



Investigation of SPR sensor for immunoglobulin detection by using Ag–Si₃N₄–BP on the sensing layer

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Abstract

Surface plasmon resonance (SPR) has gained attention as a promising method for effective label-free biosensing. Immunoglobulin (IgG) detection is very important to understand the past infection and immunity of any individual. Thus, this study aims to develop a SPR sensor with better sensitivity for detecting IgG. It emphasizes the utilization of a high-performance planar waveguide-based SPR sensor to detect IgG by analyzing a suitable sensor topology. The sensor configuration consists of five distinct layers: silver (Ag), silicon nitride (Si₃N₄), black phosphorus (BP), an enzyme, and a sensing medium. Silver (Ag) stimulates surface plasmons, while Si₃N₄ and BP are utilized to enhance absorption capabilities and serve as the bio-molecular recognition element, respectively. The proposed sensor simulation employs the transfer matrix method and an angular interrogation scheme. To assess this proposed sensor's impact, the sensing region is assessed while considering three layers: Ag, Ag-BP, and Ag–Si₃N₄. Initially, the thickness of the Ag layer is optimized by recording its transmittance and achieving a minimum transmittance of 0.0027 at a thickness of 50 nm. Subsequently, the performance parameters are assessed using four different structures with slight variations in the IgG samples. The results depict the maximum achieved sensitivities as follows: 192 °/RIU for conventional SPR, 203 °/RIU for BP-based SPR, 287 °/RIU for Si₃N₄-based SPR, and 352 °/RIU for the proposed structure. This comparative study demonstrates that the proposed SPR configuration significantly enhances sensitivity, quality factor, and detection accuracy performance.

Keywords Surface plasmon resonance · Immunoglobulin · Black phosphorus · Label free · Silicon nitride · Sensitivity · Transfer matrix method

1 Introduction

White blood cells include Immunoglobulin (IgG) glycoprotein molecules generated by plasma cells and offer infection protection. It can quickly identify viruses or bacteria. X-linked agammaglobulinemia and common variable immunodeficiency syndrome are two autoimmune and immunodeficiency illnesses for which IgG testing is crucial for the diagnosis. Therefore, the detection of IgG is a crucial regime of biosensing. In recent times,

IgG has been detected in the work by using a variety of techniques, including surface plasmon resonance (SPR), electrophoresis, radial immunodiffusion, and immunoblotting (Wu et al. 2016). A technologically advanced analytical instrument, the biosensor is capable of detecting minute biomolecules at low concentrations. For instance, the photonic crystal structure has been utilized in various ways to demonstrate biosensing applications (Yang et al. 2023; Najafgholinezhad and Olyaei 2014; Olyaei and Bahabady 2015; Bahabady and Olyaei 2015; Parandin et al. 2021; Gowdhami et al. 2022). However, detecting extremely low amounts of antibodies like IgG is a challenge for biosensors (Wu et al. 2016). Fortunately, the label-free nature of SPR biosensors makes them a promising tool. Furthermore, it offers the benefits of swift and precise detection, along with reliability. (Ravindran et al. 2023; Uniyal et al. 2023; Mudgal et al. 2023). SPR biosensors are now studied and investigated by using various structures and configurations (Bahri et al. 2022; Ebadi et al. 2020; Ben Salah et al. 2022a, b; Mao et al. 2017). Hence, it is vital to understand the basic classification of these sensors. Based on the coupling, these sensors are categorized into four types such as prism, optical fiber, waveguide, and grating-based.

Nowadays, the planar waveguide-based SPR sensor has also become popular in the detection of bio-molecular interactions like Deoxyribonucleic acid (DNA) and IgG (Mondal et al. 2023). SPR theory demonstrates that the optical light incident on the waveguide-metal interface at an angle greater than the critical angle. The light metal interaction leads to the generation of surface plasmons polaritons (SPPs). Further, the SPP oscillations set a surface plasmon wave (SPW) at the interface by applying the attenuated total reflection (ATR) (Homola et al. 1999). The SPW excites the evanescent waves, which exponentially decay in the orthogonal direction of the interface (Lee et al. 2007). These decaying waves are used for sensing the presence of bio-molecules at the sensor surface. However, prism-based sensor configurations were also utilized for similar applications due to simplicity, immunity to noise, and high sensitivity (Janith et al. 2023; Kushwaha et al. 2018a; Mudgal et al. 2020a).

