EFFECT OF MAGNESIUM OXIDE ON THE CATALYTIC PROPERTIES OF ZnO-CuO-MgO/Al₂O₃/CORDIERITE IN STEAM AND STEAM-OXYGEN REFORMING OF METHANOL

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Magnesium oxide in a ZnO-CuO-MgO/Al₂O₃/cordierite catalyst contributes to an enhanced yield of hydrogen in steam and steam-oxygen reforming of methanol and to a decreased yield of carbon monoxide in a broad temperature range (230-550 °C). Promotion by magnesium oxide and excess water in the reaction mixture (CH₃OH/H₂O from 1/5 to 1/10) levels out the sharp decrease in the hydrogen yield at 320-400 °C as a result of a decrease in the reducibility of cupric oxide, which is an active catalyst component.

Key words: methanol, steam and steam-oxygen reforming, hydrogen, ZnO-MgO-CuO/Al₂O₃/cordierite catalysts, promoting effect of MgO.

The ever increasing interest in methanol as a source of hydrogen fuel [1] has led to a search for efficient catalysts for methanol reforming, which, depending on the practical application, is carried out by decomposition (Eq. (1)), steam conversion (Eq. (2)), partial oxidation (Eq. (3)), as well as a combination of steam conversion and partial methanol oxidation known as steam-oxygen or combined reforming under conditions close to an autothermal mode (Eq. 4)):

$$CH_{3}OH \to CO + 2H_{2}, \qquad (1)$$

$$\Delta H^{0} = +91 \text{ kJ/mol}, \qquad (2)$$

$$CH_{3}OH + H_{2}O \to CO_{2} + 3H_{2}, \qquad (2)$$

$$\Delta H^{0} = +49 \text{ kJ/mol}, \qquad (3)$$

$$CH_{3}OH + 0.5O_{2} \to CO_{2} + 2H_{2}, \qquad (3)$$

$$\Delta H^{0} = -192 \text{ kJ/mol}, \qquad (4)$$

$$\Delta H^{573 \text{ K}} = 0.$$

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Fig. 1. Physicochemical characteristics of the catalyst samples: a) diffraction patterns ZnO-CuO-MgO/Al₂O₃ sample, b) TPHR profiles of the ZnO-CuO/Al₂O₃/cordierite (1) and ZnO-CuO-MgO/Al₂O₃/cordierite samples (2).

The decomposition of methanol holds interest in a number of uses of hydrogen fuel including high-temperature solid oxide fuel cells [2]. Oxidative reforming is carried out for low-temperature fuel cells with polymer-electrolyte proton exchange membranes since the carbon monoxide formed in the decomposition of methanol in addition to hydrogen deactivates the platinum electrodes of this type of fuel cell [3].

Among the variety of catalytic compositions used for reforming, Cu-ZnO-containing systems with various additives, which are employed in the industrial manufacture of methanol, have attracted considerable attention [3-6]. In previous work [7, 8], we studied the generation of hydrogen in the decomposition and partial oxidation of methanol in the presence of Cu-ZnO- M_xO_y/Al_2O_3 catalysts (M = Ce, La, Ni) supported on honeycomb cordierite structures and elucidated the effect of the components of such compositions on their catalytic properties.

In the present work, we studied the steam and combined steam-oxygen reforming of methanol in order to clarify the role of magnesium oxide as a dopant in ZnO-CuO-MgO/Al₂O₃/cordierite catalysts during these processes, especially the hydrogen yield and selectivity of CO formation.

Synthetic honeycomb cordierite elements were used as the catalyst supports $(2MgO\cdot 2Al_2O_3\cdot 5SiO_2, S_{sp} = 0.4 \text{ m}^2/\text{g})$ with an alumina coating $(Al_2O_3/\text{cordierite}, S_{sp} = 6.0 \text{ m}^2/\text{g})$. The deposition procedure was described in our previous work [9]. The active components were deposited from aqueous solutions of $ZnSO_4\cdot 7H_2O$, $Cu(NO_3)_2\cdot 3H_2O$, and $Mg(NO_3)_2\cdot 6H_2O$ with subsequent drying and roasting $(ZnSO_4\cdot 7H_2O \text{ at } 800 \text{ °C}, Mg(NO_3)_2\cdot 6H_2O \text{ at } 400 \text{ °C}, and Cu(NO_3)_2\cdot 3H_2O \text{ at } 350 \text{ °C})$. We used catalyst samples containing (mass %): 9% ZnO-7% CuO-0.5% MgO/Al_2O_3/cordierite and 6% ZnO-8% CuO/Al_2O_3/cordierite.

