#### **ORIGINAL ARTICLE**



# **Hydrothermal Synthesis of Titanate Nanotubes with Different Pore**  Structure and its Effect on the Catalytic Performance of V<sub>2</sub>O<sub>5</sub>-WO<sub>3</sub>/ **Titanate Nanotube Catalysts for NH3-SCR**

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Published online: 2 November 2018 © Springer Science+Business Media, LLC, part of Springer Nature 2018

#### **Abstract**

In this work, titanate nanotubes (TNT) with different pore structure were synthesized through hydrothermal method by using various TiO<sub>2</sub> particles as starting materials.  $V_2O_5$  and WO<sub>3</sub> was deposited on the as-synthesized TNT structure by wet impregnation. In the selective catalytic reduction of NO with NH<sub>3</sub>, it was found that the catalytic activity of  $V_2O_5-WO_3/TNT$ catalysts was unaffected by the initial different pore structure because the pore structure collapsed during the active metal impregnation and subsequent calcination. Also, kinetic analysis showed that the apparent activation energies of  $V_2O_5-WO_3/$ TNT catalysts and traditional  $V_2O_5$ -WO<sub>3</sub>/TiO<sub>2</sub> catalyst were the similar values, which indicate that the nature of active sites in the SCR reaction on both catalysts would not be significantly different.

**Keywords**  $V_2O_5$ -WO<sub>3</sub>/TiO<sub>2</sub> · TiO<sub>2</sub> nanotube · Selective catalytic reduction · Pore structure · DeNOx

## **1 Introduction**

Selective catalytic reduction (SCR) reaction is a well-known technology to remove  $NO<sub>x</sub>$  by using  $NH<sub>3</sub>$  as reducing agent [\[1](#page-4-0)]. The most commercially available catalyst is vanadium based catalysts, which shows high SCR activity in the middle temperature range (300–400 °C). In general, the commercial catalysts consist of 1–2 wt% of  $V_2O_5$  and 8–10 wt% of WO<sub>3</sub> dispersed on anatase TiO<sub>2</sub>(101) support [\[2](#page-4-1)]. Tungsten oxides are usually added to promote catalytic activity of V and to increase thermal stability of vanadium based catalysts. The biggest advantage of vanadium catalysts is their strong sulfur resistance, which allows SCR operation in combustion engines using fuel with high sulfur content [\[3](#page-4-2)]. In industrial applications, it is important to put a large amount of active metal in a limited space to enhance catalytic performance. Thus, many research groups have focused

Offshore Plant Resources R&D Center, Korea Institute of Industrial Technology, Busan 46938, Republic of Korea on the optimization of SCR active site by morphological change of TiO<sub>2</sub> supports  $[4–6]$  $[4–6]$  $[4–6]$ .

It is well known that titanate nanotubes with high surface area can be easily prepared by hydrothermal synthesis in the alkali solution [\[7](#page-4-5)]. Recently, various active metal oxides supported on the titanate nanotube (TNT) have been used in the NH<sub>3</sub>-SCR reaction. Xiong et al. prepared  $TiO<sub>2</sub>$  nanotube-supported  $V_2O_5$  catalyst, which showed much higher deNO*x* efficiency and satisfactory resistance to water and sulfur compared to raw-TiO<sub>2</sub> supported  $V_2O_5$  catalyst [\[8](#page-4-6)]. Mejía-Centeno et al. also found that  $V_2O_5-WO_3/H_2Ti_3O_7$ catalyst showed a high NO conversion at low temperature (240 °C). They suggested that the nanotube morphology can be maintained up to 480 °C [\[9](#page-4-7)]. Non-vanadium SCR catalysts with Mn, Ce and Cu as active materials have also been attempted using titanate nanotubes as support materials and most works have confirmed enhanced activity and selectivity of these catalysts [\[10](#page-4-8)–[13\]](#page-4-9). In this work, various titanate nanotubes with different pore structures were prepared using various TiO<sub>2</sub> precursor materials and tested as a support for the  $V_2O_5$ -WO<sub>3</sub> catalyst in SCR reaction.

