

# Non-Thermal Plasma-Assisted Catalytic Dry Reforming of Methane and Carbon Dioxide Over G-C<sub>3</sub>N<sub>4</sub>-Based Catalyst

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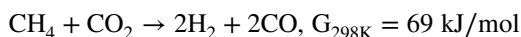
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**Abstract** In the present study, pure plasma and plasma-assisted catalytic activation of reforming of methane and carbon dioxide into syngas production were performed in a coaxial dielectric barrier discharge (DBD) plasma reactor at low temperature. For pure plasma, higher input power was favorable for the conversions of CH<sub>4</sub> and CO<sub>2</sub> but led to lower selectivities of syngas, while selectivities of syngas increased under lower flow rate of feed gases. A high CH<sub>4</sub>/CO<sub>2</sub> ratio was more selective for C<sub>2</sub> hydrocarbon formation. Novel g-C<sub>3</sub>N<sub>4</sub>-based catalysts were prepared and filled in the discharge gap at low temperature. The cooperation effect of DBD plasma with g-C<sub>3</sub>N<sub>4</sub> catalyst was achieved that contributed more to the activation of carbon dioxide than that of methane as well as the yield of CO for its low reduction potential. TiO<sub>2</sub>/g-C<sub>3</sub>N<sub>4</sub> with heterogeneous structure as packing the catalyst bulks into the discharge zone was capable of further improving the reforming of methane and carbon dioxide. TiO<sub>2</sub> mass ratio exhibited significant effect on dry reforming reactions and only TiO<sub>2</sub>/g-C<sub>3</sub>N<sub>4</sub> with 1% TiO<sub>2</sub> mass ratio presented enhanced hybrid effect than that of g-C<sub>3</sub>N<sub>4</sub> catalyst.

**Keywords** Non-thermal plasma · Methane · Carbon dioxide · G-C<sub>3</sub>N<sub>4</sub>-based catalysts

## 1 Introduction

Greenhouse gases, such as carbon dioxide (CO<sub>2</sub>) and methane (CH<sub>4</sub>), have been widely investigated through dry reforming of CH<sub>4</sub> and CO<sub>2</sub>, producing syngas (CO and H<sub>2</sub>) for source utilization and environmental protection [1–3]. The reforming of CO<sub>2</sub> and CH<sub>4</sub> has been reported via the following reaction [4–6].



However, it is a thermodynamically unfavorable reaction that high operating temperature is required for the production of syngas from methane and carbon dioxide with low H<sub>2</sub>/CO molar ratio. The traditional catalytic processes have been widely studied for the reforming of methane with carbon dioxide, while the problems of catalytic deactivation causing by coke deposition and active metals sintering at high operating temperature (above 937 K) usually restrain catalytic technology application [7]. Plasma technology can provide a large number of reactive species generated in the plasma field, including electrons, radicals, etc., which help to make the dry reforming reaction of methane. Non-thermal plasma has attracted increasing attention in recent years because of its low energy requirement [8–13]. Under non-thermal plasma, the reactant molecules such as CH<sub>4</sub> and CO<sub>2</sub> are readily captured by the high-energy electrons to give excited species and free radicals, which facilitate for further chemical reactions. A series of ionization, dissociation and excitation chemical process are initiated and the temperature of the reactants remains only at several 100 K [8].

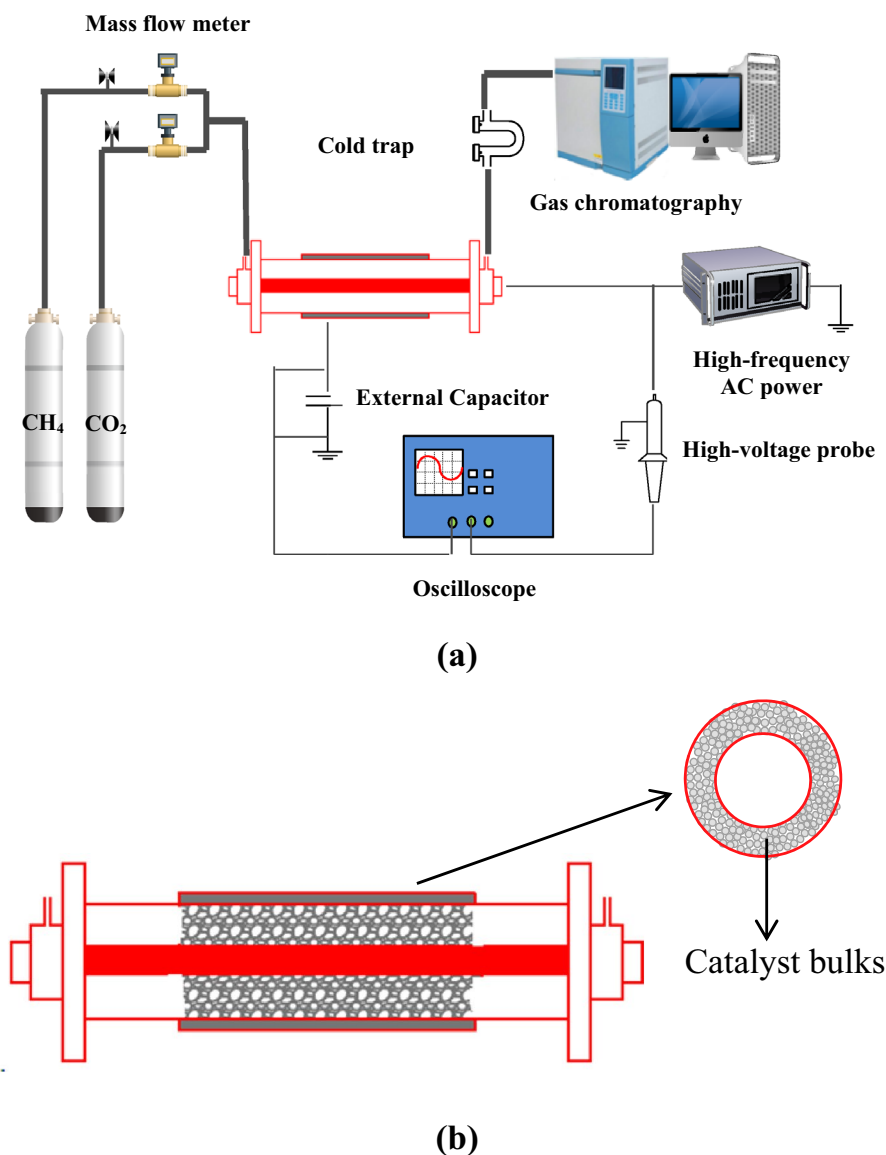
Dielectric barrier discharge (DBD) plasma, as typical non-thermal plasma, possesses advantages of high electron temperature (1–10 eV) and electron density (10<sup>18</sup>–10<sup>21</sup> m<sup>-3</sup>) [14–18], and has been widely investigated

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**Fig. 1** Experimental system (a) and schematic diagram of reactor set-up (b)



to be effective for the dry reforming reaction at low temperature [19–23]. On the other hand, the dry reforming of methane under DBD plasma alone usually suffers from low conversion of reactants, poor selectivity of desired products and undesirable energy efficiency [12, 24–26]. The combination of a heterogeneous catalyst with DBD plasma has been reported to exhibit synergetic effect on improving the reaction performance both in conversion and selectivity [27–30]. Ni-based catalysts, Ni-based bimetallic oxides and  $\text{La}_2\text{O}_3/\gamma\text{-Al}_2\text{O}_3$  catalyst have been extensively applied as catalysts in DBD reactor for the reforming of methane under atmosphere pressure [18, 29–34]. The catalyst placing in the plasma zone can affect discharge mode of DBD plasma that transfers from micro discharge to the combination of surface discharge and micro discharge [35, 36], and further the discharge stability can be destroyed in some

cases [22, 30, 37]. The activation of catalyst in the discharge is found to be after the activation of the reactants [38]. However, effect of coke formation on catalysts in discharge zone is a problem facing by combination of DBD plasma and catalyst that leads to deactivation of the catalysts, and moreover the sintering of active metals is inevitable using metal-based catalyst, both of which cause reduction of carbon balance of plasma-catalysis much lower than 100% [25, 35, 39]. Furthermore, some studies have reported that combination of plasma with catalyst doesn't play a positive role in the reforming reaction of methane [14, 40]. Therefore, it is necessary to develop novel catalyst with improving catalytic performance in discharge zone for enhancing the dry reforming of methane.

