

Plasma-Enhanced Methane Direct Conversion over Particle-Size Adjusted $\text{MO}_x/\text{Al}_2\text{O}_3$ (M = Ti and Mg) Catalysts

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Abstract Non-oxidative methane activation over particle-size adjusted alumina catalysts loaded with metal oxide (Al_2O_3 , $\text{MgO}/\text{Al}_2\text{O}_3$, and $\text{TiO}_2/\text{Al}_2\text{O}_3$) was investigated with a dielectric barrier discharge reactor using 10 % CH_4 in Ar at plasma induced temperature. Plasma-assisted catalytic activity for direct conversion of methane over the catalysts was compared with that using plasma only. Catalyst hybrid reaction in a non-thermal discharge showed that $\text{MgO}/\text{Al}_2\text{O}_3$ had the highest activity for methane conversion. C_2 , C_3 , and C_4 hydrocarbons were formed as products; ethane, ethylene, and acetylene were predominant over all catalysts. The effect of varying particle size of the $\text{MgO}/\text{Al}_2\text{O}_3$ catalyst was also examined. The conversion of methane over $\text{MgO}/\text{Al}_2\text{O}_3$ dramatically increased with decreasing catalyst particle size from 1.70 to 0.25 μm . It is interesting to note that distribution of C_2 hydrocarbons was tuned by changing the particle size of the catalyst. It was also observed that the gas flow rate, frequency, and power supplied affected direct conversion of methane and selectivity of products significantly.

Keywords Non-oxidative methane activation · DBD reactor · Metal oxide · Particle size

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Introduction

Methane is a major component of fossil fuels such as natural gas, shale gas, methane hydrates, and biomass derived resources. However, it is important to reduce the release of methane into the environment because methane has 25 times more warming potential as a greenhouse gas than carbon dioxide [1, 2]. Methane has the potential for transformation into other chemicals for further utilization in energy sources or feed stocks, but methane activation is very challenging. Methane has been used for production of synthesis gas (CO and H₂) by steam reforming under extreme conditions (700–1,100 °C and 20–30 bar) using a metal-based catalyst [3, 4]. Since the 1980s, a lot of efforts has been put into methane transformation; including direct oxidation to methanol and formaldehyde, oxidative coupling, and non-oxidative coupling. The focus has been to overcome the difficulty of breaking C–H bonds and to form the desired C–C and C–O bonds from the perspectives of both basic chemistry and engineering [5, 6].

Direct coupling of methane in the presence of oxidants has attracted much attention, because the thermodynamics of this reaction are more favorable than for non-oxidative coupling. Unfortunately, undesirable by-products (CO_x) were also formed in the oxidative coupling process at high temperatures [7]. Moreover, it is difficult to control the reaction temperature because the overall reaction is exothermic and the actual catalyst bed temperature could be much higher than the set temperature [8]. Therefore, non-oxidative conversion of methane at low temperature is preferable to the oxidative process due to its high selectivity for desirable hydrocarbons. However, a major difficulty in the catalytic and thermal direct conversion of methane remains, because the strength of its C–H bonds is greater than that of hydrocarbons that might be produced [3]. Another problem associated with thermal catalytic conversion of methane is carbon or coke deposition causing catalyst deactivation.

Non-thermal plasma technology converts the major part of electrical energy to energetic electrons rather than using it to heat gases, thus it can supersede conventional thermal catalytic technology for the direct methane coupling reaction. However, the gas-phase non-catalytic plasma reaction usually occurs via a free radical mechanism which is unfavorable for controlling the selectivity of products [9–11]. To enhance the performance of methane conversion, intense effort has been devoted to hybrid plasma-heterogeneous catalyst system by using various types of non-thermal plasma, including dielectric barrier discharge (DBD), corona, glow discharge, and gliding arc [12–15]. It has been reported that control of electron energy with a suitable design of discharge reactor as well as a proper catalyst can strongly affect product selectivity in the methane conversion reaction, particularly in DBD and corona discharge systems [16].

Dielectric barrier discharge reactors have an advantage for developing a plasma-catalytic process because the catalyst particles are placed inside the discharge zone, and it is possible to effectively transfer the active species generated by plasma, onto the catalyst surface. However, the plasma-catalyst hybrid system makes for extra complexity of the discharge state. If some solid particles exist in the discharge zone, the discharge structure and its character will vary due to changing electrical parameters (electric field strength and current density) because of shifts in the current flow near the surface. Therefore, the properties of the catalyst can be used to tune the electrical parameters in the discharge zone. Other factors, such as the hydrodynamics of the gas stream and temperature distributions, may also change according to the kind of material used in the reactor.

