



# Performance analysis of symmetrical and bidirectional 40 Gbps TWDM-PON employing m-QAM-OFDM modulation with multi-color LDs based VLC system

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Received: 23 December 2020 / Accepted: 15 July 2021 / Published online: 6 August 2021

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## Abstract

In this work, a full-duplex time and wavelength division multiplexing-passive optical network (TWDM-PON) system is analysed. Orthogonal frequency division multiplexing (OFDM) with m-quadrature amplitude modulation (m-QAM) is employed to improve the performance of TWDM-PON for downstream and upstream transmission. Simultaneously, multi-color (390–750 nm) laser diodes (LDs) are employed for visible light communication (VLC) using various VLC links to encourage the information rate of fiber/VLC optical network. A TWDM-PON utilizing 16-, 32- and 64-QAM OFDM with ten LDs based VLC system has been analysed for full-duplex multi-color VLC signals of the system. The impact of the LDs input current and high transmission rate in the proposed PON/VLC link has been investigated for m-QAM OFDM modulation. The results show that the 40/40 Gbps 16-, 32- and 64-QAM signals over ten 8000 m VLC links and a 50 km fiber link are successfully transmitted at the modulation input current of 9 mA under bit error rate (BER) of  $3.8 \times 10^{-3}$ . Also, the proposed system employing 16-, 32- and 64-QAM signals over a 10 km fiber and ten 10 m VLC links provide the maximum transmission rate of 120, 100 and 80 Gbps respectively. Moreover, the measured error vector magnitudes (EVMs) and calculated BER values for 16-QAM downstream and upstream signals, are well below the required FEC limit than high-order modulation formats. Further, the numerical analysis of the proposed system reveals the superiority of the proposed fiber/VLC links.

**Keywords** Next-generation passive optical network stage 2 (NG-PON2) · Time and wavelength division multiplexing passive optical network (TWDM-PON) · Orthogonal frequency division multiplexing (OFDM) · Quadrature amplitude modulation (QAM) · Visible light communication (VLC)

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## 1 Introduction

In this twenty-first century, the high-capacity requirements for optical networks are rising exponentially due to the rise in recent technology such as big-data analysis, cloud computing and 4 k/8 k video broadcast. Therefore, the fifth-generation (5G) mobile wireless communication systems are currently analysed and discussed. 5G wireless networks aim to achieve higher network capacity, seamless coverage, energy, spectrum regulation and cost-effectively (Bi et al. 2019; Grover et al. 2020). To address the growing demand for high-capacity and economical transmission, optical access networks based on passive optical networks (PONs) are considered as a potential candidate for 5G-transport (Hu et al. 2020). Furthermore, the traditional Gigabit-class PON networks, such as Ethernet PON (EPON) and Gigabit PON (GPON) as standardized by IEEE and ITU-T respectively include the use of time-division-multiplexing (TDM) or wavelength-division-multiplexing (WDM) techniques. However, it is found that traditional networks do not meet the foremost carrier requirements for future worldwide fiber access. This includes management, flexibility and upgradability of bandwidth, higher capacity, maximum reuse of existing optical distribution network (ODN), higher split ratio and capacity than existing deployed standards (Lee et al. 2010). Hence, in 2012, the next-generation PON (NG-PON) based 40 Gbps time and wavelength division multiplexed PON (TWDM-PON) network has been proposed and demonstrated (Kaur et al. 2017b).

To acquire 40Gbps TWDM-PON architecture, distinct solutions for modulation formats in downlink/uplink direction for example 4-level pulse amplitude modulation (4-PAM) and duobinary as well as on-off keying (OOK) have been investigated (Yeh et al. 2014). Omella, M. et al. (Omella et al. 2008) reported 10 Gbps PON using duobinary modulation over the 11 km fiber link. Zhang, W. F in (Zhang et al. 2010) demonstrate 10/10 Gbps WDM-PON using differential quadrature phase-shift keying (DQPSK) modulation and upstream OOK format at 20 km distance. Shao, Y. et al. in (Shao et al. 2017) simulated 10/10 Gbps PON using 4-PAM modulation over fiber reach of 20 km. In (Mandal and Patra 2017) a 10 Gbps hybrid WDM/TDM PON utilizing differential phase shift keying with 128 ONUs over 50 km fiber is demonstrated. However, in NG-PON access networks, the traffic rate of beyond 100 Gbps is required due to the requirement of various broadband multi-services (Kaur et al. 2014). Thus, for 40 Gbps NG-PON access using OOK, 4-PAM and duobinary on a single frequency in fiber reach of 20 km are not generally implemented owing to the fiber constraints e.g. polarization mode dispersion, complex receiver structures, chromatic dispersion (CD) as well as costlier 40 GHz transceivers (Gill et al. 2019; Yeh et al. 2014). To achieve a higher information rate (more than 100 Gbps) cost-effectively, a quadrature amplitude modulation orthogonal frequency division multiplexing (QAM-OFDM) modulation could be effectively utilized (Selvendran et al. 2019). QAM-OFDM, a spectrally efficient modulation encodes the data on various orthogonal subcarriers. On the other hand for the different channels, TDM and WDM offer time and wavelength multiplexing techniques respectively; thus restricting several consumers to access as well as share a conventional fiber link. Aside from these multiplexing techniques, OFDM can provide features such as bandwidth allocation dynamically, a high degree of freedom and ability of software reconfigurable (Grover and Sheetal 2020; Lyu et al. 2018).

Many researchers investigated the PON systems with  $m$ -QAM-OFDM (for  $m=4, 8, 16$  and  $32$ ) modulation for long-range transmission and high data rates (Bai et al. 2020; Choudhury 2018; Ju et al. 2016; Patel and Dalal 2017; Xiao et al. 2019). Hu et al. (2020) demonstrate the 10/10 Gbps OFDM-WDM-PON using 4-QAM modulation over the

transmission length of 20 km. Bi, M. et al. (Bi et al. 2019), Zhuo et al. (2020) and Chen, Q. et al. (Chen et al. 2018) demonstrated a 10 Gbps OFDM-PON system using 16-QAM modulation over 20 km and to increase the transmission rate, Huang et al. (2020) realized the 20 Gbps OFDM-PON system using 16-QAM modulation over the 20 km fiber link. Xiao, Y., and Yu, J. in (Xiao and Yu 2013) demonstrated 10 Gbps WDM radio over fiber (RoF) PON utilizing 16-QAM OFDM modulation over the 40 km fiber link. Yeh and Chow (2009) investigated an asymmetric 16/10 Gbps (downstream/upstream) TDM-PON system using 16-QAM OFDM modulation over the 100 km fiber link. Kartiwa et al. (2013) experimentally demonstrated 20 Gbps WDM-OFDM-PON using 4/8/16/32-QAM modulation schemes over the fiber link range of 20 km. Further, one of the challenges in the NG-PON utilizing m-QAM OFDM modulation is the expensive fiber installation in geographical constraints areas. For this, radio frequency-based wireless access technologies such as RoF, wireless fidelity (WiFi) as well as worldwide interoperability for microwave access (WiMax) are widely used. However, due to the limited capacity, restricted spectrum range and the presence of severe electromagnetic interference (EMI) radiations are prohibited in lots of areas such as aircrafts cabins and hospitals (Chen et al. 2016). Here, the most favourable, visible light communication (VLC) technology significantly utilized and integrated with the PON to resolve the issue (Anis et al. 2017; Savojbolaghchi et al. 2019; Yeh et al. 2018).

