

# **Investigation of Infrastructural and Management Actions to Increase the Resilience of Existing Pressurized Irrigation Networks**

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### **Abstract**

In recent decades, on-demand irrigation systems have been promoted to increase water use efficiency. This study focused on the assessment of two traditional rotational pressurized irrigation systems with a central pumping station in the Foggia Province (Italy). Irrigation system A has an area of 564 ha with 319 pipelines and 251 hydrants, and irrigation system B has an area of 445 ha with 280 pipelines and 214 hydrants. The nominal discharge of each hydrant is 10 l/s. In each of the two irrigation systems, 1000 diferent operation scenarios were investigated using the COPAM model. To evaluate the performance of the systems, the indices of Relative Pressure Defcit (*RPD*) and Reliability (*RI*) were used. Results showed that the systems are quite fexible and allow the required fow rate to be increased by 1.6 times the peak period fow rate, if necessary. With such increased discharges, it is impossible to guarantee the *RPD* (*RPD*  $\geq$  0) and *RI* (*RI*=1) indices in 47% of the hydrants in the irrigation system A and in 36.9% of the hydrants in the irrigation system B. An updated methodology for optimizing the pipe diameters starting from the current situation was also implemented. Around 23% of pipelines in each system were changed with such methodology. After the new optimization, the number of unsatisfed hydrants in both systems decreased by 94.1% (from 118 to 7 hydrants) and 82.3% (from 79 to 14 hydrants), respectively. Thus, with this methodology, the irrigation system performance can be improved.

**Keywords** Performance improvement · On-demand operation · COPAM · Relative pressure deficit · Reliability indicator

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### **1 Introduction**

Pressurized irrigation networks have higher performance and guarantee better distribution efficiency than open channels (Lamaddalena and Sagardoy [2000](#page-19-0); Khadra and Lamaddalena [2006;](#page-19-1) Daccache et al. [2010a](#page-18-0), [b;](#page-19-2) Ferrarese et al. [2021\)](#page-19-3). While allowing the production of crops with high economic value, the modernization of open channels to pressurized irrigation networks can reduce the amount of water delivered by the network by up to 40% (Díaz et al. [2012\)](#page-19-4). Pressurized irrigation networks can operate with three main delivery schedules: i) continuous fow, ii) rotational and iii) on-demand (Replogle and Gordon  $2007$ ; Anwar and Haq  $2013$ ). In the continuous flow approach, the irrigation network is constantly operated, and the discharge varies according to the irrigation requirements during the growing season. In the rotational approach, the discharge into the network is constant and assigned by the management agency. However, the duration and frequency of irrigation supply from the network change according to the requirements during the growing season. In the on-demand approach, the discharge into the network varies occurs according to farmers' demand.

Nowadays, on-demand pressurized irrigation networks have become very common and can be a good alternative to irrigation networks with diferent water-delivery schedules (Calejo et al. [2008;](#page-18-2) Fouial et al. [2017](#page-19-6)). Traditional irrigation networks with rotational irrigation schedule are more prone to inefficient management than on-demand irrigation networks (Moreno et al. [2010](#page-19-7); Maqbool et al. [2021;](#page-19-8) Monserrat and Alduan [2020](#page-19-9)). Other advantages of on-demand irrigation networks over rotational delivery schedules include high fexibility and freedom of action for farmers (Stefopoulou and Dercas [2017\)](#page-19-10). Therefore, changing the management of pressurized irrigation networks from rotational to on-demand can be very useful in improving the performance and satisfaction of farmers. There are, however, many challenges and problems in this regard for on-demand networks. One of these challenges is the high cost of the network, and there are many studies on this issue to reduce or optimize it (Córcoles et al. [2015](#page-18-3); Fernández García et al. [2017](#page-19-11); Sheibani et al. [2019](#page-19-12); Monserrat and Alduan [2020;](#page-19-9) Bajany et al. [2021\)](#page-18-4). Another major problem is the calculation of the fow rate required by the pressurized irrigation network, which is highly dependent on the cropping pattern, climatic conditions, farm irrigation efficiency, and farmers' behavior (Daccache et al. [2010b\)](#page-19-2). The most widely used method for calculating fow rates is the probabilistic method (Clément [1966;](#page-18-5) Clément and Galand [1979;](#page-18-6) Calejo et al. [2008;](#page-18-2) Khadra et al. [2013](#page-19-13)). Another important issue in converting networks from rotation schedule to ondemand delivery is to provide the minimum pressure required by each hydrant. If the pressure at the hydrants is less than the minimum required pressure, on-farm irrigation efficiency and crop yield will be affected. Moreover, actual operating conditions in ondemand networks may difer from those assumed during the design phase because of management decisions, on-farm irrigation scheduling, and changes in farmers' behavior. These can alter the pressure required at each hydrant (Pereira et al. [2003](#page-19-14); Moreno et al. [2007](#page-19-15); Salvador et al. [2011;](#page-19-16) Kanakis et al. [2014\)](#page-19-17). Another major challenge in on-demand networks is the variation in the number and location of hydrants that operate simultaneously (called "confguration"). For this reason, the performance assessment of an ondemand irrigation network is predictable only on a probabilistic basis (Daccache et al. [2010b](#page-19-2)). The above-said variation can sometimes lead to low hydraulic performance even when the required upstream fow rate in the entire network does not exceed the design fow rate (Lamaddalena and Pereira [2007\)](#page-19-18). According to the above-mentioned