Several catalysts have been used for methane activation in the presence of plasma. It has been reported that NaY zeolite showed high yield for C₂ hydrocarbons [17]. Pt/γ-Al₂O₃

catalyst was also used for methane conversion in a DBD reactor and showed high selectivity for light alkanes [18]. In the presence of catalyst particles, molecular processes include adsorption onto the catalyst surface, reaction between the adsorbed species, and desorption of the products. During this phase, the catalyst can increase the lifespan of the high-energy radicals by adsorbing their excess energy [19]. One of the key roles of the catalyst in this hybrid system is conducting reactions between short-lived active species [20]. Mlotek et al. [12] showed that when the active species generated in plasma took a relatively long time to reach the catalyst surface, most of the fast reactions were terminated in the gas phase. In this case, the catalyst could have no influence on the reaction result, indicating that the reaction result depends on the discharge condition and the configuration of the catalyst. A few literature works concentrates on studying the effect of catalyst-bed porosity, controlled by packing different size of catalyst pellets in the discharge zone. Introducing catalyst of different size into the discharge gap generates void fraction leading to significant transition of the discharge behavior [21–23]. Studies suggest that relative contribution of filamentary and surface discharges is likely to depend on many factors including particle size, particle shape, packing location, and the void fraction of the electrode gap [24, 25].

Wan et al. [26] studied the effect of catalyst size on methane conversion in the presence of microwaves and reported that activity and selectivity for aromatics varied with changing particle size of the catalyst. It was also found that micro-discharge on the surface of the catalyst particles affected conversion and selectivity.

In this work, we investigated the effect of catalyst size on plasma-assisted catalytic reaction at ambient temperature and atmospheric pressure; to selectively produce C2 hydrocarbons from methane. We also examined the catalytic performance of various metal-oxide-loaded catalysts for this reaction.

Experimental

The plasma-assisted catalytic reaction was carried out in a packed-bed DBD reactor with a volume of $56 \times 24 \times 3$ mm; between two dielectric plates attached to stainless steel electrodes. The gas distance between the electrodes was 3 mm. Figure 1 shows the scheme of the plasma reaction system. Balls (1.7 mm) of Al_2O_3 , $\text{MgO}/\text{Al}_2\text{O}_3$ (7.1 wt%) and $\text{TiO}_2/\text{Al}_2\text{O}_3$ (9.7 wt%) were provided from Sasolalumina; with BET surface areas of 201, 184, and 212 m^2/g , respectively; were crushed to different mesh sizes and placed in the reactor. These materials were prepared by sol–gel method (www.Salsoalumina.com) and the surface area was recorded using Micrometric Tristar II 3000 by N_2 adsorption isotherm at 77 K after dehydration of sample at 423 K. To examine the effect of catalyst mesh size, the ball shaped catalyst of 1.75 mm was crushed to different mesh size and filled the reactor volume. 1.21 g of 1.75 mm ball shaped catalyst was used to fill the entire volume of the reactor. When the smaller mesh size of the catalyst was used, the more amount of the catalyst was needed to occupy the same reactor volume. Argon and methane (10 mol%) flowed through this reactor at a flow-rate aimed at performing the reaction at ambient temperature and atmospheric pressure. In the non-thermal plasma reactions, the gas discharge was initiated at room temperature and the gas was heated by the plasma. A sinusoidal AC continuous supply of power (TTI, TGA 1244; Trek, 20/20C); with 0–6 kV and 1–5 kHz, was applied across the electrode. A 500 pf capacitor was connected to measure the applied power using an oscilloscope (Tektronix, DPO 5054) by integrating the single

period power and multiplying the frequency. A 100 ohm resistor was also connected to monitor the micro-discharge plasma current.

A high speed ICCD camera (Hamamatsu, ORCA-05G) was mounted near the reactor to record images of the plasma generated during a single wave interval. The reactor temperature induced during the plasma reaction was measured by an IR temperature detector (FLIR, E50). TGA experiments were carried out using a SDTQ600 Thermogravimetric Analyzer to confirm the coke amount formed. For TGA analysis, 10 mg of catalyst after plasma reaction was used. TGA began by heating up the sample in air at a heating rate of 5 °C/min (100 ml/min, atmospheric pressure). The weight change of the catalyst was recorded up to 800 °C. The weight loss of catalyst was obtained by subtracting the weight loss of the catalyst from total weight loss of mixed sample. TPO was also run in the micrometrics Autochem II (20 % O₂/He, 50 cm³/min, heating rate of 5 °C/min) for CO₂ by an TCD detector. The gaseous product species after heating the sample was also monitored by the mass spectrometer (Pfeiffer Vacuum) to analyze the composition of CO₂ and H₂O.

The gas outlet was connected to a mass spectrometer (Pfeiffer Vacuum) to identify each product. Reaction products, such as hydrogen and hydrocarbons; were analyzed using a micro gas chromatograph (Agilent, 490 Micro GC) with four columns. Then, the conversion of methane and selectivity for each product were calculated. The conversion of CH₄, selectivity for hydrocarbon products, and yield for H₂, and carbon balance were calculated using Eqs. (1), (2), (3), and (4), respectively.

$$\text{Conversion of CH}_4(\%) = \frac{\text{Moles of CH}_4 \text{ converted}}{\text{Moles of CH}_4 \text{ feed}} \times 100 \quad (1)$$

$$\text{Selectivity for C}_x\text{H}_y \text{ products } (\%) = \frac{\text{Moles of C}_x\text{H}_y \text{ produced}}{\text{Total moles of hydrocarbon products}} \times 100 \quad (2)$$

$$\text{H}_2 \text{ yield } (\%) = \frac{\text{Moles of H}_2 \text{ produced}}{2 \times \text{Moles of CH}_4 \text{ feed}} \times 100 \quad (3)$$