The X-ray diffraction was carried out using a Bruker AXS D8 Advance diffractometer. The phase composition was determined using the PDF-2 2006 data base.

Indexed phases	Unit cell parameters	Coherent scattering region, nm	
Al ₂ O ₃ , X-ray-amorphous	_	_	
$ZnAl_2O_4$, cubic	a = 8.05 Å	26	
MgO, cubic	a = 4.211 Å	38	
CuO, monoclinic	<i>a</i> = 4.662 Å, <i>b</i> = 3.416 Å, <i>c</i> = 5.118 Å,	32	
	$\beta = 99.48^\circ$, $\alpha = \gamma = 90.00^\circ$		

TABLE 1. Structural and Dimensional Characteristics of the ZnO-CuO-MgO/Al₂O₃ Sample

The temperature-programmed hydrogen reduction (TPHR) of the catalyst samples was carried out in an argon stream containing 10 vol.% hydrogen at 20-800 °C at a heating rate of 17 °C/min.

The reactions of the steam and steam-oxygen conversion of methanol were studied in a flow reactor at atmospheric pressure with gas chromatographic monitoring. The CH₃OH-H₂O(O₂)-Ar gas stream (30 cm³/min, 1250 h⁻¹) was passed through a Pyrex glass reactor with a honeycomb element as the catalyst (~1 g). The methanol–water mixture was introduced using an MS-CA 4/820 peristaltic pump and injector at 150-180 °C. The following CH₃OH/H₂O/O₂ working mixtures were used (vol.%): 4.5/45/0, 14.5/29/0, 20/20/0, 8/40/2, 14.5/29/2.2, and 26/19.5/2.2.

The reforming processes were characterized by the following indices: methanol conversion (%), hydrogen yield (moles H_2 /mole CH_3OH_{in} , in = initial), and selectivity of the formation of the carbon monoxide by-product (%). In some cases, the selectivity of methane formation was also determined.

$$\begin{split} X_{\rm CH_3OH} &= n (C_{\rm CO_2} + C_{\rm CO} + C_{\rm CH_4}) \cdot 100 / / C_{\rm CH_3OH}^{\rm in}, \\ Y_{\rm H_2} &= n C_{\rm H_2} / C_{\rm CH_3OH}^{\rm in}, \\ S_{\rm CO} &= C_{\rm CO} / (C_{\rm CO} + C_{\rm CO_2} + C_{\rm CH_4}), \\ S_{\rm CH_4} &= C_{\rm CH_4} / (C_{\rm CO} + C_{\rm CO_2} + C_{\rm CH_4}) \end{split}$$

where $C_{CH_3OH}^{in}$ is the initial methanol concentration (vol.%), C_{H_2} , C_{CO} , C_{CO_2} , and C_{CH_4} are the concentrations of the reforming products at the reactor outlet at temperature *T*, °C, and *n* is the coefficient for taking account of the increase in volume during these processes depending on the reagent concentration.

Figure 1a shows the diffraction pattern used to determine the structural and dimensional characteristics of the ZnO-CuO-MgO/Al₂O₃ composition listed in Table 1. The XRD data indicate that cupric oxide and magnesium oxide exist in the catalyst as monoclinic and cubic modifications, respectively, with mean particle diameter 32 nm (CuO) and 38 nm (MgO). The zinc-containing phase was identified as the cubic aluminate $ZnAl_2O_4$ (gahnite) with mean particle diameter 26 nm. Aluminum oxide was X-ray-amorphous.

The indices for the steam conversion and combined reforming of methanol in the presence of the $ZnO-CuO-MgO/Al_2O_3/cordierite$ catalyst are given in Fig. 2 and summarized in Table 2 in comparison with the indices for $ZnO-CuO/Al_2O_3/cordierite$.

