

# UN/ECE ICP Materials Dose-response Functions for the Multi-pollutant Situation

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**Abstract** A “multi-pollutant exposure programme” reflecting the new pollution situation where SO<sub>2</sub> is no longer the dominating pollutant has been performed by the International Co-operative Programme on Effects on Materials, including Historic and Cultural Monuments (ICP Materials) within the activities of the Convention on Long-range Transboundary Air Pollution. The main results obtained in the period 1997–2003 are summarised. Dose-response functions are presented for carbon steel, zinc, copper, bronze and limestone. Parameters involved in the functions include besides SO<sub>2</sub> and pH, which were included in the previously developed functions from

ICP Materials, also the effect of particulate matter and HNO<sub>3</sub>.

**Keywords** air pollution · corrosion · materials · dose-response functions · HNO<sub>3</sub> · particulate matter

## 1 Introduction

Dose-response functions are an important tool for mapping areas of increased risk of corrosion and for calculating corrosion costs. In the past, several dose-response functions for individual materials have been

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proposed using results based on different exposure programmes, for example the NAPAP programme (Baedecker, 1990) and Scandinavian exposure programmes (Haagenrud & Henriksen, 1996). Common for the past exposure programmes and functions was the focus on the SO<sub>2</sub> concentration, which was the main corrosion stimulator. Therefore, all these functions should in principle be denoted “dose-response functions for the SO<sub>2</sub> dominating situation”. This era culminated with the development of dose-response functions from the International Co-operative Programme on Effects of Materials including Historic and Cultural Monuments (ICP Materials) using the 8-year results (1987–1994) and these were reported at Acid Rain 2000, Tsukuba, Japan (Tidblad et al., 2001).

In the recent decades the decreasing SO<sub>2</sub> levels and the increasing car traffic causing elevated levels of nitrogen compounds, ozone and particulates has created a new multi-pollutant situation in Europe where SO<sub>2</sub> no longer is dominant. This was recognised within ICP Materials already in 1996 and a year later the ICP Materials multi-pollutant exposure program started (1997–2001). This exposure was later complemented and extended with measurements of HNO<sub>3</sub> and particulate matter by the EU project Model for multi-pollutant impact and assessment of threshold levels for cultural heritage MULTI-ASSESS (Kucera et al., 2005). The present paper summarises the development of the new dose-response functions for the multi-pollutant situation based on data from the ICP Materials multi-pollutant exposure and the MULTI-ASSESS project.

## 2 Experimental

A Task Force is organising the programme originally with Sweden as lead country and the Swedish Corrosion Institute serving as the main research centre. Since January 2005 the Chairmanship of ICP Materials is shared between Sweden (Swedish Corrosion Institute) and Italy (ENEA). Sub-centres in different countries have been appointed, each responsible for their own group of materials. All environmental measurements are reported and compiled by the environmental sub-centre, the Norwegian Institute for Air Research (NILU). In each country a National contact person has been appointed responsible for the sub-centre and/or test sites.

### 2.1 Network of Test Sites

The network consists of 29 test sites from 18 countries (Table 1). Of the 39 sites included in the original network, 21 are kept in the multi-pollutant programme. In addition, new sites have been added and include urban sites in Paris, Berlin, Tel Aviv, London, Los Angeles and Antwerpen as well as rural sites in Svanvik, Norway and Chaumont, Switzerland. This means an increase of the share of urban sites from 14 of 39 to 16 of 29 and an increase of the number of involved countries from 14 to 19.

### 2.2 Characterisation of the Environment

At each site the measured environmental data (ICP Materials, 2003a) includes climatic parameters (temperature, relative humidity, time of wetness, and sunshine radiation), gaseous pollutants (SO<sub>2</sub>, NO<sub>2</sub> and O<sub>3</sub>) and precipitation (total amount, conductivity and concentration of the ions H<sup>+</sup>, SO<sub>4</sub><sup>2-</sup>, NO<sub>3</sub><sup>-</sup>, Cl<sup>-</sup>, NH<sub>4</sub><sup>+</sup>, Na<sup>+</sup>, Ca<sup>2+</sup>, Mg<sup>2+</sup> and K<sup>+</sup>). This data is in general not measured exclusively for ICP Materials but are instead collected from nearby environmental stations. For cost reasons a test site is preferably situated where high quality measurements are already made. Thus, the analytical methods and instruments used for measuring the environmental data may vary from site to site.