C balance (%)

$$= \frac{2 \times \text{Moles of C}_2 + 3 \times \text{Moles of C}_3 + 4 \times \text{Moles of C}_4 + 5 \times \text{Moles of C}_5}{\text{Moles of CH}_4 \text{ converted}} \times 100 \quad (4)$$

Result and Discussion

Effects of the Catalyst

Experiments were carried out in the presence of catalysts at atmospheric pressure and plasma heated temperature, with 10 % CH₄/Ar mixed gas; at a total flow rate of 200 ml/min. Choice of these conditions was based on evidence that the methane activation reaction occurs well in response to micro-discharge induced by electric fields on the catalyst surfaces [27]. The mass spectroscope attached to the outlet of the reactor detected only light alkanes (C₂H₆, C₂H₄, C₂H₂, C₃H₈, C₃H₆, and C₄H₁₀) and H₂. Other hydrocarbons obtained were negligible. To investigate the effect of catalyst in a DBD reactor, a non-catalytic plasma process was also conducted with variation of applied voltage from 3 to 6 kV at

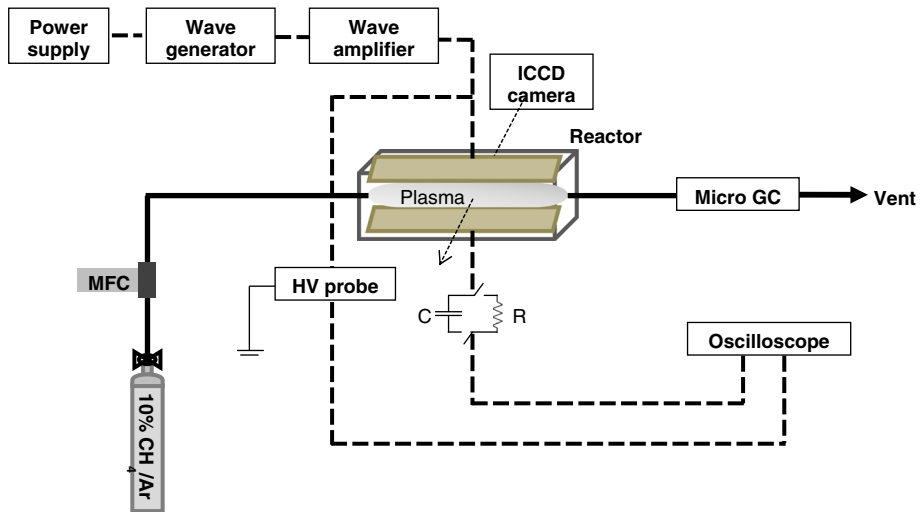


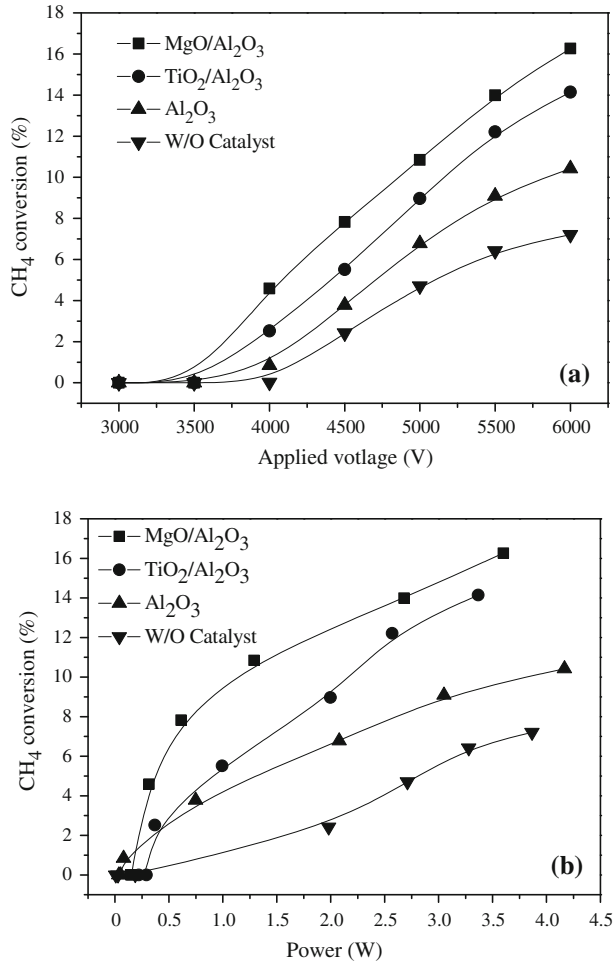
Fig. 1 Scheme of the plasma-assisted catalytic reaction system