These results indicate that in the case of a multifold water excess in the reaction mixture (CH₃OH/H₂O = 1/10) favorable for preventing caking of the active phase particles and carbonization [10], a gradual increase in the hydrogen yield is observed in the steam conversion of methanol with increasing temperature up to 275 °C (Fig. 2a, curve 1). A further increase in temperature has hardly any effect on Y_{H_2} . On the other hand, under conditions of a stoichiometric reagent ratio



Fig. 2. Temperature dependence curves for the hydrogen yield in the reforming of methanol on the 9% ZnO-7% CuO-0.5% MgO/Al₂O₃/cordierite catalyst: a, b) steam conversion before (a) and after reduction (b) of the catalyst sample *in situ* in an argon stream with 8 vol.% H₂ at 400 °C and CH₃OH/H₂O ratio 1/10 (1), 1/1 (2), and 1/2 (3); c) combined reforming for CH₃OH/H₂O/O₂ 1/5/0.25 (1), 1/2/0.15 (2), and 1/0.75/0.08 (3) ($V_{CH_3OH-H_2O-(O_2)-Ar} = 1250 h^{-1}$).

 $(CH_3OH/H_2O = 1/1)$, after an initial sharp increase in the hydrogen yield with increasing temperature up to 275-300 °C, we find a sharp drop in Y_{H_2} at 320 °C with a gradual increase upon a further increase in temperature (Fig. 2a, curve 2). We should note that a steady-state mode for the steam conversion of methanol at 320 °C is achieved at ~2 h after the decrease in Y_{H_2} . Such catalytic behavior might be attributed to caking of the copper-containing particles in the vicinity of ~300 °C [6]. However,

Catalyst composition, mass %	Composition of CH ₃ OH/H ₂ O/O ₂ reaction mixture, vol.%	CH ₃ OH conversion, %/ <i>T</i> , °C	Yield, moles H ₂ /mole CH ₃ OH	Selectivity relative to CO, %/T, °C
9% ZnO-7% CuO-0.5% MgO	4.5/45/0	84-98/225-415	2.5-2.9	$\rightarrow 0$
	14.5/29/0	55-92/415-550	1.6-2.7	$\rightarrow 0$
	20/20/0	11-91/320-580	0.3-2.7	$\rightarrow 0$
	8/40/2	85-97/425-550	2.1-2.4	<2
	14.5/29/2.2	4-83/330-580	0.1-2.2	2-14/300-535
	26/19.5/2.2	19-85/405-580	0.5-2.3	5-11/445-560
6% ZnO-8% CuO	4.5/45/0	64-97/350-530	1.9-2.8	3-24/310-530
	14.5/29/0	24-83/320-560	0.7-2.3	2-34/270-560
	20/20/0	24-81/375-540	0.7-2.4	3-42/225-540
	14.5/29/2.2	23-72/320-545	0.6-1.9	3-49/225-545

TABLE 2. Indices for the Steam and Steam-Oxygen Reforming of Methanol in the Presence of Oxide Catalysts on the Structurized Al₂O₃/Cordierite Support ($V_{CH_3OH-H_3O-(O_2)-Ar} = 1250 h^{-1}$)

taking account that the shape of curve 2 is reproduced during steam reforming when $CH_3OH/H_2O = 1/1$ after reoxidation of the ZnO-CuO-MgO/Al₂O₃/cordierite sample in a stream of 4 vol.% O₂ in argon at 450 °C, the sharp decrease in activity at 320 °C is logically explained by consumption of the desired hydrogen product in the reduction of cupric oxide, which is the active component of the reforming catalyst. The subsequent increase in the hydrogen yield with increasing temperature after reaching a minimum on the curve for the temperature dependence of Y_{H_2} may be caused by the catalytic activity of metallic copper.

An argument for this explanation of the temperature dependence is found in the markedly lower hydrogen yield in the presence of a previously reduced catalyst sample in the steam conversion of methanol in the temperature range up to 300 °C (Fig. 2b) than the corresponding values of $Y_{\rm H_2}$ for the unreduced catalyst (Fig. 2a, curves 2 and 3).

The less sharp decrease in the hydrogen yield for reagent ratio $CH_3OH/H_2O = 1/2$ in the range 270-415 °C (Fig. 2a, descending branch of curve 3) in comparison with the decrease found when $CH_3OH/H_2O = 1/1$ (300-330 °C) may be attributed to the decrease in the reducibility of cupric oxide in the presence of excess water. Such a tendency is most clearly seen under conditions of a multifold excess of steam in the reaction mixture, which leads to elimination of the minimum on curve 1 (Fig. 2a).