On the other hand, distributed coupling can be used in a metal-coated waveguide as it offers better design flexibility and monolithic integration capabilities with existing SPR technology (Lavers et al. 2020; Kim et al. 2018). The ability to build compact, monolithic, and multi-sensor systems is specially provided by a planar waveguide (PWG) and is connected to instruments by using optical fibers. Additionally, these biosensors can be miniaturized to detect chemicals or biological agents in inaccessible places (Mukundan et al. 2009). PWG-based sensors feature a unique platform that enables the detection of a wide variety of samples in conjunction with imaging systems (Moazzuzaman et al. 2021; Cherouana et al. 2023). Moreover, they possess the potential for integration with optoelectronic components and the capacity to adjust the penetration depth of the evanescent field by varying the reflection angle. (Agnarsson et al. 2010). The inclusion of PWG with the SPR phenomenon leads to resonance oscillations of SPWs (Kashyap and Nemova 2009). As a result, minimal transmittance (T_{\min}) occurs, which changes with the refractive index (RI) of the sensor surface and can be calculated using ATR (Pal et al. 2018). In general, to develop an SPR structure, a metal film comprising gold (Au) and silver (Ag) is typically deposited over the waveguide to facilitate Surface Plasmon (SP) propagation. Due to its high SPR ratio ($|\epsilon_r/\epsilon_i|$), Ag offers superior SPR performance, where ϵ_r and ϵ_i are the real and imaginary parts of the dielectric constant respectively (Sheng et al. 2019; Amirjani and Haghshenas 2018). In comparison to Au, Ag exhibits a steeper angular resonance curve, which indicates greater detection precision (Mitsushio et al. 2006; Beck et al. 2023). However, Ag lacks chemical stability, as evidenced by its quick oxidation (Jha and Sharma 2009). The inclusion of bimetallic, oxide, dielectric, and self-assembled monolayers can

prevent Ag from oxidation and sulfurization (Han et al. 2020). Preservation of Ag surfaces can be achieved through a self-assembled monolayer (SAM), which also enhances sample adherence to metal surfaces (Gahlaut et al. 2022). Dielectric materials can improve SPR performance, but it is difficult to preserve their intricate shape and optical characteristics. Some researchers have developed a hybrid structure with bimolecular recognizing elements (BREs) that offer excellent SPR performance (Yun et al. 2022; Hanson and Whelan 2023). In this work, a structure based on silicon nitride (Si_3N_4) has been presented to enhance the sensing capability of the sensor. The Si_3N_4 layer on top of the silver layer, provides immunity against oxidation. Moreover, the high refractive index of Si_3N_4 imparts excellent chemical, thermal, and biocompatibility qualities (Wu et al. 2016; Mudgal et al. 2022). To further enhance the sensing capability, two-dimensional (2D) materials like black phosphorus (BP) have been placed over the dielectric material, where they can act as a bio-molecular carrier as well as a protective layer. The unique mechanical and optoelectrical properties of BP, like higher bandgap, made it one of the most popular 2D materials in photonic sensors. In addition, BP boosts detection capabilities by enhancing interlayer coupling within the Van der Waals force. The higher absorption energy of BP makes it one of the potential candidates to be used for biomolecule binding (Nangare and Patil 2023).

In 2018, Kushwaha et al. introduced an SPR sensor for IgG detection that incorporated zinc oxide, gold, MoS_2 , and Graphene, achieving a sensitivity of $101.5^\circ/\text{RIU}$ (Kushwaha et al. 2018b). Following this, in 2020, Mudgal et al. enhanced the sensitivity of the SPR sensor using zinc oxide, bimetallic materials, BiTiO_2 , and graphene, reaching a sensitivity of $116.6^\circ/\text{RIU}$ (Mudgal et al. 2020a). Raikwar et al. in 2018 explored sensors based on gold and graphene oxide, attaining a sensitivity (S) of $143^\circ/\text{RIU}$, a detection accuracy (DA) of 0.16, and a quality factor (QF) of 23.72 RIU^{-1} (Raikwar et al. 2020). Furthermore, Singh et al. in 2020 reported improved sensor performance by incorporating gold, blue phosphorus, MoS_2 , and antimonide, achieving an S of $198^\circ/\text{RIU}$ and a DA of 0.15 (Singh et al. 2020).

Despite the various techniques and methods proposed for IgG detection, a strong demand remains for high-performance sensor technology in this field. This paper introduces an investigation of an SPR structure consisting of Ag, Si_3N_4 , and BP to detect IgG using the transfer matrix method at a wavelength of 633 nm. The Ag layer is used due to its higher SPR ratio and provides better sensitivity as a substrate layer (Mudgal et al. 2020b). However, in the presence of biomolecules Ag gets oxidized, and hence reduces the lifetime of SPR biosensors (Qu et al. 2020). To overcome the oxidation issue, an anti-reflecting layer of Si_3N_4 is placed over it. Si_3N_4 got the attention because of its excellent chemical and thermal stability with a band gap of $\sim 5 \text{ eV}$ (Blázquez et al. 2014). Finally, a layer of BP is considered because of its ability to improve the adsorption rates, which is due to higher carrier mobility, interesting optical and electrical properties, and direct band gap (Blázquez et al. 2014).

