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Surface Plasmas Versus Volume Plasma: Energy Deposition and Ozone Generation in Air and Oxygen

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Abstract The energy deposition and the ozone generation in a shielded sliding discharge were compared with those of a simple surface discharge and a pulsed corona discharge in atmospheric pressure air and oxygen. All discharges were generated by applying 160 ns, high voltage pulses. Under the same conditions, the highest energy deposition per pulse was obtained with the shielded sliding discharge. The energy deposition was lower by a factor of four for the surface discharge plasma and by an order of magnitude for the pulsed corona discharge plasma. Replacing air with the more electronegative oxygen caused a decrease in the deposited energy due to electron attachment. The threshold voltage for plasma formation in oxygen in a shielded sliding discharge was approximately 5 kV, three times less than that of the surface discharge (\geq 15 kV) and four times less than that of the pulsed corona discharge $(>=20 \text{ kV})$. A new finding of this study is that, whereas the decrease in energy in the pulsed corona discharge was ≥ 50 %, and that of the simple surface discharge ≥ 40 %, it was negligible in the shielded sliding discharge. Since the ozone generation scales with energy density, the results show that plasma reactors based on the nanosecond sliding discharge principle have major advantages in compactness, ignition voltage, and in the use of oxygen, rather than air, compared to surface discharges and corona discharges.

Keywords Nonthermal plasma · Electronegative gas · Ozone · Shielded sliding discharge - Pulsed corona discharge - Sliding discharge

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Introduction

Ozone synthesis using nonthermal plasmas is an important commercial process [[1](#page-6-0)]. Traditionally ozone is produced by employing dielectric barrier discharge (DBD) [\[2](#page-7-0)]. Recently, other nonthermal plasmas, such as those generated in pulsed corona discharges (PCD) [\[3\]](#page-7-0), pulsed glow discharges [\[4](#page-7-0)], surface-DBD (S-DBD) [\[5](#page-7-0)–[9\]](#page-7-0), shielded sliding discharge [\[10,](#page-7-0) [11](#page-7-0)], coupled sliding discharge [\[12\]](#page-7-0) or plasma hybridized with a catalyst [[13–15\]](#page-7-0) are being explored with respect to their efficiency. Both air and oxygen are used as feed for ozone synthesis [\[1\]](#page-6-0). Although air is cheaper and commonly available, oxygen is preferred due to higher ozone concentration achieved using it. However, since oxygen is an electronegative gas, increasing oxygen from 20 to 100 % results in increased losses of free electrons by electron attachment reactions such as the following [[16\]](#page-7-0).

$$
e + O_2 \rightarrow O^- + O, \tag{1}
$$

$$
e + O_2 + O_2 \to O_2^- + O_2. \tag{2}
$$

The loss of free electrons adversely affects the electron avalanche process in the electrical discharges resulting in a significant decrease in the discharge current and consequently in the energy density of the plasma. The same problem is also encountered in some other processes involving electronegative gases, e.g., halogenated hydrocarbons employed in semiconductor etching or in electrochemical lasers [[16](#page-7-0)] or those involving atmospheric pressure water vapor where ready recombination of H_3O^+ species present in the water medium causes the electron loss [[17\]](#page-7-0).

Fig. 1 Top view of electrode assemblies (top) and cross-section view of the discharge chambers through $A-$ A line (bottom) that generate pulsed corona discharges (a), surface discharge (b), and shielded sliding discharge (c). *1* High voltage electrode (anode), 2 counter electrode at ground potential (cathode), 3 dielectric layer, 4 and 5 are spacers, and 6 is the plasma channel (streamers)

Experimental

Power depositions for the discharges formed in three electrode assemblies shown in Fig. [1](#page-1-0) are compared. The power dissipation in the shielded sliding discharge (Fig. [1c](#page-1-0)) using air or oxygen as working gas is compared with that of the surface discharge (Fig. [1](#page-1-0)b) and the pulsed corona discharge (Fig. [1](#page-1-0)a) [\[10,](#page-7-0) [18](#page-7-0)]. A Compact Pulsed Power Modulator MPC3000S-OP1 (Suematsu Electronics Co., Ltd., Japan) delivered high voltage of positive polarity ($+HV$) of \sim 160 ns duration (FWHM) and peak voltages of 5–30 kV at frequencies of 500 Hz. A Tektronix P6015A voltage probe, a Pearson Electronics Current Monitor, Model 110A and Tektronix TDS 3052 oscilloscope were used to measure the temporal development of voltage and current. The energy per pulse (Ep) is the time integral (\overline{V} Idt where V and I are the discharge voltage and current, respectively) of the power.

