

ORIGINAL PAPER

Degradation of Organic Pollutants Using Atmospheric Pressure Glow Discharge Plasma

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Received: 25 September 2015/Accepted: 24 April 2016/Published online: 30 April 2016 © Springer Science+Business Media New York 2016

Abstract A method of plasma treatment in which a glow discharge was generated in the small gas gap between an electrode and a water surface was designed and employed in this study. By using this method, many active species were generated on the wastewater surface to degrade organic pollutants. The electric field distribution of the designed electrode model was simulated using the MAXWELL 3D[®] simulation software, and the discharge parameters were measured to investigate the impact of design optimization. In addition, we designed an equipotential multi-electrode configuration to treat a methyl orange solution and an azobenzene solution. The experimental and simulation results indicate that the designed electrodes can realize glow discharge with a relatively low voltage and that the generated plasma covers a large area and is in a stable state. Accordingly, the method helped reduce the cost of the reactor and improved the effectiveness of wastewater treatment.

Keywords Wastewater treatment \cdot Water surface \cdot Plasma \cdot Glow discharge \cdot Organic pollutants

Introduction

Traditional wastewater treatment methods leave residual organic pollutants that are difficult to effectively degrade in water [1-3]. However, an advanced oxidation process (AOP) can be used to effectively degrade residual organic pollutants and other pollutants [4-8]. AOPs include catalytic wet air oxidation [9-11], photochemical oxidation [12-14], and plasma oxidation, among others [15-18]. Among these methods, low-temperature plasma

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technology is a type of wastewater treatment method that applies the effects of high-energy electrons, ozone oxidation, and ultraviolet radiation. Low-temperature plasma oxidation generates strong oxidation of active species which can act at the gas–liquid interface and make the residual organic pollutants degrade. The technique primarily includes bubbles in water, droplets in gas, and a plasma jet on the liquid surface [19–24].

Existing low-temperature plasma water treatment methods generally use corona discharge; most of these techniques require the use of aeration equipment or an atomizing device, resulting in low processing efficiency, increased investment in water treatment equipment, and power loss caused by an external device [25, 26]. This study proposes a new treatment method that can generate water surface glow discharge plasma in an atmospheric pressure air environment. The discharge electrodes are placed on the liquid surface. By taking advantage of the strong field strength in the small air gap between the electrode and the water surface, glow discharges were generated and used to treat wastewater. The luminous area and plasma density of glow discharge is larger than the corona discharge. Compared to existing corona plasma treatment method, this method produces high-density glow discharge plasma, a large contact area with the fluid, a reactor with a simple structure, and high treatment efficiency. The results may lead to a new wastewater treatment method.

Results and Discussion

A structural diagram of the designed electrode model is shown in Fig. 1. In this study, a dielectric barrier discharge (DBD) in which the dielectric is composed primarily of polytetrafluoroethylene (PTFE) was used. The contact angle between the electrode on the water surface and the water surface was 115° [27]. A previous study focused on the discharge characteristics of perpendicular electrodes on the water surface [28]. The present study investigates the electric field distribution and discharge characteristics of both parallel and perpendicular electrode models on the water surface.

Electric Field Distribution

The electric field distributions of the parallel and perpendicular electrode models were simulated using the MAXWELL $3D^{\text{(B)}}$ simulation software. In the simulation, the outer diameter of the electrodes was 2 mm, the diameter of the conductor was 1.6 mm, and the horizontal spacing between the centers of the electrodes was 4 mm. The water bulk



Fig. 1 Structural diagram of the electrode laboratory model a parallel electrode model b perpendicular electrode model

conductivity during simulation is 0.01 S/m. The relative permittivity of water during simulation is 81. When a high potential (4 kV) was applied to the two electrode models as shown in Fig. 2, the maximum electric field strength of the gas gap in the models was obtained. The strong electric field area, where the electric field strength exceeded a certain value ($E \ge 3 \times 10^6$ V/m), was obtained from Fig. 2 using the Adobe Photoshop software [29, 30]. That is, the area in which the electric field strength exceeded that value was assumed to be the plasma generation area [31, 32]. The maximum electric field strength and strong electric field area shown in Table 1.

Table 1 and Fig. 2 show that the maximum electric field strength of the parallel electrode model was slightly smaller than that of the perpendicular electrode model; the reason is that the two electrodes in the parallel electrode model were arranged on the water surface and influenced each other. However, the perpendicular electrodes placed in water did not have a gas gap; therefore, the strong electric field area was considerably less than that of the parallel electrode model.