In addition to these parameters, HNO<sub>3</sub> and particulates (total mass and SO<sub>4</sub><sup>2-</sup>, NO<sub>3</sub><sup>-</sup>, Cl<sup>-</sup>, NH<sub>4</sub><sup>+</sup>, Na<sup>+</sup>, Ca<sup>2+</sup>, Mg<sup>2+</sup> and K<sup>+</sup>) have been measured within the EU 5FP MULTI-ASSESS project at all test sites with the same methodology, which is completely new in the area of materials damage estimation, considering the large network of test sites. Besides the differences in test sites, this environmental characterisation is the main difference between the original 8-year exposure programme and the presently described multi-pollutant exposure program. These measurements were performed with passive samplers for HNO<sub>3</sub> (Ferm, De Santis, & Varotsos, 2005) and particulate matter (Ferm, Watt, O’Hanlon, De Santis, & Varotsos, 2006) that were validated within the MULTI-ASSESS project. The latter also involves a description of the correlation between the deposited PM and the measured PM<sub>10</sub> concentration in the atmosphere of the test sites. Details of the measurement techniques

**Table 1** List of test sites used in the multi-pollutant exposure programme showing number, name, country and type of atmosphere

No	Name	Country	Type
1	Prague-Letnany	Czech Republic	Urban
3	Kopisty	Czech Republic	Industrial
5	Ähtäri	Finland	Rural
7	Waldhof-Langenbrügge	Germany	Rural
9	Langenfeld-Reusrath	Germany	Rural
10	Bottrop	Germany	Industrial
13	Rome	Italy	Urban
14	Casaccia	Italy	Rural
15	Milan	Italy	Urban
16	Venice	Italy	Urban
21	Oslo	Norway	Urban
23	Birkenes	Norway	Rural
24	Stockholm South	Sweden	Urban
26	Aspvreten	Sweden	Rural
27	Lincoln Cathedral	United Kingdom	Urban
31	Madrid	Spain	Urban
33	Toledo	Spain	Rural
34	Moscow	Russian Federation	Urban
35	Lahemaa	Estonia	Rural
36	Lisbon	Portugal	Urban
37	Dorset	Canada	Rural
40	Paris	France	Urban
41	Berlin	Germany	Urban
43	Tel Aviv	Israel	Urban
44	Svanvik	Norway	Rural
45	Chaumont	Switzerland	Rural
46	London	United Kingdom	Urban
47	Los Angeles	USA	Urban
49	Antwerpen	Belgium	Urban

Sites 1–39 were also used in the original exposure programme and sites 40–49 are new test sites.

can be found in the mentioned papers, which are also summarised in the MULTI-ASSESS publishable final report (Kucera et al., 2005).

### 2.3 Materials and Evaluation of Corrosion Attack

Standard specimens of carbon steel, zinc, copper, bronze, limestone, paint coated steel, and glass representative of medieval stained glass windows have been exposed in unsheltered and for some materials sheltered position on racks. The evaluation of corrosion effects on materials is done by standardised or well-established procedures: carbon steel (ICP Materials, 2003b), zinc (ICP Materials, 2003c), copper and bronze (ICP Materials, 2003d), limestone (ICP Materials, 2003e), painted steel (ICP Materials, 2003f) and glass (ICP Materials, 2003g, 2004). Also,

evaluation of corrosion effects on materials is performed at dedicated sub-centres, each responsible for a material, or group of materials, and for performing all corrosion analyses of this material regardless of where it was exposed:

- SVUOM Ltd., Prague, Czech Republic, responsible for carbon steel
- EMPA, Corrosion/Surface Protection, Dübendorf, Switzerland, responsible for zinc
- Bavarian State Department of Historical Monuments, Munich, Germany responsible for copper and cast bronze.
- Building Research Establishment (BRE Ltd.), Garston, Watford, United Kingdom, responsible for Portland limestone.
- Norwegian Institute for Air Research (NILU), Lilleström, Norway responsible for painted steel.