Graphitic carbon nitride ( $\text{g-C}_3\text{N}_4$ ) was firstly reported as a novel stable photocatalyst by Wang et al. in 2009 because

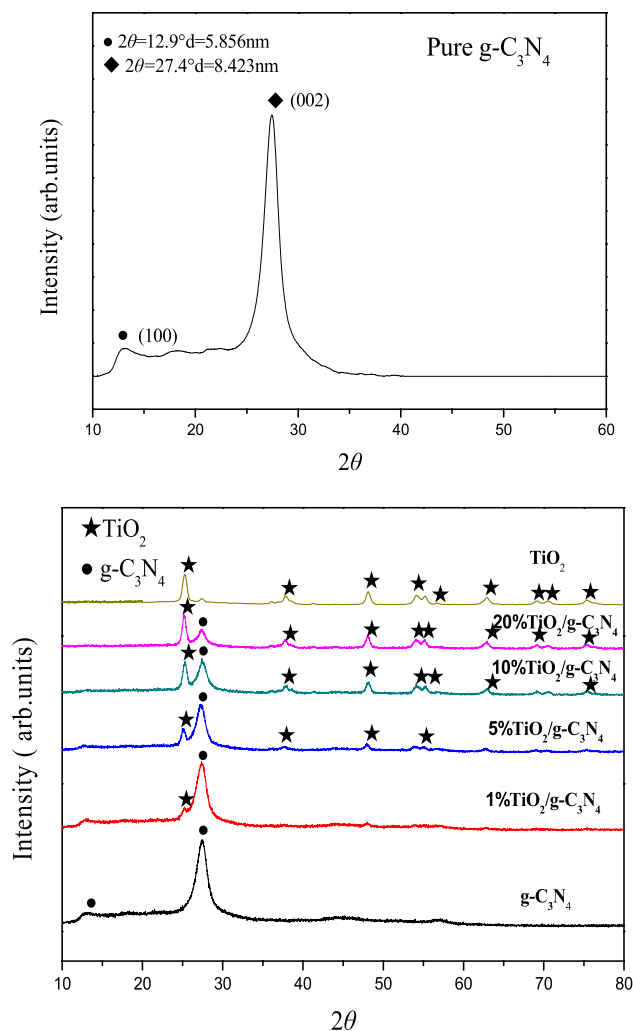
of its metal-free composition, non-toxicity and long-term stability [41], which is composed of carbon and nitrogen elements, possessing layered structure. Because of the band gap of approximately 2.7 eV [8, 42], g-C<sub>3</sub>N<sub>4</sub> has been found to possess superior properties and exhibit efficient photocatalytic performance under visible light. Goettmann et al. reported that CO<sub>2</sub> could be activated by g-C<sub>3</sub>N<sub>4</sub> [43] and Dong et al. also found that CO<sub>2</sub> could be reduced into CO [44]. Accordingly, g-C<sub>3</sub>N<sub>4</sub> exhibits good application prospect in catalytic reduction of CO<sub>2</sub>. Nevertheless, the catalytic efficiency of pure g-C<sub>3</sub>N<sub>4</sub> is far from satisfaction due to its small surface area and short lifetimes of generated electrons and holes [45]. Coupling g-C<sub>3</sub>N<sub>4</sub> and TiO<sub>2</sub> materials (g-C<sub>3</sub>N<sub>4</sub>/TiO<sub>2</sub>) is a promising strategy to improve the catalytic activity because of matched band gaps between g-C<sub>3</sub>N<sub>4</sub> and TiO<sub>2</sub>, which facilitates the separation of generated electrons from valence band (VB) of g-C<sub>3</sub>N<sub>4</sub> (−1.12 eV vs. NHE) to conduction band (CB) of TiO<sub>2</sub> (−0.29 eV vs. NHE), as the VB edge potential of g-C<sub>3</sub>N<sub>4</sub> is more negative than that of TiO<sub>2</sub>. Under the powerful driving force causing by the differences in the CB edge potentials between g-C<sub>3</sub>N<sub>4</sub> and TiO<sub>2</sub>, the generated electron–hole pairs on the g-C<sub>3</sub>N<sub>4</sub> surface are efficiently separated. TiO<sub>2</sub> acts as the acceptors of the generated electrons due to the matched band gaps between g-C<sub>3</sub>N<sub>4</sub> and TiO<sub>2</sub>. In DBD discharge zone, the high electron temperature is satisfactory to activate the g-C<sub>3</sub>N<sub>4</sub>/TiO<sub>2</sub> catalyst and it will be of important significance to exploring the feasibility of applying this novel catalyst for reforming of methane and carbon dioxide.

In this paper, CO<sub>2</sub> reforming of CH<sub>4</sub> to syngas by combination of DBD plasma with g-C<sub>3</sub>N<sub>4</sub>-based catalyst was studied under ambient conditions without extra heat to mitigate greenhouse emissions and reuse the carbon-hydrogen source. G-C<sub>3</sub>N<sub>4</sub>-based catalyst was firstly used as catalyst to convert methane and carbon dioxide because of its metal-free composition and good catalytic activity. The experimental conditions in the performed experiment and the effect of catalyst on the CO<sub>2</sub> reforming of CH<sub>4</sub> for syngas production are well investigated.

## 2 Experimental

### 2.1 Experimental System

The experimental system is shown in Fig. 1a. The non-thermal plasma-assisted catalytic experiments are performed in a coaxial DBD reactor that consists of a quartz tube with an inner diameter and thickness of 12 and 1.5 mm, respectively, as shown in Fig. 1b. A stainless tube with an inner diameter of 8 mm on the inside of the tube serves as high voltage electrode and the outer electrode is aluminum foil wrapping around the outer tube. The discharge length is



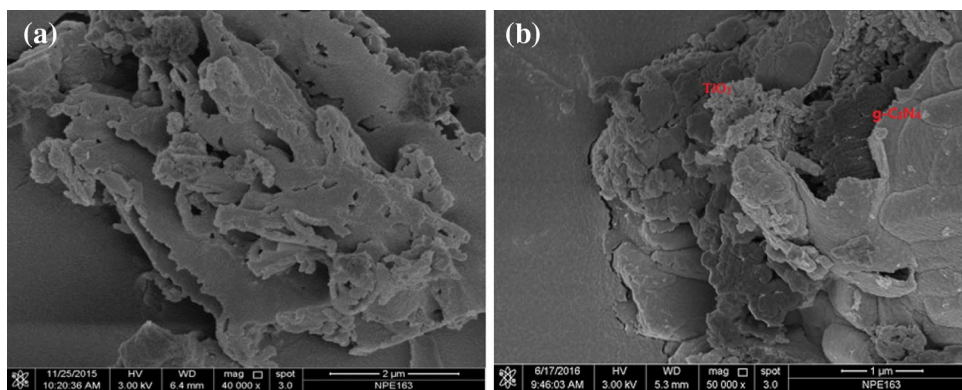
**Fig. 2** XRD patterns of pure g-C<sub>3</sub>N<sub>4</sub> and TiO<sub>2</sub>/g-C<sub>3</sub>N<sub>4</sub>

13 cm. DBD plasma is generated by an AC high-voltage generator (CTP-2000K) with a variable frequency of 4–12 kHz. A gas mixture of methane and carbon dioxide, controlled by mass flow controllers (MFC), flows to the DBD reactor. After reaction, on-line detection of the reaction mixture is performed on a gas chromatography (Shanghai Tianmei, GC7900) equipped with a thermal conductive detector (TCD) and a flame ionization detector (FID).

### 2.2 Preparation of G-C<sub>3</sub>N<sub>4</sub>-Based Catalysts

G-C<sub>3</sub>N<sub>4</sub> was prepared by heating melamine powder (heating rate 5°C/min) at 500°C in a muffle furnace for 2 h and then heated at 520°C for 2 h. After naturally cooling to room temperature, the yellow product was collected and milled into powder. TiO<sub>2</sub>/g-C<sub>3</sub>N<sub>4</sub> catalyst was prepared by mixing a certain amount of TiO<sub>2</sub> (P25) and melamine powder in absolute ethyl alcohol, stirring for 3 h, treating

**Fig. 3** SEM images of **a** g-C<sub>3</sub>N<sub>4</sub> and **b** 1% TiO<sub>2</sub>/g-C<sub>3</sub>N<sub>4</sub>



by ultrasound for 1 h, dried for 8 h, and finally heated at the same conditions of preparing g-C<sub>3</sub>N<sub>4</sub>. The product was milled into small pieces with average diameter of approximately 0.4–1.0 mm. TiO<sub>2</sub>/g-C<sub>3</sub>N<sub>4</sub> with different contents of TiO<sub>2</sub> was obtained. In the plasma-assisted catalytic experiments, the catalyst packed in the plasma zone was shown in Fig. 1b.

### 2.3 Characterization of Catalysts

The crystallinity characteristic of catalyst was determined using a X-ray diffractometer (Shimadzu, XD-3A) with Cu K $\alpha$  radiation at a scanning speed of 5 °C/min. The morphology of catalyst was observed on a NOVA Nano SEM 450 field-emission scanning electron microscope (FESEM). UV–Vis diffuse reflection spectra (UV-DRS) were recorded on UV–Vis spectrometer (UV-2450, Shimadzu) in the range of 200–800 nm using BaSO<sub>4</sub> as the reflectance standard. The X-ray photoelectron spectroscopy (XPS) measurement was performed using ESCALAB™ 250Xi XPS spectrometer equipped with Al K $\alpha$  radiation in the fixed analyzer transmission mode. All peaks in XPS spectra have already been calibrated with C 1s peak at 284.6 eV. The Brunauer–Emmett–Teller (BET) of the catalyst was analyzed by nitrogen adsorption–desorption at 77 K in a Quantachrome AS-1 Fully automatic physical nitrogen adsorption instrument. The BET surface area was determined using adsorption data in a relative pressure (P/P<sub>0</sub>) range of 0.05–0.3, and the Barrett–Joyner–Halenda (BJH) method was used to determine the pore-size distribution.