Discharge Characteristics

In this study, a sine-wave power supply with a frequency of 5–60 kHz and an output voltage of 0 to ± 10 kV was adopted. A schematic diagram of the main discharge circuit is shown in Fig. 3 [27]. A resistance R2 is connected in series in the circuit. According to the Ohm's law, the discharge current is obtained by measuring the voltage on the resistance R2. In the experiment, the voltage was increased slowly, and we assume that when the discharge current occurred, the voltage of the parallel electrodes was 3.7 kV, and that of the perpendicular electrodes was 3.5 kV. The voltage was increased to 6 kV, and a snapshot of the discharge top view of the two electrode structures. The discharge voltage–current waveforms are shown in Fig. 5.

It can be concluded from Fig. 4 that a large stable plasma area was generated in both electrode models. However, the discharge areas of the two models were different. The discharge area of the parallel electrodes was larger than that of the perpendicular electrodes. From Fig. 5, it is clear that the instantaneous short pulse current of the parallel electrodes was greater than that of the perpendicular electrodes. This suggests that the plasma generation area of the parallel electrodes was much larger. The discharge



Fig. 2 Simulated electric field distribution diagram a parallel electrode model b perpendicular electrode model

	Maximum electric field strength (V/m)	Strong electric field area (mm ²)
Parallel electrode model	7.551×10^{6}	1.39
Perpendicular electrode model	9.586×10^{6}	0.64

 Table 1
 Electric field simulation results for the two electrode models



Fig. 3 Main discharge circuit



Fig. 4 Plasma discharge phenomenon under voltage of 6 kV a parallel electrode model b perpendicular electrode model

phenomenon in which the discharge is generally considered the diffusion type, with a discharge current on the order of milliamps, is known as a glow discharge. Other studies have used a strict definition of glow discharge in which there is only one discharge process in both the positive and negative half-cycles of an alternating current, and there is only one peak in the current waveform. The discharge form in which many discharges are generated in a half-cycle is called a glow-like discharge. However, the glow discharge was generated by a nanosecond pulse power, and the duration of each glow discharge was short, similar to that of several discharges in a half-cycle. Therefore, the current magnitude, and in particular the current density, was the main basis for defining this as a glow discharge. As seen in Fig. 5, several instantaneous short pulse currents appear in the half-cycle of voltage in the discharge voltage–current waveform of the two electrode models. The discharge currents of the parallel electrode and perpendicular electrode models were ~ 18 and 8 mA,



Fig. 5 Change in discharge voltage and current with time under voltage of 6 kV **a** parallel electrode model **b** perpendicular electrode model

respectively, fitting the current characteristics of a glow discharge. Therefore, the discharge form of the two electrode models could be conceptually considered a glow discharge or glow-like discharge.

Immersion Depth

The outer diameter of the electrodes was 2 mm, and they were spaced at a distance of 3 mm between their centers. The electric field simulation results for various immersion depths of the electrodes are shown in Fig. 6, and Table 2 lists the electric field parameters for different immersion depths.

From Fig. 6 and Table 2, it is clear that as the immersion depth increased, the angle of the gas gap between the electrode and the water surface gradually increased and the maximum electric field strength decreased. Therefore, when the electrodes were tangential to the water surface, the initial discharge voltage decreased to the minimum, and a larger plasma area was generated. The contact area between the generated active particles and the liquid surface was larger, and the treatment was more effective.

Horizontal Distance

The outer diameter of the electrodes was 2 mm. The electric field results of simulations in which the horizontal distance between the two electrodes was varied are shown in Fig. 7, and Table 3 lists the discharge parameters for parallel electrodes with different horizontal distances.



Fig. 6 Electric field simulation for different immersion depths a 0 mm, b 0.5 mm, c 1.0 mm and d 1.5 mm

Immersion depth (mm)	Maximum electric field strength (V/m)	Strong electric field area (mm ²)
0	7.5506×10^{6}	1.39
0.5	7.4011×10^{6}	0.87
1.0	7.2178×10^{6}	0.56
1.5	5.5574×10^{6}	0.18

Table 2 Electric field parameters for different immersion depths of electrode on water surface



Fig. 7 Electric field simulation results for different horizontal distances a 3 mm, b 4 mm and c 5 mm

Table 3 Discharge parameters for different horizontal distances

Horizontal distance (mm)	Maximum electric field strength (V/m)	Initial discharge voltage (kV)
3	7.5664×10^{6}	3.9
4	8.0589×10^{6}	3.8
5	6.6204×10^{6}	4.0



Fig. 8 Structural diagram of the plasma reactor

As seen in Fig. 7 and Table 3, when the horizontal distance was 4 mm, the maximum electric field strength was the largest. Whether or not the horizontal spacing increased, the power line cannot have a maximum concentration in the gas gap, which implies that the maximum electric field strength of the arrangement was relatively low. Therefore, the initial discharge voltage is smaller when the horizontal distance of the electrodes was 4 mm than that when the distance is 3 or 5 mm. The discharge area for 4 mm distance is larger than the other two cases when the same voltage is applied to the electrodes. So the treatment was more effective for 4 mm distance.