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#### **2 Experimental**

#### **2.1 The Preparation of Catalysts**

Titanate nanotube (TNT) was synthesized by conventional hydrothermal synthesis. Specifically,  $3 \text{ g}$  of TiO<sub>2</sub> powder (DT51, P25, Sigma) was added to 10 M NaOH solution and mixed vigorously in a Teflon lined autoclave. White slurry in the autoclave was heated at 150 °C for 24 h under static condition. After cooling down to the room temperature, the slurry was filtered with 3 L of 0.2 M HCl solution and subsequently washed with 3 L of distilled water. The obtained white powder was dried at 105 °C overnight, which was designated by the name of its precursor  $TiO<sub>2</sub>$  powder (ex. TNT-DT51). As-synthesized TNT was impregnated with ammonium metavanadate  $(NH<sub>4</sub>VO<sub>3</sub>)$  and ammonium metatungstate  $((NH_4)_6H_2W_{12}O_{40})$  dissolved in oxalic acid solution. The samples were dried at 105 °C and calcined at 500 °C for 4 h in air condition. The  $V_2O_5$  and WO<sub>3</sub> contents of catalysts were 3 wt% and 10 wt%, respectively. Prepared catalysts were designated as VW/the type of TNT.

#### **2.2 Characterization Techniques**

The morphological properties of samples were observed with a field emission scanning electron microscope (JSM-6360 (JEOL)) with the accelerating voltage of 20 kV, and the samples were coated with Pt metal with MSC-101 (JEOL) before measurements.  $N_2$  adsorption & desorption isotherms were obtained by using ASAP 2010 apparatus of Micromeritics. BET surface areas were calculated in the  $P/P_0$  range of 0.05–0.20. X-ray diffraction patterns were obtained by using Ultra X18 (Rigaku) with a Cu K $\alpha$  radiation, and the patterns were normally recorded with the step size of 0.02° at the scan speed of 5°/min. A series of Raman spectra were obtained using 532 nm laser excitation on DXR2xi (Thermo, USA) Raman spectrometer at NCIRF (National Center for Inter-university Research Facilities, Seoul National University, Korea).

#### **2.3 Measurements of Catalytic Activity**

The standard selective catalytic reduction (SCR) reaction was carried out in a fixed bed tubular reactor with a diameter of half inch. Normally, 0.12 g of the catalyst particles sieved in the size of 180–250 µm were used, and the total flow rate of the simulated exhaust gas was 200 mL min−1. The inlet concentration of the reactants was 500 ppm NO, 500 ppm NH<sub>3</sub>, 10% O<sub>2</sub>, 10% H<sub>2</sub>O, 5% CO<sub>2</sub> balanced with N<sub>2</sub>. Space velocity of the reaction system was determined to be 100,000 mL  $g^{-1} \cdot h^{-1}$ . The reaction temperature was increased from 100 to 450  $\degree$ C with 50  $\degree$ C intervals and the activity was measured at steady state. NO*x* chemiluminescence analyzer (42i High level, Thermo Scientific) was utilized to measure NO*x* concentration of outlet gas. Fourier transform infrared spectroscopy (FT-IR) equipped with a 2 m gas cell was used to measure the concentration of  $N_2O$ .  $NO<sub>x</sub>$  conversion was calculated by using the following equation.

$$
NO_x \text{ conversion } (\%) = \frac{[NO_x]_{in} - [NO_x]_{out}}{[NO_x]_{in}} \times 100
$$

In kinetic analysis, the internal and external mass transfer effects were neglected below 250 °C. The differential equation was derived using the previously reported plug flow reactor model as follows [[14\]](#page-4-10):

$$
\ln(-\ln(1-x)) = -\frac{E'}{R}\frac{1}{T} + \ln\left(\frac{P}{FR}V_{cat}A'\right)
$$

where  $x$  is the NO fractional conversion;  $F$  is the total gas molar flow rate;  $V_{cat}$  is the catalyst volume;  $R$  is the ideal gas constant;  $P$  is the total pressure;  $T$  is the temperature;  $E'$  is the apparent activation energy; *A*ʹ is the pre-exponential factor. The apparent activation energy was calculated by linear fitting between  $1/T$  and  $ln(-ln(1-x))$ .

#### **3 Results and Discussion**

The morphology of TiO<sub>2</sub> (P25) before and after hydrother-mal treatment was shown in Fig. [1](#page-2-0). The initial  $TiO<sub>2</sub>$  particles have a spherical morphology of 30–40 nm diameter, and individual particles have been observed to aggregate to form large particles. After hydrothermal treatment in 10 M NaOH solution and subsequent HCl washing, long and thin tubular particles were obtained. Each tube has a diameter of 15–20 nm and a length of several hundred nm. It can be seen that the nanotubes are randomly entangled to form large aggregates. Since the tube is hollowed, the nanotube itself has a pore structure with an inner diameter about 10 nm. In addition, the external space between nanotubes present in the nanotube aggregates can also contribute to the porous structure.