3 kHz (Fig. 2a). No conversion of methane was observed until 3.5 kV, but the plasma was initiated at 4 kV and low conversion of methane was obtained. Conversion of methane increased steadily to 7.2 % with increasing voltage (to 6 kV). The temperature in the reactor recorded by the IR thermal detector was 53 °C without catalyst and 56 °C with catalyst. The temperature of the reactor increased slightly, as increased applied voltage and frequency. Gas temperature should be regarded as approximate values reflecting however the trend of the temperature increasing with time. When Al_2O_3 was introduced to the reactor, the plasma was also generated at 4 kV. Conversion of methane over Al_2O_3 was higher than with no catalyst, and reached 10.4 % at 6 kV. Conversion of methane over $\text{TiO}_2/\text{Al}_2\text{O}_3$ was higher than that over Al_2O_3 , and reached 14.1 % at 6 kV. The $\text{MgO}/\text{Al}_2\text{O}_3$ catalyst induced even better conversion of methane (16.2 % at 6 kV). SiO_2 of same mesh size was also used as a catalyst, which gave low activity even compared to the plasma itself.

The energy required to generate plasma was calculated from the corresponding Q–V Lissajous plots (Fig. 3) [28, 29]. The area of the Q–V parallelogram, obtained using a 500 pf capacitor, equals the discharge-energy dissipated during one cycle of the AC voltage. Figure 2b shows the conversion of methane over Al_2O_3 , $\text{TiO}_2/\text{Al}_2\text{O}_3$, and $\text{MgO}/\text{Al}_2\text{O}_3$ catalysts; as a function of the discharge energy. $\text{TiO}_2/\text{Al}_2\text{O}_3$ required less energy to obtain the same conversion of methane than Al_2O_3 . Moreover, $\text{MgO}/\text{Al}_2\text{O}_3$ needed less energy than $\text{TiO}_2/\text{Al}_2\text{O}_3$. When the applied voltage fixed at 6 kV, generated discharge power was decreased from 4.18 W for Al_2O_3 , 3.36 W for $\text{TiO}_2/\text{Al}_2\text{O}_3$, and 3.60 W $\text{MgO}/\text{Al}_2\text{O}_3$, respectively. This indicates that metal-oxide doping affects the energy efficiency of the system. Figure 2b also clearly shows that the energy required for DBD to convert methane is lower when catalyst is used. The onset voltage of catalysts in a packed-bed DBD reactor is higher than that for plasma only, because of changes in electric field and filamentary discharge densities [30].

Figure 4 shows the patterns of plasma-current generated in the DBD reactor; which consisted of a sine function wave and sharp peaks of high-energy electrons. A sufficiently

Fig. 2 Conversion of methane over metal-oxide loaded alumina catalysts (0.5 mm) with plasma, as a function of **a** applied voltage and **b** power



high density of high-energy electrons in the plasma current; characterized by a large number of micro-discharge filaments, is able to activate hydrocarbons at room temperature and atmospheric pressure. In general, it is believed that DBD involves a large number of micro-discharges (about 10^6 micro-discharges per cm^2 per second) [31]. The short lifetime of the current spikes may help to minimize excessive local heating.

Figure 5 shows the catalytic performance of Al_2O_3 , $\text{TiO}_2/\text{Al}_2\text{O}_3$, and $\text{MgO}/\text{Al}_2\text{O}_3$ for methane activation with plasma at 6 kV and 3 kHz. As mentioned earlier, conversion of methane was enhanced when catalyst was used. Among the catalysts tested, $\text{MgO}/\text{Al}_2\text{O}_3$ showed the highest methane conversion. No matter which catalyst (Al_2O_3 , $\text{TiO}_2/\text{Al}_2\text{O}_3$, or $\text{MgO}/\text{Al}_2\text{O}_3$) was used, selectivity for ethane and propane dropped; while selectivity for ethylene, acetylene, and propylene rose. From a modeling study of methane activation using only DBD, it was found that ethane and propane are the most favored products [32]. Therefore, this means that these early products acted as catalysts in this reaction. Each catalyst showed selectivity for different products. The activation of methane to CH_x fragments is mainly caused by electric discharge. At this time, electric conductivity and

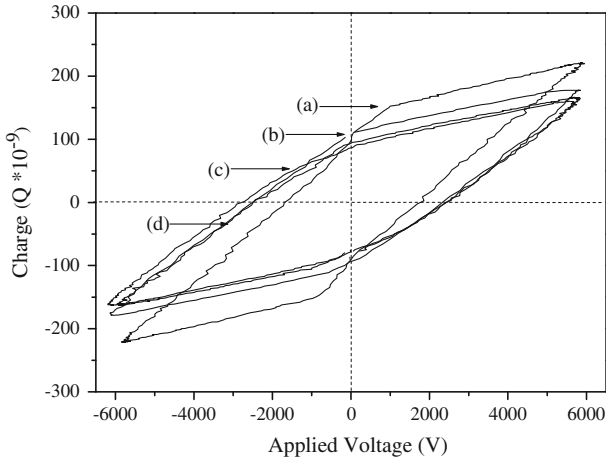


Fig. 3 Q–V patterns of **a** w/o catalyst, **b** Al_2O_3 , **c** $\text{TiO}_2/\text{Al}_2\text{O}_3$, and **d** $\text{MgO}/\text{Al}_2\text{O}_3$ catalysts (0.5 mm of particle size) at 6 kV and 3 kHz