- Institute of Chemistry, Academy of Fine Arts, Vienna, Austria responsible for glass materials representative of medieval stained glass windows.

### 3 Results and Discussion

Selected results of environmental and corrosion data are presented as bar graphs in Fig. 1, 2, and 3 giving annual values of temperature, relative humidity, precipitation, HNO<sub>3</sub>, SO<sub>2</sub>, particulate total deposition, and limestone, zinc and steel corrosion. Worth noting is the relatively high HNO<sub>3</sub> concentration in Paris in combination with the elevated corrosion levels for zinc and to a lesser extent limestone but not for steel at this site. This observation is also reflected in the developed dose-response functions described below where HNO<sub>3</sub> proved to be a significant parameter for limestone and zinc but not for the other materials.

#### 3.1 Statistical Evaluation of Results

The statistical analysis is based on corrosion values of carbon steel, zinc, copper, bronze and limestone after 1, 2 and 4 years of exposure in the multi-pollutant programme. One important criterion for the developed dose-response functions is that they should be suitable for mapping areas with increased risk of corrosion. Therefore the environmental parameters have been restricted to those that are easily available and these are given in Table 2 together with the corrosion attack parameters, including abbreviations and units. For temperature a maximum of the corrosion effect of SO<sub>2</sub> is observed at about 9–11°C. The increasing part can be related to the increased time of wetness. The decreasing part is attributed to a faster evaporation of moisture layers e.g. after rain or dew periods and a surface temperature above the ambient temperature due to sun radiation which result in a decrease of the surface time of wetness (Tidblad et al., 2001). For relative humidity the transformed variable Rh<sub>60</sub> = (Rh – 60) when Rh > 60; otherwise 0 is frequently used in the dose-response functions. The new important parameter HNO<sub>3</sub> is not easily available but may be calculated from other easily available parameters i.e., temperature, relative humidity, NO<sub>2</sub> and O<sub>3</sub> (Kucera et al., 2005).

The statistical results presented here are the result of linear/non-linear regression. Other techniques for producing regression functions have also been tested and these give in some cases better results but may involve combination of terms that are difficult to justify based on physical/chemical arguments. The result of the analysis is summarised in Table 3.

The climatic parameters (T, Rh and Rain) are all included in almost all of the functions. Both pH and SO<sub>2</sub> are included in all of the functions and these parameters were also present in the dose-response functions developed previously. NO<sub>2</sub> is not included in any of the functions directly but as will be seen below it is closely related to the HNO<sub>3</sub> concentration. The remaining parameters are included as an additional contribution depending on material. The effects of HNO<sub>3</sub> (zinc and limestone) and PM (carbon steel, bronze and limestone) are new. In the following the functions for the individual materials will be presented briefly.