Experimental Decoloration of Organic Solutions

The water treatment plasma reactor is shown in Fig. 8. The reactor is composed of a discharge power supply and cylindrical electrodes. The outer diameter of the electrodes was 2 mm, and the horizontal distance between them was 4 mm; the electrodes were tangential to the water surface, and the depth of the solution to be treated was 3 mm.

Examples of industrial wastewater include dyeing wastewater, chemical industrial wastewater, and coking wastewater [31, 32]. In this study, methyl orange and azobenzene solutions were selected as the sample solutions. The concentration of the methyl orange solution and the azobenzene solution were 10 mg/L, and the volume was 50 mL. Two solutions were at rest during processing, and the temperature of two solutions was 10 °C. Place the solution for 10 min after completing the plasma treatment and then the absorbance of the two solutions was tested using a UV spectrophotometer to evaluate the decoloration rate of the pending solutions according to the formula [20, 33].

$$Decoloration \ rate = \frac{A_0 - A_t}{A_0} \times 100 \ \% \tag{1}$$

where A_0 is the absorbance of the initial solution, and A_t is the absorbance of the solution after treatment.

The absorption curves are different curves which can demonstrate the absorptive capacity of the Light-absorbing substance solution to different wavelengths of light. The absorption curves of the methyl orange solution at treatment times of 0, 5, 10, and 15 min are shown in Fig. 9a. The maximum absorption wavelength of the methyl orange solution



Fig. 9 Absorption *curves* of the methyl orange and azobenzene solutions **a** methyl orange solution **b** azobenzene solution

was 464 nm. With increasing treatment time, the absorbance of the methyl orange solution decreased. When the time was 15 min, the decoloration rate of the methyl orange solution was 93 %.

The absorption curves of the azobenzene solution at treatment times of 0, 5, 10, and 15 min are shown in Fig. 9b. The maximum absorption wavelength of the azobenzene solution was 431 nm. With increasing treatment time, the absorbance of the azobenzene solution decreased. When the time was 15 min, the decoloration rate of the azobenzene solution was 85 %.

The plasma contains a large number of free electrons, ions, neutral particles, and atoms and molecules in their excited states, as well as free radicals and so on. Because of the gas gap formed between the electrode and the water surface, a glow discharge occurs, and a large, stable plasma area is acquired for treating the wastewater surface. The methyl orange and azobenzene molecules react with many high-energy particles and strong oxidizing radicals (HO, HO₂, H₂O₂), breaking the bonds between organic molecules and opening the rings to form chain molecules. The generated chain molecules can further interact with the active particles. The ozone, free radicals, and other substances can oxidize and decompose pollutants to achieve the effect of decoloration. At the same time, the discharge process is accompanied by the effects of UV photolysis, supercritical water oxidation and so on. Finally, all of the above processes together degrade the two organic solutions to inorganic ions, water, and other compounds [34–36]. Because the pending solutions were maintained in a stationary state during the treatment, the organic molecules in the solution diffused with increasing treatment time.

Conclusions

The glow discharge plasma treatment of wastewater was presented in this paper. The electrode models for the method were discussed and analyzed by simulations and experiments. The conditions for generating a uniform and stable glow discharge plasma at the water surface in atmospheric pressure air were explored. Moreover, a methyl orange solution and an azobenzene solution were treated using the plasma reactor. The following conclusions were drawn:

- (1) The electric field distribution and discharge characteristics of parallel electrode and perpendicular electrode models were compared. The glow discharge by the perpendicular electrode model was obtained at a low applied voltage, and a larger glow discharge area was generated by the parallel electrode model.
- (2) The field strength of the gas gap can be affected by various factors such as the immersion depth of the parallel electrodes and the horizontal distance between them. A suitable electrode layout can sharply reduce the discharge voltage and result in a steady large plasma area, achieving more effective wastewater treatment.
- (3) A methyl orange solution and an azobenzene solution were treated by the plasma reactor. The decoloration rates of the two organic solutions were 93 and 85 %, respectively, after 15 min

As the above conclusions demonstrate, the electrode structure we designed can generate a glow discharge plasma at the water surface in an atmospheric pressure air environment and can be used in industrial wastewater treatment. Thus, this study provides a new method for plasma water treatment.

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