For future 5G wireless access networks, VLC is regarded as a prominent technology because of its protocol transparency, high reliability, high security, eco-friendly, license-free spectrum (375–780 nm), infrastructure flexibility, energy efficiency and less cost. Also, as compared with traditional radio frequency (RF) wireless access, VLC has EMI-free wireless access the indoor as well as outdoor environments. Besides, VLC can be installed and utilized for the backup optical fiber, point-to-point (P2P) last-mile access and organization connectivity to offer the system security in the presence of geographical constraints (Mallick et al. 2020; Mohd Nor et al. 2019; Prabu et al. 2017). Since wireless communication and illumination can be obtained simultaneously, light-emitting diode (LED)-based VLC has been frequently studied (Jani et al. 2019; Ma et al. 2018; Wu et al. 2017). Chen et al. (2020) reported the 157.5 Mbps data rate transmission in  $2 \times 2$  multiple inputs–multiple-output (MIMO)-OFDM VLC system over 0.5 m VLC link. Li et al. (2015) reported the 682 Mbps data rate transmission over 1 m VLC link in VLC system employing OFDM modulation. Also, Lu et al. (2019) and Deng et al. (2018), reported the faithful transmission at 30 Mbps and 3.63 Gbps information rate over 3.5 m VLC link respectively OFDM-VLC system. Chow et al. (2013) reported the successful 6.14 Mbps data rate transmission over the 2 m VLC link in OFDM-VLC system. Zhang et al. (2018), experimentally revealed the reliable 1.87 Gbps data rate transmission over a 0.8 m VLC link in VLC-WDM system employing OFDM. Chi and Shi (2015) experimentally demonstrated a 1.6 Gbps VLC system utilizing OFDM modulation over 1.1 m VLC link. Moreover, in (Mukherjee et al. 2020) a full-duplex 12/10 Gbps hybrid OFDM based free-space and wireless-over-fiber transport system over 50 km bidirectional fiber as well as 12 m downstream free-space link and 8 m upstream wireless link has been demonstrated. In (Mallick et al. 2018), a bidirectional wireless-over-fiber based on OFDM employing polarization multiplexing technique at 10 Gbps along with 6.25 Gbps for OFDM downlink transmission and 5 Gbps along with 2.5 Gbps OFDM uplink transmission over 50 km fiber along with 10 m downstream and 5 m upstream wireless links is successfully demonstrated. In (Mandal et al. 2018) a bidirectional WDM hybrid fiber-wireless/fiber-wired/fiber-VLC/fiber-invisible VLC (IVLC) at 10 Gbps/50 GHz millimeter wave (MMW), 10 Gbps/100 GHz MMW over 50 km fiber along with 10 m RF and 40 m optical wireless link in downstream transmission is demonstrated. Also, the upstream data at 2.5 Gbps is transmitted over 50 km fiber

and 10 m free-space transmission link successfully. However, as the increasing of information rate and transmission range, an LED-based VLC system encounters heavy traffic because of the extremely finite modulation bandwidth of LEDs and the divergence of light (He et al. 2016b). However, multi-input multi-output (MIMO) technology has been generally studied in (Alqahtani et al. 2019; Deng et al. 2012; Guerreiro et al. 2020; Saraereh et al. 2019) during previous few years and applied to various wireless OFDM systems as it can improve the reliability and capacity of the systems. But there are still major issues like channel correlation, hardware impairments and implementations, modulation and interference management which need to be address for future based wireless systems (Lu et al. 2014). Besides this the integrated power line communication (PLC)-VLC system also act as an economical and efficient backbone network but it has some issues like low transmission speed, disturbance sensitivity, channels' cross-modulation, nonlinear distortions, huge size and high cost of inductors as well as capacitors utilized in PLC system (Fusheng et al. 2016). On the other hand, the laser diode (LD) based VLC systems show high pumping efficiency, modulation bandwidth, coherency and high power for point-to-point communication. Hence, the positive features of PON utilizing OFDM modulation with LDs based VLC system have attracted numerous researchers' attention towards hybrid wired/wireless links. Recently, various works on OFDM using LD based VLC system as visible laser light communication (VLLC) have been investigated and analyzed. Wei et al. (2017), presented the transmission of 2.5 Gbps-10 GHz data in fiber-VLLC system utilizing OFDM over 20 km wired and 8 m VLLC link. Shi et al. (2018), demonstrated the successful transmission at 3.2 Gbps information rate in OFDM/offset QAM (OFDM/OQAM) on the basics of VLLC-WDM system over 50 km wired and 4.5 m VLLC links. However, these fiber-VLLC systems using a single LD are applicable for short range access networks at low transmission rate. Therefore, LDs of different wavelengths with a high output power and modulation bandwidth are regarded one of the preferred solution for constructing a long-range and high-speed VLC system. It could be of interest to study an energy-efficient NG-PON based TWDM-PON using m-QAM-OFDM modulation using multi-color LDs based VLC system. Although numerous previous work have been demonstrated on the VLLC-OFDM system, but no one work studied the TWDM-OFDM PON performance with the multi-color LDs based VLC system.

Thus, in this work, a symmetrical as well as full-duplex four wavelengths TWDM-PON using m-QAM OFDM modulations with multi-color LDs based VLC system is proposed as well as analysed. Here, TWDM-PON system employing downstream and upstream wavelengths (four pairs) are engaged within 15 GHz bandwidth where each OFDM band is modulated at 16-, 32-, and 64-QAM formats. Also, in the system coherent detection is utilized to offer supreme frequency selectivity at receiver. For the moment, the multi-color LDs based VLC system is utilized as an optimal solution for constructing a next-generation fiber-VLC system. Here, in Sect. 2, the proposed system architecture is presented. In Sect. 3, the numerical analysis of the proposed PON/VLC link under fiber impairments is illustrated. Section 4 illustrates results and discussion followed by the conclusion in Sect. 5.

