



# The effect of molybdenum on the characteristics and catalytic properties of $M/Cs_{1.5}H_{1.5}PW_{12}O_{40}/Al_2O_3$ ( $M = Ni$ or/and $Mo$ ) nanocatalysts in the hydrocracking of *n*-decane

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## Abstract

In this research,  $M/Cs_{1.5}H_{1.5}PW_{12}O_{40}/Al_2O_3$  ( $M = Ni$  or/and  $Mo$ ) nanocatalysts were prepared via 2 steps with the impregnation method and the effect of molybdenum on the characteristic and catalytic properties of the prepared samples was studied. The synthesized samples were characterized by X-ray diffraction (XRD), temperature programmed reduction, temperature programmed desorption (TPD), and energy dispersive X-ray spectroscopy techniques. Morphology of the samples was studied by field emission scanning electron microscope (FESEM) and surface area, pore volume and pore size of the compounds were measured by BET method. In the XRD patterns of the prepared catalysts, the  $H_3PW_{12}O_{40}$  phase was observed. The FESEM images showed that the synthesized particles were in nanoscale. The results of TPD studies indicated that the total acid site of  $Ni-Mo/Cs_{1.5}H_{1.5}PW_{12}O_{40}/Al_2O_3$  catalyst was more than the others. The catalytic activity of the nanocatalysts in hydrocracking of *n*-decane indicated that  $Ni-Mo/Cs_{1.5}H_{1.5}PW_{12}O_{40}/Al_2O_3$  nanocatalyst had the highest catalytic activity.

**Keywords** Heteropoly acid · Molybdenum · Nanocatalyst · Hydrocracking · Nickel · Alumina

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## Introduction

The most popular heteropoly acids are those having the Keggin structure,  $\text{H}_3\text{PW}_{12}\text{O}_{40}$  (HPW). The main disadvantages of HPWs are high solubility in water and their very low surface area (less than  $10 \text{ m}^2 \text{ g}^{-1}$ ), which hinders accessibility to the acidic sites. In addition, the HPW has excessive acidity and an overhigh cracking activity, which increases the probability to undergo secondary reactions [1–4]. By substituting a fraction of the proton with monovalent ions such as  $\text{Cs}^+$ ,  $\text{K}^+$ ,  $\text{Rb}^+$  and  $\text{Ag}^+$ , the heteropoly acids are turned into insoluble salts, which can be used as a reasonably good heterogeneous solid acid catalyst. The Cs-exchanged Keggin-type heteropoly acid is also well maintained at high temperatures, usually over  $500 \text{ }^\circ\text{C}$  [5–9]. There are many studies about the effect of Cs content in HPW on the catalytic performance of these catalysts in various catalytic processes [8, 10].  $\text{H}_3\text{PW}_{12}\text{O}_{40}$  and  $\text{Cs}_x\text{H}_{3-x}\text{PW}_{12}\text{O}_{40}$  compounds have been used as catalysts in hydrocracking of extra-heavy oils and reported the optimum Cs content ( $x = 2.2$ ) which induces the best activity in this process [5]. For overcoming the low surface area of HPW, a feasible way is to prepare supported HPW catalysts. One approach to obtain supported HPW catalysts is the impregnation of a support with a heteropoly acid solution followed by evaporation of the solvent. Several supports, such as silica–alumina [11], silica gel [12], silica [13] and BEA zeolite [14] have been used to enhance the dispersion of the HPW. In this case, the accessibility to HPW acid sites has been increased, while its solubility in polar media decreased [15]. Extensive studies have been carried out over Cs salt of HPA supported on metal oxides for the hydrocracking reaction [4, 12, 16]. The effect of Cs content on the catalytic performance of the reduced  $\text{Ni-Cs}_x\text{H}_{3-x}\text{PW}_{12}\text{O}_{40}/\text{Al}_2\text{O}_3$  catalysts for hydrocracking of *n*-decane in the presence of thiophene and pyridine has been reported. The highest catalytic activity for these catalysts belongs to  $\text{Ni-CsH}_2\text{P}_{12}\text{W}_{40}/\text{Al}_2\text{O}_3$  catalyst [16]. In another work, the behavior of non-sulfided bimetallic  $\text{Ni-Co-H}_3\text{PW}_{12}\text{O}_{40}/\text{SiO}_2$  catalysts has been reported. The results indicated the promotional effects of Co to hydrocracking activity of these catalysts [17]. Generally, hydrocracking supported catalysts are bifunctional, i.e. the acid sites which provide the cracking function and metal sites with a hydrogenation–dehydrogenation function [18]. Hence, active hydrocracking catalysts are composed of acidic supports such as  $\text{SiO}_2$ ,  $\text{Al}_2\text{O}_3$ ,  $\text{ZrO}_2$ , active carbon, modified zeolite etc., and active metals (e.g. Mo, W) with promoters (e.g. Ni, Co) [19–23].