points, the question arises as to whether it is possible and convenient to convert pressurized networks from rotational water-delivery schedule into on-demand networks or not. Therefore, the main aim of this study is to investigate the possibility of converting the management of a traditional rotational pressurized irrigation network into an ondemand irrigation network. Many existing pressurized irrigation networks have a central pumping station, and the pressure required of all network hydrants supply by this station. Few studies have reported the possibility of converting the water delivery management of these networks from a traditional rotational into on-demand. For this purpose, two irrigation networks with a central pumping station in Italy have been studied: their performance has been assessed based on defned evaluation indices, for rotational and on-demand water delivery schedules. Such indicators have been used to improve the optimization of the networks.

### **2 Materials and Methods**

#### **2.1 Case Study**

In the present study, two pressurized irrigation networks in the province of Foggia (Puglia region, Southern Italy) were investigated. The irrigation network A has 319 sections, 251 hydrants over an area of 564 ha; the irrigation network B has 280 sections, 214 hydrants over an area of 445 ha. Both networks are pressurized. The nominal discharge of each hydrant is 10  $\frac{1}{s}$ . The irrigation season starts on April 1<sup>st</sup> and ends on September  $30<sup>th</sup>$ . The energy required for both networks is guaranteed by a pumping station which, for each network, consists of three parallel horizontal electric pumps and an emergency pump. The minimum required pressure head for all hydrants of the two networks is  $H_{\text{min}} = 20m$ . Table [1](#page-2-0) shows some information on the two irrigation networks studied and Fig. [1](#page-3-0) shows their schematic view, provided by the Management Agency.

<span id="page-2-0"></span>



<span id="page-3-0"></span>**Fig. 1** Schematic view of the two pressurized irrigation networks under study; **a** Study area; **b** Irrigation network A; **c** Irrigation network B

#### **2.2 Performance Analysis of on‑demand Pressurized Irrigation Networks**

Two models called ICARE (CTGREF [1979;](#page-18-7) Béthery et al. [1981](#page-18-8); Béthery [1990\)](#page-18-9) and AKLA (Lamaddalena and Sagardoy [2000](#page-19-0)) are commonly used to evaluate the performance of ondemand pressurized irrigation networks. The ICARE model was developed to estimate the entire generated sets of hydrants' confgurations, assuming the hydrant discharge is constant. The limitation of this model is that it is not capable of detecting pressure-defcient hydrants, so the AKLA model was developed, which allows the detection of hydrants with pressure defcits (Lamaddalena and Pereira [2007\)](#page-19-18). Lamaddalena and Sagardoy ([2000\)](#page-19-0) presented a software package (called COPAM) where the two models, ICARE and AKLA, along with a procedure for the optimization of the pipe network diameters, are integrated. The COPAM software package (Ver. 1.01, FAO, I&D Paper No 59) was used for the assessment of the two abovementioned Italian irrigation systems. Further details of this study are provided below.