## 2 System architecture

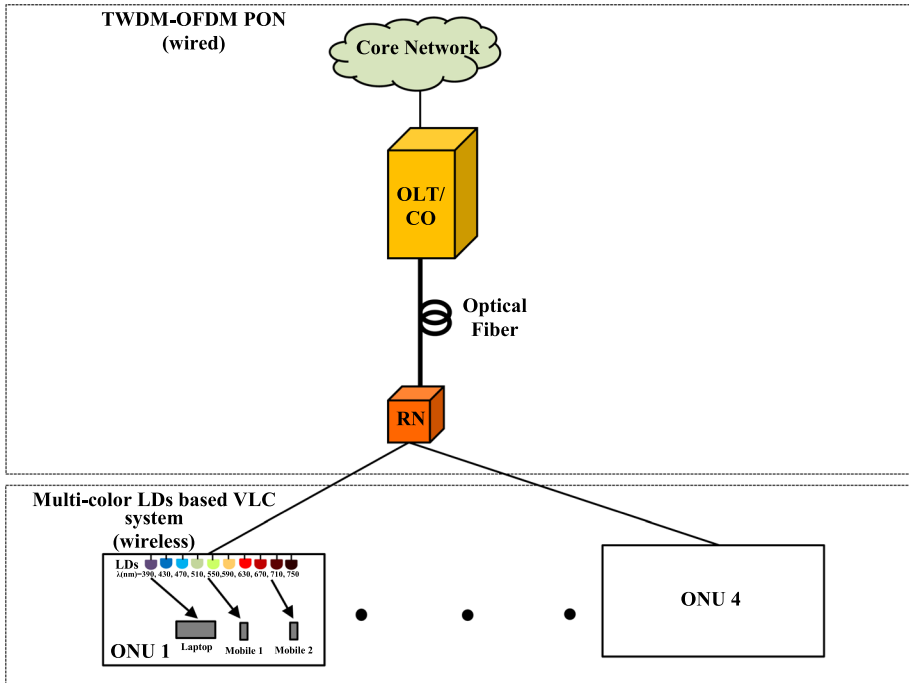
Figure 1 presents the architecture of TWDM-OFDM PON with the multi-color LDs based VLC system. The incoming signal from an optical line terminal (OLT) passed through a fiber cable followed by a remote node (RN) is employed to allot the incoming signals to the four no. of optical network units (ONUs). The wired (fiber) and wireless (VLC)

applications are obtained by linking optical fiber and through the wireless VLC channels by utilizing multi-color LDs (390–750 nm) in the ceiling (Chen et al. 2016).

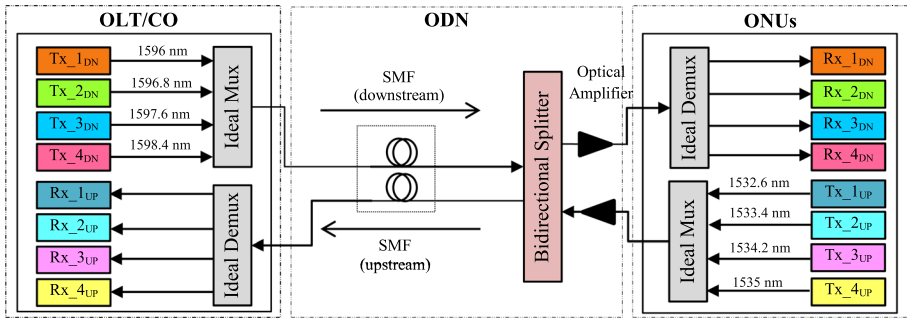
The proposed architecture of the NG-PON2 based bidirectional 40Gbps (4×10Gbps) TWDM-PON (1:8 split ratio) using m-QAM OFDM modulation using the LD based VLC system is illustrated in Fig. 2. At OLT, four pairs of downstream (Tx<sub>DN</sub>) and upstream (Tx<sub>UP</sub>) wavelengths ({1596, 1532.6}, {1596.8, 1533.4}, {1597.6, 1534.2} and {1598.4, 1535}) in nm (channel spacing=0.8 nm) used for bidirectional transmission in the system.

In Fig. 2, for downlink, four downlink wavelengths with OFDM signals are multiplexed through ideal multiplexer, directed through a single-mode fiber (SMF) and passed to a passive splitter for downstream transmission. After amplification by using an optical amplifier (OA), the downlink signals are distributed to ONUs using an ideal de-multiplexer (Lin et al. 2015). At the users' side, the receiver chooses its definite wavelength to decode the OFDM signal. Then VLC signals are generated by multi-LDs based VLC system per OFDM wavelength. Ten colors set of LDs are utilized per VLC system to construct a wireless system. In the uplink direction, each ONU passed boosted OFDM signals are firstly de-multiplexed as well as decoded and then passed through multi-color LDs based VLC links per OFDM signal. The m-QAM modulation formats tend to transmit 100Gbps and more data over a channel but also suffers from fiber impairments which hinders the faithful wired/wireless distance (Yeh et al. 2014).

The schematic diagram of a full-duplex 10/10 Gbps TWDM PON system with m-QAM-OFDM modulation over SMF for wired and free space optics (FSO) link i.e. VLC wireless transmission, is presented in Fig. 3 using OptiSystem 17.0 software. In



**Fig. 1** Semantic diagram of the proposed TWDM-OFDM PON system employing multi-color LDs VLC system



**Fig. 2** Schematic diagram of full-duplex 4 × 10 Gbps TWDM-OFDM PON with LDs based VLC system

this system, for system design, the global parameters are no. of samples ( $= 32,768$ ) and symbol rate ( $= 5 \times 10^9$  symbols/sec). For bidirectional transmission, both OLT and ONUs consists of four pairs of transmitters/receivers. Also, the downstream wavelengths (1596–1598.4 nm) and the upstream wavelengths (1532.6–1535 nm) follow the ITU-T channel spacing of 0.8 nm (100 GHz). The information is emitted at these frequencies by utilizing four pairs of continuous wave (CW) lasers (linewidth = 0.15 MHz and input power = -6 dBm). A single downstream transmitter is illustrated in Fig. 3a which comprises a pseudo-random bit sequence (PRBS) generator offering the random binary sequences at 10 Gbps which are fed to m-QAM where  $m = 16$ -, 32- and 64 with 4-, 5- and 6-bits per symbol sequence generator respectively. The m-QAM signals output is transmitted to an OFDM modulator for mapping over 512 subcarriers, through the serial to parallel converted. 512 subcarriers are employed with a fast Fourier transform (FFT) having 1024 points and a null cyclic prefix (Kaur et al. 2017b).

An OFDM modulator provides the in-phase (I) as well as quadrature (Q) components of the incoming signal for the data transmission in I/Q optical modulator and to filtered by two low pass cosine roll-off filters (roll-off factor = 0.2) to forward for signal modulation. The I/Q optical modulator consists a laser signal, two electrical gain components, two mach-Zehnder modulators (MZMs) (extinction ratio = 60 dB) followed by an optical power combiner (size =  $2 \times 1$ ) (Kachhatiya and Prince 2016). Further, four downstream OFDM signals are multiplexed at distinct wavelengths for transmission over an optical fiber. Then, the signal is forward to a splitter, an OA (gain = 13 dB and noise figure = 4 dB) to improve the receiver’s receiver sensitivity and transferred to the receiver section where to demodulate the TWDM-OFDM signals an opposite operation is accomplished. For signal reception (at ONU side), a de-multiplexed single user signal is passed to the four number of of X couplers (coupling coefficient = 0.5) in addition to a local oscillator and phase shifter (phase shift =  $90^\circ$ ) for coherent orthogonal reception. Again the signal is fed to the four PIN photodetectors (PDs) (responsivity = 1 A/W, dark current = 10 nA and thermal noise =  $1 \times 10^{-22}$  W/Hz) followed by two electrical subtractors, two electrical amplifiers (gain = 20 dB) and OFDM demodulator. After coherent OFDM demodulation, a single polarization digital signal processing (DSP) unit executes necessary functions to recover the received signals and for nonlinearities losses compensation as shown in Fig. 3b. In DSP unit, bessell filter is utilized to filter the required signal having specific samples/symbol ( $= 8 \times$  samples per bit) and bandwidth