The above brief survey of the literature reveals that dielectric materials, while capable of enhancing SPR performance, face challenges in maintaining their intricate shape and optical characteristics. Researchers have introduced a hybrid structure incorporating BREs for superior SPR performance. This work attempts to bring depth and novelty to the investigation of BRE-based structures by proposing a multilayer structure for the detection of IgG. Literature has not widely explored the effect of different configurations of hybrid structures. To evaluate the influence of the suggested sensor, an analysis of the sensing area is conducted, taking into account three layers: Ag, Ag-BP, and Ag- Si_3N_4 . Each layer has a predefined role in the functioning of this biosensor. For instance, Si_3N_4 is utilized to boost sensing capability. To further elevate sensing capabilities, two-dimensional (2D) materials

like black phosphorus (BP) have been applied over the dielectric material, serving as a bio-molecular carrier and protective layer.

The remainder of this article is structured into several sections as follows. Section 2 sheds light on various aspects of design considerations, including transmitting power, reflectivity, and performance parameters. Section 3 begins by presenting the scheme for optimizing the thickness of the sensing layer, followed by an analysis of the sensor's performance. The final subsection in this section highlights a comparison of this work with similar studies that have been reported. Finally, the last section, Sect. 4, concludes this work by emphasizing the significant findings of this study and discussing its potential future prospects.

2 Design considerations

This section explicates the proposed planar waveguide-based SPR sensor's design and analysis process, including mathematical equations and design parameters.

2.1 Transmitting power

Figure 1 shows the schematic of the considered PWG-based SPR sensor for IgG detection. The overall structure is divided into two sections: initially, a lossless single-mode single-layer waveguide is employed as the initial component to couple the incident light and generate surface plasmons (SPs). This segment is positioned at the exposed portion of the waveguide. In the second segment, the structure interacts with the test samples. The primary design constraints for a PWG-based SPR sensor include the appropriate substrate material and operating wavelength. The phase matching between waveguide and SP modes is attained due to the low-index glass substrate when the sensor operates in a liquid RI medium. To facilitate the fabrication of waveguides and to cut down the cost of raw slides, the substrate glass having an RI of 1.46 can be used (Rahman et al. 2017). Conversely, the investigation of a PWG SPR sensor is prompted by the stability and inertness of the metal layer to the external environment (Duvencek et al. 1997). However, the sensor's performance diminishes when there are changes in the optical properties of the metal film.

To create this biosensor (Raikwar et al. 2020), a dielectric slab was introduced between two layers with lower refractive indices. Both instances utilized the well-known optical phenomenon called Total Internal Reflection (TIR) to propagate and guide light along the

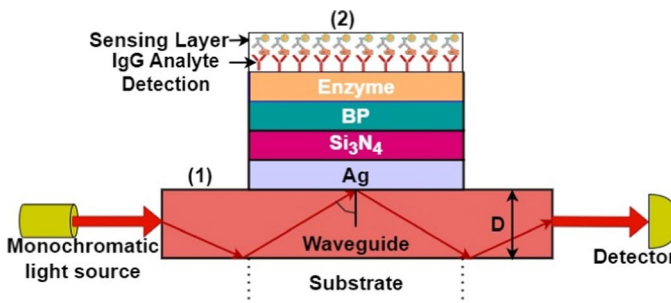


Fig. 1 Schematic of the proposed PWG-based SPR sensor

core. In this proposed setup, the first layer consisted of a waveguide with Ag immobilization, having a diameter represented as 'D.' Additionally, the third layer was composed of Si_3N_4 , while the fourth and fifth layers were formed by BP and ELISA:OPD enzymes, respectively. The respective thicknesses of the layers of Ag, Si_3N_4 , BP, and enzyme were denoted as d_2 , d_3 , d_4 , and d_5 . A light source was employed to emit a light beam with a central wavelength of 633 nm, which triggered surface plasmon polaritons (SPP) at the interface between the waveguide and the metal. The collected light was then directed to a spectrometer on the opposite side for analysis. Considering that a beam of power, P is launched at an angle of θ , and at the spectrometer, a power of dP is collected at an angle of $d\theta$. Then, the mathematical expression for dP can be written as (Loan et al. 2014; Diéguez et al. 2009);

$$dP \propto P(\theta)d\theta \quad (1)$$

where $P(\theta)$ is the modal power proportional to the incident angle which is mathematically manifested in Eq. (2) (Hossain et al. 2021).

$$d\theta = \frac{n_c^2 \sin \theta \cos \theta}{(1 - n_c^2 \cos^2 \theta)^2} \quad (2)$$

where n_c is the RI of the core waveguide.