#### 3.2 Dose-response Functions

##### 3.2.1 Carbon Steel

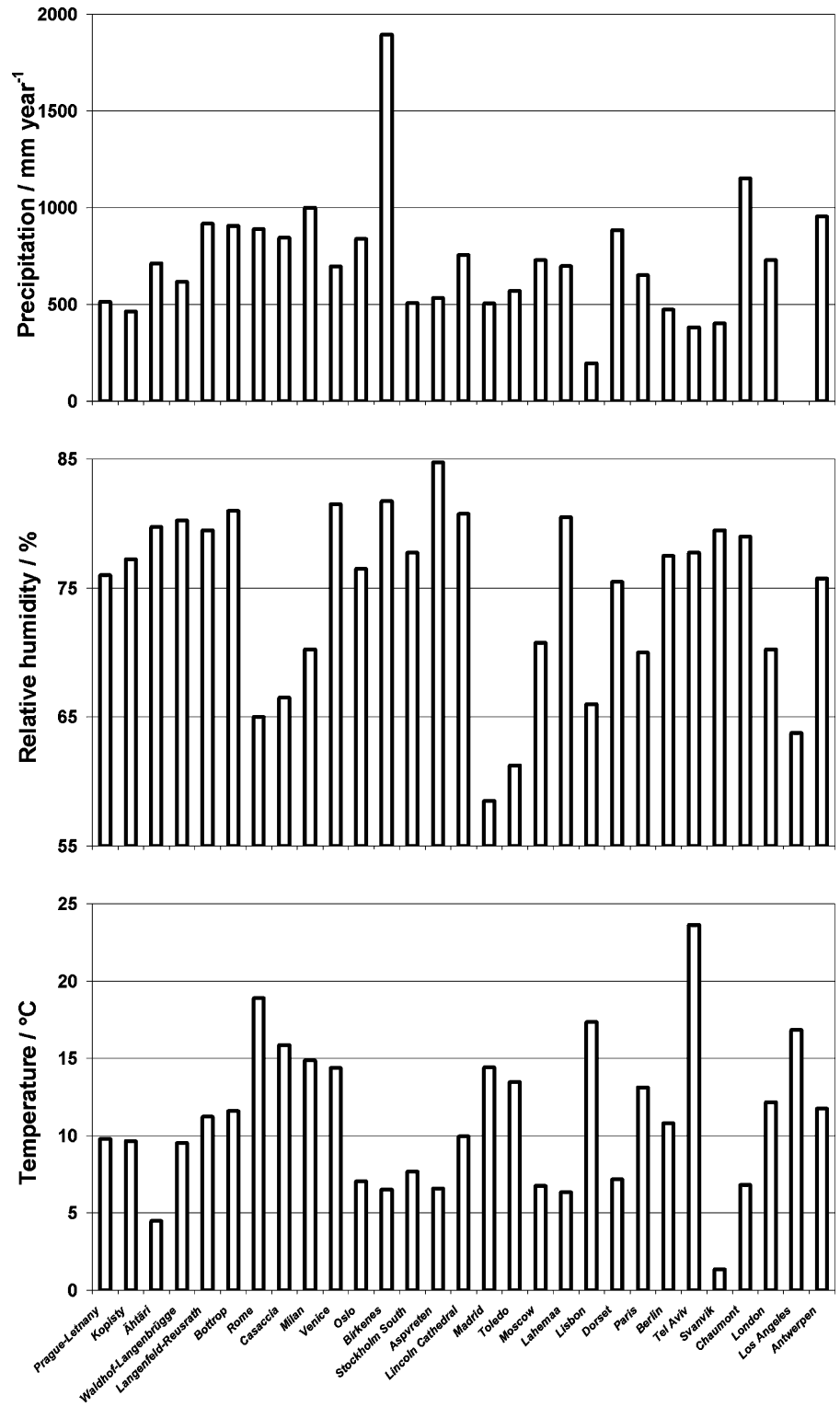
No previous dose-response function exists from the 8-year ICP Materials exposure programme. However, a recently developed function based on work within ISO TC 156/WG4 with the aim of future revision of ISO 9223 resulted in the following equation describing the corrosion attack after 1 year of exposure

$$r_{\text{corr}} = 1.77[\text{SO}_2]^{0.52} e^{0.020\text{Rh}} e^{f(T)} + g(\text{Cl}^-, \text{Rh}, T)$$