#### **2.2.1 Maximum Possible Inflow to the Network and Pipelines**

`The maximum possible infow into the networks was calculated on the basis of Clément's frst model (Lamaddalena and Sagardoy [2000\)](#page-19-0):

$$
Q = \sum R_i P_i d_i + U(P_q) \sqrt{\sum R_i P_i (1 - P) d_i^2}
$$
 (Clément's first equation) (1)

in which,  $Q$  is the discharge (l/s);  $R$  is the number of hydrants,  $d$  is the nominal discharge of each hydrant  $(l/s)$ ,  $U(P_q)$  is the operation quality, P is the elementary probability of each hydrant, which is calculated using Eq. ([2\)](#page-4-0):

<span id="page-4-1"></span><span id="page-4-0"></span>
$$
P = \frac{q_s A}{rRd}
$$
 (2)

where,  $q_s$  is the network hydro module (l/s/ha), *A* is the irrigated area (ha) and *r* is the coefficient of utilization. A hydrant configuration refers to the number of hydrants that are open simultaneously. The number of possible configurations is given by Eq.  $(3)$  $(3)$ .

$$
C_R^K = \frac{R!}{K!(R-K)!} \tag{3}
$$

where,  $C_R^K$  is the number of possible configurations when delivering the discharge *Q* corresponding to the  $K$  hydrant in simultaneous operation. In the present study, 1000 different random confgurations were considered for the network evaluation and further optimization.

Clément's second formula was also used in this study to calculate the peak discharge. It allows the diferent approaches to be compared.

Clément's second model is:

$$
Q = \sum R_i P_i d_i + u' \sqrt{\sum R_i P_i (1 - P) d_i^2}
$$
 (Clément's second equation) (4)

#### **2.3 Performance Indicators**

Two models (ICARE and AKLA) were used to analyze and evaluate the irrigation networks under study. A configuration is defined as a group of hydrants in operation  $(j)$ corresponding to a fixed value of the discharge upstream of the network  $(Q(l/s))$ . A hydrant confguration is considered to be satisfed and without problems when the following equation is true for all hydrants in operation:

$$
(H_j)_r \ge H_{\min} \tag{5}
$$

where,  $(H_j)_r$  is the hydraulic height of the hydrant in configuration *r* and  $H_{\min}$  is the minimum required pressure of the hydrant (m). This model indicates only that the irrigation network under study has some problems and is not able to identify the location of the failing hydrants. To solve this problem, AKLA model was used. In this model, two indicators were defined: ii) the relative pressure deficit, and ii) the reliability. Both are used to evaluate the performance of the irrigation network. The relative pressure defcit (RPD) index for each hydrant is defned as follows (Lamaddalena and Sagardoy [2000\)](#page-19-0):

$$
\Delta H = \frac{H_{j,r} - H_{\min}}{H_{\min}}\tag{6}
$$

The reliability index of each hydrant is also calculated using Eq. ([7\)](#page-5-0):

<span id="page-5-0"></span>
$$
\alpha_{j} = \frac{\sum_{R=1}^{C} I h_{j,r} I p_{j,r}}{\sum_{R=1}^{K} I h_{j,r}}
$$
(7)

where,  $\alpha_j$  is the reliability of the hydrant *j*, if the hydrant is open in configurations *r* :  $I h_{i,r} = 1$ , if the hydrant is closed in configurations *r*:  $I h_{i,r} = 0$ , if the pressure height in the open hydrant  $j$  in the composition  $r$  is higher than the minimum pressure height required  $I_{i}$ <sub>*P<sub>ir</sub>* = 1, if the pressure height in the open hydrant *j* in the configurations *r* is lower than</sub> the minimum pressure height required  $I_{p_{i,r}} = 0$  and *C* is the total number of configurations.

### **3 Results and Discussion**

#### **3.1 Inflow to Irrigation Network**

Figure [2](#page-6-0) shows the results of calculations of the infow discharge for both pressurized irrigation networks A and B. Diferences are in the range between -10% and+10%. Clément's second equation estimates a higher upstream discharge than the frst equation. The discharges calculated by Clément's second equation in the networks A and B are, respectively, 15.65% and 17.64% greater than the values estimated by the frst equation. The reason is attributed to the difference between two parameters of operating quality coefficient  $(U_p(q))$ in the first equation and the saturation coefficient  $(u')$  in the second equation. Most researchers use Clément's frst formula, which is also used in this study. The maximum upstream required discharges for the network A and B are, respectively, 300 l/s and 230 l/s. Therefore, the operating point  $P_{NewA}(300l/s, 271m.a.s.l)$  in irrigation network A, and the operating point  $P_{New,B}(230l/s, 249m.a.s.l)$  in irrigation network B, are considered as new base points for on-demand operation. Such points are very diferent from those computed during the design stage: i.e., Points  $P_{oldA}(184.41/s, 271m.a.s.l)$  and  $P_{oldB}(145.51/s, 249m.a.s.l)$ .

