

High sensitivity photonic crystal fber surface plasmon resonance sensor based on indium tin oxide

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Abstract

In this paper, we propose a high sensitivity photonic crystal fber surface plasmon resonance sensor based on indium tin oxide (ITO). We select ITO flm to improve the sensing performance. According to numerical simulation results, the maximum wavelength sensitivity of the sensor can reach 28,500 nm/RIU. It has the high wavelength resolution of 3.5×10^{-6} RIU and the refractive index detection range is 1.33–1.40. Considering the simple structure and excellent sensing performance, the sensor can detect the refractive index of liquid in a wide range and accurately detect the refractive index of liquid such as blood plasma, hemoglobin, etc.

Keywords Photonic crystal fber · Simple structure · High sensitivity · Sensor · Surface plasmon resonance

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In the past decades, there has been a great interest in the design of artifcial micro nano structure devices, such as absorbers (Qin et al. [2020\)](#page-8-0), lenses (Zhao et al. [2020\)](#page-8-1), logic gates (Ge et al. [2020\)](#page-7-0), topological waveguide devices (Hou et al. [2020](#page-8-2)) and biosensors (Wang et al. [2019\)](#page-8-3) et al. Among these optical devices, surface plasmon resonance (SPR) sensors are widely used in environmental monitoring, biochemical analysis, etc. Although the Kretschmann-Raether structure was proposed in 1968 to excite the SPR efect, the disadvantages of its structure, such as the large size, limit the miniaturization of the sensor (Kretschmann and Raether [1968](#page-8-4)). After the concept of photonic crystal being proposed in 1987, photonic crystal fber (PCF) gradually entered the vision of scientists. Due to its good transmission characteristics, researchers applied PCF to SPR sensor (Bender and Dessy [1994;](#page-7-1) Liu and Wang [2020\)](#page-8-5).

Currently, two kinds of design methods have been proposed based on PCF-SPR sensors: one is internal sensing and the other is external sensing (Ramani and Kumar [2021](#page-8-6)). In terms of internal sensing, in 2020, Liu and Ma ([2020](#page-8-7)). However, the internal sensing technology requires liquid penetration and selective metal coating, the structure and manufacturing process are both complex (Haider et al. [2018\)](#page-7-2). A simpler method is external sensing which directly coating a flm of material on the outer surface of the PCF. In 2019, Liu et al. ([2019a,](#page-8-8) [b\)](#page-8-9). proposed an eccentric nuclear photonic quasicrystal fber (PQF) sensor based on SPR with a sensitivity of 21,000 nm/RIU and in 2020, Nashaye Raf et al. ([2020\)](#page-8-10). proposed a PCF sensor based on SPR with a sensitivity of 8000 nm/RIU. However, their structures are complex and their sensitivities are relatively low.

The performance of SPR sensors is highly depend on the conductor material of the plasma layer used in the sensor. Conductor material of the plasma layer is commonly silver or gold. Compared with gold and silver, indium tin oxide (ITO) is a cheaper and better conductor. ITO also has adjustable photoelectric properties and low loss in the infrared range. So we adopted ITO as the conductor material. In 2020, Chao Liu et al. designed an ITO SPR sensor with a sensitivity of 15,000 nm/RIU(Liu [2020\)](#page-8-11). But its sensitivity is relatively low. The sensitivity of the sensor described above can be improved greatly and the structure can be simplifed.

In this paper, a high sensitivity photonic crystal fber (PCF) surface plasmon resonance sensor based on indium tin oxide (ITO) is proposed. By using single air hole size type, the sensor structure is greatly simplifed with only four air holes which are easy to manufacture. By optimizing the sensor structure parameters, it can achieve high sensitivity of 28,500 nm/RIU, resolution of 3.5×10^{-6} RIU and the refractive index detection range of the sensor is 1.33–1.40. Our proposed sensor can be widely used in chemical and medical felds.

2 Structural design and theoretical modeling

The cross-section model of the proposed sensor is shown in Fig. [1a](#page-2-0). We choose fused silica as the background material. Inside the perfect matching layer (PML) is the analyte layer whose thickness is 3.5 μm and the thickness of the PML is 1.5 μm which is used to absorb radiation energy (Islam et al. [2019](#page-8-12)). The thickness of the ITO flm is t.

Fig. 1 a The cross section of the proposed sensor; **b–c** The fundamental mode light feld diagram of x-pol and y-pol when RI=1.39; **d**-**e** the SPP mode light feld diagram of x-pol and y-pol when RI=1.39.

In the coverage area of the background material, there are four air holes with diameter of d which arranged in a square and the distance between air holes is Λ . Figure [1](#page-2-0)b-e show light feld diagram of the fundamental mode and SPP mode in the two polarization modes.