Since molybdenum is an active phase in conventional catalysts, in this work, we have used both molybdenum and HPW for preparing new catalysts. Thus, the series of  $\text{M/Cs}_{1.5}\text{H}_{1.5}\text{PW}/\text{Al}_2\text{O}_3$  ( $\text{M} = \text{Ni}$  or/and  $\text{Mo}$ ) nanocatalysts by impregnation method have been prepared and the synthesized samples characterized with conventional techniques. The effect of molybdenum on the catalytic activity of the nanocatalysts in hydrocracking of *n*-decane has also been studied.

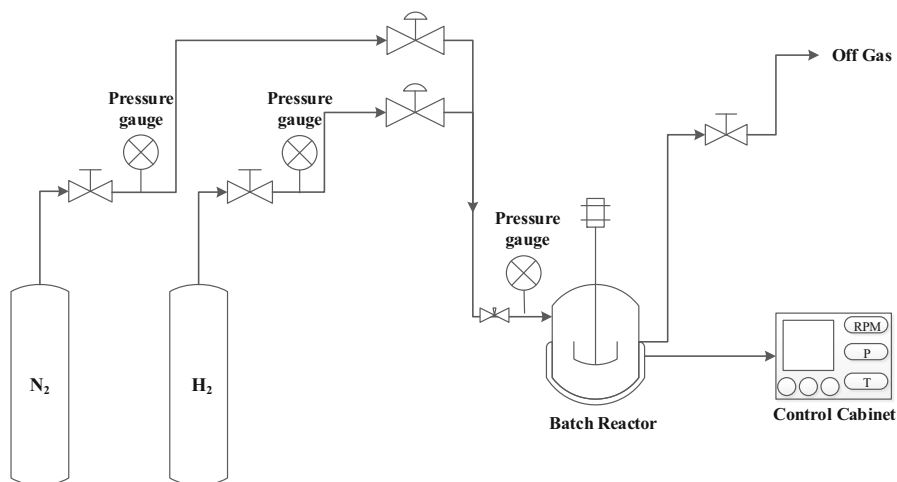
## Experimental

In this work, we have prepared the  $M/Cs_{1.5}H_{1.5}PW/Al_2O_3$  ( $M = Ni$  or/and  $Mo$ ) nanocatalysts by impregnation and characterized the synthesized samples with conventional methods. The catalytic activity of the nanocatalysts in hydrocracking of *n*-decane has also been studied.

The samples were prepared via two steps with the impregnation method. First, the alumina support (Sasol Chemical Co., specific surface area  $273\text{ m}^2\text{ g}^{-1}$ , 40–70 mesh) was impregnated with a solution containing the desired quantities of  $Ni(NO_3)_2$  (BDH, 98%),  $(NH_4)_6Mo_7O_{24}\cdot 4H_2O$  (Merck, 99%), and  $Cs_2CO_3$  (Merck, 99.99%). Impregnated samples were dried overnight at  $120\text{ }^\circ\text{C}$  and then calcined at  $400\text{ }^\circ\text{C}$  for 3 h using a heating ramp of  $2\text{ }^\circ\text{C min}^{-1}$ . In the second step, the obtained samples were impregnated with a solution containing the desired quantities of  $H_3PW_{12}O_{40}$  (Merck, 99%). The obtained products were finally dried overnight at  $120\text{ }^\circ\text{C}$  without calcination.

Powder X-ray diffraction (XRD) patterns were obtained on X' Pert Pro diffractometer equipment with a copper anode ( $Cu\ K_\alpha$  monochromatized radiation source,  $\lambda = 1.54056\text{ \AA}$ ). The surface area (BET), pore volume and pore size of the catalysts were measured using  $N_2$  at  $-196\text{ }^\circ\text{C}$  on an adsorption instrument (Quantasorb, Quantachrome). The morphologies and quantitative analysis of the samples were determined by field emission scanning electron microscopy (FE-SEM) on TESCAN Mira3-XMU microscope equipped with energy dispersive X-ray spectroscopy (EDX). Temperature programmed desorption (TPD) and temperature programmed reduction (TPR) studies were performed using a semiautomatic microthermics TPD/TPR 2900 apparatus to investigate the acid properties and reduction behavior of the catalysts, respectively.

The catalytic performance of the prepared catalyst was evaluated in a 300 ml batch type stainless steel autoclave reactor (452 HC reactor, Parr instrument). Schematic diagram of the experimental setup for hydrocracking of *n*-decane is shown in Fig. 1. The reaction test was carried out as follows: 20 g of *n*-decane (Merck, 99%) was charged into a reactor and 2 g of catalyst was added to the reactor. After the leak test of the reactor and purging with hydrogen (99.999%) for three times to remove air from the reactor, all the catalysts were reduced by a flow of  $H_2$  at  $200\text{ }^\circ\text{C}$  for 1 h during stirring at 300 rpm. Then the reactor was pressurized to 3 MPa with hydrogen and the reactor was heated to achieve the reaction temperature ( $300\text{ }^\circ\text{C}$ ), which took 4 h. The pressure and temperature were recorded continuously during the reaction using a data logging instrument (4842 reactor controller, Parr instrument). When reaction time elapsed, the reactor was rapidly quenched to the ambient temperature. The reactants and products were analyzed by a gas chromatograph (VARIAN model CP-3800) equipped with capillary column (100 m) and FID detector. For comparison, an industrial hydrocracking catalyst (NiMo/ASA) was applied for hydrocracking of *n*-decane under the same condition. Conversion of the hydrocracking process was calculated by Eq. 1 and selectivity of the catalyst to the desired product was obtained by Eq. 2.