### 2.4 Analytical Method

In the present work, the reactants and products were analyzed by an on-line gas chromatography. The CH<sub>4</sub> and CO<sub>2</sub> conversions, products selectivities, yields of products, and carbon balance are defined as follows:

$$C_{\text{CO}_2}(\%) = \frac{\text{CO}_2 \text{ converted (mol/s)}}{\text{CO}_2 \text{ input (mol/s)}} \times 100$$

$$C_{\text{CH}_4}(\%) = \frac{\text{CH}_4 \text{ converted (mol/s)}}{\text{CH}_4 \text{ input (mol/s)}} \times 100$$

$$S_{\text{CO}}(\%) = \frac{\text{CO produced (mol/s)}}{\text{CO}_2 \text{ converted (mol/s)} + \text{CH}_4 \text{ converted (mol/s)}} \times 100$$

$$S_{\text{H}_2}(\%) = \frac{\text{H}_2 \text{ produced (mol/s)}}{2 \times \text{CH}_4 \text{ converted (mol/s)}} \times 100$$

$$S_{\text{C}_2\text{H}_6}(\%) = \frac{\text{C}_2\text{H}_6 \text{ produced} \times 2 \text{ (mol/s)}}{\text{CO}_2 \text{ converted (mol/s)} + \text{CH}_4 \text{ converted (mol/s)}} \times 100$$

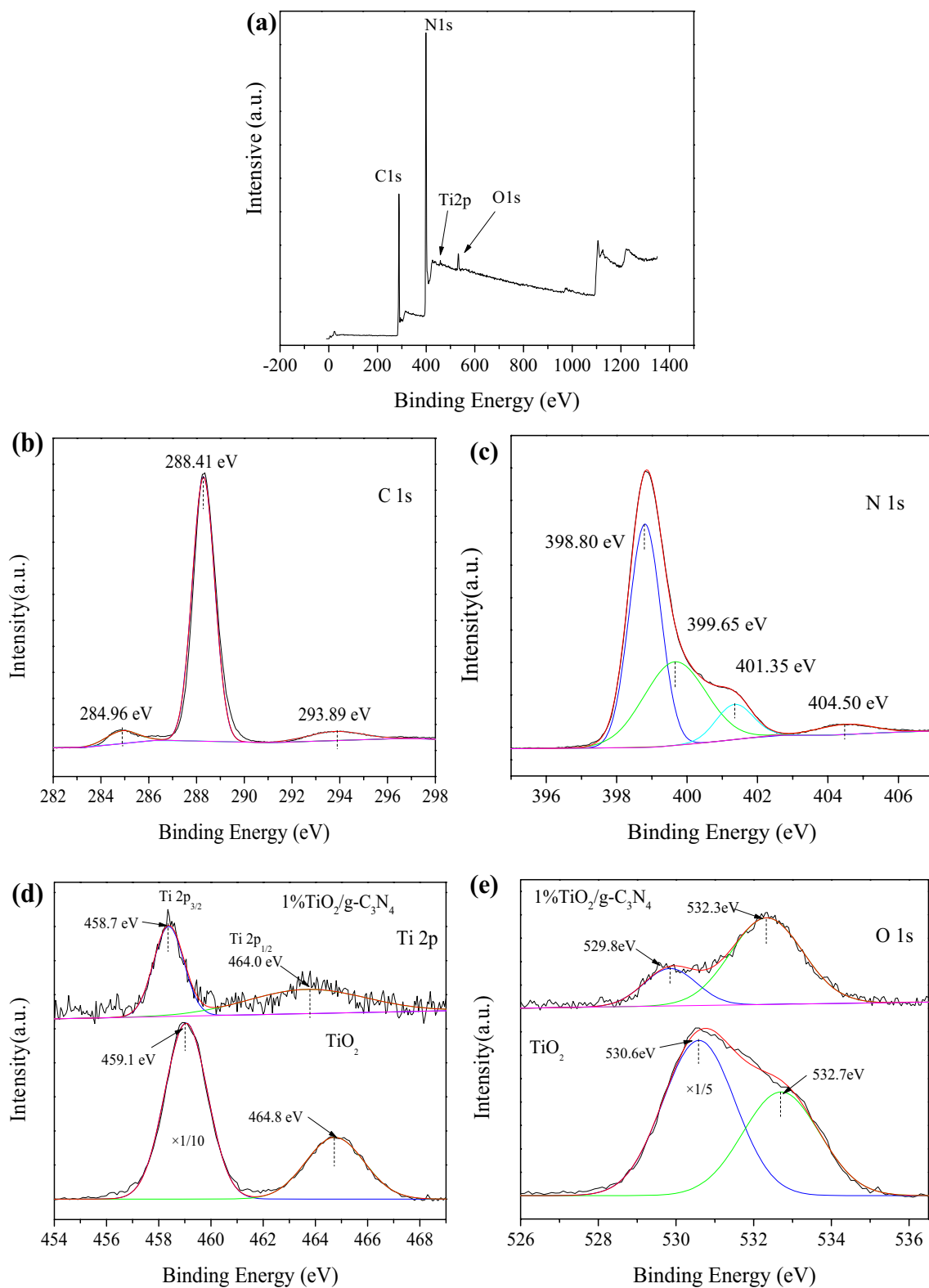
$$Y_{\text{CO}}(\%) = \frac{\text{CO produced (mol/s)}}{\text{CO}_2 \text{ input (mol/s)} + \text{CH}_4 \text{ input (mol/s)}} \times 100$$

$$Y_{\text{H}_2}(\%) = \frac{\text{H}_2 \text{ produced (mol/s)}}{2 \times \text{CH}_4 \text{ input (mol/s)}} \times 100$$

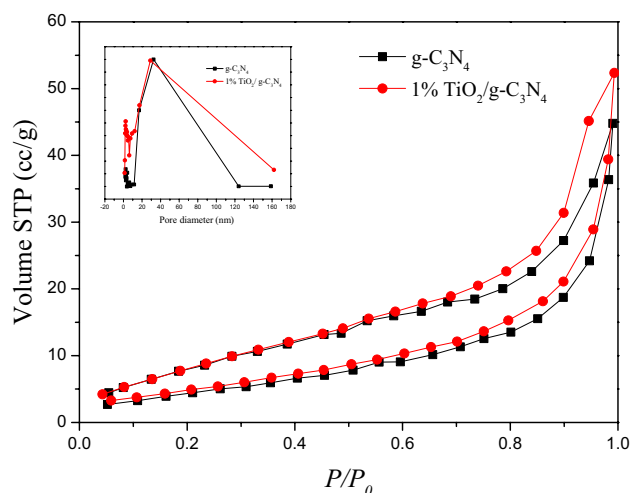
$$Y_{\text{C}_2\text{H}_6}(\%) = \frac{\text{C}_2\text{H}_6 \text{ produced (mol/s)} \times 2}{\text{CO}_2 \text{ input (mol/s)} + \text{CH}_4 \text{ input (mol/s)}} \times 100$$

$$S_{\text{CH}_4 \text{ to CO}_2}(\%) = \frac{\text{CO produced (mol/s)} - \text{CO}_2 \text{ converted (mol/s)}}{\text{CH}_4 \text{ converted (mol/s)}} \times 100$$

$$B_{\text{carbon}}(\%) = \frac{\text{CO produced (mol/s)} + \text{CO}_2 \text{ produced (mol/s)} + \text{C}_x\text{H}_y \text{ produced (mol/s)} \times x}{\text{CO input (mol/s)} + \text{CH input (mol/s)}} \times 100$$



**Fig. 4** XPS of **a** survey spectrum, **b** C 1s and **c** N 1s for 1% TiO<sub>2</sub>/g-C<sub>3</sub>N<sub>4</sub>, **d** Ti 2p and **e** O 1s for 1% TiO<sub>2</sub>/g-C<sub>3</sub>N<sub>4</sub> and pure TiO<sub>2</sub>



**Fig. 5** Nitrogen adsorption–desorption isotherms and corresponding pore size distribution (*inset*) of the  $g\text{-C}_3\text{N}_4$  and 1%  $\text{TiO}_2/g\text{-C}_3\text{N}_4$

Specific energy density (*SED*) and energy utilization efficiency (*E*) are defined as:

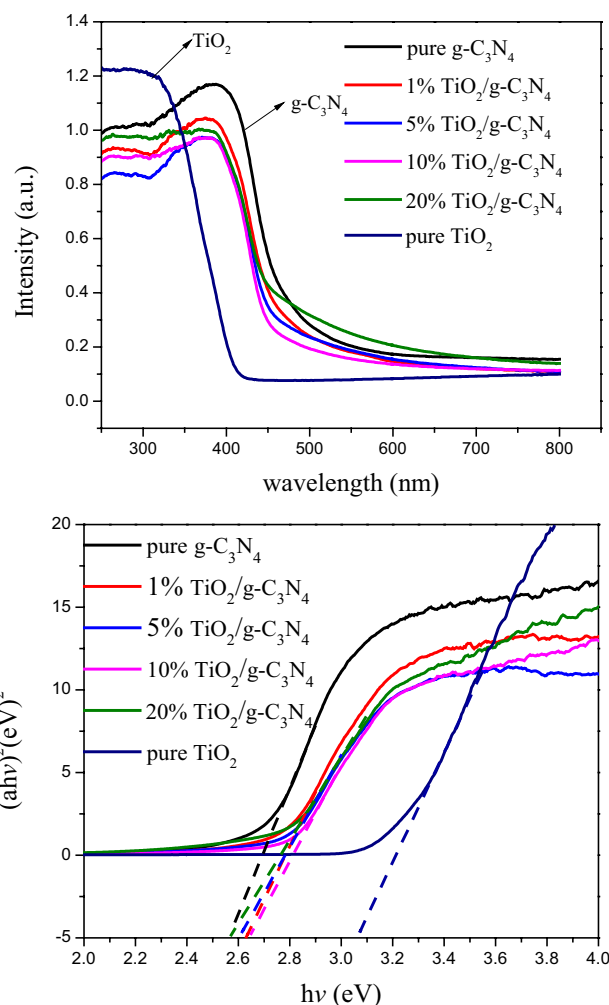
$$SED \text{ (kJ/L)} = \frac{\text{Discharge power (kW)}}{\text{CO}_2 \text{ flow rate (L/s)} + \text{CH}_4 \text{ flow rate (L/s)}}$$

$$E \text{ (mol/kJ)} = \frac{\text{CO}_2 \text{ converted (mol/s)} + \text{CH}_4 \text{ converted (mol/s)}}{\text{Power input (kW)}}$$