The electrodes were made of aluminum foil (ALF200L from Intertape Polymer Groups, USA) of 50 μ m thickness that was glued to a dielectric frame using an acrylic adhesive (Fig. [1a](#page-1-0)). The width of the electrodes $(#1 \text{ and } #2 \text{ in Fig. 1a})$ $(#1 \text{ and } #2 \text{ in Fig. 1a})$ $(#1 \text{ and } #2 \text{ in Fig. 1a})$ was kept at 6 mm, the interelectrode gap was 16 mm, and the effective length of the center electrode was 89 mm. The electrode assembly of Fig. [1a](#page-1-0) forms pulsed corona discharges in the inter-electrode gap upon application of the HV pulses. The same electrodes were glued to a dielectric sheet made of soda glass with dimensions 2.4 mm \times 76 mm \times 152 mm as shown in Fig. [1b](#page-1-0) to generate a surface discharge [\[18\]](#page-7-0). The electrode configuration for the shielded sliding discharge is shown in Fig. [1](#page-1-0)c [[10](#page-7-0), [18](#page-7-0)]. It was formed by connecting an aluminum foil to the ground electrode #2 and by wrapping it around the opposite side of the dielectric, covering the entire inter-electrode gap area.

The spacer (#4 in Fig. [1](#page-1-0)b, c) was made of silicon measuring 4 mm \times 76 mm \times 152 mm, from which a 4 mm \times 51 mm \times 127 mm block (defining the inside dimensions of the reactor) was cut from the center. The gas inlet and outlet were nylon tubes of 2.0 mm ID and 2.3 mm OD extending through opposite corners of the spacer and sealed using silicon glue. Spacer #5 in the case of Fig. [1](#page-1-0)a was of the same dimension as the spacer #4 described above except that it was made of acrylic sealed with silicon glue. Its thickness was 15 mm instead of 4 mm. The thickness of the spacer was increased to avoid surface plasma formation in the case of the pulsed corona discharge as explained earlier [\[10\]](#page-7-0).

The experiments were carried out at atmospheric pressure and room temperature. All gas volumes are expressed under conditions of 25 $^{\circ}$ C and 1 atmospheric pressure with the exception of ozone concentration which is expressed in grams of ozone per normal cubic meter (g/Nm³), where normal stands for 1 atmospheric pressure and 0 °C. Dry air (UN1002 from Airgas USA) or oxygen (UN1072 from Airgas USA) were supplied from a pressurized gas cylinder at a flow rate (Q) of 1 liter per minute (L/min) in all the experiments. Specific input energy which is energy dissipated in reactor per unit volume of gas processed in joules per litter (J/L). When the feed gas was switched, it was allowed to run for about half an hour before experiment was started. Ozone was analyzed based on an UV absorption technique using an ozone analyzer (gFFOZ, IN USA, Inc., Needham, MA, USA) with an accuracy of 1 % of the reading and is recorded in grams of ozone per normal cubic meter (g/Nm³), where normal stands for 1 atmospheric pressure and 0° C. The experimental procedures and statistical treatment of the data was the same as in our earlier study [[11](#page-7-0)].

Results and Discussion

Figure 2 shows that the energy per pulse increased with the increase in peak applied voltage in all cases, but the plasma initiation threshold voltage and the increase in the energy deposition with increase in peak voltage strongly depended on the type of discharge. Pulsed corona discharges required the highest voltages, i.e., >15 kV in air and \geq 20 kV in oxygen. Surface discharges required a lower voltage \geq 15 kV, and the energy per pulse was more than double that of pulsed corona discharges at the same voltage. The shielded sliding discharge required a peak voltage of only about 5 kV, and the energy per pulse was about an order of magnitude higher compared to that of pulsed corona discharges at the same voltage which is in accordance with our earlier studies [\[10\]](#page-7-0). The new finding of this study is that when air was replaced with oxygen as a working gas, the energy per pulse decreased by \geq 50 % in the case of pulsed corona discharge and \geq 40 % in the case of the surface discharge, but almost no decrease was observed in the case of a shielded sliding discharge at the same applied voltage.