Furthermore, by using the reflectance value of the waveguide and metal interface, the normalized transmitted power for a single reflection can be written as (Hossain et al. 2021)

$$P_{\text{trans}} = \frac{\int_{\theta_{\text{cr}}}^{\pi/2} R_p^{N_{\text{ref}}(\theta)} P(\theta) d\theta}{\int_{\theta_{\text{cr}}}^{\pi/2} P(\theta) d\theta} \quad (3)$$

where $N_{\text{ref}}(\theta) = \frac{L}{D} \tan \theta$ is the summation of light reflections in the device, θ is the incident angle with the normal to the core metal layer interface in the sensing region of length L , and D is the diameter of the waveguide (Hossain et al. 2021). The transmitting power responses are plotted for the proposed structure by exploiting the angular interrogation technique to assess the sensor's performance. To investigate the structure RI of the designed parameters taken into consideration, such as Ag of $0.056206 + 4.2776i$ (Beck et al. 2023), Si_3N_4 of 2.0394 (Wu et al. 2016; Gahlaut et al. 2022), BP of $(3.5 + 0.1i)$ (Hossain et al. 2021), and an enzyme of $1.8 + 0.3i$ (Wu et al. 2016). The thickness of the metallic layer is optimized by following the iteration approach, whereas the thicknesses of Si_3N_4 , BP, and enzyme layers are 5 nm, 0.53 nm, and 0.11 nm, respectively (Mudgal et al. 2022; Nangare and Patil 2023). Finally, the topmost layer of the sensor comprises the sensing medium in the presence of IgG with RI of 1.343 and 1.353 (Wu et al. 2016).

2.2 Reflectivity

Since the transfer matrix method (TMM) is an effective method that doesn't require any estimates, it is used to measure the reflectivity (R_p) of an N-layered structure. Here, the thickness and dielectric constant of the k^{th} layer along the z-axis are represented by d_k and ϵ_k , respectively. Additionally, the tangential fields derived by linking the boundary conditions (perfectly matched layers i.e. PML are used as boundary conditions with a meshing of

0.029 μm in both directions) demonstrate the relationship between the initial ($Z = Z_1 = 0$) and final ($Z = Z_{N-1}$) conditions as given in Eq. (4) (Nangare and Patil 2023):

$$\begin{bmatrix} P_1 \\ Q_1 \end{bmatrix} = H \begin{bmatrix} P_{N-1} \\ Q_{N-1} \end{bmatrix} \tag{4}$$

where, P_{N-1} , Q_{N-1} , P_1 , and Q_1 signify the N^{th} boundary tangential electrical and magnetic (EM) fields and the fields at the first layer boundary, respectively. The expression for the characteristics matrix (H_{ij}) of the proposed structure in the presence of a monochromatic light source with TM polarization is discussed in Eq. (5) (Yun et al. 2022). Furthermore, the transverse RI (l_k) and arbitrary stage constant (β_k) for the k^{th} layer are given by Eq. (6) and (7), respectively. The evaluation of wave impedance (Z_k) and input angle (θ_k) can be done by using Eq. (8) and (9), respectively.

$$H_{ij} = \left[\prod_{k=1}^{N-1} \begin{pmatrix} \cos \beta_k & -i\epsilon_k \sin \beta_k / \epsilon_k \\ -i\epsilon_k \sin \beta_k & \cos \beta_k \end{pmatrix} \right] = \begin{bmatrix} H_{11} & H_{12} \\ H_{21} & H_{22} \end{bmatrix} \tag{5}$$

where

$$l_k = \left[\frac{\mu_k}{\epsilon_k} \right]^{1/2} \cos \theta_k = \sqrt{\frac{\epsilon_k - (n_c \sin \theta)^2}{\epsilon_k^2}} \tag{6}$$

and

$$\beta_k = \frac{2\pi}{\lambda} l_k \cos \theta_k (Z_k - Z_{k-1}) = \frac{2\pi}{\lambda} d_k \sqrt{\epsilon_k - (n_c \sin \theta)^2} \tag{7}$$

$$Z_k = \frac{k_x l_k \cos \theta_k}{(2\pi c / \lambda_{633}) \epsilon_k^2} \tag{8}$$

$$\theta_k = \left(\cos \sqrt{1 - (l_{k-1} / l_k) (\sin \theta)^2} \right)^{-1} \tag{9}$$