### 3 Results and Discussion

#### 3.1 Characterization of Catalysts

The phase structures of the prepared catalysts are determined by XRD analysis. XRD patterns of pure  $g\text{-C}_3\text{N}_4$ , and  $\text{TiO}_2/g\text{-C}_3\text{N}_4$  prepared at different mass ratios of  $g\text{-C}_3\text{N}_4$  and  $\text{TiO}_2$  are illustrated in Fig. 2. The pure  $g\text{-C}_3\text{N}_4$  shows two characteristic diffraction peaks at  $13.1^\circ$  and  $27.4^\circ$  (JCPDS No. 87-1526). The minor peak of (100) at  $13.1^\circ$  and the stronger peak of (002) at  $27.4^\circ$  correspond to the inter-layer structural packing [46] and the interplanar graphitic stacking of aromatic system [47], respectively. The phases of  $\text{TiO}_2$  are observed in the  $\text{TiO}_2/g\text{-C}_3\text{N}_4$  samples. With the increase of the mass ratio of  $\text{TiO}_2$  in the  $\text{TiO}_2/g\text{-C}_3\text{N}_4$ , the intensity of the diffraction peak of (101) at  $25.2^\circ$ , assigning to anatase phase (JCPDS No. 21-1272) of  $\text{TiO}_2$ , becomes stronger, while the



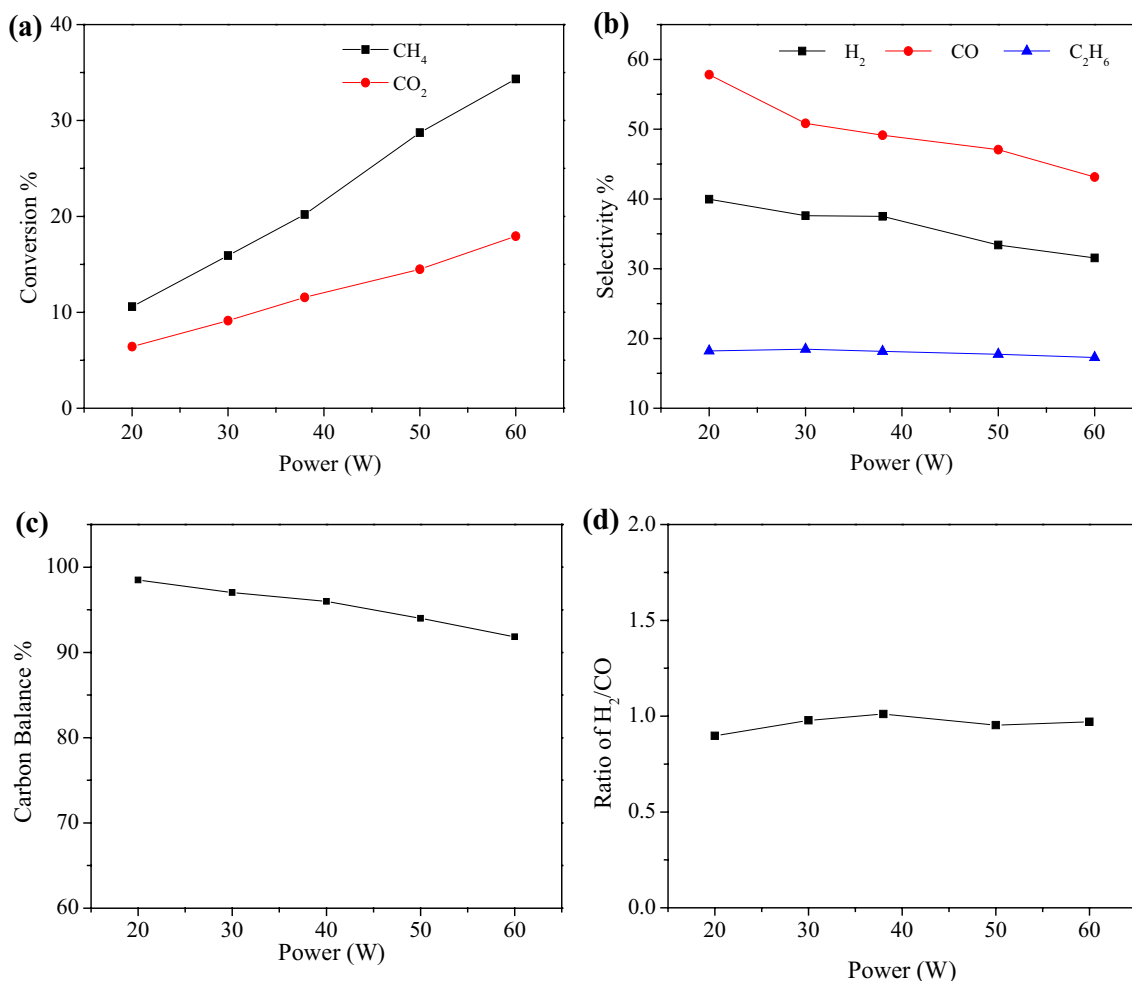
**Fig. 6** UV–vis absorption spectra of pure  $g\text{-C}_3\text{N}_4$ , pure  $\text{TiO}_2$ , and  $\text{TiO}_2/g\text{-C}_3\text{N}_4$  composite with different ratios

diffraction peak intensity at  $27.6^\circ$  of  $g\text{-C}_3\text{N}_4$  becomes weaker. In addition, the peak positions for all  $\text{TiO}_2/g\text{-C}_3\text{N}_4$  samples are observed to keep unchanged, indicating that  $\text{TiO}_2$  probably deposits on the surface of  $g\text{-C}_3\text{N}_4$ .

SEM imaging is performed to observe the morphologies of  $g\text{-C}_3\text{N}_4$  and  $\text{TiO}_2/g\text{-C}_3\text{N}_4$ . From the point of the entire field of vision (Fig. 3a), it fills with large number of continuous lamellar  $g\text{-C}_3\text{N}_4$  with 2D lamellar structure. As shown in Fig. 3b, after mixing  $\text{TiO}_2$  (1%) with  $g\text{-C}_3\text{N}_4$ ,  $\text{TiO}_2$  is loaded on the surface of  $g\text{-C}_3\text{N}_4$ , which is benefited for the formation of heterojunction between  $g\text{-C}_3\text{N}_4$  and  $\text{TiO}_2$ . The surface

**Table 1** Specific surface area of the as-prepared samples with the different amount of  $\text{TiO}_2$  in  $\text{TiO}_2/g\text{-C}_3\text{N}_4$  composite

Sample	$g\text{-C}_3\text{N}_4$	1% $\text{TiO}_2/g\text{-C}_3\text{N}_4$	5% $\text{TiO}_2/g\text{-C}_3\text{N}_4$	10% $\text{TiO}_2/g\text{-C}_3\text{N}_4$	20% $\text{TiO}_2/g\text{-C}_3\text{N}_4$
Specific surface area ( $\text{m}^2/\text{g}$ )	14.1	18.2	22.1	33.5	21.5
Pore volume ( $\text{cc/g} \times 10^{-3}$ )	0.0072	0.0087	0.0108	0.017	0.011



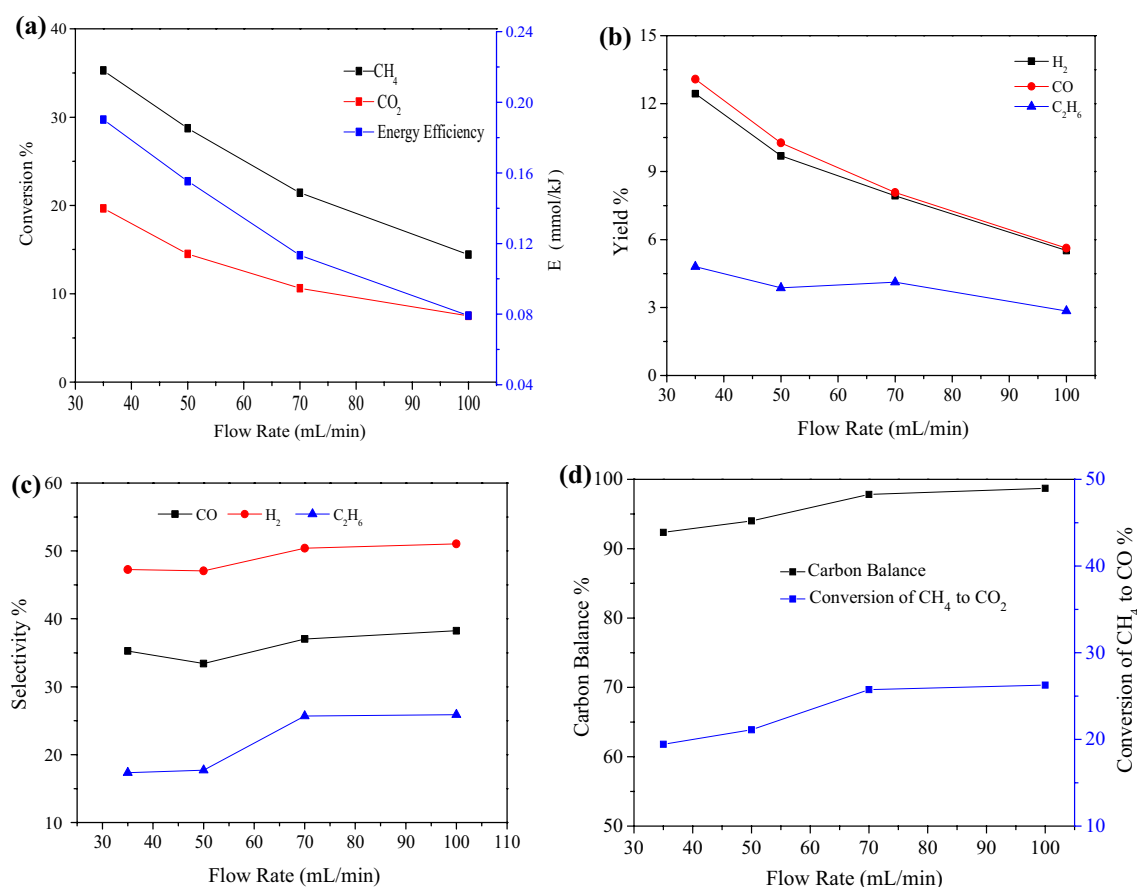
**Fig. 7** Effect of discharge power on the performance of dry reforming reaction: **a** conversion of reactants; **b** selectivity of main products; **c** carbon balance; **d** ratio of H<sub>2</sub>/CO (CH<sub>4</sub>/CO<sub>2</sub>=1:1, feed flow rate 50 mL/min)

of TiO<sub>2</sub> is rough and porous, possibly being caused by the agglomeration of TiO<sub>2</sub> to some extent due to the calcination treatment.