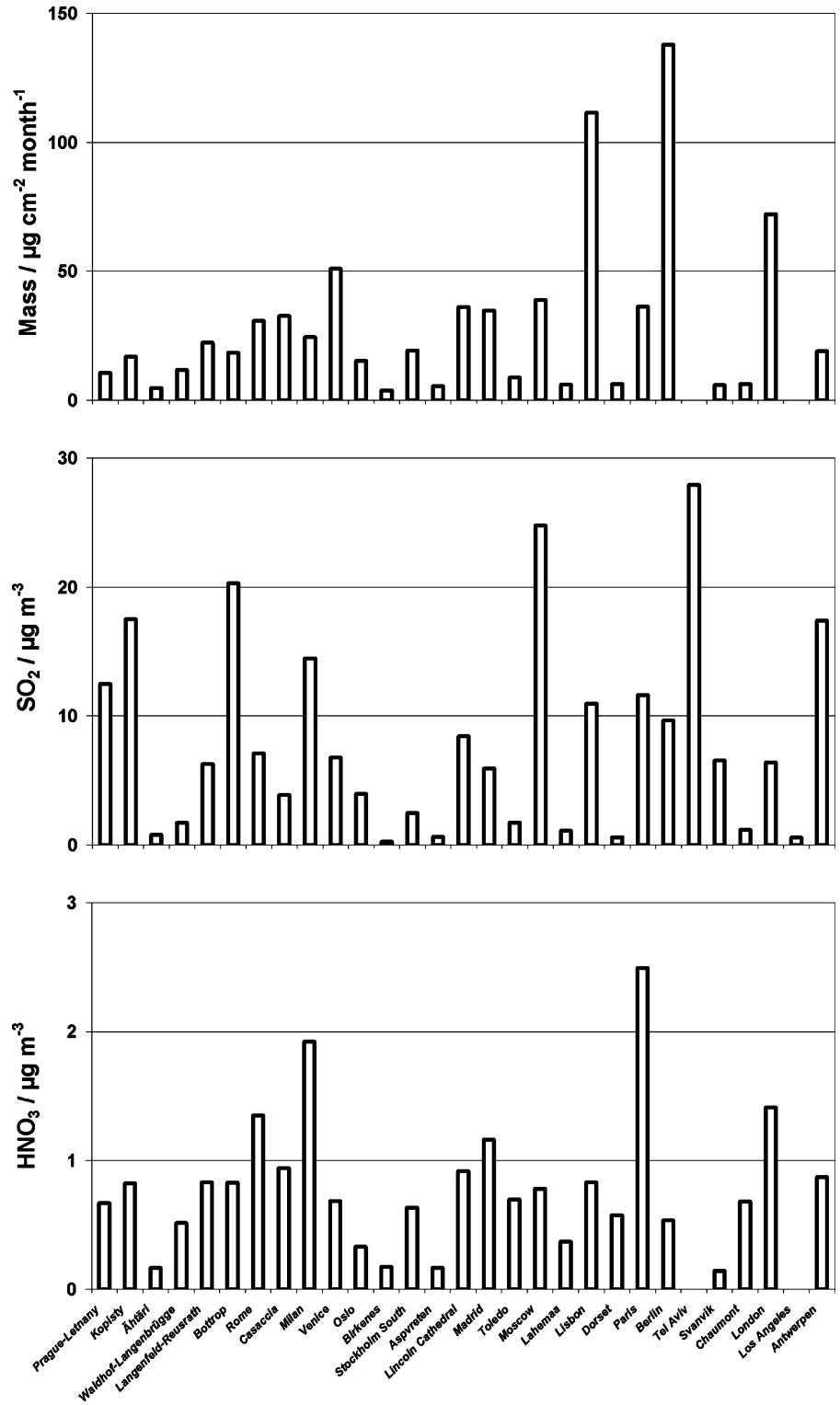
where  $r_{\text{corr}}$  is measured in  $\mu\text{m}$ ,  $f(T) = 0.15(T - 10)$  when  $T < 10^\circ\text{C}$ ; otherwise  $-0.054(T - 10)$ , and  $g(\text{Cl}^-, \text{Rh}, T)$  is a function describing the effect of dry deposition of chloride in combination with relative humidity and temperature. The temperature interval used in the derivation of this function was from  $-20$  to  $+30^\circ\text{C}$  while the multi-pollutant database only includes values from  $0$  to  $+25^\circ\text{C}$ . Since the multi-pollutant data set did not disagree with this temperature function it was used in the resulting multi-assess function

$$\text{ML} = 29.1 + t^{0.6} \left( 21.7 + 1.39[\text{SO}_2]^{0.6} \text{Rh}_{60} e^{f(T)} + 1.29\text{Rain}[\text{H}^+] + 0.593\text{PM}_{10} \right)$$