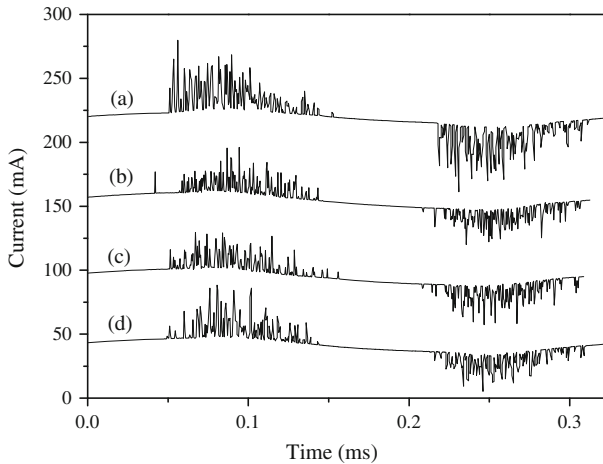
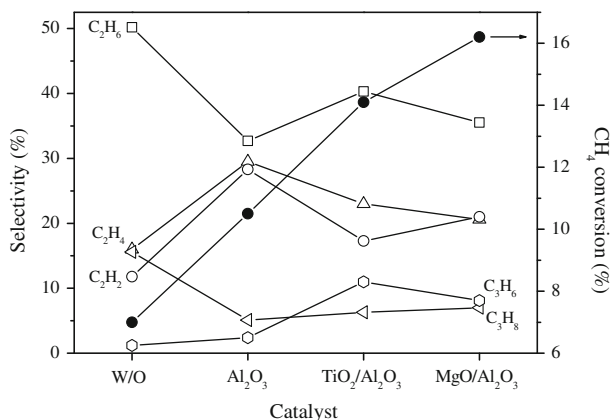


Fig. 4 Micro-discharge current patterns of **a** w/o catalyst, **b** Al_2O_3 , **c** $\text{TiO}_2/\text{Al}_2\text{O}_3$, and **d** $\text{MgO}/\text{Al}_2\text{O}_3$ catalysts (0.5 mm of particle size) at 6 kV and 3 kHz

surface charge of the catalyst would affect the type of radical formed. Barrier heating on the surface of the catalyst can be caused by a vibrational de-excitation process, or by a recombination of ions and electrons. The barrier is charged locally by the micro-discharge filaments, and this causes the barrier to heat strongly [33]. This local barrier heating on the surface of the catalyst increases the activity of the reaction. In this case, the dielectric constant and band gap of the catalyst may affect the occurrence of micro-discharge filaments [34]. Micro-discharge efficiency on the surface of MgO , TiO_2 , and Al_2O_3 differs, and this causes a difference in the temperature on the surface of the catalyst; resulting in different catalytic activity. Also, polymerization of radicals on the surface of the catalyst would depend on the nature of the catalyst, quite evident when the metal oxide catalysts

Fig. 5 Catalytic performance of Al_2O_3 , $\text{TiO}_2/\text{Al}_2\text{O}_3$, and $\text{MgO}/\text{Al}_2\text{O}_3$ catalysts (0.5 mm of particle size) in a methane-conversion reaction assisted with plasma at 6 kV and 3 kHz



were compared with SiO_2 [16, 35, 36]. Therefore, the selectivity for products can be varied using the qualities of the catalyst. To determine thoroughly the reaction factors in this kind of reaction system, further studies are needed.

Effect of Catalyst Particle Size

Previous research has not been focused on the study of catalyst particle-size in plasma-assisted reactions. Therefore, balls of $\text{MgO}/\text{Al}_2\text{O}_3$ catalyst were crushed to different sizes and placed in the DBD reactor. The reaction was performed at 3 kHz and 6 kV at a flow rate of 200 ml/min; with 10 % CH_4 in Ar. Table 1 shows the effect of catalyst particle size on plasma-assisted methane activation. When 1.75 mm balls of $\text{MgO}/\text{Al}_2\text{O}_3$ were used in the reactor, conversion of methane was 9.5 % and the energy utilized was 3.5 W (1,050 kJ/l). Conversion of methane increased with decreasing particle size. Selectivity for ethane and propane decreased significantly with decreasing particle size; while selectivity for acetylene increased with decreasing particle size. Selectivity for ethylene and propylene also increased slightly when smaller $\text{MgO}/\text{Al}_2\text{O}_3$ catalyst was used. These results indicate that filling the reactor with smaller catalyst particles increased the surface interaction between the catalyst and reaction species by stabilizing the radical; resulting in increased conversion of methane and changes in selectivity for products.

Q–V plots for $\text{MgO}/\text{Al}_2\text{O}_3$ of different particle sizes show a steady decrease in the capacitor voltage; leading to a lower energy in the system with decreasing particle-size of the catalyst (Fig. 6). Light emitted from excited molecules or radicals during the relaxation were captured by a high speed camera. Figure 7 displays the plasma-catalyst images recorded during the reaction. Figure 7a shows the uniform plasma pattern between the DBD electrodes when catalyst was not used. The smaller the catalyst particle used, the lighter the plasma observed on the catalyst surface. This indicates that the enhanced activity of the smaller catalyst is due to improved interaction between the surface of the catalyst and the plasma.