The various kind of TiO<sub>2</sub> particles (DT51, P25, Sigma) were used to synthesize TNT in the same condition. As-synthesized TNTs were dried at 100 °C in air, and pretreated in vacuum condition to eliminate water inside the pore before BET analysis.  $N_2$  adsorption desorption curves of prepared TNTs were shown in Fig. [2](#page-2-1). It was confirmed that TNTs with a large pore volume were successfully synthesized regardless of the type of raw  $TiO<sub>2</sub>$  particles (Table [1](#page-3-0)). However, the pore volume, size or BET surface area of each TNT were slightly different from each other. For example, TNT-DT51



**Fig. 1** Field emission SEM images of **a** the starting  $TiO<sub>2</sub>$  particle (P25), and **b** the as-synthesized TNT

<span id="page-2-1"></span><span id="page-2-0"></span>



and TNT-P25 have similar surface areas of 360  $\mathrm{m}^2/\mathrm{g}$ , but TNT-P25 has a much larger pore volume and size than TNT-DT51. In the case of TNT-S, surface area and pore volume are much smaller than others. It seems that the initial size and morphology of  $TiO<sub>2</sub>$  particle can affect the degree of entanglement of nanotubes in hydrothermal synthesis. The tight and dense entanglement of nanotubes can make the small void between nanotube networks.

It is necessary to investigate the pore collapse property of nanotube structures which occurs mainly after the impregnation of the active metal oxide and subsequent calcination process. The collapse of pore structure is an important factor because it can reduce the number of exposed active sites and reduce the reaction rate, and the reduction of surface area

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can lead to sintering of the dispersed active metal oxide. In this experiment, 3 wt%  $V_2O_5$  and 10 wt% WO<sub>3</sub> are loaded on TNTs and calcined at 500 °C for 4 h in air condition. The changes of pore structure of various VW/TNT catalysts were analyzed and shown in Fig. [2.](#page-2-1) The common feature of the three kinds of VW/TNTs is the total collapse of small pores less than 3 nm. Also, it can be seen that pore size distribution curves shifted to large pore size region for all cases, which can be attributed to shrinkage of nanotube aggregates. Thus, at least in this case, the inner surface of nanotubes with small diameter can no longer function as valid surface area for dispersed V or W active sites after calcination at 500 °C. Regardless of initial morphology of TNTs, pore volume and surface area of VW/TNT catalysts are all similar each other

<span id="page-3-0"></span>**Table 1** Textural properties of the prepared TNT, VW/TNT and VW/  $TiO<sub>2</sub>$  catalysts

Sample	$S_{BET} (m^2 g^{-1-1})^a$	$V_{\text{pore}} (cm^3 g^{-1})^b$	Average pore size (nm)
TNT-DT51	364	0.98	10.7
<b>TNT-P25</b>	363	1.31	14.4
TNT-S	270	0.73	10.8
TiO <sub>2</sub> (DT51)	83	0.29	14.0
VW/TNT-DT51	100	0.36	14.5
VW/TNT-P25	121	0.34	11.2
<b>VW/TNT-S</b>	114	0.40	14.1
VW/TiO <sub>2</sub> (DT51)	74	0.26	13.8

<sup>a</sup>BET surface areas were measured in the  $P/P_0$  range of 0.05–0.20 <sup>b</sup>Pore volumes were calculated at  $P/P_0$ =0.97

as shown in Table [1.](#page-3-0) Hence, it seems difficult to maintain the structural advantages of TNT after V impregnation and calcination. In the case of  $TiO<sub>2</sub>(DT-51)$ , however, it can be seen that the structural characteristics are almost same before and after V and W impregnation and calcination process.