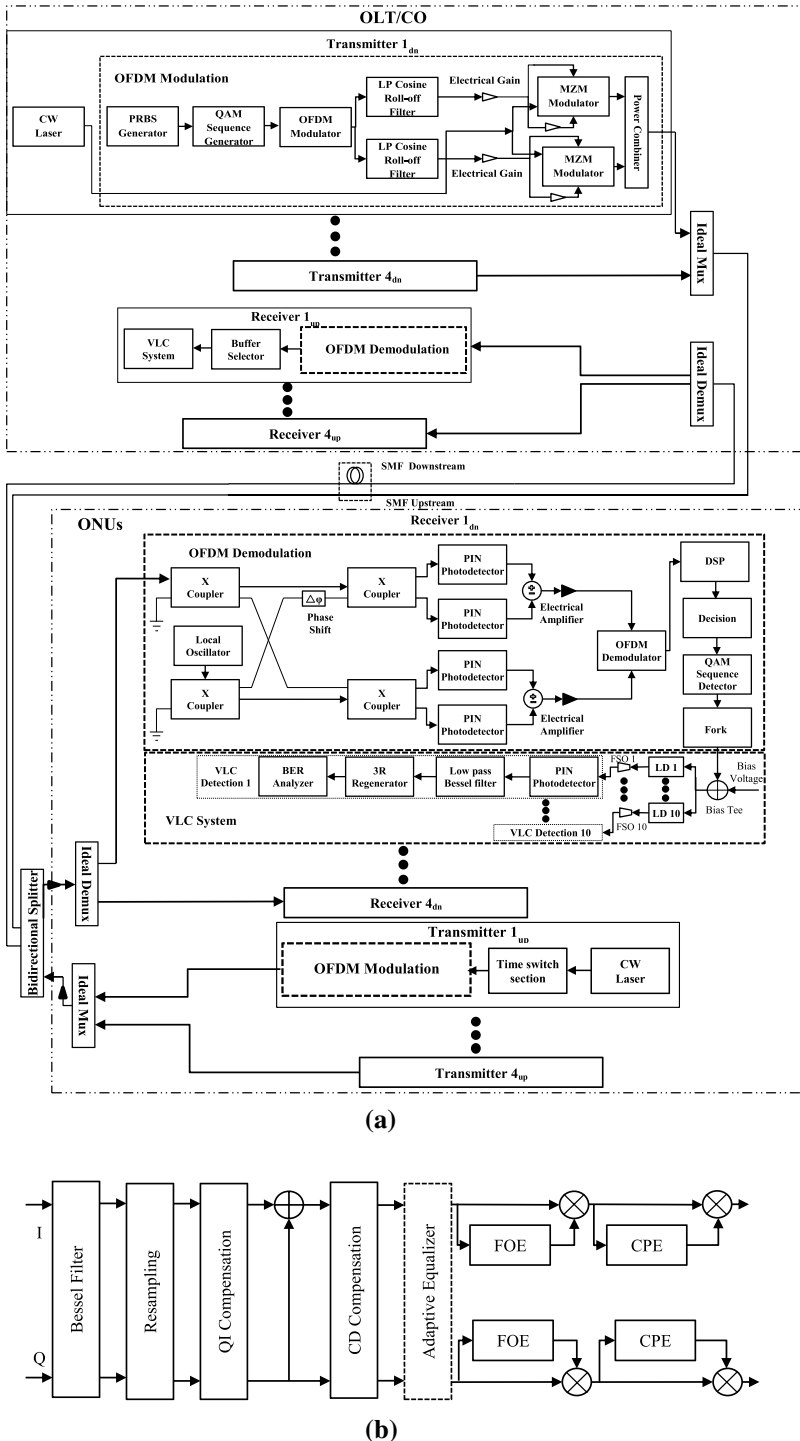


Fig. 3 Schematic diagram of a bidirectional four wavelengths 10/10 Gbps TWDM-PON utilizing m-QAM OFDM modulation with multi LDs based VLC system and single-polarization DSP unit

(= 0.75 × symbol rate) whereas resampling is utilized at rate = 4 samples/symbol. The rest of the DSP sub-unit are explained as follows (Yang et al. 2013):

IQ compensation is utilized to minimise the phase along with amplitude imbalances within respective I and Q received signals. Mathematically, for coherent receiver including DSP component, the 90° phase shift among I and Q components is produced by 90° optical and hybrid and 180° phase shift between balanced detection. The optical hybrid output  $E_1$ ,  $E_2$ ,  $E_3$  and  $E_4$  by neglecting imbalance and loss is given as (Guerreiro et al. 2020):

$$E_1 = \frac{1}{\sqrt{2}} [E_r + E_o] \tag{1}$$

$$E_2 = \frac{1}{\sqrt{2}} [E_r - E_o] \tag{2}$$

$$E_3 = \frac{1}{\sqrt{2}} [E_r - jE_o] \tag{3}$$

$$E_4 = \frac{1}{\sqrt{2}} [E_r + jE_o] \tag{4}$$

where  $E_r$  and  $E_o$  depicts the received optical and local oscillator input signals. CD compensation (through Back-Propagation algorithm) is utilized to eliminate CD as well as fiber nonlinearity. Also, photocurrent i.e.  $I_1$  and  $I_2$  from two photodetectors at coherent receiver are given as (Guerreiro et al. 2020):

$$I_1 = \frac{1}{2} \left\{ |E_r|^2 + |E_o|^2 + 2Re[E_r E_o^*] \right\} \tag{5}$$

and

$$I_2 = \frac{1}{2} \left\{ |E_r|^2 + |E_o|^2 - 2Re[E_r E_o^*] \right\} \tag{6}$$