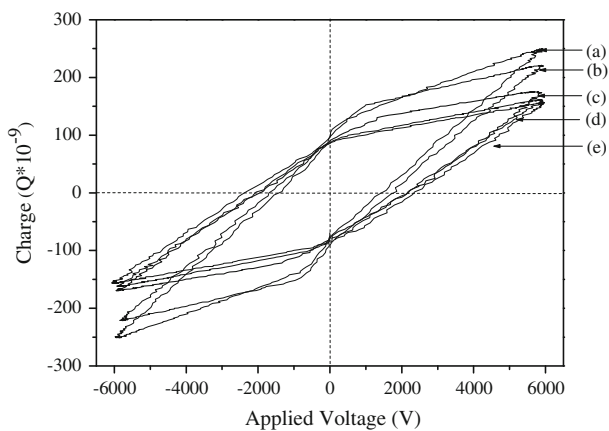
Carbon species deposited on the catalyst was confirmed by TGA analysis for the used catalyst. Figure 8 shows TGA profile of used $\text{MgO}/\text{Al}_2\text{O}_3$ catalyst with different particle sizes. TGA profile in Fig. 8 shows that as-synthesized catalyst $\text{MgO}/\text{Al}_2\text{O}_3$ gives the least weight loss, while the weight loss increases as the particle size decreases indicating that carbon deposition was increased. The deposited amount of carbon was calculated from the

Table 1 Catalytic performance of MgO/Al₂O₃ with different particle size in plasma assisted methane conversion reaction

Mesh size (mm)	Power (W)	Conv. (%)	H ₂ Yield (%)	Selectivity for products (%)							B _{carbon} (%)
				C ₂ H ₆	C ₂ H ₄	C ₂ H ₂	C ₃ H ₈	C ₃ H ₆	n-C ₄ H ₁₀	i-C ₄ H ₁₀	
1.75	3.5	9.5	4.9	48.1	18.6	10.5	14	5.1	3	0.7	82
1.00	3.2	9.8	5.1	42.8	23	14	10.3	6.5	2.6	0.7	80
0.50	3.4	16.2	7.1	35.5	25.6	22	7.3	8.1	1.2	0.3	76
0.25	3.3	23.0	8.1	27.4	30.3	28	3.6	9.7	0.5	0.5	71

Reaction conditions: 3 kHz, 6 kV, plasma induced temperature, 200 ml/min of 10 % CH₄/Ar

Fig. 6 Q–V patterns of MgO/Al₂O₃ at 6 kV and 3 kHz; in relation to different catalyst particle size: **a** w/o catalyst, **b** 1.75 mm, **c** 1.00 mm, **d** 0.50 mm, and **e** 0.25 mm



weight loss in the TGA experiments. The carbon balance obtained from the TGA profiles were similar to that obtained from Micro GC. A lower carbon balance was obtained when catalyst of smaller particle size was used. This indicates that the formation of solid carbon was favored by increasing the interaction between reactants and the catalyst surface. The TPO and mass spectrometer results from used catalyst also shows high amount of CO₂ and low amount of H₂O indicating very low composition of H in the deposited carbon (data not shown). The low amount of H content in the coke indicates major amount of solid product being formed by the agglomeration of monomolecular, active carbon species rather than polymerization of acetylene, ethylene, and propylene. Acetylene and propylene are well-known solid-carbon precursors during pyrolysis (combustion process). The presence of H species does specify that a similar phenomenon occurred in this plasma process. Further studies are required to explain the reasons for this result.

Stability Check

To check the stability of catalyst, plasma reaction was performed using 0.5 mm of MgO/Al₂O₃ for 400 min at 6 kV and 3 kHz with 200 ml/min flow of 10 % CH₄ in Ar. The result is represented in Fig. 9. Conversion of methane was 16 % and it remained relatively uniform during the entire reaction time. Formation of C₂ and C₃ hydrocarbons was