XRD patterns of the prepared VW/TNT catalysts are shown in Fig. [3](#page-3-1)a. The sharp peak at 25.4° can be attributed to the anatase  $TiO<sub>2</sub>$  phase. It is known that the phase of as-synthesized TNT is titanate  $(H_2Ti_3O_7)$  before thermal treatment [\[15](#page-4-11)]. Wrapping of layered titanate leads to the formation of titanate nanotube structure. Phase transformation from titanate to anatase occurs during calcination. In the case of VW/TNT catalysts, it was confirmed that all titanate phase completely converted to the anatase phase. No peaks related to  $V_2O_5$  or  $WO_3$  are found except the peak of anatase phase, which indicates that V and W are well dispersed on



<span id="page-3-1"></span>**Fig. 3 a** XRD patterns and **b** Raman spectra of the prepared VW/ TNT catalysts

the TNT surface. Raman spectra of the prepared VW/TNT catalysts are also shown in Fig. [3b](#page-3-1) since small nanocrystals of  $V_2O_5$  or  $WO_3$  might not be able to be detected on the surface by XRD. No sharp peak at 994 cm<sup>-1</sup> was observed for the series of VW/TNT catalysts, which means that the nanocrystals of  $V_2O_5$  was not formed after calcination. Meanwhile, the peak at ~800 cm<sup>-1</sup> was found in all samples, indicating the presence of small nanocrystals of  $WO_3$ .

Various VW/TNT catalysts are tested in standard SCR reaction (Fig. [4](#page-3-2)a). Regardless of the type of TNT, VW/TNT catalysts exhibit similar SCR performance over the entire temperature range. N<sub>2</sub>O selectivity was less than 1% over the whole temperature. This implies that initial pore structure of TNT cannot affect the activity of VW/TNT catalysts. Meanwhile, there is a large difference between VW/TNT series and VW/TiO<sub>2</sub>. At low temperature below 300  $^{\circ}$ C, VW/TiO<sub>2</sub> exhibits much higher NO<sub>x</sub> removal rate than VW/ TNT catalysts. However, VW/TNT catalysts exhibit more stable SCR performance than  $VW/TiO<sub>2</sub>$  at high temperature



<span id="page-3-2"></span>**Fig. 4** Standard NH3-SCR activity over the prepared VW/TNT catalysts compared to to  $VW/TiO<sub>2</sub>$  catalyst. Reaction conditions:  $[NO]=[NH<sub>3</sub>]=500$  ppm,  $[O<sub>2</sub>]=10\%$ ,  $[H<sub>2</sub>O]=10\%$ ,  $[CO<sub>2</sub>]=5\%$  balanced with N<sub>2</sub>, GHSV = 100,000 mL min<sup>-1</sup> g<sup>-1</sup>. **b** kinetic analysis for the tested catalysts below 250 °C

of 300–450 °C. In Fig. [4](#page-3-2)b, kinetic analysis was carried out from the NO*x* conversion data in order to understand the catalytic difference of  $VW/TiO<sub>2</sub>$  and  $VW/TNT$  catalyst. It was assumed that the internal and external mass transfer effects can be neglected below 250 °C [[16\]](#page-4-12). VW/TNT and  $VW/TiO<sub>2</sub>$  catalysts have quite similar standard SCR apparent activation energies in the range of 51–55 kJ/mol, which is consistent with previous report [[14\]](#page-4-10). This observation indicates that the mechanistic nature of V-W active sites are nearly unchanged, and the different reaction rates of the two catalysts are due to the number of active sites. The number of active sites of VW/TNT may be less than that of VW/  $TiO<sub>2</sub>$  because the active metal in TNT is buried by the collapse of tube structure. Meanwhile, the decreasing activity of VW/TiO<sub>2</sub> at high temperatures above 300 °C is known to be due to  $NH_3$  oxidation catalyzed by large  $VO<sub>x</sub>$  cluster. It can be seen that the large surface area of TNT is advantageous in dispersing V sites to prevent the formation of large VO*x* clusters.

In summary, TNTs with different pore structures were obtained by using various  $TiO<sub>2</sub>$  particles. Such difference, however, was not retained after V and W impregnation and subsequent calcination process, and the SCR performance of the various VW/TNT catalysts showed little difference. A series of VW/TNT catalysts exhibited lower NO*x* removal rate than conventional  $VW/TiO<sub>2</sub>$ , which may arise from the loss of active site by the collapse of tube structures based on the kinetic analysis. Stable SCR performance of VW/ TNT catalysts at high temperature above 300 °C suggested that the advantage of using TNT is to prevent the formation of large VO*x* species that are detrimental to SCR activity.

**Acknowledgements** The authors acknowledge the World Class 300 Project Programs (0458-20170019) funded by the Korea Institute for Advancement of Technology (KIAT) for the financial support.

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