To the best of our knowledge negligible energy loss when the feed gas is changed from air to the more electronegative oxygen in the shielded sliding discharge is being reported for the first time. So we verified it by several alternate ways in the following experiments. When the thickness of the dielectric layer in the shielded sliding discharge assembly of Fig. [1c](#page-1-0) was decreased from 2.4 to 1 mm, the energy per pulse was increased by about a factor of two. The reduction in the energy per pulse when replacing air with oxygen again was not affected by this change in the reactor geometry. We have reported several versions of shielded sliding discharges, all of them scalable in a compact configuration with high gas throughput; these are coupled sliding discharge [\[12\]](#page-7-0), surface-dielectric barrier discharge, and coupled surface-dielectric barrier discharge [\[9\]](#page-7-0). When the present experiments were repeated using those electrode assemblies with electrodes of the same or similar dimensions as in Fig. [1,](#page-1-0) the same trend was observed. That is, the decrease in energy per pulse was negligible upon replacing air with oxygen at the same applied voltage.

Fig. 2 Energy per pulse versus peak voltage with air and with oxygen as working gas in different types of electrical discharges. The pulse frequency was 500 Hz and the flow rate of the gas was 1 L/min. Symbols represent experimental values and the *lines* in the figures are just a visual guide of the trends

In the case of plasmas developing along a dielectric surface (Fig. [1b](#page-1-0) and [1c](#page-1-0)), the plasma draws additional electrons from the surfaces on which it is sliding [[19](#page-7-0)]. The generation of these electrons is considered to compensate in part for the free electron capture by oxygen. Particularly, the anions like O^- and O_2^- may be adsorbed on the surface and ultimately may decay and release free electrons through reactions such as the following [[16](#page-7-0)].

$$
O^- + O_2/surface \rightarrow O + O_2/surface + e,
$$
\n(3)

$$
O_2^- + O_2/surface \rightarrow O_2 + O_2/surface + e. \tag{4}
$$

In the case of a shielded sliding discharge, the counter electrode overlapping the electrode at close proximity (2.4 mm in this case) significantly enhances electric fields at the edges of the electrode fostering initiation of more plasma channels [\[12\]](#page-7-0). Further, re-distribution of electric fields favors stronger attraction of the plasma to the surface favoring more electron emissions through surface mediated reactions. These factors explain the increased energy per pulse and the significantly less adverse effect of replacing air with more electronegative oxygen.

Ozone synthesis using air and oxygen as feed was used to compare the chemical efficiency of the reactors employed in this study (Fig. 3). The following is observed from the results.

- 1. Ozone concentration was dependent on the feed gas composition; it is significantly higher in oxygen than in air (20 % oxygen), which is in agreement with earlier literature [\[1\]](#page-6-0).
- 2. The ozone concentration was found to be dependent on the deposited electrical energy and almost independent of the type of discharge, particularly under the condition of specific input energy \200 J/L. Deviations from the common curve were observed when specific input energy was >200 J/L.

The main reaction channel for ozone formation form oxygen is the following [\[20–23\]](#page-7-0):

Fig. 3 Ozone concentration versus specific input energy for the three electrical discharge types. The flow rate of air or oxygen feed was 1.0 L/min and pulse frequency was 500 Hz. The energy was varied by varying the applied voltage (Fig. [2](#page-3-0)). The same symbols were used as in Fig. 2

$$
e^* + O_2 \to e + 2O,\tag{5}
$$

$$
O + O_2 + M \rightarrow O_3 + M,\tag{6}
$$

where 'e^{*}' represents a high-energy electron, 'e' represents a relatively low-energy electron, and 'M' is a third collision partner that can be O_2 , N_2 , a solid surface in contact with the plasma, etc. Ozone yield is generally lower in air than in oxygen because dissociation and/or excitation of nitrogen competes with the dissociation of oxygen, leading to synthesis of unwanted by-products like nitrogen oxides (NOx) in addition to ozone. An increase in specific input energy increases the rates of these reactions leading to high ozone concentration, but, at the same time, increases the local temperature in the plasma leading to destruction of some of the ozone formed.