Thus, the ultimate complex detected signal comprising I and Q phase components are presented as (Guerreiro et al. 2020):

$$I(t) = I_I(t) + jI_Q(t) = 2E_r E_o^* \tag{7}$$

After this, to de-multiplex the polarization of received signal, an adaptive equalizer offers a butterfly structure. Frequency offset estimation (FOE) is employed to reduce the phase as well as frequency unmatched between the local oscillator at receiver side and transmitter. Further, the signal obtained at the input single polarization DSP unit,  $R(k)$  with data symbol,  $I(k)$  and zero-mean Gaussian random variable,  $N(k)$  is expressed as (Yang et al. 2013):

$$R(k) = I(k) \cdot e^{j(2\pi f_k T + \varphi_k)} + N(k) \tag{8}$$

where  $\varphi_k$ ,  $\Delta f$  and  $T$  depict carrier phase, carrier frequency offset and symbol period respectively. Again, the fourth power  $R(k)$  can be expressed as (Yang et al. 2013)



$$R^A(k) = C \cdot e^{Aj(2\pi\Delta f k T + \varphi_k)} + Z(k) \quad (9)$$

where  $C$  is the constant amplitude,  $Z(k)$  mean noise process together with zero-mean. Also, taking into account the signal's spectral density, the frequency offset can be represented as (Yang et al. 2013):

$$R^A(k) = \frac{1}{4} \arg\{\max[|G(f)|]\} \quad (10)$$

where

$$|G(f)| = \frac{1}{n} \sum_{k=0}^{n-1} C^A(k) \cdot e^{-j(2\pi\Delta f k T)} \quad (11)$$

where  $n$  means block length. Then, carrier phase estimation (CPE) is utilized to offer optimum output in terms of distance and information rate. In 2D complex plane, the estimated required space  $|s_{k,b}|^2$  to the adjacent constellation point by decision component is expressed as (Yang et al. 2013):

$$|s_{k,b}|^2 = |G_k e^{-j\varphi_b} - X_{k,b}|^2 \quad (12)$$

where  $X_{k,b}$  denotes the decision  $G_k e^{-j\varphi_b}$ . At last for polarization, the decoding of received sequences, parallel to serial conversion processed to acquire the final output bits.

After the DSP unit, a decision component followed by an m-QAM sequence generator is used for coherent downlink traffic detection. OFDM demodulator performance parameters should be identical with the transmitter to recover the m-QAM symbols at receiver side. The m-QAM sequence detector signifies the binary sequences and demapped the received electrical signal to retrieve the bit sequences (Kachhatiya and Prince 2018; Kaur et al. 2017a). Then for wireless transmission, a  $1 \times 10$  fork is used for copying the incoming signal into ten numbers of ideal single-mode LDs (390, 430, 470, 510, 550, 590, 630, 670, 710 and 750 nm) based VLC system. Here, each ideal single-mode LD provides no internal cavity losses over the visible light range (375–780 nm). Further, to drive each LD (input power = 5 dBm and modulation peak current = 9 mA), the DC bias signal (4 V) and incoming electrical signals are integrated using a bias tee and transmitted via the FSO link. Each VLC system consists of ten numbers of FSO links corresponding to ten numbers of multi-color LDs for high speed and long-range point-to-point communication. Then, the received signal is detected using PIN PD followed by a low pass Bessel filter (LPF) (cut-off frequency = 3.75 THz), 3R regenerator for recovering the received signal and bit error rate (BER) analyzer to obtain the output.

Considerably, for uplink direction,  $4 \times 10$  Gbps m-QAM OFDM signals are produced with four upstream TWDM wavelengths (1532.6–1535 nm). The uplink 40 Gbps traffic transmitted from the ONUs and detected at CO side. Also, these independent upstream wavelengths are transmitted by using CW lasers and each CW laser wavelength is passed through a time switch section for upstream transmission as shown in Fig. 4.

Eight pairs of two cascaded dynamic selects  $Y$  per wavelength, to transmit the information at definite timeslot (TS) and switching time ( $TS_1$  and  $TS_2$ ) are used for the upstream time switch section as (Kumari et al. 2019):

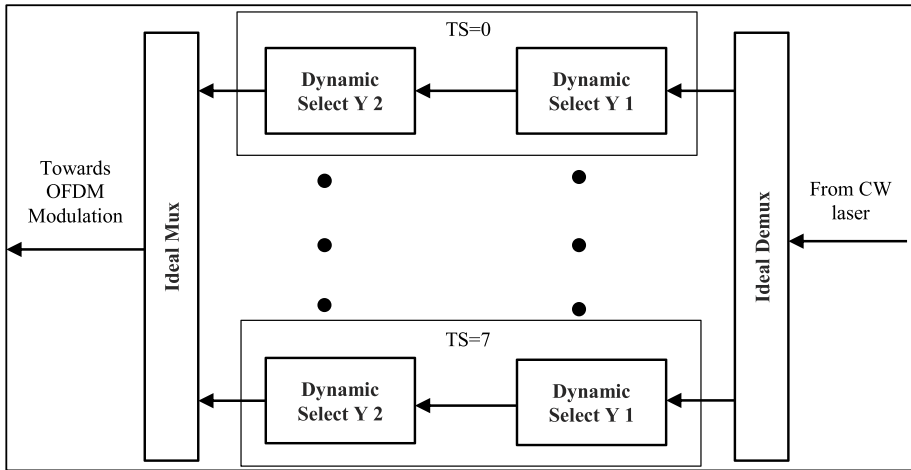


Fig. 4 Upstream time switch section

$$Ts_1 = TS \cdot \left(\frac{1}{\text{Bitrate}}\right) \cdot \left(\frac{SL}{T}\right) \tag{13}$$

and

$$Ts_2 = Ts_1 + \left(\frac{TW}{T}\right) \tag{14}$$

where TS (=0 to 7), SL (=8192), T (=8) and TW (=0.81 × 10<sup>-06</sup> s) denote the timeslot, sequence length, number of customers utilizing the same upstream wavelength and time window respectively at a reference wavelength of 1550 nm. Table 1 shows the switching time of the proposed system.

In the time switch section, an ideal multiplexer is employed to deliver the OFDM modulation switching information in upstream direction and passed through an OFDM modulator and an OA. Then each uplink wavelength is detected at the OLT side employing an OFDM demodulator. To choose the recent simulation iteration a buffer selector is utilized. Then the received signal is transferred towards a multi-color LDs based VLC system for uplink wireless communication. In ODN section, two identical SMF links using a

**Table 1** Switching Time for the upstream transmission at 10 Gbps

Timeslot	T <sub>s1</sub> (s)	T <sub>s2</sub> (s)
0	0	0.10 × 10 <sup>-06</sup>
1	0.10 × 10 <sup>-06</sup>	0.20 × 10 <sup>-06</sup>
2	0.20 × 10 <sup>-06</sup>	0.30 × 10 <sup>-06</sup>
3	0.30 × 10 <sup>-06</sup>	0.40 × 10 <sup>-06</sup>
4	0.40 × 10 <sup>-06</sup>	0.51 × 10 <sup>-06</sup>
5	0.51 × 10 <sup>-06</sup>	0.61 × 10 <sup>-06</sup>
6	0.61 × 10 <sup>-06</sup>	0.71 × 10 <sup>-06</sup>
7	0.71 × 10 <sup>-06</sup>	0.81 × 10 <sup>-06</sup>

bidirectional splitter are employed to isolate the uplink and downlink wavelengths in the ONUs side. Table 2 presents the parameters utilized in this proposed work.

The schematic designed layout for the TWDM PON system with 16-, 32- and 64-QAM-OFDM modulation using OptiSystem software is shown in Fig. 5.