The XPS survey spectrum of TiO<sub>2</sub>/g-C<sub>3</sub>N<sub>4</sub> sample is shown in Fig. 4a, in which C 1s, N 1s, Ti 2p and O 1s can be observed. The weak peaks of Ti and O are the results of low amount of TiO<sub>2</sub> in the TiO<sub>2</sub>/g-C<sub>3</sub>N<sub>4</sub> composite. Figure 4b shows the spectrum of C 1s for TiO<sub>2</sub>/g-C<sub>3</sub>N<sub>4</sub> sample. The peaks at about 284.96, 288.41 and 293.89 eV correspond to C–C, C–N–C and C–(N)<sub>3</sub> groups in the g-C<sub>3</sub>N<sub>4</sub>, respectively [48]. Figure 4c shows the spectrum of N 1s for TiO<sub>2</sub>/g-C<sub>3</sub>N<sub>4</sub> that displays four peaks, ascribable to sp<sub>2</sub> hybridized nitrogen (C=N–C) at about 398.8 eV, tertiary N in N–(C)<sub>3</sub> at about 399.65 eV, N atoms in amino moieties at about 401.35 eV [49], and weak peak located at 404.2 eV which is due to the charging effects or positive charge localization in the

heterocycles [50]. Figure 4d presents the Ti 2p spectra of TiO<sub>2</sub>/g-C<sub>3</sub>N<sub>4</sub> and pure TiO<sub>2</sub>. Two peaks for Ti 2p<sub>3/2</sub> and Ti 2p<sub>1/2</sub> of pure TiO<sub>2</sub> located at 459.1 and 464.8 eV, and the peaks at 458.7 and 464.0 eV correspond to Ti 2p<sub>3/2</sub> and Ti 2p<sub>1/2</sub> of TiO<sub>2</sub>/g-C<sub>3</sub>N<sub>4</sub>, respectively. Comparison of O 1s spectra of TiO<sub>2</sub>/g-C<sub>3</sub>N<sub>4</sub> and pure TiO<sub>2</sub> is shown in Fig. 4e. The binding energies of 530.6 eV and 532.7 eV for pure TiO<sub>2</sub> can be ascribed to Ti–O bond and O–H bond, respectively [48]. Compared with pure TiO<sub>2</sub>, O 1s spectrum of TiO<sub>2</sub>/g-C<sub>3</sub>N<sub>4</sub> shows the negative shift with an order of 0.8 eV, and the same shift of Ti 2p in Fig. 4b is also observed, which indicates that chemically bound interfaces may be formed between g-C<sub>3</sub>N<sub>4</sub> and TiO<sub>2</sub> phase.

The nitrogen adsorption–desorption isotherms of g-C<sub>3</sub>N<sub>4</sub> and 1% TiO<sub>2</sub>/g-C<sub>3</sub>N<sub>4</sub> were present in Fig. 5. It can be seen that both samples have the isotherms type of H4 according to the IUPAC (International Union of Pure and



**Fig. 8** Effect of total flow rate on the performance of plasma dry reforming reaction: **a** conversion of reactants and energy efficiency; **b** yield of main products; **c** selectivity of main products; **d** carbon balance ( $\text{CH}_4/\text{CO}_2=1:1$ , discharge power 50 W)

Applied Chemistry) classification, which indicates irregular pore structure and micropore and mesopore both exist in the samples [51]. The graph insert in Fig. 5 shows the pore-size distributions of  $\text{g-C}_3\text{N}_4$  and 1%  $\text{TiO}_2/\text{g-C}_3\text{N}_4$ , which are broad and the samples are mainly composed by mesopore. Specific surface area ( $S_{\text{BET}}$ ) of the as-prepared samples with different amount of  $\text{TiO}_2$  in  $\text{g-C}_3\text{N}_4$  was shown in Table 1. The  $S_{\text{BET}}$  increases with the increasing amount of  $\text{TiO}_2$  except 20% $\text{TiO}_2/\text{g-C}_3\text{N}_4$ , which is possibly attributed to the sintering caused by calcine process.

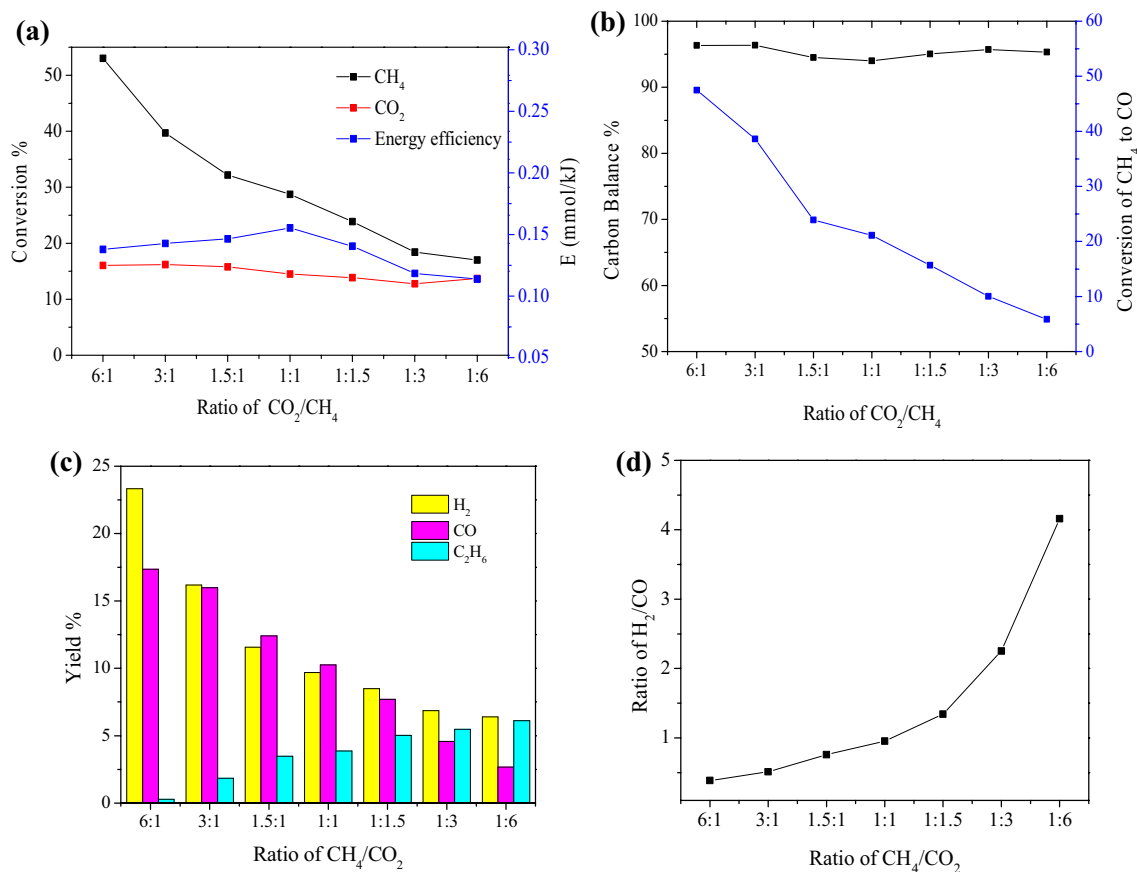
The optical absorption properties of  $\text{TiO}_2$ ,  $\text{g-C}_3\text{N}_4$  and as-prepared  $\text{TiO}_2/\text{g-C}_3\text{N}_4$  samples are investigated by UV-DRS analysis, as shown in Fig. 6. The absorption edge for  $\text{TiO}_2$  is under 400 nm, only having a response to UV light. The  $\text{g-C}_3\text{N}_4$  exhibits a wider photo-absorption till visible light, the main absorption edge of which occurs at approximately 500 nm due to its wide band gap of 2.57 eV. For  $\text{TiO}_2/\text{g-C}_3\text{N}_4$  samples, a certain extent red-shift of the absorption edge to visible region and a certain extent blue-shift of the absorption edge to UV region are observed as compared to pure  $\text{TiO}_2$  and pure  $\text{g-C}_3\text{N}_4$ , respectively, indicating the band gap

of  $\text{g-C}_3\text{N}_4$  becomes narrower when combining it with  $\text{TiO}_2$ . In the plasma zone, the catalyst is expected to be excited by the active species in the plasma with energy higher than 2.7 eV, exhibiting catalytic performance on reforming of methane efficiently.