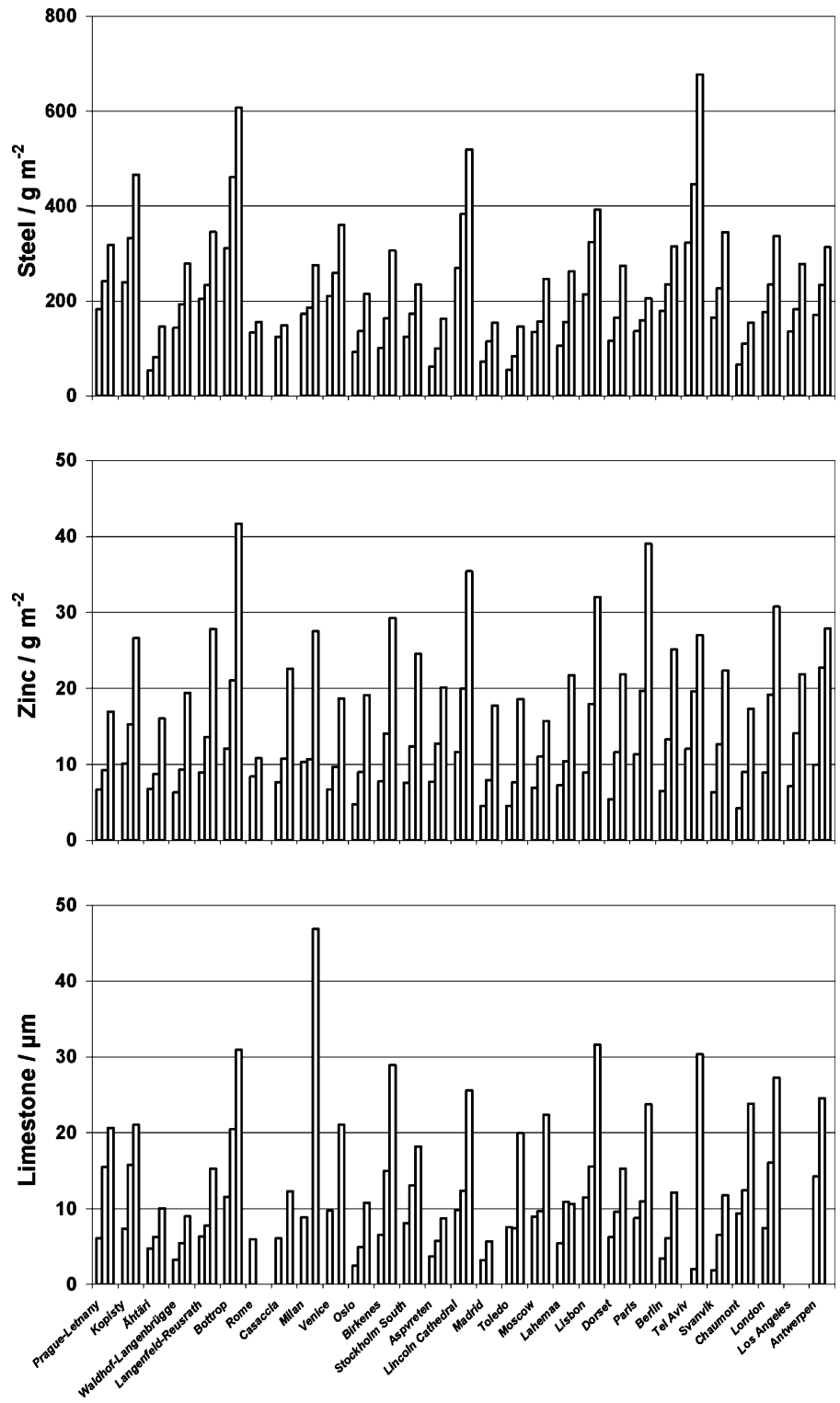
**Fig. 1** Amount of precipitation (*top*), relative humidity (*middle*) and temperature (*bottom*) data for the multi-pollutant exposure (1997–2001)



**Fig. 2** Particulate deposition (*top*), SO<sub>2</sub> (*middle*) and HNO<sub>3</sub> (*bottom*) data for the multi-pollutant exposure (2002–2003 for particulate deposition and HNO<sub>3</sub>, 1997–2001 for SO<sub>2</sub>)



**Fig. 3** Corrosion attack of carbon steel, zinc and limestone exposed in the multi-pollutant exposure (1997–2001) for 1 (left bars), 2 (middle bars) and 4 (right bars) years of exposure