The dispersion relationship of the proposed sensor with the refractive index of 1.39 is shown in Fig. [2](#page-2-1). It can be seen from Fig. [2](#page-2-1) that the resonance wavelengths of two polarization modes are both at 1865 nm. Because the structure is symmetrical, the mode felds and loss spectrum are similar for both polarization modes. Therefore, in the subsequent parameter optimization process, the y-polarization mode of the structure is selected for analysis. It can be seen from Fig. [2](#page-2-1) when the incident wavelength is shorter than the resonance wavelength, the energy of the fundamental mode is well confned in the fber core. As the wavelength of the incident light increases, the fundamental mode gradually couples with the SPP mode. There is a sudden change in $Re(n_{\text{eff}})$ for both modes when the wavelength reaches the resonance wavelength, the energy of the fber core transferred to the SPP mode.

The dispersion relationship of the fused silica is calculated by Sellmeier equation (Soghra et al. [2022](#page-8-13)):

Fig. 2 a–b Dispersion relation of the fundamental mode, SPP mode, and confnement loss spectrum when n = 1.39, d = 4.1 μm, Λ = 7.6 μm and t = 50 nm

$$
n^{2}(\lambda) = 1 + \frac{B_{1}\lambda^{2}}{\lambda^{2} - C_{1}} + \frac{B_{2}\lambda^{2}}{\lambda^{2} - C_{2}} + \frac{B_{3}\lambda^{2}}{\lambda^{2} - C_{3}}
$$
(1)

In this expression, B_1 , B_2 , B_3 , C_1 , C_2 and C_3 are 0.6961663, 0.4079426, 0897479400, 0.0046791486, 0.0135120631 and 97.9340025, respectively. Here, λ is the incident light wavelength in vacuum.

The dielectric constant of ITO is expressed by Eq. [2](#page-3-0) (Liu et al. [2019a,](#page-8-8) [b](#page-8-9)):

$$
\varepsilon_m(\lambda) = \varepsilon_\infty - \frac{\lambda^2 \lambda_c}{\lambda_p^2 (\lambda_c + i\lambda)}\tag{2}
$$

In this expression, $\lambda p = 5.6497 \times 10^{-7}$ m and $\lambda c = 11.21076 \times 10^{-6}$ m are the plasmonic wavelength and collision wavelength of ITO, respectively, ε_{∞} = 3.80 is the dielectric constant for the infinite value of the frequency of ITO, and λ is the operating wavelength in micron.

The confnement loss of this sensor can be expressed by Eq. [3](#page-3-1) (Wang and Li [2019](#page-8-14)):

$$
Loss(dB/cm) = 8.686 \times k_0 \times \text{Im}(n_{\text{eff}}) \times 10^4 \tag{3}
$$

In this expression, $k_0 = 2\pi/\lambda$ is the wave number, λ is in micron. Im[n_{eff}] is the imaginary part of the effective refractive index.

The sensitivity of this sensor can be expressed by Eq. [4](#page-3-2) (Aslam Mollah and Islam [2020\)](#page-7-3):

$$
S_{\lambda}(nm/RIU) = \frac{\Delta \lambda_{peak}}{\Delta n}
$$
 (4)

In this expression, $\Delta \lambda_{peak}$ is resonance peak offset, Δn is the refractive index variation value.

The resolution is this sensor can be expressed by Eq. [5](#page-3-3) (Wang et al. [2021](#page-8-15)):

$$
R(RIU) = \Delta n \frac{\Delta \lambda_{\text{min}}}{\Delta \lambda_{peak}}
$$
 (5)

In this expression, $\Delta \lambda_{min}$ represents the offset of the wavelength.

3 Results and discussion

In order to improve the sensing performance, we systematically studied the infuence of structural parameters on the loss spectrum. The following analysis of structural parameters was performed at the analyte refractive index of 1.39 and 1.40.

Figure [3](#page-4-0) shows the loss spectrum of different air hole diameters when the refractive index are 1.39 and 1.40 with the air hole spacing Λ = 7.4 µm and the thickness of the ITO layer $t=50$ nm.

It can be seen from Fig. [3](#page-4-0) that with the increase of the air hole diameter, the loss spectrum is red-shifted and the peak value of the loss spectrum gradually decreases. Because increasing the diameter of the air hole can better restrict the transmission of light in the fber core, the light leaking to the ITO layer is reduced. The peak value of the loss spectrum decreases. When the air hole diameter is 4.0 μ m, 4.1 and 4.2 μ m, the sensitivities are 18,500 nm/RIU, 19,500 nm/RIU and 20,000 nm/RIU at the refractive index changes from

1.39 to 1.40, respectively. However when the air hole diameter is 4.2 μm, the peak value of loss spectrum is relatively low. Therefore, the optimal parameter of the air hole diameter d is [4](#page-4-1).1 μm. The air hole spacing Λ also has great influence on sensor performance. Figure 4 shows the loss spectra of the air hole spacing Λ of different parameters at refractive index 1.39 and 1.40 when the air hole diameter $d=4.1$ µm and thickness $t=50$ nm of ITO layer. It can be seen from Fig. [4](#page-4-1) that the loss spectrum is blue-shifted with the increase of the air hole spacing Λ and the peak of the loss spectrum gradually increases. Moreover, the peak value of the loss spectrum increases because enlarging the air hole spacing will make more light leakage into the ITO layer.

