removal. The  $R^2$  value of Hasley model was found to be  $0.692$ and 0.674 for  $Fe<sub>3</sub>O<sub>4</sub>$  nanoparticles and  $Fe<sub>3</sub>O<sub>4</sub>/NiO$ composite.

The Freundlich and Langmuir isotherms are part of the three-parameter Redlich-Peterson empirical adsorption model (Naik et al., [2023](#page-20-18)). The isotherm has the following linear form

$$
\ln \frac{C_e}{q_e} = B \ln C_e - \ln A \tag{11}
$$

<span id="page-12-0"></span>

where *A* (L  $g^{-1}$ ) and *B* (L mg<sup>-1</sup>) are the Redlich-Peterson isotherm constants. Figure [12](#page-13-0) e illustrates the plot of  $ln(C_e/q_e)$  against  $lnC_e$ . The values of the Redlich-Peterson isotherm constants are presented in Table [4](#page-14-0). The  $R^2$  value of Redlich-Peterson was found to be 0.950 and 0.977 for  $Fe<sub>3</sub>O<sub>4</sub>$  nanoparticles and  $Fe<sub>3</sub>O<sub>4</sub>/NiO$  composite.

#### 3.9 Thermodynamic Study

Thermodynamic parameters were calculated in order to analyze the thermodynamics of the adsorption of Cr(VI) ions onto  $Fe<sub>3</sub>O<sub>4</sub>$  nanoparticles and  $Fe<sub>3</sub>O<sub>4</sub>/NiO$ composite. The  $\Delta G$  denotes the spontaneity of the adsorption process.  $\Delta H$  determines whether the sorption process is endothermic or exothermic. The following equations were used to determine the thermodynamic parameters.

$$
\ln C_e = -\ln K_o + \Delta H/RT \tag{12}
$$

$$
\Delta G = \Delta H - T\Delta S \tag{13}
$$

Using the above equation, the plot of  $\ln C_e$  vs 1/*T* is shown in Fig. [12](#page-13-0) (Raghav & Kumar, [2018](#page-20-19)). Table [5](#page-15-0) shows the thermodynamic parameters for Cr(VI) adsorption on both the adsorbents. The calculated  $\Delta G$  values were as follows:  $-56.74, -58.61,$ and −60.49 kJ mol<sup>-1</sup> for Fe<sub>3</sub>O<sub>4</sub> nanoparticles and − 57.43, − 59.32, and − 61.22 kJ mol<sup>-1</sup> for  $Fe<sub>3</sub>O<sub>4</sub>/NiO$  composite at 303 K, 313 K, and 323 K, respectively. The negative values of Δ*G* demonstrated that the sorption process of Cr(VI) by adsorbents was feasible and spontaneous. The negative Δ*H* values of−59.27 and−61.31 kJ mol−1 for  $Fe<sub>3</sub>O<sub>4</sub>$  nanoparticles and  $Fe<sub>3</sub>O<sub>4</sub>/NiO$  composite, respectively, proved the exothermic nature of the process.

Furthermore, positive Δ*S* values suggested that the adsorbent surface had an affinity for the  $Cr(VI)$ ion and that the degrees of disorder and randomness

<span id="page-13-0"></span>**Fig. 12 a** Freundlich, **b** Temkin, **c** Harkins–Jura, **d** Hasley, **e** Redlich-Peterson isotherm plots for  $Fe<sub>3</sub>O<sub>4</sub>$ nanoparticles and  $Fe<sub>3</sub>O<sub>4</sub>/$ NiO composite



at the solid-solution interface were high in show in Fig. [13](#page-15-1).

# 3.10 Variation of Adsorbent Dose

The dosage of the adsorbent is a crucial functional component that signifcantly afects the removal efficiency and adsorption capacity. It is critical to assess the effectiveness and efficiency of the adsorption process. The adsorbent dosage should show high removal efficiency and a suitable capacity to adsorb. Figure [14](#page-15-2) depicts the infuence of adsorbent dose on percentage removal and adsorption capacity of Cr(VI). As is well known, upon increasing Fe<sub>3</sub>O<sub>4</sub> nanoparticle dosage from 0.01 to 0.14 g  $L^{-1}$ , a reduction in adsorption capacity from 125 to 17.75 mg  $g^{-1}$  occurs while improving removal efficiency from 50 to 99.4%. Also, adsorption capacity decreases from 147.5 to 17.786 mg  $g^{-1}$ , and removal efficiency increases from 59 to 99.6% for Fe<sub>3</sub>O<sub>4</sub>/NiO as dosage increases from 0.01 to 0.14 g  $L^{-1}$ . On increasing the adsorbent's dosage, the