**Table 2** Parameters used in the statistical evaluation

Parameter description	Abbreviation	Unit
Time	t	years
Temperature	T	°C
Relative humidity	Rh	%
Amount of precipitation	Rain	mm year <sup>-1</sup>
pH of precipitation	pH	decades (dimensionless)
Acidity of precipitation <sup>a</sup>	[H <sup>+</sup> ]	mg l <sup>-1</sup>
SO <sub>2</sub> concentration	[SO <sub>2</sub> ]	µg m <sup>-3</sup>
NO <sub>2</sub> concentration	[NO <sub>2</sub> ]	µg m <sup>-3</sup>
O <sub>3</sub> concentration	[O <sub>3</sub> ]	µg m <sup>-3</sup>
HNO <sub>3</sub> concentration	[HNO <sub>3</sub> ]	µg m <sup>-3</sup>
PM concentration (<10 µm)	PM <sub>10</sub>	µg m <sup>-3</sup>
Mass loss	ML	g m <sup>-2</sup>
Surface recession	R	µm

<sup>a</sup> Calculated directly from pH

where  $f(T)$  is as stated above  $0.15(T-10)$  when  $T < 10^\circ\text{C}$ ; otherwise  $-0.054(T-10)$  and the remaining parameters are given in Table 2.

### 3.2.2 Zinc

The dose-response function for zinc from the 8-year ICP Materials exposure programme is

$$\text{ML}_{8\text{-year}} = 1.4[\text{SO}_2]^{0.22} e^{0.018\text{Rh}} e^{f(T)} t^{0.85} + 0.029\text{Rain}[\text{H}^+]t$$

where  $f(T) = 0.062(T - 10)$  when  $T < 10^\circ\text{C}$ , otherwise  $-0.021(T-10)$ . Since again the multi-pollutant data set did not disagree with this temperature function it was used in the resulting multi-assess function

$$\text{ML} = 1.82 + t (1.71 + 0.471[\text{SO}_2]^{0.22} e^{0.018\text{Rh}} e^{f(T)} + 0.041 \text{Rain}[\text{H}^+] + 1.37[\text{HNO}_3])$$

**Table 3** Environmental parameters used in the dose-response functions

Material	T	Rh	Rain	pH	SO <sub>2</sub>	O <sub>3</sub>	HNO <sub>3</sub>	PM <sub>10</sub>
carbon steel	X	X	X	X	X			X
zinc	X	X	X	X	X		X	
copper	X	X	X	X	X	X		
bronze	X	X	X	X	X			X
limestone		X	X	X	X		X	X

The main difference between the previous 8-year function and the new multi-pollutant function is the inclusion of HNO<sub>3</sub>. This is also a difference between zinc and carbon steel where HNO<sub>3</sub> is not included. Comparing Figs. 2 and 3 this is also manifested when comparing the corrosion attack at the sites Milan and Paris, which both have high HNO<sub>3</sub> levels and the corrosion attack of carbon steel is relatively low while the corrosion attack of zinc and also limestone, which is also affected by HNO<sub>3</sub> (see below), are higher.

### 3.2.3 Copper

The dose-response function from the 8-year ICP Materials exposure programme is

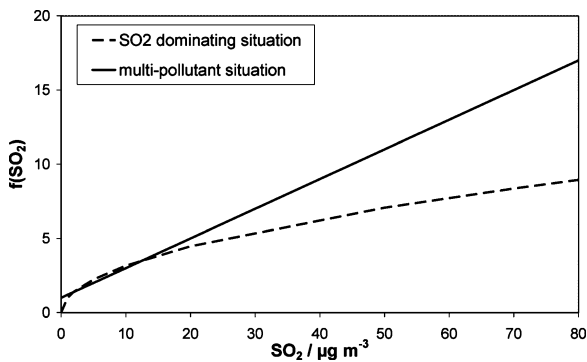
$$\text{ML}_{8\text{-year}} = 0.0027[\text{SO}_2]^{0.32} [\text{O}_3]^{0.79} \text{Rh} e^{f(T)} t^{0.78} + 0.050\text{Rain}[\text{H}^+]t^{0.89}$$

where  $f(T) = 0.083(T - 10)$  when  $T < 10^\circ\text{C}$ , otherwise  $-0.032(T-10)$ . The multi-pollutant data set did not disagree with this temperature function and the resulting multi-assess function is

$$\text{ML} = 3.12 + t (1.09 + 0.00201 [\text{SO}_2]^{0.4} [\text{O}_3] \text{Rh}_{60} e^{f(T)} + 0.0878\text{Rain}[\text{H}^+])$$

The function for copper is very similar to the previously developed function, which also included ozone.