**Fig. 1** Schematic diagram of the experimental setup for hydrocracking of *n*-decane in 300 ml batch type stainless steel autoclave reactor

$$\text{Conversion \%} = \frac{\sum X_i}{n_{\text{Feed}}} \times 100 \quad (1)$$

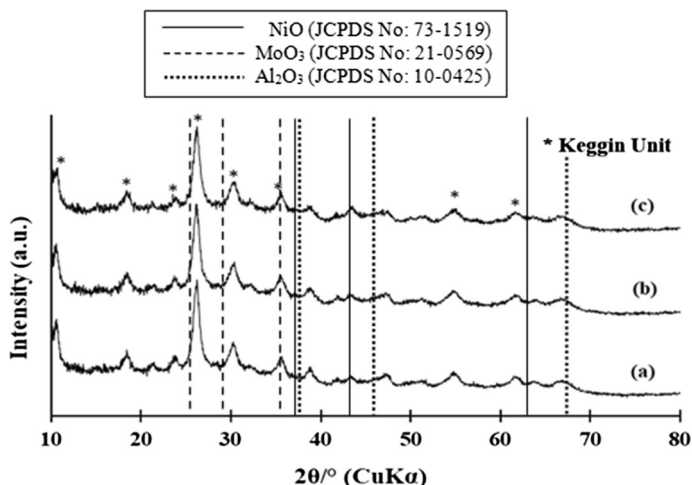
$$P_i \text{ Selectivity \%} = \frac{X_i}{\sum X_i} \times 100 \quad (2)$$

here  $P_i$  is a desired product and  $X_i$  is mole number of  $P_i$  and  $n_{\text{Feed}}$  is mole number of the feed.

## Results and discussion

The XRD patterns of the  $M/\text{Cs}_{1.5}\text{H}_{1.5}\text{PW}/\text{Al}_2\text{O}_3$  ( $M = \text{Ni}$  or/and  $\text{Mo}$ ) samples are presented in Fig. 2. The comparison of the XRD patterns of the prepared catalysts indicate that the keggin structure of  $\text{Cs}_x\text{H}_{3-x}\text{PW}$  phase ( $10.5^\circ$ ,  $18^\circ$ ,  $23.6^\circ$ ,  $25.9^\circ$ ,  $30^\circ$ ,  $35.1^\circ$ ,  $54.3^\circ$  and  $62.2^\circ$ ) (JCPDS No:50-1857) is observed in the patterns [24, 25]. It is clear that no diffraction peaks of  $\text{NiO}$  (JCPDS No:73-1519),  $\text{MoO}_3$  (JCPDS No:21-0569) and  $\text{Al}_2\text{O}_3$  (JCPDS No:10-0425) appeared in the patterns. It is elucidated that  $\text{Ni}$  and  $\text{Mo}$  were dispersed well on the support and no segregation of those took place in impregnation process. The crystallite sizes of the prepared samples, calculated by the Scherrer equation using the intense peak ( $2\theta = 26$ ), are presented in Table 1. This table shows that the size of the prepared particles are in nanoscale.

Elemental analysis, surface area, pore volume and pore diameter of the samples are given in Table 1. The elemental composition of the prepared catalysts was examined via EDX. EDX analysis at different points on the samples also confirmed



**Fig. 2** XRD patterns of  $M/Cs_{1.5}H_{1.5}PW/Al_2O_3$  ( $M = Ni$  or/and  $Mo$ ) catalysts prepared by impregnation technique: **a**  $Mo/Cs_{1.5}H_{1.5}PW/Al_2O_3$ , **b**  $Ni-Mo/Cs_{1.5}H_{1.5}PW/Al_2O_3$ , **c**  $Ni/Cs_{1.5}H_{1.5}PW/Al_2O_3$

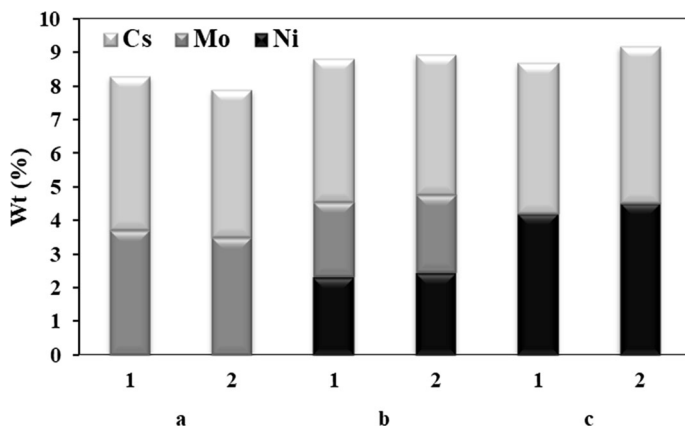
**Table 1** Elemental analysis results, crystallite size of the kegggin structure of  $Cs_xH_{3-x}PW$  phase (Calculated by Scherrer equation) and Physical properties of the catalysts