Such diferences are mainly due to the change in the cropping pattern, which is currently more water demanding than the design pattern, due to the impact of climate change and to the change in farmers' behavior. These are the main causes of some performance failures recorded in the two irrigation systems.

#### **3.2 Current Status of Irrigation Networks**

The Indexed Characteristic Curves were drawn for 1000 random hydrant confgurations for upstream discharges ranging as:  $30l/s \le Q \le 600l/s$  and  $30l/s \le Q \le 500l/s$ , respectively, for irrigation networks A and B (Fig. [3](#page-7-0)). The Indexed Characteristic Curves analysis shows that the old operating points  $P_{oldA}(184.4l/s, 271m.a.s.l)$  and  $P_{oldB}(145.5l/s, 271m.a.s.l)$ for both networks are located on the upper envelope area. It indicates that both networks in the initial management conditions can provide the minimum pressure head required by most hydrant confgurations. New base points in irrigation networks A and B  $(P_{0, A}(300l/s, 271m.a.s.l)$  and  $P_{0, B}(230l/s, 249m.a.s.l)$ , are respectively located on indexed



<span id="page-6-0"></span>**Fig. 2** Comparison of discharges calculated based on Clément's frst and second equations **a** Irrigation network A **b** Irrigation network B

characteristic curves of 70% and 83%. In other words, for the irrigation networks A and B, the minimum pressure head ( $H_{\text{min}} = 20m$ ) is satisfied in 70% and 83% of configurations at the discharges of 300 l/s and 230 l/s respectively. Such performance is still acceptable for both networks and indicates a very good fexibility of the designed systems.

Figure [4](#page-8-0) shows the changes in the relative pressure deficit indicator as well as its envelope curves at 100%, 90% and 10%, for each hydrant at the new base points for 1000 random confgurations. In both networks, the hydrants that are most exposed to

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<span id="page-7-0"></span>**Fig. 3** Indexed characteristic curves in the current situation for **a** Irrigation network A and **b** Irrigation network B

insufficient pressure are identified. Based on the lower curve, in irrigation network A, 47% of hydrants do not provide the minimum required pressure. Of these, 10.9% of hydrants have less than zero pressure (meaning that water cannot fow from those hydrants), 10.3% have a pressure in the range of 0–10 m and 25.8% have a pressure in the range of 10–20 m. Also, in irrigation network B, the amount of pressure in 36.9% of hydrants is lower than the minimum required pressure: 6.6% have less than zero pressure, 8.2% have the pressure in the range of 0–10 m and 22.1% in the range of 10–20 m. Based on the curve 90% (except for 10% of the minimum pressure of each hydrant),



**Hydrants Numbering** 

<span id="page-8-0"></span>**Fig. 4** Changes in the relative pressure defcit index and its curves at three levels (upper, 90% and lower) in each hydrant obtained from 1000 random confgurations at the new base point **a** Irrigation network A and **b** Irrigation network B

in irrigation networks A and B, in 10.7% and 3.0% of hydrants, the minimum required pressure is not satisfed.

Figure [5](#page-9-0) also shows the changes in the reliability indicator (*RI*) of hydrants at the new base points for 1000 random confgurations. The closer the index is to 1, the better the hydrant performance and the minimum required pressure is satisfed. In irrigation networks A and B, respectively, 9 and zero hydrants  $(3.5\% \text{ and } 0\%)$  are in the range of  $RI \leq 0.8$ ; 14 and 10 hydrants (5.6% and 4.7%) are in the range of 0.8 *< RI <* 0.9 and 228 and 204 hydrants (90.8% and 95.3%) are in the range  $RI \geq 0.9$ . Figure [6](#page-10-0)a shows the changes in the percentage of unsatisfed hydrants (PUH) against the discharge for the existing piezometric pressure heights (271 for irrigation network A and 249 for irrigation network B). At the new base points, in irrigation networks A and B, respectively, there is the possibility of not



# (a) Irrigation Network A

<span id="page-9-0"></span>**Fig. 5** Changes in reliability indicator for each hydrant obtained from 1000 random confgurations at the new base point **a** Irrigation network A and **b** Irrigation network B

supplying the required pressure to 10% and 8% of the hydrants, with 90% probability of occurrence.