Based on higher energy per pulse, one can expect strong negative effect of temperature in the case of shielded sliding discharge compared to the other two discharges. Further, the plasma tends to localize more around the high voltage electrode in a shielded sliding discharge compared to sliding discharge and pulsed corona discharge as illustrated by images of the plasmas shown in Fig. 4. It is a plausible explanation for the slightly better ozone generation efficiency by a sliding discharge than by a shielded sliding discharge, particularly when the specific input energy was more than 200 J/L.

Measured temperature of the exhaust gas was no more than a few degrees higher compared to initial temperature in ozone synthesis experiments of Fig. [3.](#page-4-0) One can expect more heating of gas in the case of shielded sliding discharge due to higher energy density in it. However, plasma in this study was in contact with dielectric surface which most likely dissipated major fraction of heat from the plasma channels.

Fig. 4 Time integrated of images of about hundred consecutive discharge events in air at repetition rate of 500 Hz and 26, 25 and 19 kV for pulsed corona discharge, sliding discharge and shielded sliding discharge, respectively

The results in Fig. [3](#page-4-0) show that for all discharge types with energy deposition and consequently increasing ozone concentration from 1 to 20 g/Nm^3 , the energy yield for the ozone generation decreases gradually from 250 to 150 g/kWh. These concentrations and energy yield values are comparable to \sim 17 g/Nm³ with an energy yield \sim 85 g/kWh in a surface-DBD formed in micro-channels on an aluminum substrate [\[8\]](#page-7-0), 0.2 to 43 g/Nm³ ozone produced in a surface-DBD with energy yield 170 to 75 g/kWh [[6\]](#page-7-0), and \sim 100 g/ Nm³ ozone and 180–200 g/kWh energy yield in surface-DBD with forced cooling of electrodes [\[7](#page-7-0)]. It should be mentioned here that this comparison of ozone efficiencies is a qualitative one because energy yield is dependent on multiple factors, including ozone concentration, power dissipation, and temperature of cooling liquid [\[24\]](#page-7-0). Nanosecond pulses as in this study are also known to be more efficient than the sinusoidal driving voltage [[25\]](#page-7-0). Results of this study are valid for positive polarity pulses only. It needs to be mentioned because ozone and its precursor O are produced more efficiently by employing negative polarity pulses than positive polarity pulses when the feed gas is air [\[10,](#page-7-0) [11](#page-7-0), [26](#page-7-0)]. However, this dependence of ozone efficiency on the polarity of the voltage pulse disappears in the case of oxygen feed [[11\]](#page-7-0).

The voltage pulses employed in this study had a duration of approximately 160 ns (full width at half maximum). Earlier studies indicate that the efficiency for ozone can be increased by employing voltage pulses of shorter duration. For example, the highest ozone energy yield known to us with oxygen feed is about 700 g/kWh reported for the case of short duration pulses of 5 ns, but at a much higher peak voltage of 60 kV at negative polarity [[3\]](#page-7-0). There is a potential of further improvement by employing a dielectric layer made of materials known to catalyze ozone formation in electrical discharges, e.g., alumina [[14](#page-7-0), [15](#page-7-0)] and silica gel [[13](#page-7-0)].

Conclusions

Although the energy cost for ozone synthesis under a constant flow rate of oxygen feed only depends on the deposited energy and is consequently almost the same for all three discharge types, the shielded sliding discharge has an advantage, due to its high energy deposition in a smaller volume and consequently its high energy density in the discharge plasma compared to pulsed corona discharge. Another advantage is its relatively low discharge voltage, allowing its use in very compact plasma reactors. In addition, it is found for the first time in this study that the decrease in energy density was the smallest in shielded sliding discharges when air is replaced by electronegative oxygen. This again shows that this type of discharge has an advantage for uses where electronegative gases like oxygen, halogens, halogenated compounds or water vapors need to be added in the composition of the process gas.

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