### 3.2 Effect of Discharge Power on the Plasma Dry Reforming Reaction

Under non-thermal plasma, the discharge power determines the strength of the internal electric field and the electron energy, which is important for inelastic collisions between energetic electrons and reactant molecules. In the present work, the conversions of  $\text{CO}_2$  and  $\text{CH}_4$  were found to increase from 6% and 11% to 18% and 34%, respectively, with the discharge power increasing from 20 to 60 W. High level of discharge power provides more energy for the formation of active species, such as electrons, 'OH, and O', which are likely to attack  $\text{CH}_4$  and  $\text{CO}_2$ , leading to enhanced conversions of reactants. It is also found that the conversion of  $\text{CH}_4$  is





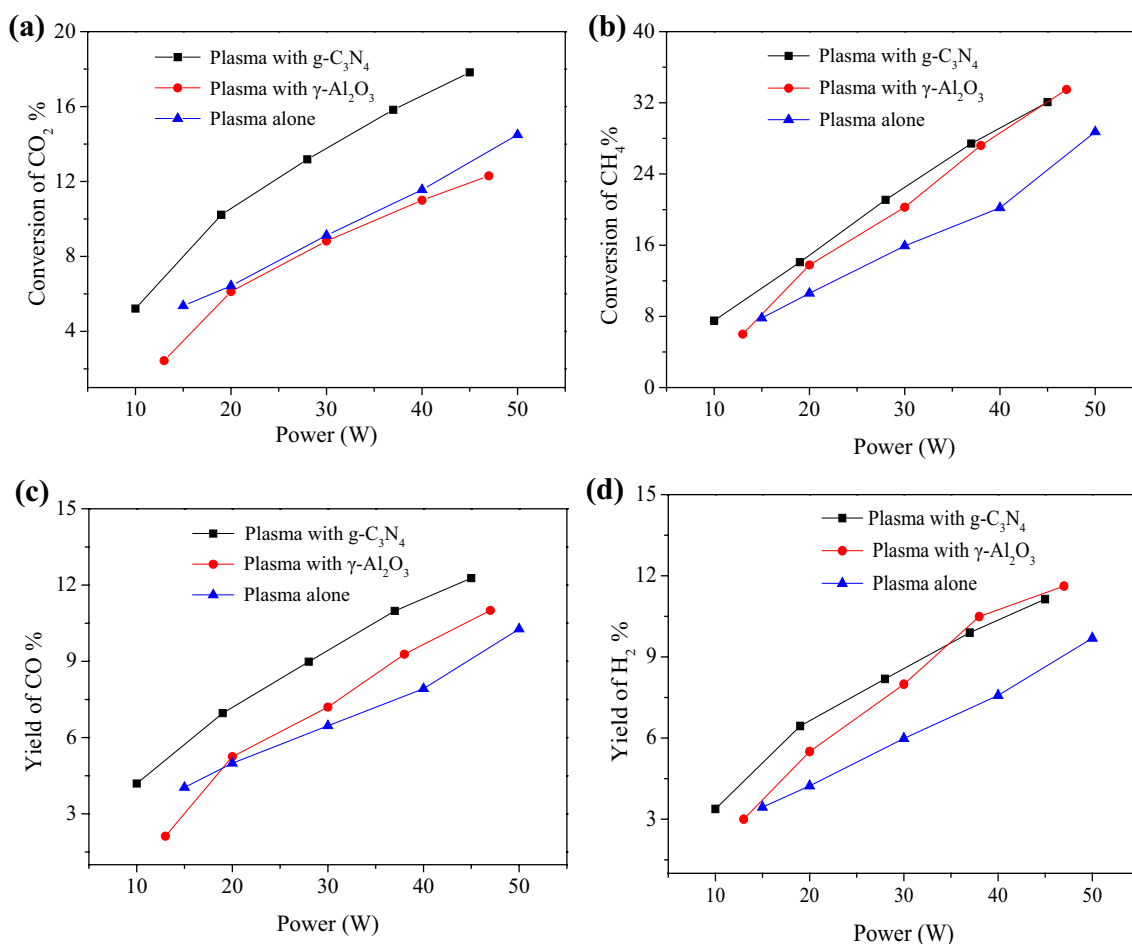
**Fig. 9** Effect of CO<sub>2</sub>/CH<sub>4</sub> ratio on the performance of dry reforming reaction: **a** conversion of reactants and energy efficiency; **b** carbon balance and the ratio of CH<sub>4</sub> convert to CO; **c** yield of main products; **d** ratio of H<sub>2</sub>/CO (feed flow rate 50 mL/min, discharge power 50 W)

always higher than that of CO<sub>2</sub> as shown in Fig. 7a. Similar result is also reported in [30]. With the increase of discharge power, the balance between the dehydrogenation rates of CH<sub>x</sub> (x = 1–4) radicals and the dissociation rate of active CO<sub>2</sub> species can be deteriorated causing by the excess energy. The result of the breaking of the balance favors for the reaction between H and O but is disadvantageous for the generation of CO from C and O atoms [52]. The selectivities of CO and H<sub>2</sub> decreased with the increase of discharge power (Fig. 7b), indicating the coke formation at higher energy level, the results of which consist with the conversions of CO<sub>2</sub> and CH<sub>4</sub>. Gaseous hydrocarbon, C<sub>2</sub>H<sub>6</sub>, existing in the products, is possibly formed by the complex reaction between two CH<sub>3</sub> radicals. In Fig. 5b, the selectivity of C<sub>2</sub>H<sub>6</sub> hardly changed with the increasing discharge power, suggesting that C<sub>2</sub>H<sub>6</sub> formation was not affected by the discharge power. The carbon balance was found to decrease with the increase of discharge power (Fig. 7c), further supporting the facts of coke formation at higher energy level. As shown in Fig. 7d, discharge power exhibited

less effect on the H<sub>2</sub>/CO ratio, which indicated the consistent changes of H<sub>2</sub> formation and CO formation was not affected with the increase of discharge power.

### 3.3 Effect of Total Flow Rate on the Plasma Dry Reforming Reaction

The total flow rate of feed determines the residence time of the reactants in the discharge zone and its effect on the plasma dry reforming reaction is shown in Fig. 8. For a constant input power, the conversions of CH<sub>4</sub> and CO<sub>2</sub> decreased from 35.3% and 19.7% to 14.4% and 7.5% (Fig. 8a), respectively, and the yields of CO and H<sub>2</sub> both decreased by approximately 56% (Fig. 8b), but the selectivities of CO and H<sub>2</sub> changed slightly (Fig. 8c), with the increase of total flow rate from 35 to 100 mL/min. The total flow rate also influenced the formation of the hydrocarbon byproduct, C<sub>2</sub>H<sub>6</sub>, the yield of which decreased by 42%, while the selectivity of it increased obviously. It is apparent that increasing the total flow rate benefits the conversion of CH<sub>4</sub> to hydrocarbon byproduct. As shown



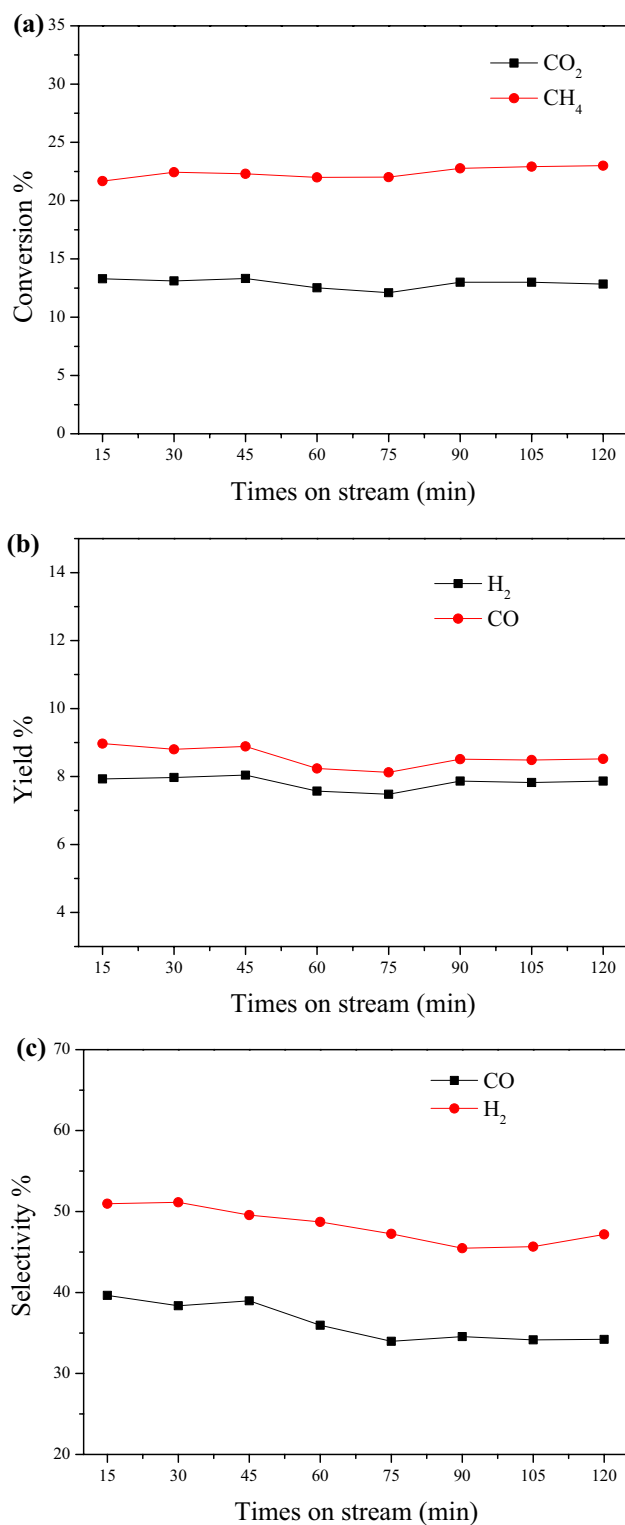
**Fig. 10** Effect of packing  $g\text{-C}_3\text{N}_4$  catalyst and  $\gamma\text{-Al}_2\text{O}_3$  in plasma discharge area on the performance of plasma dry reforming reactions: **a** conversion of  $\text{CH}_4$ ; **b** conversion of  $\text{CO}_2$ ; **c** yield of  $\text{CO}$ ; **d** yield of  $\text{H}_2$ . ( $\text{CH}_4/\text{CO}_2 = 1:1$ , feed flow rate 50 mL/min)