### 3 Numerical analysis

In this section the basic numerical analysis of the proposed PON/VLC link including fiber impairments issues is presented to validate the feasibility of the proposed system under fiber impairments. The proposed coherent detection OFDM in TWDM PON and VLC system offers high receiver sensitivity for long reach transmission. As in coherent OFDM the large number of subcarriers can cause the channels interference and hence degrades the system performance while using the too small polarization results in reduction in the spectrum utilization. In general without using DSP component, the CD,  $D$  in the proposed fiber/VLC link,  $l$  is presented using the education  $D = l[d + s(\lambda - 1550)]$  in ps.nm where  $\lambda$ ,  $d$  and  $s$  are wavelength, dispersion coefficient and slope coefficient respectively at reference wavelength of 1550 nm. For 10 km fiber and 10 m of VLC range at data rate of 10 Gbps the calculated  $D$  is approximate 205 ps.nm and for 50 km and 10 m of fiber and VLC ranges respectively at same data rate is calculated as 1020 ps.nm which is below than defined tolerance of 1176 ps/nm at transmission rate of 10 Gbps per wavelength. But with increase in transmission distance and transmission rate the, the value for  $D$  increases and hence performance of the system decreases. Also, at higher transmission rate causes spreading of optical pulses or inter-symbol interference (ISI) (Kumari et al. 2020; Mandal et al. 2021).

Again, for the proposed fiber/VLC link the pulse broadening,  $\Delta t$  using the expression  $\Delta t = dl\Delta\lambda$  in ps where  $\Delta\lambda$  means spectral line width is 84 ps over 50 km wired and 10 m VLC link ranges at 10 Gbps data rate. In addition, the calculated unwanted side bands i.e. four wave mixing (FWM) wavelengths  $W$ , for  $N$  channels with 0.8 channel spacing in fiber

**Table 2** Proposed work SMF/VLC link parameters

Component Name	Parameters	Value	Unit	
SMF	Wavelength (reference)	1550	nm	
	Length	10–50	km	
	Attenuation	0.2	dB/km	
	Dispersion	16.75	ps/nm/km	
	Dispersion slope	0.075	ps/nm <sup>2</sup> /k	
	Effective area	80	μm <sup>2</sup>	
	Nonlinear index of refraction	$26 \times 10^{-21}$	m <sup>2</sup> /W	
	Temperature	300	K	
FSO	Range	10–8000	m	
	Attenuation	8	dB/km	
	Aperture diameter	Transmitter	5	Cm
		Receiver	10	Cm
	Beam divergence angle	1108	Mrad	

**Fig. 5** Simulation diagram of full-duplex 4×10 Gbps TWDM-PON using m-QAM OFDM modulation with VLC system **a** downstream transmitter, **b** OFDM channel, **c** bidirectional channel, **d** downstream Receiver, **e** coherent detection, **f** upstream transmitter and **g** upstream receiver

link is approx. 21 using the expression is  $W = \frac{N^2}{2(N-1)}$ . Hence, there is need to control the subcarriers in coherent OFDM. In addition, DSP unit can also affect the performance of system in terms of long reach distance and high speed transmission capacity by minimizing fiber impairments such dispersion, non-linear effects and polarization losses. The impact of fiber nonlinearities because of the fiber transmission along with their mitigation utilizing the proposed CO-OFDM with DSP unit receiver are illustrated as follows (Kumari et al. 2020; Mandal et al. 2021):

A polarization independent phenomenon i.e. chromatic dispersion (CD) can be compensated before demultiplexing as well as equalizing the received signal to retrieve the two orthogonal polarization channels at transmitter side. The expression for CD can be expressed as (Kumari et al. 2020; Renaudier et al. 2010):

$$D(x, \varphi) = \exp\left(-i\frac{d\lambda^2}{4\pi c}\varphi^2\right) \tag{15}$$

where  $x$  and  $\varphi$  are transmission distance and angular frequency respectively.  $i, d, \lambda$  and  $c$  are imaginary part, dispersion coefficient, wavelength and speed of light respectively. Practically by employing finite impulse response (FIR) filters of DSP unit, CD can be compensated and CD compensation amount depends on calculation capacity of state of knowledge technologies. The DSP unit’s primary part is received signal demultiplexing to retrieve the orthogonal polarization transmitted at the transmitter side using FIR filters. The optical signal received at single-polarization filter structure is given as (Renaudier et al. 2010):

$$y_{out} = h_y \cdot y_{in} \tag{16}$$

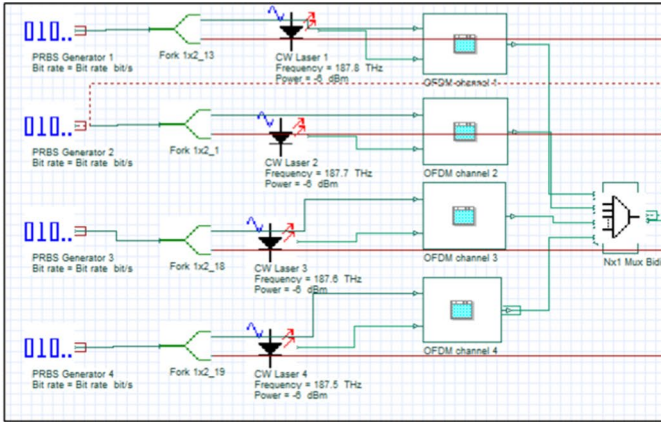
where  $y_{in}$  means input signal,  $y_{out}$  presents the output signal.  $h_y$  means the adaptive FIR filter with tap coefficient. Moreover, frequency domain equalizers are mostly used as a most popular and promising CD filters and its transfer function for coherent transmission system is represented in Eq. (15) (Xu 2017). After two polarization channels separation by the adaptive equalizer, phase-tracking is done in digital domain. To recover and remove the persisting phase mismatch between the signal and the local oscillator, CPE process is used (Renaudier et al. 2010). For CPE one-tap normalized LMS filter is effectively employed for coherent m-QAM transmission in the proposed system and the tap weight can be presented as (Xu 2017):

$$w(n + 1) = w(n) + \frac{\varepsilon}{|y_{in}(n)|^2} y_{in}^*(n) e(n) \tag{17}$$