The effect of the CH_3OH/H_2O ratio on the temperature dependence of the hydrogen yield in the combined reforming of methanol (Fig. 2c) is analogous to the effect described above for the steam conversion of the substrate.

We should note that the steam conversion of methanol on ZnO-CuO-MgO/Al₂O₃/cordierite in the broad temperature range from 230 to 550 °C proceeds virtually without formation of carbon monoxide as a side-product (Table 2). The selectivity relative to CO did not exceed 2% in the combine reforming of the substrate in the case of a five-fold excess of water (CH₃OH/H₂O/O₂ = 1/5/0.25). On the other hand, with a higher CH₃OH/H₂O ratio (CH₃OH/H₂O/O₂ = 1/2/0.15), including under conditions close to the autothermal mode (CH₃OH/H₂O/O₂ = 1/0.75/0.08), the selectivity for CO formation reaches 11%-14%, which may be a consequence both of methanol decomposition and the reverse water–gas shift reaction: CO₂ + H₂ \rightarrow CO + H₂O.

Literature data indicate that magnesium oxide prevents the caking of particles of the active phase of CuO-ZnO catalysts [11]. We should note that the surface of the ZnO-CuO/Al₂O₃/cordierite sample after maintenance in a methanol–argon stream at ~500 °C is a continuous conglomerate of particles without visible boundaries due to caking [7].

In addition to stabilization of the highly dispersed state of the active phase, MgO decreases the reducibility of cupric oxide, possibly, due to formation of a mixed oxide system MgCu₂O₃ [12]. This hypothesis is supported by the thermal-programmed reduction results: the temperature range and temperature for the maximum of hydrogen absorption by the surface of the ZnO-CuO-MgO/Al₂O₃/cordierite sample (350-550 °C, $T_m = 425$ °C) significantly exceed the corresponding values for ZnO-CuO/Al₂O₃/cordierite (220-365 °C, $T_m = 305$ °C) (Fig. 1b). These differences in reducibility are apparently manifest in the less sharp decrease in the activity of the catalysts modified with magnesium oxide in the steam conversion of methanol for reagent ratio CH₃OH/H₂O = 1/2 (2.5-1.6 moles H₂/mole CH₃OH/270-415 °C) in comparison with the decrease found for the binary ZnO-CuO sample (2.2-0.7 moles H₂/mole CH₃OH/270-320 °C). Higher temperatures for the decrease in the activity of ZnO-CuO-MgO/Al₂O₃/cordierite are observed both in steam and combined reforming than found for ZnO-CuO/Al₂O₃/cordierite. In contrast to the case of the ZnO-CuO-MgO/Al₂O₃/cordierite are soft to the reaction mixture. Furthermore, the values of Y_{H_2} in the presence of ZnO-CuO/Al₂O₃/cordierite are somewhat lower than for the MgO-modified catalyst with a sharp increase in the selectivity relative to CO formation ($S_{CO} \rightarrow 50\%$), which may be attributed to predominance of methanol decomposition. The presence of methanol terorming of methanol decomposition. The presence of methanol terorming of the soft steam and combined reforming of methanol terorming of methanol decomposition. The presence of methanol terormation ($S_{CH_4} \approx 1\%$ -4%, 350-550 °C) is apparently due to a

side-reaction methanation: $\text{CO} + 3\text{H}_2 \rightarrow \text{CH}_4 + \text{H}_2\text{O}$.

Thus, the ZnO-CuO/Al₂O₃/cordierite catalyst modified with magnesium oxide gives a higher hydrogen yield in the steam and steam-oxygen conversion of methanol along with decreased selectivity relative to carbon monoxide formation as a side-product in the broad temperature range from 230 to 550 °C. Extrema are noted on the temperature dependence curve for $Y_{\rm H_2}$ (a minimum at 320-400 °C). Promotion by magnesium oxide and an excess of water in the reaction mixture (CH₃OH/H₂O = from 1/5 to 1/10) level out the sharp decrease in the hydrogen yield. This effect is attributed to a decrease in the reducibility of cupric oxide, which is the active component of the catalyst.

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