in Fig. 6d, the carbon balance as well as conversion of  $\text{CH}_4$  to  $\text{CO}$  increased with the total flow rate, because increase of the flow rate would reduce the collision chance among  $\text{CH}_x$  active species, and thus more  $\text{CH}_4$  was converted to low-carbon hydrocarbon compounds such as  $\text{C}_2\text{H}_6$  and  $\text{CO}$  instead of long chain hydrocarbons. Energy efficiency is found to decrease when increasing the total flow rate, which is caused by the reduction of residence time of reactants and active species in plasma zone. On the consideration of the effect of the total flow rate on the dry reforming reaction, the optimal flow rate of 50 mL/min is selected in the following experiments.

### 3.4 Effect of $\text{CO}_2/\text{CH}_4$ Ratio on the Plasma Dry Reforming Reaction

Effect of reagent composition on the plasma dry reforming reaction is performed by varying the  $\text{CO}_2/\text{CH}_4$  ratios from 6/1 to 1/6 at a constant total flow rate (50 mL/min)

and a constant discharge power (50 W). The results are shown in Fig. 9. With the increase of molar ratio of  $\text{CH}_4$  to  $\text{CO}_2$ , the conversion of  $\text{CH}_4$  was always higher than that of  $\text{CO}_2$ . However, the  $\text{CO}_2/\text{CH}_4$  ratio had greater influence on the conversion of  $\text{CH}_4$  which decreased from 53% to 17% obviously but the conversion of  $\text{CO}_2$  changed slightly. As shown in Fig. 9b, the yields of  $\text{H}_2$  and  $\text{CO}$  both decreased with the increase of molar ratio of  $\text{CH}_4$  to  $\text{CO}_2$  while the yield of  $\text{C}_2\text{H}_6$  increased. Figure 9c further exhibited the fact that increasing the amount of  $\text{CH}_4$  in the feed gas would restrain its conversion to  $\text{CO}$ . These experimental results can be explained by the possible reactions involving active methane species, the amount of which increase with the  $\text{CH}_4$  molar, and thus more active methane species involve in recombination reaction than methane oxidation to form  $\text{CO}$ , generating more hydrocarbons [18, 30]. In the present studied range of  $\text{CO}_2/\text{CH}_4$  ratios, the carbon balance kept at approximately 95% while the ratio of  $\text{H}_2/\text{CO}$  increased significantly with the increasing  $\text{CH}_4/\text{CO}_2$  ratio (Fig. 9d). This result further



**Fig. 11** Stability of  $g\text{-C}_3\text{N}_4$  catalyst with the increase of reaction time: **a** conversion, **b** yield and **c** selectivity

confirms that increasing  $\text{CH}_4/\text{CO}_2$  ratio leads to less oxygen, favoring for the production of hydrocarbon accompanying by carbon deposition.

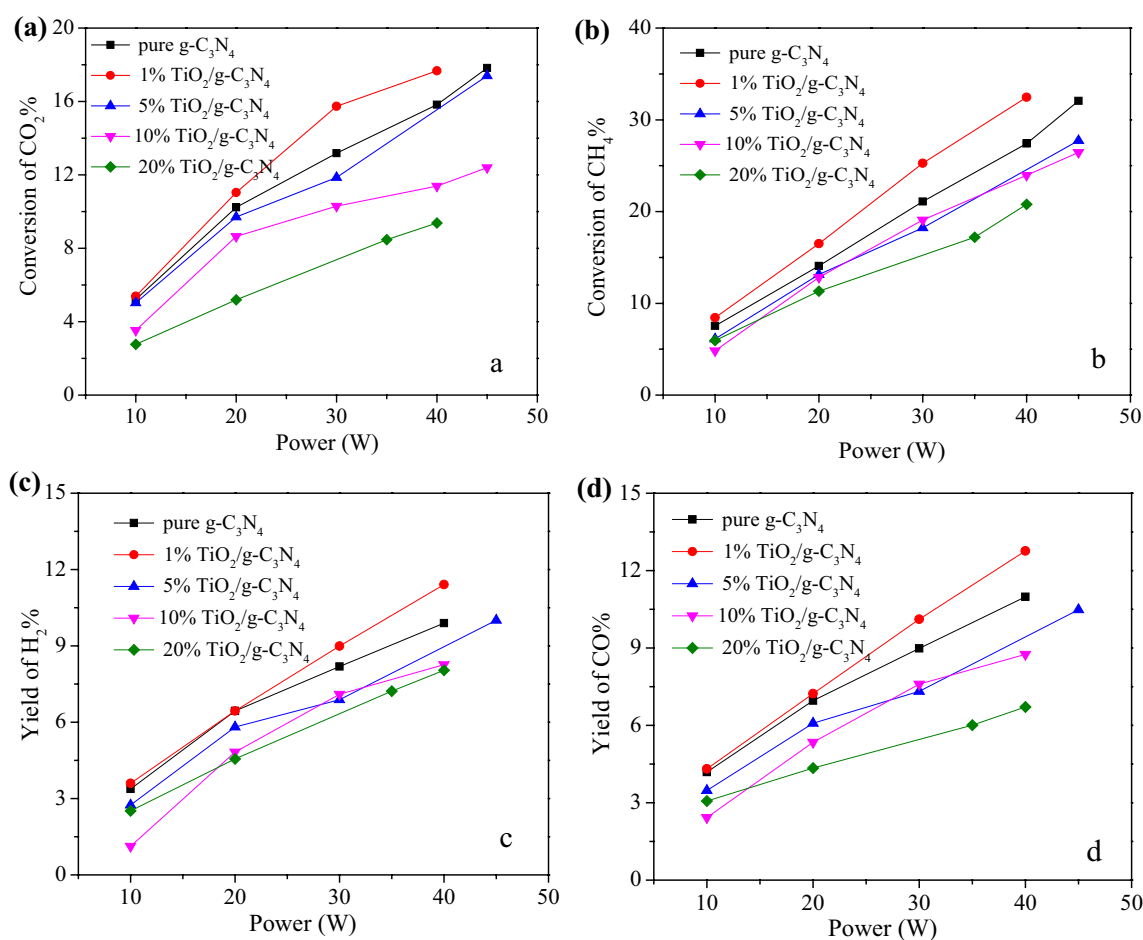
### 3.5 Plasma-Catalyst Association

Combination of non-thermal plasma with catalysts has been widely investigated in dry reforming reactions aiming at improving the conversion and selectivity. For non-thermal plasma, most of the electrical energies provided by the input power are consumed for energetic electrons production, which play key role in plasma-alone assisted dry reforming by way of reacting with reactants molecules to generate excited species. With the presence of catalyst bulks in the discharge gap, surface discharge may occur on the surface of the catalyst and the catalyst can trap energetic electrons in the active particles. Accordingly, effect of catalyst on the discharge process other than catalytic activity should be under consideration to clarify the plasma-catalyst association for dry reforming reaction.

In the present work, samples of  $g\text{-C}_3\text{N}_4$  and  $\gamma\text{-Al}_2\text{O}_3$  with the same particle size are placed in the discharge zone, respectively. The  $\gamma\text{-Al}_2\text{O}_3$  has no catalytic activity and here helps to explore how the drying reforming reaction is influenced by the sample packing that might cause the discharge process change. Effect of input power on the conversions of reactants and the yields of  $\text{CO}$  and  $\text{H}_2$  over the catalyst samples placed at the DBD reactor is shown in Fig. 10. As  $\gamma\text{-Al}_2\text{O}_3$  was packed in the discharge zone, the conversion of  $\text{CH}_4$  as well as yield of  $\text{H}_2$  increased to some extent, while the conversion of  $\text{CO}_2$  changed slightly and the increase in yield of  $\text{CO}$  was lower than that of  $\text{H}_2$ . The results exhibit the fact that the change of discharge mode causing by  $\gamma\text{-Al}_2\text{O}_3$  packing would affect the dry reforming reaction. After  $\gamma\text{-Al}_2\text{O}_3$  packing, the discharge mode transfers from filament discharge to the combination of filament discharge and surface discharge. Polarization field is formed on the surface of  $\gamma\text{-Al}_2\text{O}_3$  particles, making the electric field intensity in local area strengthen. The reason of the enhancements of the conversion of  $\text{CH}_4$  and yield of  $\text{H}_2$  is due to lower dissociation energy of  $\text{CH}_4$  than that of  $\text{CO}_2$ . The followings are the main reactions happened in the discharge zone.