Catalyst	Element* (Wt%)					Surface area ( $m^2g^{-1}$ )	Pore volume ( $cm^3g^{-1}$ )	Pore size (nm)	Crystallite size (nm)
	Cs	Ni	Mo	P	W				
$Al_2O_3$	–	–	–	–	–	273	0.718	10.5	–
$Mo/Cs_{1.5}H_{1.5}PW/Al_2O_3$	4.6	–	3.70	0.79	37.6	126	0.271	8.6	10.23
$Ni-Mo/Cs_{1.5}H_{1.5}PW/Al_2O_3$	4.3	2.32	2.20	0.78	34.2	162	0.298	7.3	9.74
$Ni/Cs_{1.5}H_{1.5}PW/Al_2O_3$	4.5	4.20	–	0.68	35.8	156	0.305	7.9	9.98

\*Calculated by EDX method

the uniform composition of the compound (Fig. 3). Table 1 also indicates that the surface area, pore volume and pore diameter of  $Al_2O_3$  after impregnation decrease remarkably. It is reported that during impregnation the pore walls of  $Al_2O_3$  can be eroded with acidic HPW aqueous solution and also the pores partially can be blocked with  $Ni/Mo$  species which lead to reducing the surface area of  $Al_2O_3$  [12, 26, 27].

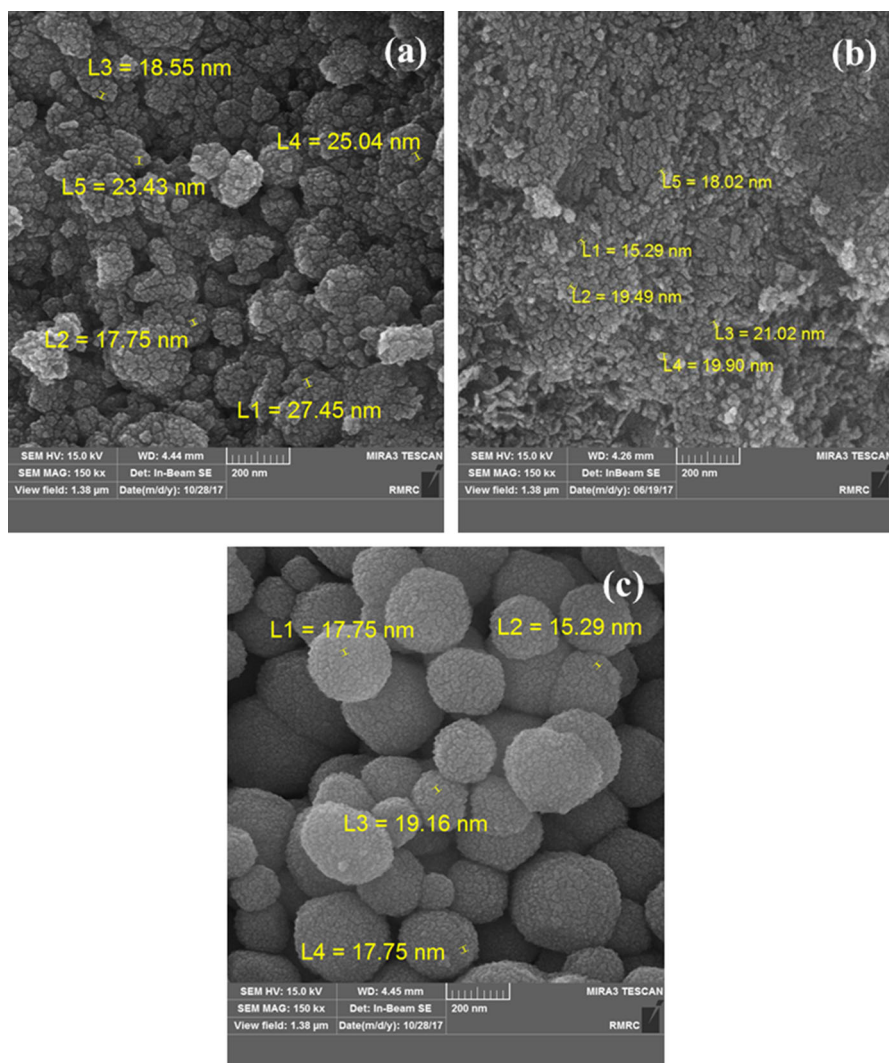
The FE-SEM images are indicated in Fig. 4. These images show that the synthesized particles are actually agglomerated and homogeneous nano-size crystallites are nearly in spherical shape.