Parameters λ , μ_k , $\overline{k_x}$ and θ represent the wavelength, permeability, incident wave vector, and incident angle, respectively. The expression for calculating the reflection coefficient (r_p) and the Fresnel’s mode (R_p) is described in Eq. (10) and (11), respectively:

$$r_p = \frac{(H_{11} + H_{12}l_n) - (H_{21} + H_{22}l_n)}{(H_{11} + H_{12}l_n) + (H_{21} + H_{22}l_n)} \tag{10}$$

$$R_p = |r_p|^2 \tag{11}$$

Here it is pertinent to note that the third-dimensional thickness of the suggested structure is considerably greater than the feature size within the computational plane (2D). Consequently, the impact of substrate thickness on the obtained outcomes can be disregarded by assuming, through mathematical means, that the structure is infinite in the third dimension (Ben Salah et al. 2019; Chao et al. 2021). As a result, all our

simulations are conducted in 2D, allowing for a substantial reduction in computational time without sacrificing calculation accuracy.

2.3 Performance parameters

In general, the performance of the SPR sensor is analyzed in terms of Sensitivity (S), Quality Factor (QF), and Detection Accuracy (DA). Parameter S is the ratio of change in resonance angle ($\nabla\theta_{res}$) to the RI (∇n). The width of the SPR spectrum in context to 50% of maximum transmittance is known as Full Width at Half Maximum (FWHM). The ratio of sensitivity to FWHM describes QF. The ratio of $\nabla\theta_{res}$ and FWHM gives the value of DA. In addition, we have also evaluated the dip-figure of merit (DFOM), which is the ratio of S and minimum transmittance (T_{min}). The mathematical formulation of the parameters as mentioned earlier is given in Eqs. (12–15) (Han et al. 2020).

$$\text{Sensitivity (S)} = \frac{\text{Change in resonance angle } (\nabla\theta_{res})_o}{\text{Change in refractive index } (\nabla n)} / \text{RIU} \quad (12)$$

$$\text{QF} = \frac{S}{\text{Full width half maximum (FWHM)}} (\text{RIU}^{-1}) \quad (13)$$

$$\text{DA} = \frac{\nabla\theta_{res}}{\text{FWHM}} \quad (14)$$

$$\text{DFOM} = \frac{S}{T_{min}} \quad (15)$$

3 Results

3.1 Optimization of Ag thickness

To achieve the best performance of the structure, it's necessary to optimize the thickness of the Ag (silver) film. This optimization aims to maximize the absorption of energy from the optical signal, which is indicated by achieving minimum transmittance (T_{min}) performance (Sheng et al. 2019). Figure 2 depicts the transmittance responses for various Ag film thicknesses, ranging from 40 to 60 nm in 5 nm increments. Table 1 contains the estimated values of T_{min} and resonance angle (θ_{res}) for the data in Fig. 2. Notably, the lowest T_{min} value of 0.0027 and a θ_{res} of 81.10° are achieved when the Ag film thickness is 50 nm. As the thickness of the Ag film changes, θ_{res} shifts right, indicating that the proposed sensor exhibits Surface Plasmon Resonance (SPR) properties (Amirjani and Haghshenas 2018). Consequently, an Ag film thickness of 50 nm has been selected for further analysis of the proposed sensor.

Fig. 2 Transmittance responses for the proposed sensor at different Ag thicknesses

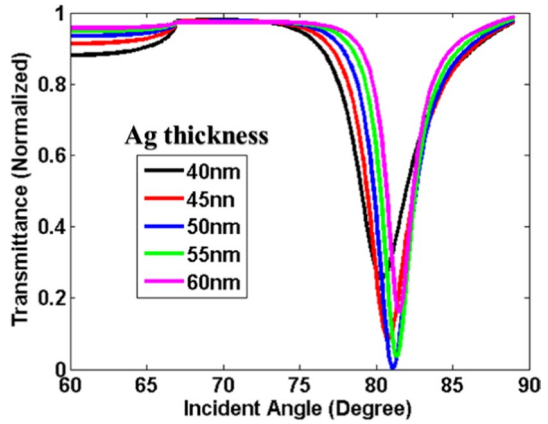


Table 1 Transmittance and resolution angle versus Ag thicknesses

| Ag thickness | T_{min} | θ_{res} (°) |
|--------------|-----------|--------------------|
| 40 nm | 0.2546 | 80.35 |
| 45 nm | 0.0850 | 80.80 |
| 50 nm | 0.0027 | 81.10 |
| 55 nm | 0.0349 | 81.34 |
| 60 nm | 0.1605 | 81.48 |