Adsorbent	Adsorption isotherm	Parameters	Values
$Fe_{3}O_{4}$	Langmuir type 1	$q_{\rm m}$ (mg/g)	96.15
		$K_{\text{L}}$ (L/mg)	0.014
		$R_{\rm L}$	0.003
		$R^2$	0.991
	Langmuir type 2	$q_{\rm m}$ (mg/g)	103
		$K_{\text{L}}$ (L/mg)	0.003
		$R_{\rm L}$	0.015
		$R^2$	0.821
	Langmuir type 3	$q_{\rm m}$ (mg/g)	98.02
		$K_{\text{L}}$ (L/mg)	0.0098
		$R_{\rm L}$	0.005
		$R^2$	0.48
	Freundlich	$K_{\rm F}$	140.54
		n	1.92
		1/n	0.522
		$R^2$	0.692
	Temkin	$b_{\rm T}$ (kJ/mol)	0.089
		$B_T$ (J/mol)	28.69
		$K_T$ (L/mg)	0.061
		$R^2$	0.893
	Harkins-Jura	$A_{HJ}$	2930
		$B_{\rm HJ}$	0.094
		$R^2$	0.425
	Hasley	$K_{\rm H}$	13.006
		$n_{\rm H}$	1.916
		$R^2$	0.692
	Redlich-Peterson	B	0.781
		A	118.77
		$R^2$	0.950

<span id="page-14-0"></span>**Table 4** Isotherm parameters of  $Fe<sub>3</sub>O<sub>4</sub>$  nanoparticles and  $Fe<sub>3</sub>O<sub>4</sub>/NiO$  composite

**Table 4** (continued)

Adsorbent	Adsorption isotherm	Parameters	Values
Fe <sub>3</sub> O <sub>4</sub> /NiO	Langmuir type 1	$q_{\rm m}$ (mg/g)	150
		$K_{\text{L}}$ (L/mg)	0.004
		$R_{\rm L}$	0.012
		$R^2$	0.987
	Langmuir type 2	$q_{\rm m}$ (mg/g)	107
		$K_{\text{L}}$ (L/mg)	0.012
		$R_{\rm L}$	0.0038
		$R^2$	0.961
	Langmuir type 3	$q_{\rm m}$ (mg/g)	103.26
		$K_{\text{L}}$ (L/mg)	0.014
		$R_{\rm L}$	0.0035
		$I\!\!R^2$	0.666
	Freundlich	$K_{\rm F}$	179.82
		n	1.96
		1/n	0.51
		$R^2$	0.875
	Temkin	$b_T$ (kJ/mol)	0.127
		$B_T$ (J/mol)	19.84
		$K_{\rm T}$ (L/mg)	0.237
		$R^2$	0.631
	Harkins-Jura	$A_{\rm HJ}$	3640
		$B_{\rm HJ}$	0.215
		$R^2$	0.325
	Hasley	$K_{\rm H}$	167.55
		$n_{\rm H}$	2.475
		$R^2$	0.674
	Redlich-Peterson	B	0.759
		A	141.837
		$R^2$	0.977

number of unsaturated sites in the process increases, or the agglomeration of  $Fe<sub>3</sub>O<sub>4</sub>$  nanoparticles and  $Fe<sub>3</sub>O<sub>4</sub>/NiO$  composite results in a reduction in the accessible surface area and the adsorption capacity (Nodehi et al., [2022](#page-20-13)).

# 3.11 Variation of pH

Particularly, compared to  $Fe<sub>3</sub>O<sub>4</sub>$  nanoparticles,  $Fe<sub>3</sub>O<sub>4</sub>$ /  $NiO$  composite had greater  $Cr(VI)$  removal efficiency. As can be seen in Fig. [15a](#page-16-0), a pH range of 4 to 9 was used to investigate the efect of pH on the ability of  $Fe<sub>3</sub>O<sub>4</sub>$  nanoparticles and  $Fe<sub>3</sub>O<sub>4</sub>/NiO$  composite to remove Cr(VI). For both adsorbents, the greatest  $Cr(VI)$  removal efficiency was noted at pH 5. As demonstrated in Fig. [15a](#page-16-0), in a pH range of 4 to 5, the % adsorption increases, while a further increase in pH up to 9 results in a dramatic decrease in % adsorption. The percentage adsorption for Cr(VI) reached 90% and 94.5% for Fe<sub>3</sub>O<sub>4</sub> nanoparticles and Fe<sub>3</sub>O<sub>4</sub>/ NiO composite at  $pH = 5$ . Generally, chromium exists