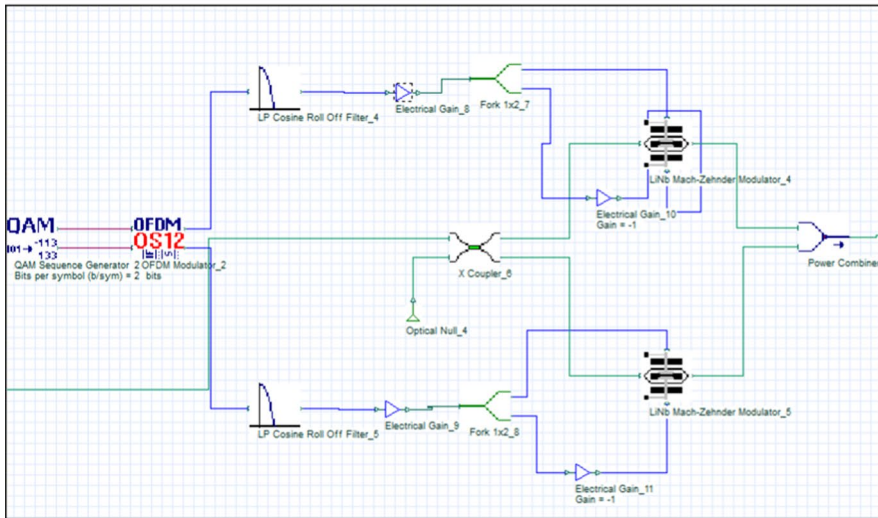
where

$$e(n) = D(n) - w(n) \cdot y_{in}(n) \tag{18}$$

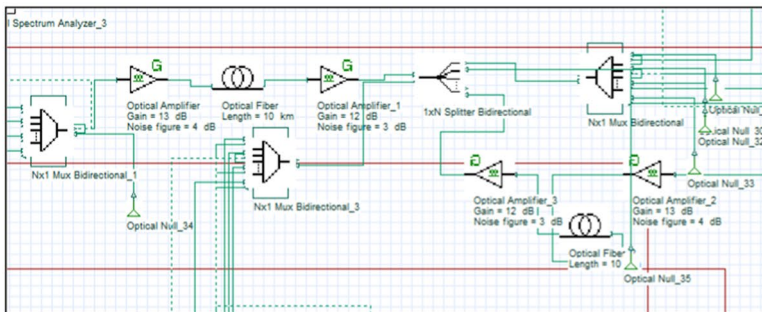
where  $w(n + 1)$  presents the tap weight;  $n, D(n)$  and  $e(n)$  mean symbol index, desired symbol and carrier phase estimation error between output signal and desired symbol respectively. Also,  $\varepsilon$  means the step size in one-tap normalized LMS filter in the DSP unit. Thus



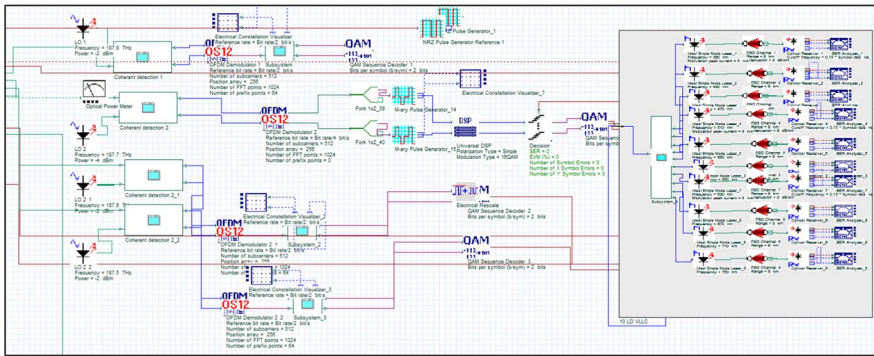
(a) Downstream transmitter



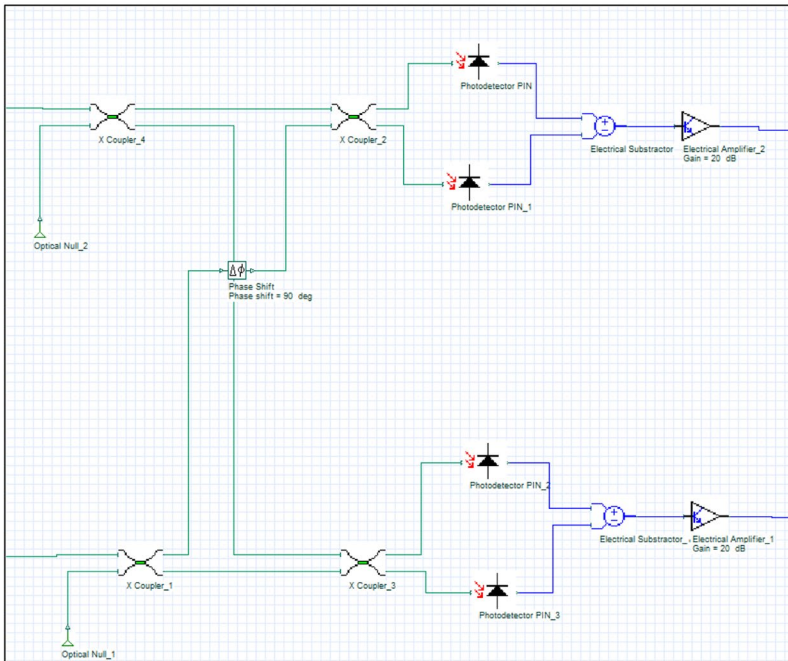
(b) OFDM channel



(c) Bidirectional channel



(d) Downstream Receiver



(e) Coherent detection

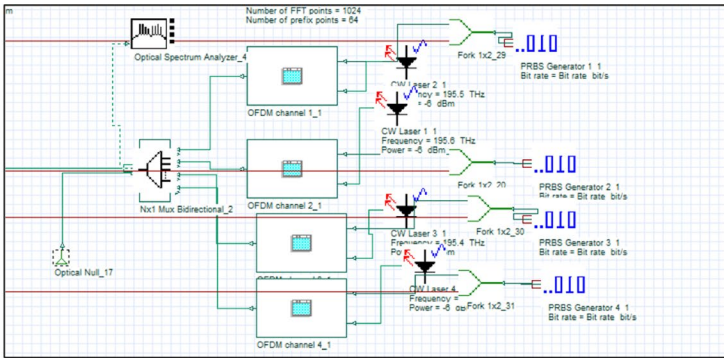
Fig. 5 (continued)

BER in m-QAM coherent transmission system can be expressed as (Mandal et al. 2021; Xu 2017):

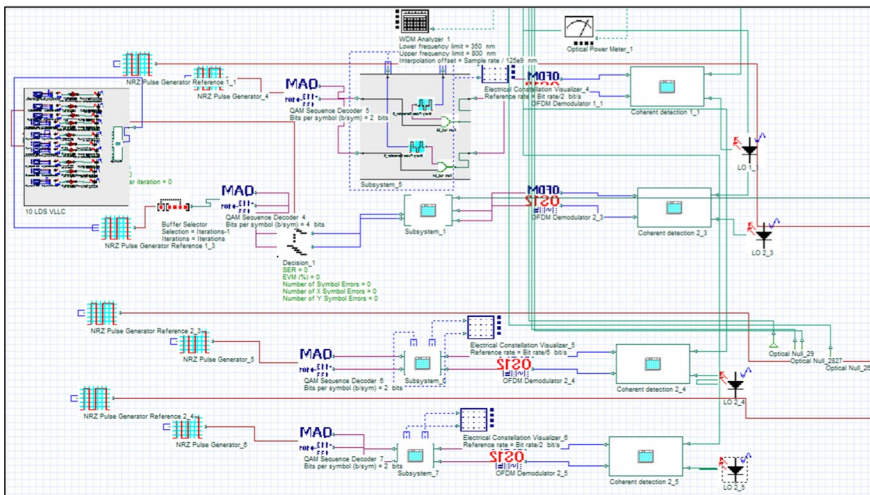
$$BER = \frac{1}{\log_2(m)} \operatorname{erfc}\left(\frac{\pi}{m\sqrt{2\delta}}\right) \tag{19}$$

where  $\delta$  means the phase noise variance.