In summary, the irrigation network A at a discharge of 300 l/s with a piezometric elevation of 271 m.a.s.l and from 1000 random confgurations can supply water at the required pressure to all confgurations with a 60% probability of occurrence. Similar conditions are achieved for the irrigation network B with a probability of occurrence of 60% (Fig. [6](#page-10-0)a). Figure [6b](#page-10-0) shows the changes in the number of random confgurations versus the required pressure head. As the number of random confgurations increases, the pressure head required by the network (while maintaining maximum efficiency)



<span id="page-10-0"></span>**Fig. 6 a** Percentage probability of occurrence of unsatisfed hydrants (PUH), calculated using 1000 random confgurations, for new base points **b** Changes in the number of random confgurations against the required water head to supply pressure to all hydrants for both studied irrigation networks

increases too. For the two irrigation networks A and B, the available pressure heads (65 and 43 m, respectively for the two networks A and B) can satisfy the minimum pressure head at hydrants up to 480 and 500 random confgurations, respectively. Therefore, to improve the network's performance and, consequently, to increase the hydrant pressure head, the approaches described below are reported.

### **3.3 Optimization of Studied Irrigation Networks and Re‑evaluation of their Performance**

By changing the network operation management from the initial design to the current ondemand situation, the network base points change to new ones. The maximum possible discharge required for networks A and B is 300 l/s and 230 l/s, respectively. To provide the required discharge with the minimum pressure head at hydrants, diferent approaches can be introduced. The use of electric booster pumps and increased pressure at the central pumping station are among the suggested solutions. Still, one of the main drawbacks of these solutions is the high construction, hydromechanical and energy costs.

Another approach to supply the minimum required pressure in failure hydrants is to reduce their nominal discharge. Adopting this approach depends on the on-farm network management. The degree of freedom of hydrants indicates the freedom of farmers to irrigation schedule. The lowest degree of freedom should be not less than 2 times



<span id="page-11-0"></span>**Fig. 7** Identifcation of unsatisfed pressure hydrants in the operating conditions of the new base point; **a** Pressurized irrigation network A **b** Pressurized irrigation network B

the continuous specific discharge,  $q<sub>s</sub>$ , (FAO I&D paper n. 44). The actual degree of freedom of the hydrants for both networks is more than 12 times  $q_s$ , which is very high. In this regard, the nominal discharge of unsatisfed hydrants (as shown in Fig. [7](#page-11-0)) was reduced from 10 l/s to 6 l/s and the networks were re-evaluated. In both irrigation networks, the new base point was obtained in the upper envelope area (Fig. [8](#page-12-0)a). Also, the percentage of unsatisfed hydrants in both networks reached zero percent after reducing the nominal discharge (Fig. [8](#page-12-0)b). Also, by examining the RPD index, the number



<span id="page-12-0"></span>**Fig. 8 a** Indexed characteristic curves after reducing the nominal discharge of low-pressure hydrants **b** Percentage probability of occurrence of unsatisfed hydrants (PUH), calculated using 1000 random confgurations, after reducing the nominal discharge of low-pressure hydrants

of hydrants with a pressure below the minimum required pressure in the mentioned networks was reduced from 118 and 79 hydrants to zero and 46 hydrants, respectively (Fig. [9\)](#page-13-0). Moreover, despite cost savings and no change in the structure of the network, except for the fow regulators into the hydrants, this approach could reduce comfort for farmers and could make operation managers skeptical about the application of this approach. But the most stable method can be diameter reduction based on COPAM software, which will be fully described below.