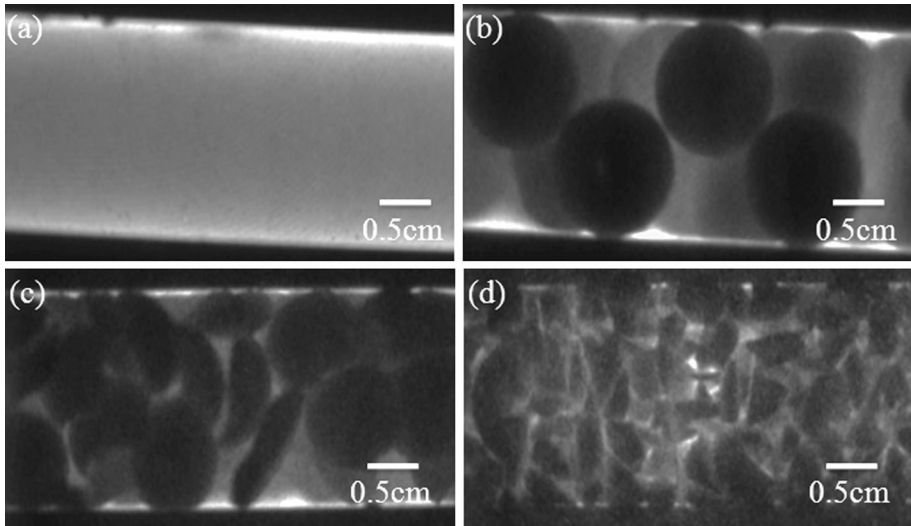
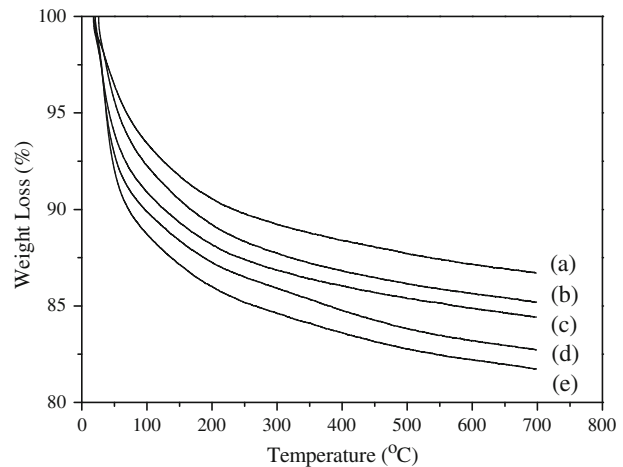


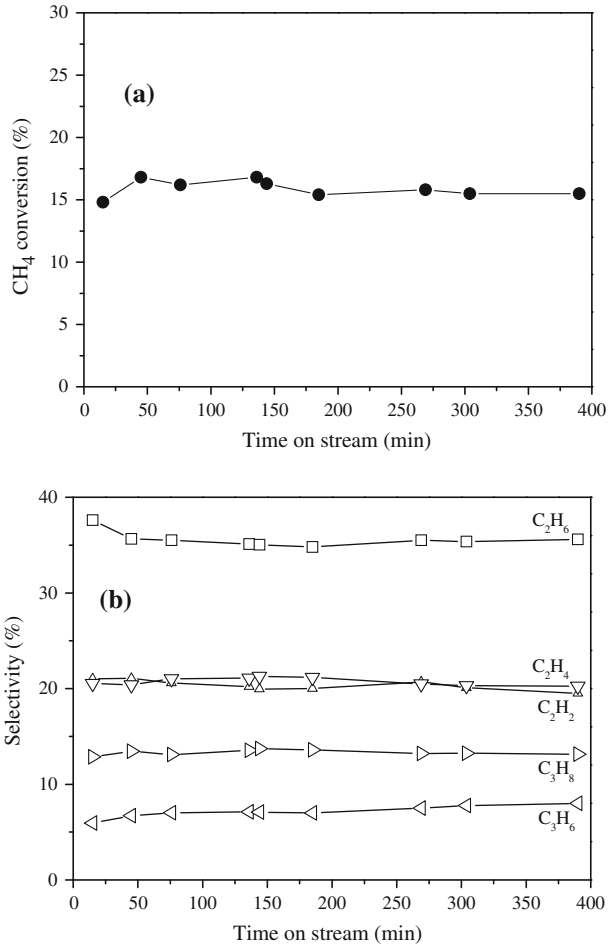
Fig. 7 ICCD images of $\text{MgO}/\text{Al}_2\text{O}_3$ in a plasma; with different catalyst particle sizes: **a** w/o catalyst, **b** 1.75 mm, **c** 1 mm, and **d** 0.5 mm

Fig. 8 TGA profiles of $\text{MgO}/\text{Al}_2\text{O}_3$ catalysts with different particle sizes: **a** Fresh 1.75 mm, **b** 1.75 mm, **c** 1 mm, **d** 0.5 mm and **e** 0.25 mm used, respectively



predominant; with negligible production of other hydrocarbons. However, the total carbon balance of the products was only about 70 %, indicating that a lot of methane was converted to solid carbon species during the reaction. Carbon deposition on the reactor wall was also observed and carbon species deposited on the catalyst was confirmed by TGA analysis of the used catalyst. A lower carbon balance was obtained when catalyst of smaller particle size was used. This means that the formation of solid carbon was favored by increasing the interaction between reactants and the catalyst surface. We have not yet determined whether the solid product was coming from the polymerization of acetylene, ethylene, and propylene; or was formed by the agglomeration of monomolecular, active carbon species. Acetylene and propylene are well-known solid-carbon precursors during

Fig. 9 Time-on-stream over MgO/Al₂O₃ catalyst (0.5 mm particle size) for plasma-assisted methane conversion at 6 kV and 3 kHz generating 3.4 W of discharge power



pyrolysis (combustion process). It seems that a similar phenomenon occurred in this plasma process. Further studies are required to explain the reasons for this result.