**Fig. 3** Ni, Mo and Cs distribution observed at two points the samples by EDX for  $M/Cs_{1.5}H_{1.5}PW/Al_2O_3$  ( $M = Ni$  or/and  $Mo$ ) catalysts: **a**  $Mo/Cs_{1.5}H_{1.5}PW/Al_2O_3$ , **b**  $Ni-Mo/Cs_{1.5}H_{1.5}PW/Al_2O_3$ , **c**  $Ni/Cs_{1.5}H_{1.5}PW/Al_2O_3$

To examine the acidic properties of the  $M/Cs_{1.5}H_{1.5}PW/Al_2O_3$  ( $M = Ni$  or/and  $Mo$ ) catalysts,  $NH_3$ -TPD was carried out. According to the experimental work of Jiang and et al. the strength of acidic sites can be classified by  $NH_3$ -desorption temperature as weak ( $150$ – $350$  °C), moderate ( $350$ – $500$  °C) and strong ( $\geq 500$  °C) acidic sites [28]. The  $NH_3$ -TPD profiles of the prepared samples are shown in Fig. 5. All profiles presented an intense peak which can be assigned to weak acidic sites. In addition, these profiles indicate that moderate and strong acidic sites exist in the samples. These results show that in  $Ni-Mo/Cs_{1.5}H_{1.5}PW/Al_2O_3$  catalyst weak and moderate acidic sites are more than the other catalysts, while strong acidic site in  $Ni/Cs_{1.5}H_{1.5}PW/Al_2O_3$  catalyst is more than the other ones. These results also confirm that total acid sites of  $Ni-Mo/Cs_{1.5}H_{1.5}PW/Al_2O_3$  catalyst is more than the others (Table 2). Increasing total acid sites can be correlated to the formation of  $MoNiO_x$  phase. This result is in agreement with the literature [29]. Meng et al. reported that in  $NiMo/Beta-KIT-6$  catalysts, all  $NiMo$  based catalysts contained both weak and moderate acid sites in  $NiMo/BK$  catalysts.

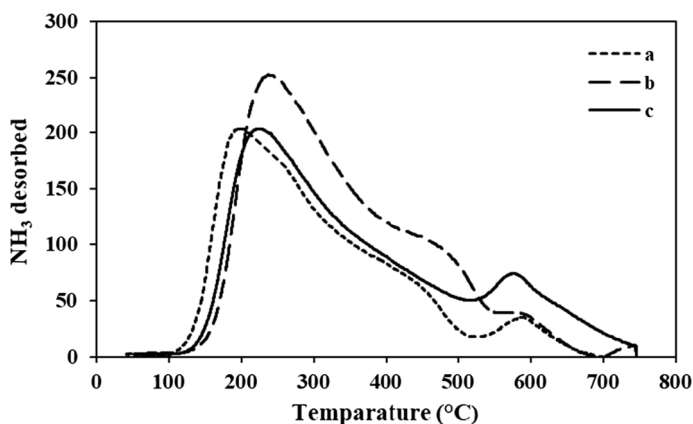
The  $H_2$ -TPR profiles of catalysts are shown in Fig. 6. It is interesting to notice that the reduction peak of  $NiO$  Bulk is not observed in these profiles. According to literature the  $NiO$  reduction peak appears at  $300$  °C [28]. Also, in the presence of  $H_3PW$  species,  $NiO$  reduction occurs at higher temperature around  $530$  °C [16]. When  $Cs$  replaces with  $H$  in  $H_3PW$  species, the interaction of  $NiO$  with these species is weaker and reduction occurs at lower temperature, so that the peaks observed at about  $420$ – $500$  °C can be attributed to the reduction of  $Ni(II)$ . The peak observed at about  $490$  °C for TPR profile of a sample could be assigned to reduction of  $Mo(VI)$  to  $Mo(IV)$  [30, 31]. This peak is also seen in Fig. 6b, which is covered by  $NiO$  reduction peak. The peaks at  $680$  °C and  $710$  °C can be attributed to different intermediate composition such as  $Al_2(MoO_4)_3$  (Fig. 6a) [32]. These peaks can also be seen in Fig. 6b containing  $Ni$  and  $Mo$ , although they are overlap with a strong peak in the  $700$  °C. This strong peak corresponds to the reduction of  $Ni(II)$  that



**Fig. 4** FE-SEM images of catalysts prepared by impregnation technique: **a** Mo/Cs<sub>1.5</sub>H<sub>1.5</sub>PW/Al<sub>2</sub>O<sub>3</sub>, **b** Ni-Mo/Cs<sub>1.5</sub>H<sub>1.5</sub>PW/Al<sub>2</sub>O<sub>3</sub>, **c** Ni/Cs<sub>1.5</sub>H<sub>1.5</sub>PW/Al<sub>2</sub>O<sub>3</sub>

interacts with the support [33]. The reduction peak near 740 °C corresponds to the reduction of Cs<sub>1.5</sub>H<sub>1.5</sub>PW species [14, 16]. It can be noticed from Table 2 that the H<sub>2</sub> consumption per gram of catalyst in Ni-Mo/Cs<sub>1.5</sub>H<sub>1.5</sub>PW/Al<sub>2</sub>O<sub>3</sub> catalyst is higher than that of for the other samples that indicate higher reducibility of catalyst. It seems that the higher amount of H<sub>2</sub> consumption for Ni-Mo/Cs<sub>1.5</sub>H<sub>1.5</sub>PW/Al<sub>2</sub>O<sub>3</sub> catalyst was related to MoNiO<sub>x</sub> phase which could be formed due to the reaction between Mo and Ni.