#### **3.3.1 Modification and Optimization of Network Pipe Diameters**

In this session, the rehabilitation of the two networks A and B is proposed by using the optimization process available through this methodology; in irrigation networks A and B, the diameters of 72 and 65 pipelines (respectively, 22.6% and 23.2% of the total network) were changed (Fig. [10\)](#page-14-0). After optimization, the pressure head in all nodes became higher than the minimum required pressure  $(H_{\text{min}} = 20m)$ . Also, the new base points for both irrigation networks have been moved from the intermediate area to the upper envelope area (Fig. [11](#page-15-0)). It is also possible to reduce the upstream piezometric elevation in both irrigation networks A and B, from 271 and 249 m.a.s.l to 265 and 240.5 m.a.s.l, respectively. This reduction in piezometric elevation will reduce energy costs. Energy costs typically account for 55 to 70 percent of total network operation and maintenance costs (FAO 59). Therefore, the costs of changing the diameter of the pipes, after a certain period of time, will be compensated by reducing the costs related to energy consumption (Córcoles et al. [2015](#page-18-3)).



<span id="page-13-0"></span>**Fig. 9** Changes in the relative pressure defcit index in each hydrant obtained from 1000 random confgurations, after reducing the nominal discharge of low-pressure hydrants; **a** Irrigation network A and **b** Irrigation network B

After optimization, the number of hydrants that do not supply the minimum required pressure is reduced to 7 and 14 hydrants for networks A and B, respectively (2.8% and 6.5% of the total network) (Fig. [12](#page-16-0)). Figure [13](#page-17-0) also shows the condition of the hydrants of both irrigation networks. The *RI* index in all hydrants, except in very few cases, has reached 1 (the most desirable condition).

### **3.4 Initial Design of on‑demand Networks**

If the studied irrigation networks were designed from the beginning by using COPAM model, the costs of the pipes would have been less than the costs for the rehabilitation of the networks.

# (a) Irrigation Network A



# (b) Irrigation Network B



<span id="page-14-0"></span>**Fig. 10** Changes in pipelines diameter in the optimization stage; **a** Irrigation network A and **b** Irrigation network B

# (a) Irrigation Network A



<span id="page-15-0"></span>**Fig. 11** Indexed characteristic curves after optimization of pipelines **a** Irrigation network A and **b** Irrigation network B



<span id="page-16-0"></span>Fig. 12 Changes in the relative pressure deficit index in each hydrant obtained from 1000 discharge confgurations, after optimizing the pipelines, **a** Irrigation network A and **b** Irrigation network B



<span id="page-17-0"></span>**Fig. 13** Position of unsatisfed hydrants after optimization, based on relative pressure defcit index; **a** Pressurized irrigation network A and **b** Pressurized irrigation network B

# **4 Conclusions**

In the present study, the feasibility of changing management options of two pressurized irrigation networks was investigated. The COPAM model was used to evaluate the performance and rehabilitate the networks. Results showed that it is possible to improve the network performance by analyzing the current situation and then by identifying diferent options. Currently, the analysis carried out showed that for the irrigation networks A and B, it is not possible to supply the minimum pressure head at 47% and 36.9% of hydrants.

Reducing the nominal discharge in unsatisfed hydrants improved the performance of the networks. In this case, the possible dissatisfaction of farmers should be further analyzed in detail. The Rehabilitation by optimization of pipe diameter was performed. The diameters of 72 and 65 pipes were modifed in irrigation networks A and B, respectively. Using this approach, the number of failing hydrants in the two irrigation networks decreased from 118 and 79 hydrants to 2.8% (7 hydrants) and 6.5% (14 hydrants), respectively and the amount of energy required by the networks decreased. Also, the option to increase the upstream piezometric elevation was analyzed but this solution may cause excessive energy consumption, so it should be further analyzed. Therefore, it is possible to convert water delivery management in the pressurized irrigation network with a central pumping station from a traditional rotational into on-demand and it is recommended.

**Authors' Contributions** Conceptualization: [Younes Aminpour, Nicola Lamaddalena], Methodology: [Younes Aminpour], Formal analysis and investigation: [Younes Aminpour, Eisa Maroufpoor, Nicola Lamaddalena], Writing—original draft preparation: [Younes Aminpour]; Writing—review and editing: [Eisa Maroufpoor], Resources: [Nicola Lamaddalena], Supervision: [Eisa Maroufpoor, Nicola Lamaddalena].

**Data Availability** The datasets used and/or analyzed during the current study are available from the corresponding author on reasonable request.

# **Declarations**

**Ethics Approval and Consent to Participate** Not applicable.

**Consent for Publication** Not applicable.

**Competing Interests** The authors declare that they have no competing interests.

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