In case of  $g\text{-C}_3\text{N}_4$ , the conversions of  $\text{CH}_4$  and  $\text{CO}_2$  increased and the yields of  $\text{H}_2$  and  $\text{CO}$  were all higher than those obtained in plasma-alone system. As a novel



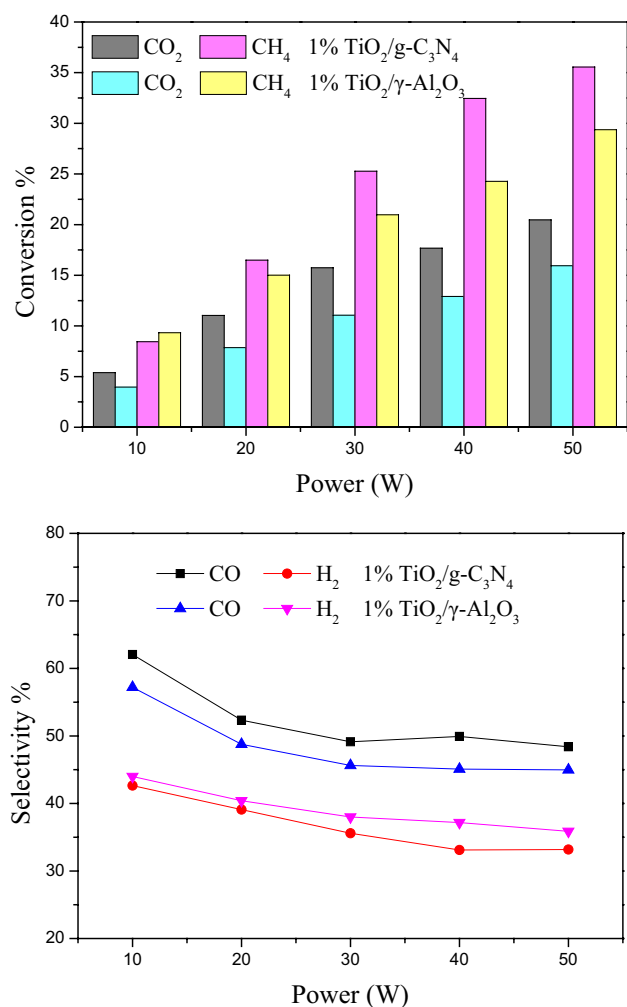
**Fig. 12** Effect of  $\text{TiO}_2/\text{g-C}_3\text{N}_4$  composite packing in discharge area with different  $\text{TiO}_2$  mass ratios on the performance of dry reforming reaction: **a, b** conversions of reactants; **c, d** yield of products. ( $\text{CH}_4/\text{CO}_2=1:1$ , feed flow rate 50 mL/min)

metal-free catalyst, it can be excited by DBD plasma because its narrow band gap (2.7 eV), and moreover, the generated electrons have a strong reducing ability because of extremely negative position ( $-1.35$  vs. NHE) of the  $\text{g-C}_3\text{N}_4$  conduction band, which is expected to favor the conversion of  $\text{CO}_2$  in the dry reforming reaction. Furthermore, the results are also higher than those using  $\gamma\text{-Al}_2\text{O}_3$  particles in plasma zone. The cooperation effect of DBD plasma with  $\text{g-C}_3\text{N}_4$  catalyst is verified. Compared with plasma-alone, stronger externally applied electric field as well as stronger micro- and surface discharges are formed as packing  $\text{g-C}_3\text{N}_4$  catalyst into DBD plasma zone. More excited species are adsorbed on the surface of the catalyst and favors the conversion of the reactants comparing, achieving desired products [34].

The stability of  $\text{g-C}_3\text{N}_4$  prepared in this study was tested under the conditions of discharge power 30 W, flow rate of feed gas 50 mL/min and molar ratio of  $\text{CH}_4/\text{CO}_2$  1:1. The product was detected every 15 min by the on-line detection and the results was shown in Fig. 11. After 120 min

treatment, the as-prepared catalyst performed a favorable stability in the conversion of  $\text{CH}_4$  and  $\text{CO}_2$ . The yield and selectivity of main products of  $\text{H}_2$  and  $\text{CO}$  slightly decrease after 45 min reaction which may be attributed to the carbon formation during the collision of high energy electrons and  $\text{CH}_4$ .

Pure  $\text{g-C}_3\text{N}_4$  usually suffers from small surface area and short lifetimes of generated electrons and holes. Approach of constructing heterogeneous structure by coupling  $\text{g-C}_3\text{N}_4$  and  $\text{TiO}_2$  materials is a promising strategy to improve the charge separation efficiency. Accordingly,  $\text{TiO}_2/\text{g-C}_3\text{N}_4$  catalysts with different  $\text{TiO}_2$  mass ratio were prepared in the present work and the catalytic activity towards dry reforming reaction is explored. As shown in Fig. 12, the  $\text{TiO}_2$  mass ratio exhibited significant effect on dry reforming reactions. Only  $\text{TiO}_2/\text{g-C}_3\text{N}_4$  with 1%  $\text{TiO}_2$  mass ratio presented a hybrid effect as packing the catalyst bulks to the discharge zone. The efficient separation of electrons and holes occurred when mixing  $\text{TiO}_2$  (1%) with  $\text{g-C}_3\text{N}_4$ . However, further increasing mass ratio of  $\text{TiO}_2$  restrained



**Fig. 13** Conversions of CH<sub>4</sub> and CO<sub>2</sub>, and selectivities of CO and H<sub>2</sub> as the DBD reactor packing with 1% TiO<sub>2</sub>/g-C<sub>3</sub>N<sub>4</sub> and 1% TiO<sub>2</sub>/γ-Al<sub>2</sub>O<sub>3</sub> catalysts, respectively

the conversions of feed gases and also the yields of CO and H<sub>2</sub>. The reasons can be explained by the higher dispersion of TiO<sub>2</sub> on the surface of g-C<sub>3</sub>N<sub>4</sub> with further increasing the mass ratio of TiO<sub>2</sub>, which could adsorb more high energy electrons and thus reduce the reaction probability between high energy electrons and g-C<sub>3</sub>N<sub>4</sub>. In the present work, the electron energy might not be higher enough to excite TiO<sub>2</sub>, whose band gap is 3.1 eV, and thus excitation of g-C<sub>3</sub>N<sub>4</sub> is expected to play significant role in the plasma-assisted catalytic reaction and 1% of TiO<sub>2</sub> is believed to contribute to improve separation of electrons and holes generated on g-C<sub>3</sub>N<sub>4</sub>. Control experiment was further carried out with 1% TiO<sub>2</sub>/γ-Al<sub>2</sub>O<sub>3</sub>, which prepared in same synthesis procedure of 1% TiO<sub>2</sub>/g-C<sub>3</sub>N<sub>4</sub>, and the results are shown in Fig. 13. As the discharge area packing with 1% TiO<sub>2</sub>/g-C<sub>3</sub>N<sub>4</sub> and 1% TiO<sub>2</sub>/γ-Al<sub>2</sub>O<sub>3</sub> catalysts, respectively, with the increasing of discharge power, conversions of CO<sub>2</sub> and CH<sub>4</sub> increase while the selectivities of main products

decrease, which is in accordance with aforementioned result. Comparing the catalytic activity of TiO<sub>2</sub>/g-C<sub>3</sub>N<sub>4</sub> with TiO<sub>2</sub>/γ-Al<sub>2</sub>O<sub>3</sub> combining with DBD plasma, TiO<sub>2</sub>/g-C<sub>3</sub>N<sub>4</sub> exhibits better performance in both CO<sub>2</sub> and CH<sub>4</sub> conversion and the selectivity of CO, while the selectivity of H<sub>2</sub> is slightly lower than that using TiO<sub>2</sub>/γ-Al<sub>2</sub>O<sub>3</sub> catalyst. The experimental result further proves the good catalytic activity of TiO<sub>2</sub>/g-C<sub>3</sub>N<sub>4</sub> composite in conversion of CO<sub>2</sub> and CH<sub>4</sub> and enhancing CO selectivity. However, the detailed mechanism of DBD plasma- g-C<sub>3</sub>N<sub>4</sub>-based catalysis has not been fully understood yet. The appropriate optimization of the DBD plasma-assisted g-C<sub>3</sub>N<sub>4</sub>-based catalytic system is needed to be further studied.

## 4 Conclusion

Dry reforming of methane and carbon dioxide under pure plasma and synthetic action of plasma-assisted g-C<sub>3</sub>N<sub>4</sub>-based catalysis was investigated in DBD reactor. In pure plasma process, input power, total flow rate of feed gas and CH<sub>4</sub>/CO<sub>2</sub> ratio affected the reaction. High input power and low total flow rate favored for increasing the conversions of reactants. The selectivities of CO and H<sub>2</sub> decreased with the input power, indicating the coke formation at higher energy level, and only the ratio of CH<sub>4</sub>/CO<sub>2</sub> had a significant influence on the products ratio of H<sub>2</sub>/CO. Combining DBD plasma with g-C<sub>3</sub>N<sub>4</sub> catalyst, the conversions of CH<sub>4</sub> and CO<sub>2</sub> increased and the yields of H<sub>2</sub> and CO were all higher than those obtained in plasma-alone system, which was attributed to the synergistic effect of plasma and g-C<sub>3</sub>N<sub>4</sub> catalyst. In the DBD plasma assisted with 1% TiO<sub>2</sub>/g-C<sub>3</sub>N<sub>4</sub> composite system, the maximum conversion rate of reactants and yield of product were obtained. With further increasing the mass ratio of TiO<sub>2</sub>, more high energy electrons could be adsorbed and thus reduced the reaction probability between high energy electrons and catalyst. The present study makes it clear that a synergy between g-C<sub>3</sub>N<sub>4</sub>-based catalyst and DBD plasma is achieved.

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