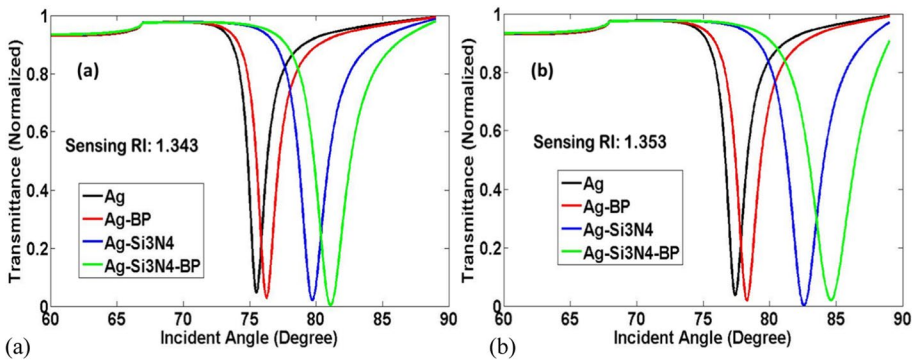


Fig. 3 Transmittance responses for all considered structures at sensing RI: **a** 1.343 and **b** 1.353

3.2 Sensing performance analysis

The impact of the proposed structure is assessed by comparing its performance to that of three other structures: Ag, Ag-BP, and Ag-Si₃N₄. In Fig. 3a and b, the transmittance responses of all these structures are displayed under sensing medium refractive indices (RIs) of 1.343 and 1.353, respectively. As the number of layers increases, the spectral width widens due to a damping effect. Specifically, the Full Width at Half Maximum (FWHM) values are 1.46, 1.68, 2.25, and 2.70 degrees for Ag, Ag-BP, Ag-Si₃N₄, and the

Table 2 Assessed parameters of θ_{res} , $\nabla\theta_{\text{res}}$ and ∇n for Fig. 3a and b

| Structure | $\theta_{\text{res}} (^{\circ})$ | | $\nabla\theta_{\text{res}} (^{\circ})$ | ∇n |
|---------------------------------------|----------------------------------|---------------|--|------------|
| | $n_s = 1.343$ | $n_s = 1.353$ | | |
| Ag | 75.50 | 77.42 | 1.92 | 0.01 |
| Ag-BP | 76.26 | 78.29 | 2.03 | 0.01 |
| Ag-Si ₃ N ₄ | 79.71 | 82.58 | 2.87 | 0.01 |
| Ag-Si ₃ N ₄ -BP | 81.10 | 84.62 | 3.52 | 0.01 |

Table 3 Measured parameters of S, QF, DA and DFOM for Fig. 3a and b

| Structure | Sensitivity ($^{\circ}/\text{RIU}$) | QF (RIU^{-1}) | DA | DFOM |
|---------------------------------------|---------------------------------------|--------------------------|------|-----------|
| Ag | 192 | 131.51 | 1.31 | 4120.17 |
| Ag-BP | 203 | 120.83 | 1.21 | 7024.22 |
| Ag-Si ₃ N ₄ | 287 | 127.55 | 1.27 | 14422.11 |
| Ag-Si ₃ N ₄ -BP | 352 | 130.37 | 1.30 | 130370.37 |

proposed structure, respectively. The sensing of the analyte is carried out in two steps: in the first step, an RI of 1.343 is considered in the sensing medium, and transmittance curves for Ag, Ag-BP, Ag-Si₃N₄, and Ag-Si₃N₄-BP are plotted in Fig. 3a. For all the combinations the incident angle varied from 75.50 to 81.10°. Secondly, the transmittance curves are recorded for all the aforementioned structure combinations and the incident angle varies from 77.42 to 84.62°, and plotted in Fig. 3b.

The trend of T_{min} values is inversely proportional to the number of layers, resulting from variations in penetration lengths at the waveguide-metal interface. The obtained T_{min} values for Ag, Ag-BP, Ag-Si₃N₄, and the proposed structure are as follows: for Fig. 3a, they are 0.0466, 0.0289, 0.0199, and 0.0027, respectively. Similarly, in Fig. 3b, the T_{min} values are 0.0366, 0.0187, 0.0011, and 0.0203 for Ag, Ag-BP, Ag-Si₃N₄, and the proposed structure, respectively.