<span id="page-15-0"></span>





<span id="page-15-1"></span>**Fig. 13** Linear dependence of  $ln(C_e)$  on 1/*T* based on adsorption thermodynamics for  $Fe<sub>3</sub>O<sub>4</sub>$  nanoparticles and  $Fe<sub>3</sub>O<sub>4</sub>/NiO$ composite

in the pH range of 1–6 in the form of  $HCrO<sub>4</sub><sup>-</sup>$ , followed by  $CrO_4^2$  and  $Cr_2O_7^2$  ions. In an acidic environment, the adsorbent surface was protonated with  $H^+$  ions, which facilitated the electrostatic attraction of  $Cr(VI)$  ions in the form of  $HCrO<sub>4</sub><sup>-</sup>$  ions to the positively charged adsorbent surface. When the pH is increased, the surface of both adsorbents becomes less positively charged, reducing electrostatic attractions between the adsorbent surface and negatively charged species and thereby lowering adsorption efficiency. With increasing solution  $pH$ , the competition of OH− for the few adsorption sites became more intense. As a result, pH 5 was chosen as the most suitable condition in this study. Hence, all subsequent adsorption tests were carried out at pH 5 to achieve maximum removal of Cr(VI) onto both adsorbents (Kang et al., [2022\)](#page-20-20).

# 3.12 Variation of Contact Time

Another aspect that infuences adsorption capacity is contact time. The equilibrium adsorption contact time and the rate at which it is reached are two important characteristics of adsorption. To assess the



<span id="page-15-2"></span>**Fig. 14** Variation of adsorbent dose **a** Fe<sub>3</sub>O<sub>4</sub> nanoparticles and **b** Fe<sub>3</sub>O<sub>4</sub>/NiO composite



<span id="page-16-0"></span>**Fig. 15** Variation of **a** pH, **b** contact time, and **c** initial concentration

Cr(VI) adsorption behavior by  $Fe<sub>3</sub>O<sub>4</sub>$  nanoparticles and  $Fe<sub>3</sub>O<sub>4</sub>/NiO$  composite, the effect of contact time between the adsorbent and adsorbate was optimized in this work by altering the contact duration from 5 to 70 min (Fig. [15b](#page-16-0)). At 60 min, the maximal adsorption capacity occurs, demonstrating fast adsorption at the start of the adsorption. The capacity of adsorption reached 48 mg g<sup>-1</sup> and 49.8 mg g<sup>-1</sup> for Fe<sub>3</sub>O<sub>4</sub> nanoparticles and  $Fe<sub>3</sub>O<sub>4</sub>/NiO$  composite in the first 60 min of the process, respectively. After achieving equilibrium, increasing the contact time had no further infuence on sorption. The remaining ions in solution have a harder time difusing to and interacting with the adsorbent as time goes on because the adsorbent sites are gradually flled up. The huge surface area accessible for Cr(VI) adsorption causes rapid adsorption at the start of the contact time. According to the fndings, the equilibrium time for the elimination of Cr(VI) was 60 min (Nodehi et al., [2022](#page-20-13)).

# 3.13 Variation of Initial Concentration

Initial concentration variations are one of the most important criteria for optimizing the related values between contaminants in aqueous media and adsorbents in equilibrium studies. The efect of initial Cr(VI) concentration on the adsorption capacity of Fe<sub>3</sub>O<sub>4</sub> nanoparticles and Fe<sub>3</sub>O<sub>4</sub>/NiO composite was examined at concentrations varying from 2 to 20 mg  $L^{-1}$ . Figure [15](#page-16-0) c illustrates how the Cr(VI) adsorption capacity increases from 12.25 to 115.625 mg g−1 and 12.4375 to 119.375 mg  $g^{-1}$  for Fe<sub>3</sub>O<sub>4</sub> nanoparticles and  $Fe<sub>3</sub>O<sub>4</sub>/NiO$  composite, respectively, as the starting solution concentration rises from 2 to 20 mg  $L^{-1}$ (Koohi et al., [2021](#page-20-10)). As the concentration of Cr(VI) increases above the previously indicated threshold, the active adsorbent sites are rapidly occupied. Hence, the adsorbent is unable to absorb any further Cr(VI) values. The saturation of the adsorbent surface inhibits further adsorption (Mahmoudi & Behnajady, [2018\)](#page-20-14). At initial concentration of 10 mg  $L^{-1}$ , maximum percentage removal and sufficient adsorption capacity were observed for  $Fe<sub>3</sub>O<sub>4</sub>$  nanoparticles and Fe<sub>3</sub>O<sub>4</sub>/NiO composite. Therefore, 10 mg L<sup>-1</sup> was chosen as an optimal adsorbate concentration for study of both the adsorbents.