Effect of Feed Flow Rate

Figure 10 shows the influence of the feed gas flow-rate on the reaction result. MgO/Al₂O₃ was used as a catalyst in plasma. Variation of the flow rate changed the conversion of methane; as well as selectivity for products. At high flow rates, the conversion of methane was very low due to the short contact time of gas with the catalyst. This indicates that higher conversion of methane can be achieved by lowering the flow rate. At lower flow rates, the molecules stayed in the plasma longer and had more chances to collide with energetic species such as electrons. This caused an increase in methane conversion [37]. Formation of CH₃ radicals is initiated from the reaction of methane and electrons in the early stage of the plasma reaction; leading to abundant amounts of methyl radicals and to formation of ethane. It has been reported that CH_x fragments are formed first by dissociation of CH₄ via collision with metastable Ar, and then ethylene and acetylene can be

Fig. 10 Effect of feed flow-rate on the catalytic performance of MgO/Al₂O₃ (0.5 mm particle size) for plasma-assisted, methane conversion at 6 kV and 3 kHz

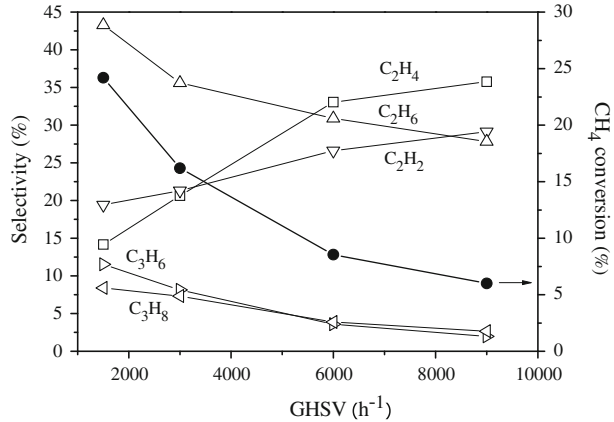
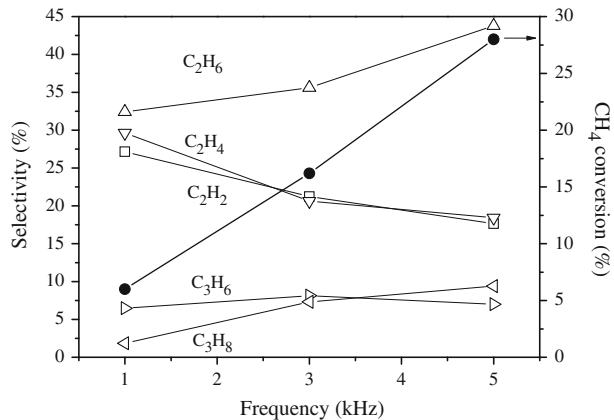


Fig. 11 Effect of frequency on the catalytic performance of MgO/Al₂O₃ (0.5 mm particle size) for plasma-assisted methane conversion at 6 kV



formed via recombination [38]. Moreover, the reaction of CH₃ with an 'H' or electron is also able to produce other radical species (e.g., CH₂ and H₂) [37, 39]. The homologous reaction of CH₂ leads to the formation of ethylene. Because electron collisions with molecules are faster than collisions with ions or radicals [40, 41], longer residence time of molecules in the plasma will produce larger amounts of ethane and will inhibit formation of ethylene.

Effect of Frequency of the Alternating Current

Figure 11 shows the effect of the frequency of the alternating current, on the methane conversion reaction using MgO/Al₂O₃ catalyst. The frequency of the alternating current had a significant effect on the conversion of methane. Methane conversion increased with increasing frequency. High frequency implies application of a large amount of energy. When large amounts of power are supplied, the concentration of high-energy species increases in the plasma zone. These are easily able to break the chemical bonds of methane. Therefore, conversion of methane may be increased by increasing the power applied. Selectivity for products also varied according to the frequency. Selectivity for

acetylene and ethylene was high at a low frequency. As frequency increased, selectivity for ethane increased; while selectivity for acetylene and ethylene decreased.

Conclusions

Methane activation over Al_2O_3 , $\text{MgO}/\text{Al}_2\text{O}_3$, and $\text{TiO}_2/\text{Al}_2\text{O}_3$ catalysts was carried out in a DBD reactor. The conversion of methane over the catalysts was greater than in the absence of catalyst. In all cases, C_2 hydrocarbons were the dominant products. The loading of MgO or TiO_2 on Al_2O_3 increased the conversion of methane; as well as the selectivity for C_3 hydrocarbons. The particle size of the catalyst used had a considerable effect on the conversion of methane; as well as on the selectivity for products. Higher conversion of methane, and higher selectivity for acetylene, ethylene, and propylene; was obtained with a smaller particle size of the catalyst, but more deposition of solid carbon species also occurred. Greater conversion of methane was achieved by supplying more energy to the DBD reactor, by lowering the flow rate, and by increasing the frequency of the alternating current. Selectivity for acetylene and ethylene was enhanced by supplying less energy, by increasing the flow rate, and by decreasing the frequency of the alternating current.

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