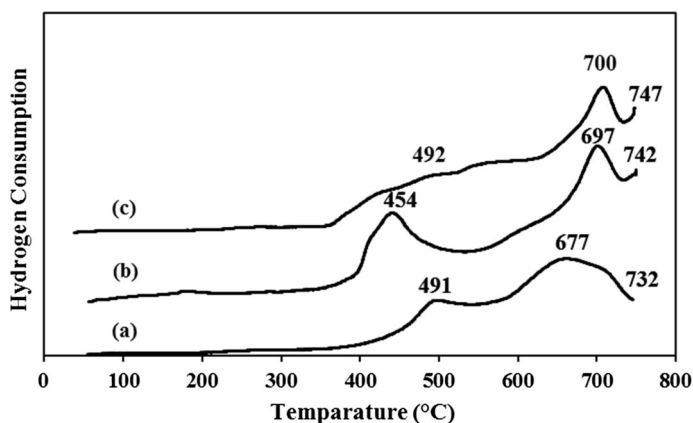
The catalytic evaluation results for the reduced M/Cs<sub>1.5</sub>H<sub>1.5</sub>PW/Al<sub>2</sub>O<sub>3</sub> (M = Ni or/and Mo) catalysts in hydrocracking of *n*-decane are shown in Figs. 7 and 8 and



**Fig. 5** NH<sub>3</sub>-TPD profiles of M/Cs<sub>1.5</sub>H<sub>1.5</sub>PW/Al<sub>2</sub>O<sub>3</sub> (M = Ni or/and Mo) catalysts: **a** Mo/Cs<sub>1.5</sub>H<sub>1.5</sub>PW/Al<sub>2</sub>O<sub>3</sub>, **b** Ni–Mo/Cs<sub>1.5</sub>H<sub>1.5</sub>PW/Al<sub>2</sub>O<sub>3</sub>, **c** Ni/Cs<sub>1.5</sub>H<sub>1.5</sub>PW/Al<sub>2</sub>O<sub>3</sub>

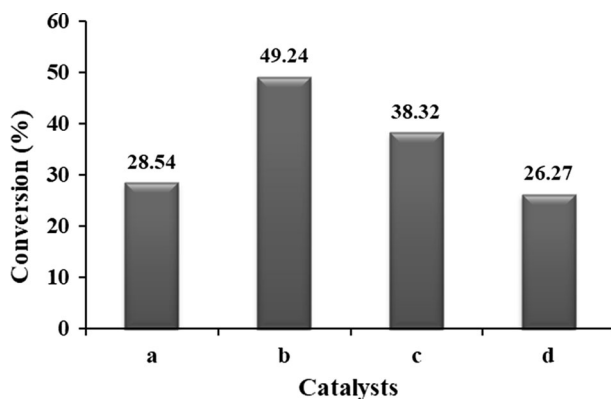
**Table 2** H<sub>2</sub> and NH<sub>3</sub> consumption (mmol/g) of the prepared nanocatalysts

Samples	H <sub>2</sub> consumption (mmol of H <sub>2</sub> /g cat)	NH <sub>3</sub> consumption (mmol of NH <sub>3</sub> /g cat) (total acidity)
Mo/Cs <sub>1.5</sub> H <sub>1.5</sub> PW/Al <sub>2</sub> O <sub>3</sub>	1.9456	0.6699
Ni–Mo/Cs <sub>1.5</sub> H <sub>1.5</sub> PW/Al <sub>2</sub> O <sub>3</sub>	3.9023	1.1295
Ni/Cs <sub>1.5</sub> H <sub>1.5</sub> PW/Al <sub>2</sub> O <sub>3</sub>	3.0890	1.0125