# 3.14 Comparative Study

In Table [6](#page-17-0) study the comparative study the relative adsorption capacity of diferent adsorbents for removal of Cr(VI).

# 3.15 Regeneration Studies

It is highly benefcial to conduct researches on the rate of desorption and the capacity to recover adsorbent during the reuse of regenerated adsorbents. Additionally, adsorbent regeneration research is crucial for environmental considerations in addition to economic ones. Figure [16](#page-18-0) depicts the regeneration and reuse performance of  $Fe<sub>3</sub>O<sub>4</sub>$  nanoparticles and  $Fe<sub>3</sub>O<sub>4</sub>/NiO$  composites over six successive adsorption–desorption experiment cycles. For this work, NaOH solution  $(0.1 \text{ M})$  was used as the desorption medium. Fe<sub>3</sub>O<sub>4</sub> nanoparticles and Fe<sub>3</sub>O<sub>4</sub>/NiO composite after the experiment were stirred continuously for 30 min in NaOH solution. After six cycles, the percentage removal of Cr(VI) by  $Fe<sub>3</sub>O<sub>4</sub>$  nanoparticles and  $Fe<sub>3</sub>O<sub>4</sub>/NiO$  composite was reduced from 97 to 54% and 98.45 to 71%, respectively. That could be explained by the fact that not all of the Cr(VI) molecules that had been previously adsorbed during the regeneration process were really desorbed. Our findings demonstrated that  $Fe<sub>3</sub>O<sub>4</sub>$  nanoparticles and  $Fe<sub>3</sub>O<sub>4</sub>/NiO$  composites are promising materials for the elimination of Cr(VI) from a reusability perspective since they can be rapidly regenerated by NaOH eluting treatment and reutilized well in the following cycle (Koohi et al., [2021](#page-20-10)).

<span id="page-17-0"></span>**Table 6** The relative adsorption capacity of diferent adsorbents for removal of Cr (VI)

S. no	Materials	$Q_{\rm e}$ (mg/g)	References
1	$Fe3O4/C$ nanocomposites	64.0	Su et al., (2019)
2	$Fe3O4/graphene oxide (GO)/clay composite$	71.47	Esmaeili & Tamjidi, (2020)
3	Chitosan@Fe <sub>3</sub> O <sub>4</sub>	16.94	Sanchayanukun & Muncharoen, (2019)
4	$g - C_3 N_4 / Fe_3 O_4$ nanocomposites	59.2	Duan et al., (2019)
5	Graphene oxide-magnetic composite	3.197	Neolaka., (2020)
6	Core-shell $Fe3O4@Ce-Zr binary oxide$	66.7	Yu & Fu, (2020)
7	Magnetic greigite/biochar composite	23.25	Wang et al., (2020)
8	Magnetic biochar nanocomposites	80.96	Santhosh et al., $(2020)$
9	$Fe3O4$ -coated nanofibers based on cellulose acetate	193.2	Karamipour et al., (2020)
10	Magnetic composite functionalized with 3-aminopropyl triethoxysilane	64.92	Nnadozie & Ajibade, (2020)
11	$Fe3O4$ nanoparticle	96.15	This work
12	$Fe3O4/NiO$ composite	150	This work



<span id="page-18-0"></span>**Fig. 16** Regeneration studies of  $Fe<sub>3</sub>O<sub>4</sub>$  nanoparticle and  $Fe<sub>3</sub>O<sub>4</sub>/NiO$  composite

### 3.16 Mechanism

The pH values afect the diferent forms of chromium that are present in solutions. In acidic solutions,  $Fe<sub>3</sub>O<sub>4</sub>/$ NiO was protonated and had a positively charged surface. The primary forms that were present were  $Cr_2O_7^{2-}$  and HCrO<sup>4−</sup>. Consequently, electrostatic interactions between the positively charged surface and chromate anions served as the primary adsorption processes of Cr(VI).After adsorption, FTIR was also used to describe  $Fe<sub>3</sub>O<sub>4</sub>$  nanoparticle and  $Fe<sub>3</sub>O<sub>4</sub>/NiO$  composite. Moreover, a minor shift in the peak's position from 3401 to 3408  $cm^{-1}$  for Fe<sub>3</sub>O<sub>4</sub> nanoparticle and 3491 to 3497 cm<sup>-1</sup> could be seen for Fe<sub>3</sub>O<sub>4</sub>/NiO composite, showing an electrostatic interaction between the Cr(VI) and the adsorbent. These were most likely caused by the electrostatic interactions  $(Fe-OH_2^+...$  $HCrO<sup>4−</sup>$ ), according to earlier studies (Miao et al., [2021](#page-20-24); Sirajudheen et al., [2020;](#page-21-22) Yang et al., [2020\)](#page-21-23).