Resonance angles and their changes for Fig. 3 are detailed in Table 2. Furthermore, parameters related to SPR, such as Sensitivity (S), Quality Factor (QF), Detection Accuracy (DA), and Dip- Figure of Merit (DFOM), are evaluated using Eqs. (12–15) and are presented in Table 3. Notably, the proposed structure, Ag-Si₃N₄-BP, achieves the highest sensitivity of 352 °/RIU, surpassing conventional Ag, Ag-BP, and Ag-Si₃N₄ by 1.85, 1.73, and 1.23 times, respectively. This exceptional performance is attributed to the strong absorption capabilities of Si₃N₄ and BP (Homola et al. 1999; Mudgal et al. 2022). The proposed sensor configuration also provides wavelength flexibility, enhanced resolution, reduced cross-sensitivity, biocompatibility, longer lifetime, minimal signal damping, and improved integration. The layer of Si₃N₄ is also used to attain the anti-reflecting behavior that further resists the oxidation of Ag. Additionally, the performance improvement is due to the excellent optical properties and higher SPR ratio of Ag to confine SP to deep sub-wavelength and leading to sensitivity enhancement.

The QF and DA performances of the proposed structure are nearly on par with the conventional sensor due to the sharp resonance dip of Ag. They are approximately 1.07 and 1.02 times greater than the Ag-BP and Ag-Si₃N₄ structures, respectively. Moreover, the proposed structure boasts the highest DFOM, standing at 130,370.37. This value is significantly higher, being 31.64 times greater than the conventional structure, 18.56 times

Fig. 4 Graphical representation of sensitivity and DFOM with respect to the structures

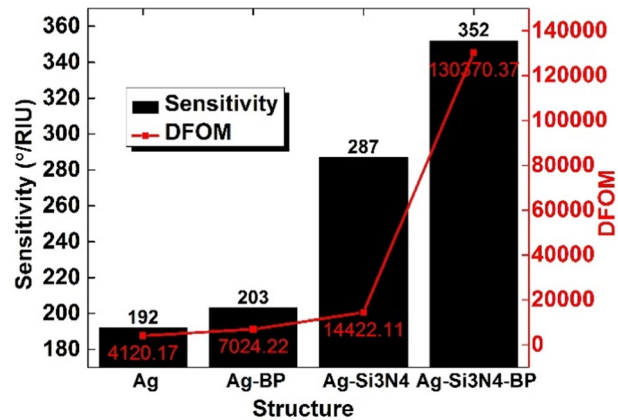
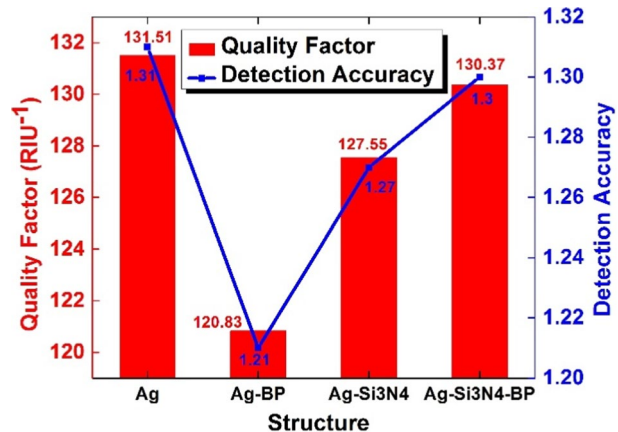


Fig. 5 Plots of QF and DA w.r.t the structures

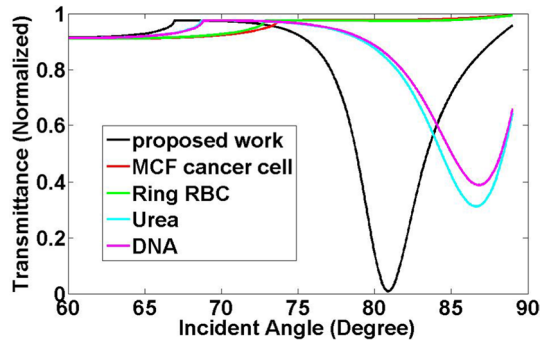


greater than Ag-BP, and 9.04 times greater than Ag-Si₃N₄. For a visual representation of the SPR performance, including sensitivity and DFOM, please refer to Fig. 4. Additionally, Fig. 5 provides a graphical representation of the assessed QF and DA values for all structures. The QF and DA performances of the proposed structure are almost equal to the conventional sensor because of the sharp resonance dip of Ag. They are approximately 1.07 and 1.02 times greater than those of the Ag-BP and Ag-Si₃N₄ structures, respectively.

Similarly, the proposed structure has achieved the highest DFOM of 130370.37, which is 31.64, 18.56, and 9.04 times greater than the conventional, Ag-BP and Ag-Si₃N₄, respectively. The graphical representation of the computed SPR performance of sensitivity and DFOM for all structures is mentioned in Fig. 4. The representation of assessed QF and DA is provided in Fig. 5.