It can be seen from Fig. [4](#page-4-1) that when the air hole spacing Λ = 7.4 µm, the loss spectrum has no obvious peak under the condition of the refractive index of 1.40 which severely affects sensor performance. The air hole spacing Λ = 7.6 µm is similar to the peak of the loss spectrum of the air hole spacing $Λ = 7.8$ μm. But the sensitivity of 28500 nm/RIU when the air hole spacing Λ = 7.6 µm is higher than that the sensitivity

of 22500 nm/RIU when the air hole spacing $Λ = 7.8$ μm. Therefore, we choose the air hole spacing $\Lambda = 7.6 \mu m$ as the optimal size.

It can be seen from Fig. [5](#page-5-0) that the peak of the loss spectrum is the highest when the thickness $t = 50$ nm of the ITO layer. Although the sensor sensitivity is greater at the thickness $t = 55$ nm of the ITO layer, the full width at half maximum (FWHM) of the loss spectrum is too large when the refractive index is 1.40. Therefore, the thickness $t=50$ nm of the ITO layer is the optimal size.

The excitation of the SPP mode mainly depends on the ITO layer and the thickness of the ITO layer also has a signifcant impact on the performance of the sensor. If the thickness of the ITO layer is too large, the electric feld does not easily break down the ITO layer, resulting in a decrease the peak of the loss spectrum. If the ITO layer is too thin, the surface plasma wave will be strongly damped because of radiation damping.

proposed sensor

Figure [6](#page-5-1) shows the loss spectrum of the proposed sensor with the diferent refractive index. It can be seen from Fig. [6](#page-5-1) that the loss spectrum is red-shifted with the increase of the refractive index. When the refractive index increases, the real part of the efective refractive index of the SPP mode increases, while the real part of the efective refractive index of the fundamental mode does not change, which results in red shifting of the loss spectrum. The maximum value of the loss spectrum is 243.42 dB/cm when the refractive index $n = 1.39$. The change of sensitivity with refractive index is shown in Table [1](#page-6-0). The sensitivity and resolution of the sensor are calculated by Eqs. [4](#page-3-2) and [5](#page-3-3), respectively. The sensitivity is 28,500 nm/RIU when the refractive index is 1.39–1.40 and the sensor resolution is 3.5×10^{-6} RIU. It can be seen that the sensor's refractive index detection range is 1.33–1.40.

Figure [7](#page-6-1) is the ftting curve for variation of resonance wavelength with analyte RI. The fitting coefficient is R^2 = 0.99026. Table [2](#page-7-4) shows the performance of our proposed sensor compared with other sensors, it can be seen that our sensor has achieved the high sensitivity and the structure is simple.

References	Refractive index range	Maximum sensitivity (nm/RIU)	Air holes number
Liu(2020)	$1.33 - 1.39$	8000	17
Liu and Sun (2020)	$1.33 - 1.39$	21,000	17
Hossaina and Hossain (2020)	$1.42 - 1.46$	15,000	36
Chao Liua and Fua (2019)	$1.33 - 1.40$	14,200	16
Kaur and Singh (2019)	1.385-1.40	10,000	19
This paper	$1.33 - 1.40$	28,500	4

Table 2 Performance comparison with similar sensors

4 Conclusion

In this paper, we propose a high sensitivity photonic crystal fber (PCF) surface plasmon resonance sensor based on indium tin oxide (ITO). The highest sensitivity is 28,500 nm/ RIU and the resolution is 3.5×10^{-6} RIU. The sensor has a refractive index detection range of 1.33–1.40, which includes various chemical solutions and biochemicals, such as red blood cells (1.40) , white blood cells (1.36) , human intestinal mucosa $(1.329-1.338)$, 10% glucose solution (1.3477), acetone (1.36), human liver (1.369) (Wang and Li [2019](#page-8-14)), etc. The sensor achieves high-sensitivity detection of the analyte, and the simple structure also provides more feasibility for practical fabrication.

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Data availability Any datasets in this manuscript are owned by the authors, and the authors may be contacted to request any data used in the manuscript if required.

Declarations

Confict of interest The authors declare that they have no known competing fnancial interests or personal relationships that could have appeared to infuence the work reported in this paper.

Ethical approval For this manuscript, the declaration of ethical approval is not applicable.

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