### 3.17 Cost Analysis

Cost-efectiveness is a key consideration for adsorbents utilized in the industry.  $Fe<sub>3</sub>O<sub>4</sub>$  nanoparticles and  $Fe<sub>3</sub>O<sub>4</sub>/NiO$  composites were prepared using the chemicals of analytical reagent grade. Both the dry  $Fe<sub>3</sub>O<sub>4</sub>$  nanoparticles and the  $Fe<sub>3</sub>O<sub>4</sub>/NiO$  composite are currently expensive in the lab, costing roughly US \$110.00 and \$149.07 per kg, respectively. However, the cost of Cr(VI) adsorption on both adsorbents is reasonable when compared to more conventional adsorbents. It is anticipated that in the future, industrial-grade raw materials intended for commercial applications would take the place of analytical-grade compounds in the large-scale synthesis of adsorbents. As a result, the price of the adsorbents and their use will go down significantly (Soni et al., [2020b](#page-21-24)).

### **4 Conclusion and Future Perspective**

Efective adsorbents are essential, as evidenced by the rise in water scarcity and the requirement for water treatment. Presently, contaminated water is treated using magnetic nanoparticles and their composites that have been tailored in terms of size, content, magnetic properties, and structure.  $Fe<sub>3</sub>O<sub>4</sub>$  nanoparticles and  $Fe<sub>3</sub>O<sub>4</sub>/NiO$  composite have been successfully synthesized and used as promising sorbents for Cr(VI) adsorption. Adsorption variables such as dose, contact time, initial concentration, and pH were all taken into account and optimized. The prepared adsorbents were comprehensively characterized by various techniques to understand the surface parameters and physical properties necessary for good adsorption. The results were successfully described by the Langmuir isotherm model, which demonstrated monolayer coverage with a chemisorption-type adsorption mechanism. The utmost adsorption capacities of the  $Fe<sub>3</sub>O<sub>4</sub>$  nanoparticles and Fe<sub>3</sub>O<sub>4</sub>/NiO composite were 96.15 mg g<sup>-1</sup> and 150 mg  $g^{-1}$ , respectively. The  $R_L$  results also demonstrated that adsorption is feasible. The kinetic modeling revealed that the experimental fndings ft well with the PSO model. Following adsorption, an external magnetic feld was employed to remove the adsorbents from the aqueous medium, and six adsorption/desorption cycle experiments demonstrated that Cr(VI) adsorbents were exceptionally reusable. As a result of these fndings, it is possible to conclude that the developed  $Fe<sub>3</sub>O<sub>4</sub>$  nanoparticle and  $Fe<sub>3</sub>O<sub>4</sub>/NiO$  composite can be used as a low-cost, easily available precursor with good reusability, easy separation, and high efficiency as an adsorbent to remove chromium from wastewater.

The following are our major conclusions and future perspectives:

(1)  $Fe<sub>3</sub>O<sub>4</sub>$  nanoparticles and their composites have the advantages of being inexpensive, tunable, and having outstanding magnetic properties as adsorbents.

- (2) In comparison to other adsorbents that have been previously described,  $Fe<sub>3</sub>O<sub>4</sub>$  nanoparticles and their composites exhibit a larger sorption capacity and a fast sorption rate.
- (3) The adsorption properties of  $Fe<sub>3</sub>O<sub>4</sub>$  nanoparticles and their composites are infuenced by various factors, including surface area, surface charge, annealing temperature, functional groups, and cation distribution.
- (4) Regeneration of these adsorbents can be accomplished by using low concentrations of acids or bases or by adjusting the pH of the solution. Furthermore, consistent adsorption–desorption patterns have been noted after multiple regeneration cycles.
- (5) A broad pH range is required for  $Fe<sub>3</sub>O<sub>4</sub>$  nanoparticles and their composites to function in realworld scenarios.
- (6) Comparing magnetic adsorbents to various new generation adsorbents, an additional beneft is their simple sorption-magnetic separation-regeneration properties, which speed up the cyclic and repeated use of magnetic adsorbents over extended periods of time.
- (7) Prior to being used as either catalysts that promote organic processes or for the breakdown of organic pollutants, more research is required on pollutant-loaded magnetic sorbents.

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**Data Availability** The data used to support the fndings of this study are available from the corresponding author upon request.

### **Declarations**

**Competing Interests** The authors declare no competing interests.

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