In addition, the selectivity test of the proposed sensor is also carried out in the presence of IgG, MCF cancer cells ($n=1.401$), ring red blood cells (RBC) ($n=1.395$), urea ($n=1.36$) and DNA ($n=1.361$). The selectivity test is done by recording the transmittance curve for all the used biomolecules as shown in Fig. 6. From the results, it can be observed that the transmittance for IgG molecules is nearly $<1\%$ which is due to the presence of a specific enzyme. However, for other biomolecules, the transmittance is nearly $>30\%$.

Fig. 6 Selectivity test of the proposed sensor



It may be relevant to mention here that in practical cases, plasmonic losses and fabrication imperfections play an important role in the sensor performance. In the context of planar waveguides, a crucial aspect is managing signal dispersion, particularly regarding the waveguide height, which is required to be above 200 nm. At greater heights, dispersion patterns align across frequencies, while at smaller heights, variations in dispersion curves become more pronounced (Syms and Solymar 2014). Achieving optimal waveguide thickness is essential for precise mode confinement. During fabrication, meticulous attention to layer deposition is necessary to prevent air bubbles and ensure a uniform distribution of metallic layers. Non-uniform distribution may lead to scattering, compromising the comprehensive confinement of optical signals and potentially reducing sensor performance.

3.3 Comparative study analysis

Finally, the performance of the proposed sensor is compared with recent existing sensors and reported in Table 4. This study reveals that the proposed sensor outperforms existing sensors in terms of Sensitivity (S), Quality Factor (QF), and Detection Accuracy (DA). The attained performance parameters are S of $352^\circ/\text{RIU}$, QF of 130.37RIU^{-1} and DA of 1.30. Moreover, the proposed work has evaluated the performance of DFOM as a new SPR parameter and found that the maximum DFOM is 130370.37. Therefore, it can be concluded that the proposed PWG-based SPR sensor contributes a better SPR performance by utilizing the structure of Ag-Si₃N₄-BP to detect the bio-molecular interaction.

4 Conclusion

A high-performance planar waveguide-based SPR sensor for IgG detection has been presented in this work. The sensor structure consists of five layers: waveguide, Ag, BP, enzyme layer and sensing medium. To assess the impact of different design elements, three additional structures were investigated for performance analysis. The optimization process focused on the Ag thickness, leading to a minimum transmittance of 0.0027 achieved at an Ag thickness of 50 nm. Furthermore, the performance parameters were systematically analyzed across the four considered structures, considering minimal variations in IgG samples. Results show that the proposed structure, having Ag-Si₃N₄-BP as main constituents, has accomplished the highest sensitivity, 1.85, 1.73, and 1.23 times greater than the conventional Ag, Ag-BP and Ag-Si₃N₄, respectively. The comparative study with existing sensor

Table 4 Comparative study of the proposed and existing sensors

| References | Structure | Sensitivity ($^{\circ}$ /RIU) | QF (RIU $^{-1}$) | DA | DFOM |
|----------------------------|--|--------------------------------|-------------------|------|-----------|
| Kushwaha et al. (2018a) | Zinc Oxide–Au–MoS ₂ –Graphene | 101.5 | – | – | – |
| Mudgal et al. (2020a) | Bimetallic–BiTiO ₂ –Graphene | 116.6 | – | – | – |
| Raikwar et al. (2020) | Au–Graphene Oxide | 143 | 23.71 | 0.16 | – |
| Singh et al. (2020) | Au–blueP–MoS ₂ –Anti–monene | 194.8 | – | 0.15 | – |
| Karki et al. (2022) | Prism–Ag–MXene–ZnO–Graphene | 136.50 | 38.7 | – | – |
| Islam et al. (2022) | Prism–Cr–Ag–BP–Graphene Oxide | 352 | 76.48 | – | – |
| Muthumanicam et al. (2023) | TiO ₂ –Cu–BaTiO ₃ | 552 | 136.97 | 0.27 | – |
| Rumi et al. (2024) | Al/BTO/Al/MoS ₂ | 262 | – | 1.64 | – |
| Akib et al. (2024) | CaF ₂ –Cu–BP–Graphene | 410 | 94.25 | 0.47 | 91.87 |
| This work | Ag–Si ₃ N ₄ –BP | 352 | 130.37 | 1.30 | 130370.37 |

structures is also explored, and it is observed that the proposed SPR amplifies the sensitivity and heightens the DFOM performance. Therefore, these findings suggest that the proposed SPR sensor, with its superior sensitivity and DFOM, holds great promise for IgG detection in the biomedical field. Notably this work can also be extended in future to investigate surface Immunoglobulin (SI_g) densities.

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Declarations

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