**Fig. 4** Illustration of the difference between the  $\text{SO}_2$  dependence in dose-response functions for the  $\text{SO}_2$  dominating situation and for the multi-pollutant situation

### 3.2.4 Bronze

The dose-response function from the 8-year ICP Materials exposure programme is

$$\begin{aligned} \text{ML}_{8\text{-year}} = & 0.026[\text{SO}_2]^{0.44} \text{Rhe}^{f(T)} t^{0.86} \\ & + 0.029 \text{Rain}[\text{H}^+] t^{0.76} \\ & + 0.00043 \text{Rain}[\text{Cl}] t^{0.76} \end{aligned}$$

where  $[\text{Cl}]$  is the chloride concentration in precipitation ( $\text{g l}^{-1}$ ) and  $f(T) = 0.060(T - 11)$  when  $T < 11^\circ\text{C}$ , otherwise  $-0.067(T - 11)$ . The multi-pollutant data set did not disagree with this temperature function and the resulting multi-assess function is

$$\begin{aligned} \text{ML} = & 1.33 + t(0.00876[\text{SO}_2]e^{f(T)} \text{Rh}_{60} \\ & + 0.0409 \text{Rain}[\text{H}^+] + 0.038 \text{PM}_{10}) \end{aligned}$$

The main difference between the two functions is that the effect of chloride, expressed as wet deposition, has been replaced with particulate deposition, which may partly be a substitute for a chloride effect term.

### 3.2.5 Portland Limestone

The dose-response function from the 8-year ICP Materials exposure programme is

$$\begin{aligned} \text{R}_{8\text{-year}} = & 2.7[\text{SO}_2]^{0.48} e^{-0.018T} t^{0.96} \\ & + 0.019 \text{Rain}[\text{H}^+] t^{0.96} \end{aligned}$$

The multi-pollutant data set *did* disagree with this temperature function and no effect of temperature

could be estimated. Instead a relative humidity term proved effective for both  $\text{SO}_2$  and  $\text{HNO}_3$ .

$$\begin{aligned} R = & 3.1 + t(0.85 + 0.0059 \text{Rh}_{60}[\text{SO}_2] \\ & + 0.078 \text{Rh}_{60}[\text{HNO}_3] + 0.054 \text{Rain}[\text{H}^+] \\ & + 0.0258 \text{PM}_{10}) \end{aligned}$$

The new functions should be used in multi-pollutant situations, while the previous ICP Materials functions (Tidblad et al., 2001) are preferable for areas where  $\text{SO}_2$  is the dominating pollutant. This is illustrated in Fig. 4. In the interval with moderate  $\text{SO}_2$  concentrations (0–20  $\mu\text{g m}^{-3}$ ) the difference between the two functions is not significant. The main difference between the two functions is at higher  $\text{SO}_2$  concentrations (60–80  $\mu\text{g m}^{-3}$ ) where the linear function wrongly predicts higher values.

## 4 Conclusions

Dose-response functions suitable for mapping and calculations of cost of corrosion damage have been developed for the new multi-pollutant situation for carbon steel, zinc, copper, bronze and limestone exposed in unsheltered position. Both pH and  $\text{SO}_2$  are included in all of the functions and these parameters were also present in the previous dose-response functions developed for  $\text{SO}_2$  dominating situations. The new functions should be used in multi-pollutant situations, while the previous ICP Materials functions are preferable for areas where  $\text{SO}_2$  is the dominating pollutant. Besides  $\text{SO}_2$  and acid rain, the effects of  $\text{HNO}_3$  and particulate matter have been included in dose-response functions for metallic materials for the first time.  $\text{NO}_2$  is not included in any of the functions directly but is closely related to  $\text{HNO}_3$ , which is included for zinc and limestone. The effect of particulate matter is included for carbon steel, bronze and limestone.

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