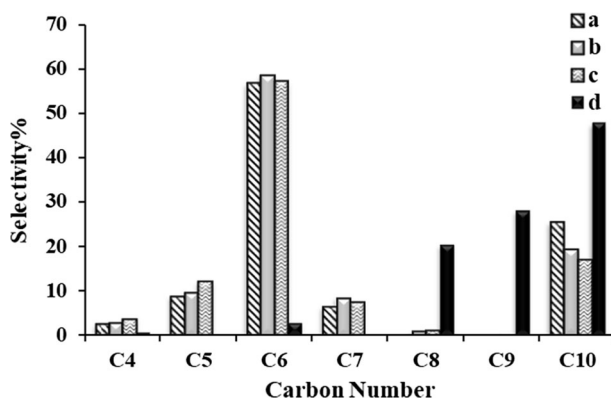


**Fig. 6** H<sub>2</sub>-TPR profiles of M/Cs<sub>1.5</sub>H<sub>1.5</sub>PW/Al<sub>2</sub>O<sub>3</sub> (M = Ni or/and Mo) catalysts: **a** Mo/Cs<sub>1.5</sub>H<sub>1.5</sub>PW/Al<sub>2</sub>O<sub>3</sub>, **b** Ni–Mo/Cs<sub>1.5</sub>H<sub>1.5</sub>PW/Al<sub>2</sub>O<sub>3</sub>, **c** Ni/Cs<sub>1.5</sub>H<sub>1.5</sub>PW/Al<sub>2</sub>O<sub>3</sub>





**Fig. 7** Conversion of  $M/Cs_{1.5}H_{1.5}PW/Al_2O_3$  ( $M = Ni$  or/and  $Mo$ ) catalysts in hydrocracking of  $n$ -decane: (Reaction conditions:  $T = 300\text{ }^\circ\text{C}$ ,  $P = 3\text{ MPa}$ ,  $t = 4\text{ h}$ ,  $20\text{ g}$  of  $n$ -decane and  $2\text{ g}$  of the catalyst): **a**  $Mo/Cs_{1.5}H_{1.5}PW/Al_2O_3$ , **b**  $Ni-Mo/Cs_{1.5}H_{1.5}PW/Al_2O_3$ , **c**  $Ni/Cs_{1.5}H_{1.5}PW/Al_2O_3$ , **d** industrial catalyst



**Fig. 8** Selectivity of  $M/Cs_{1.5}H_{1.5}PW/Al_2O_3$  ( $M = Ni$  or/and  $Mo$ ) catalysts in hydrocracking of  $n$ -decane: (Reaction conditions:  $T = 300\text{ }^\circ\text{C}$ ,  $P = 3\text{ MPa}$ ,  $t = 4\text{ h}$ ,  $20\text{ g}$  of  $n$ -decane and  $2\text{ g}$  of the catalyst): **a**  $Mo/Cs_{1.5}H_{1.5}PW/Al_2O_3$ , **b**  $Ni-Mo/Cs_{1.5}H_{1.5}PW/Al_2O_3$ , **c**  $Ni/Cs_{1.5}H_{1.5}PW/Al_2O_3$ , **d** industrial catalyst

**Table 3** Selectivity of prepared nanocatalysts in hydrocracking of  $n$ -decane

Samples	Selectivity (%)						
	C <sub>4</sub>	C <sub>5</sub>	C <sub>6</sub>	C <sub>7</sub>	C <sub>8</sub>	C <sub>9</sub>	C <sub>10</sub>
$Mo/Cs_{1.5}H_{1.5}PW/Al_2O_3$	2.6	8.8	56.7	6.4	0	0	25.5
$Ni-Mo/Cs_{1.5}H_{1.5}PW/Al_2O_3$	2.8	9.7	58.6	8.6	0.9	0	19.4
$Ni/Cs_{1.5}H_{1.5}PW/Al_2O_3$	3.8	12.2	57.3	7.6	1.2	0.5	17.4
Industrial catalyst	0.7	0	2.8	0	20.5	28.2	47.8

**Table 3.** The catalytic performance of the prepared catalysts was compared with that of a typical NiMo/ASA industrial catalyst. By addition of Ni to the Mo/Cs<sub>1.5</sub>H<sub>1.5</sub>PW/Al<sub>2</sub>O<sub>3</sub> catalyst, the conversion of *n*-decane increases. Classically, the middle acidity amount of a catalyst would favor the hydrocracking activity [14]. In the Ni–Mo/Cs<sub>1.5</sub>H<sub>1.5</sub>PW/Al<sub>2</sub>O<sub>3</sub> catalyst, weak and moderate acidic sites are more than the other catalysts and amount of total conversion of this catalyst is more than the others.

As can be observed in Fig. 7, the hydrocracking activity of Mo/Cs<sub>1.5</sub>H<sub>1.5</sub>PW/Al<sub>2</sub>O<sub>3</sub> catalyst is low. By partially and completed substitution of Ni for Mo in the Mo/Cs<sub>1.5</sub>H<sub>1.5</sub>PW/Al<sub>2</sub>O<sub>3</sub> catalyst, the order of catalysts activity is: Ni–Mo/Cs<sub>1.5</sub>H<sub>1.5</sub>PW/Al<sub>2</sub>O<sub>3</sub> > Ni/Cs<sub>1.5</sub>H<sub>1.5</sub>PW/Al<sub>2</sub>O<sub>3</sub> > Mo/Cs<sub>1.5</sub>H<sub>1.5</sub>PW/Al<sub>2</sub>O<sub>3</sub>. Meanwhile, the activities of the prepared catalysts are more than activity of industrial catalyst. Furthermore, the order of the acidity of the catalysts is coincident with the order of catalytic activity. It can be concluded that higher acidity leads to higher catalytic activity. It is evident that the activity of the Mo/Cs<sub>1.5</sub>H<sub>1.5</sub>PW/Al<sub>2</sub>O<sub>3</sub> catalyst with addition of Ni increased from 28.54% to 49.24% while, the activity of Ni/Cs<sub>1.5</sub>H<sub>1.5</sub>PW/Al<sub>2</sub>O<sub>3</sub> catalyst is lower than that of Ni–Mo/Cs<sub>1.5</sub>H<sub>1.5</sub>PW/Al<sub>2</sub>O<sub>3</sub> catalyst. This result could be due to interaction between Ni and Mo, which leads to increasing the reducibility of Ni in this catalyst. This result is also proved by TPR experiment. Similar results were reported by B. Qiu and et al. for enhancing the reducibility of Ni–H<sub>3</sub>PW/SiO<sub>2</sub> catalyst by Co, which increases the hydrocracking activity of such bimetallic catalyst [17].

The distribution of the obtained products in the presence of the prepared catalysts for hydrocracking of *n*-decane is shown in Fig. 8. For all the prepared catalysts the main products is C<sub>6</sub> hydrocarbons while the commercial catalyst leads to production of heavier hydrocarbon such as C<sub>10</sub> hydrocarbons including 3-methyl C<sub>9</sub>, 2-3-dimethyl C<sub>8</sub> and 3-3-4 trimethyl C<sub>7</sub>. For all samples the amounts of < C<sub>4</sub> hydrocarbons are negligible and selectivity of the catalysts for these compounds are not considered in Fig. 8.

The production of C<sub>10</sub> hydrocarbons in the presence of all the catalysts indicates that isomerization process is also occurred. However, this process is more notable for industrial catalyst. In addition, 94% of the C<sub>6</sub> components are branched hydrocarbons which confirm the isomerization process. Also, according to the results, it can be explained that the Ni–Mo/Cs<sub>1.5</sub>H<sub>1.5</sub>PW/Al<sub>2</sub>O<sub>3</sub> catalyst has higher selectivity to C<sub>6</sub> products than the other catalysts. Thus, it is more likely that this catalyst produce middle distillate hydrocarbons in hydrocracking process. The use of the commercial catalyst resulted in a comparatively lower C<sub>6</sub> product selectivity (2.8%) compared to that of Ni–Mo/Cs<sub>1.5</sub>H<sub>1.5</sub>PW/Al<sub>2</sub>O<sub>3</sub> catalyst (58.6%). In fact, all of the prepared catalysts were more proper than the commercial catalyst for producing the middle distillate products (see Table 3). Generally, the hydrocracking process usually carried out using a metal/acid bifunctional catalyst [14], over which the alkanes are dehydrogenated-hydrogenated on the metallic sites and hydrocracked on the acidic sites. The hydrocracking of *n*-decane on the M/Cs<sub>1.5</sub>H<sub>1.5</sub>PW/Al<sub>2</sub>O<sub>3</sub> (M = Ni or/and Mo) catalysts occurs through bifunctional mechanism as well, hydrocracking mechanism on the acidic sites and hydrogenation reaction mechanism on the metallic sites. According to the aforementioned discussion, the

high activity of Ni–Mo/Cs<sub>1.5</sub>H<sub>1.5</sub>PW/Al<sub>2</sub>O<sub>3</sub> catalyst for hydrocracking was apparently attribute to the unique structure of the HPW, which did not mere act as an acid site, but also cooperated with the hydrogenation metal site to act as hydrogen supply.

## Conclusions

M/Cs<sub>1.5</sub>H<sub>1.5</sub>PW/Al<sub>2</sub>O<sub>3</sub> (M = Ni or/and Mo) catalysts were successfully prepared by impregnation method and evaluated as catalyst for hydrocracking of *n*-decane. The obtained results indicated that using both molybdenum and nickel in these catalysts has an important role in chemical and physical properties and catalytic behavior of them in *n*-decane hydrocracking. The NH<sub>3</sub>-TPD results indicate that in Ni–Mo/Cs<sub>1.5</sub>H<sub>1.5</sub>PW/Al<sub>2</sub>O<sub>3</sub> catalyst weak and moderate acidic sites are more than the other catalysts, the catalyst shows the highest activity. The best result was obtained on the Ni–Mo/Cs<sub>1.5</sub>H<sub>1.5</sub>PW/Al<sub>2</sub>O<sub>3</sub> catalyst with the C<sub>6</sub> selectivity of 58.5% and *n*-decane conversion of 49.24%. The results show that C<sub>6</sub> and C<sub>10</sub> component are branched hydrocarbons which confirm the isomerization process is also occurred during hydrocracking process. Moreover, the interaction between the metal (Ni or/and Mo) and the Cs<sub>1.5</sub>H<sub>1.5</sub>PW of the catalyst offers the sufficient reactive hydrogen on the surface of the catalysts.

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