(f) Upstream transmitter



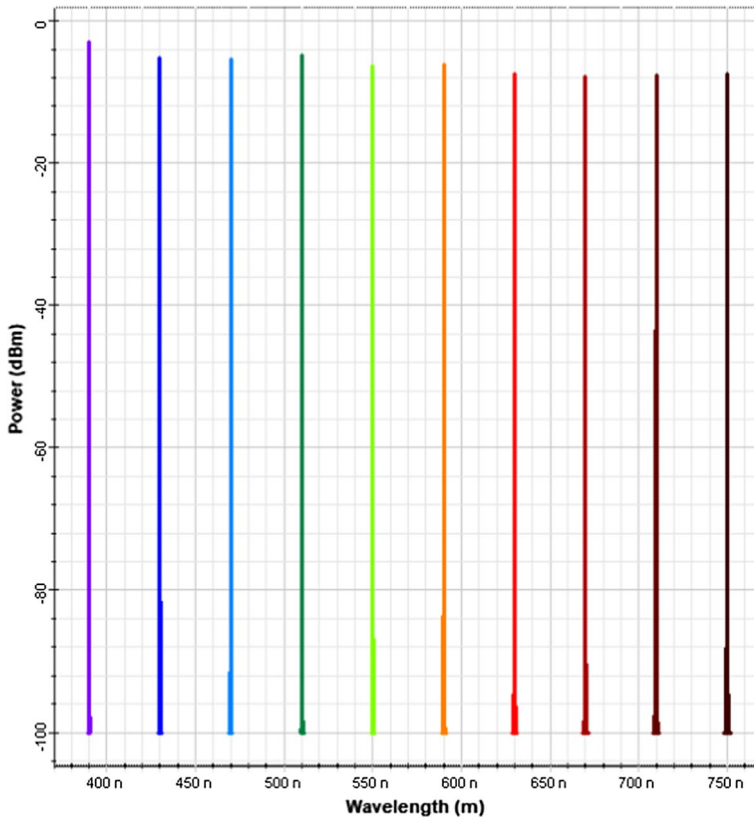
(g) Upstream receiver

Fig. 5 (continued)

### 4 Results and discussion

This section describes the performance analysis of the proposed PON/VLC link for a single downstream OFDM (1596.8 nm) and a single upstream OFDM (1533.4 nm) signal where each signal consists of ten different color VLC links. Figures 6, 7, 8, 9, 10 show optical spectra, BER and error vector magnitudes (EVM) performance of the proposed wired/wireless links in the presence of fiber distortions and noise.

Figure 6 presents the optical spectrum of the downstream multi-color LDs based VLC signals, which is obtained from an optical spectrum analyzer. It shows ten wavelengths (ten colors) from ten LDs where each LD having input power and modulation peak current of 5dBm and 9 mA respectively in the proposed system. Figure 7 illustrates the output of the proposed PON/VLC link having 10 m VLC and 50 km SMF reach at 10 Gbps data rate in downstream direction at each stage.



**Fig. 6** The optical spectrum of multi-color LDs signals in the visible range

Figure 8a–f illustrate the BER versus data rate of 16-, 32- and 64-QAM OFDM downstream and upstream signals over the 10 m VLC and 10 km fiber links. The dotted line at BER of  $3.8 \times 10^{-3}$  presents the minimum BER value for the successful receipt of the signal under the forward error correction (FEC) of 7% (Wei et al. 2017). From figures, it is observed that as the data rate increases, the BER of the downstream and upstream VLC signals increases for all three modulations. BER values increase due to the significant impacts of fiber nonlinearity at high data rate. Also, it can be observed that the VLC signal at 750 nm wavelength achieves superior performance over other wavelengths for all m-QAM modulations. This is because the VLC signal at 750 nm wavelength has high multipath fading resilience than other wavelengths. Further, it can be noticed that 16-QAM performs better than 32- and 64-QAM modulation formats. For the downstream and upstream 16-QAM VLC signals, the minimum BER (at 7%



FEC limit) for better network performance is measured as  $6.29 \times 10^{-4}$  and  $6.32 \times 10^{-4}$  respectively at the transmission rate of 30Gbps. Similarly, at the same acceptable limit, for 32-QAM modulation, the BER is measured as  $1.62 \times 10^{-3}$  and  $1.64 \times 10^{-3}$  at the information rate of 25 Gbps whereas for 64-QAM modulation the BER is measured as  $3.38 \times 10^{-3}$  and  $3.68 \times 10^{-3}$  at 20 Gbps in the downstream and upstream directions respectively. The results observed demonstrate a reliable transmission of aggregate 120 Gbps, 100 Gbps and 80 Gbps data over 10 m VLC and 10 km fiber links with acceptable BER ( $3.8 \times 10^{-3}$ ) for 16-, 32- and 64-QAM modulations respectively in downstream and upstream directions. Moreover, Fig. 8 provides the constellation diagrams for 16-, 32- and 64-QAM modulation formats at 10 Gbps, 20 Gbps and 30 Gbps data rates which illustrates that received signal performs better at a lower data rate.

Table 3 illustrates that the previously demonstrated works in the literature deploy 16-, 64- and 128 QAM modulation formats capable of delivering maximum information only up to 10 m VLC and 10 km fiber link reach at 10 Gbps under the BER of  $10^{-3}$ . However, under the same BER, the higher information rate of 10 Gbps over the wired-wireless links per channel (10 km wired and 10 m wireless) than previous work is obtained for the proposed TWDM PON system.

Figure 9a and b present the EVM(%) with respect to received optical power of 16-, 32- and 64-QAM OFDM downstream and upstream signals over the 10 m VLC (at 750 nm) and 10 km fiber links at the information rate of 10 Gbps. EVM is utilized to measure the received signal quality under the impact of fiber distortion and is determined from its constellation diagram. EVM is generally illustrated in percentage (%) and the EVM(%) of the received signals with the symbol sequence of  $S$  and its decision of  $[S]_d$  is given as follows (Sheetal and Singh 2018):

$$EVM(\%) = \sqrt{\frac{|s - [s]_d|^2}{|s_d|^2}} \times 100\% \quad (20)$$

where (...) indicates the mean value. From Fig. 9, it can be noticed that the EVM(%) reduces with the increment in received optical power introducing in the deflated error during information transmission. For the downstream direction, EVM(%) for 16-QAM is measured as 18.44, 8.75 and 5.27 whereas for 32-QAM is measured as 18.43, 13.75 and 11.73 and for 64-QAM is measured as 18.04, 15.93 and 15.24 at the received optical power of -20 dBm, -12 dBm and -2 dBm respectively. Again, for upstream direction, EVM(%) for 16-QAM is measured as 22.40, 10.53 and 5.68 whereas for 32-QAM is measured as 20.71, 13.55 and 11.88 and for 64-QAM is measured as 20.71, 15.75 and 14.84 at a received optical power of -20 dBm, -12 dBm and -2 dBm respectively. At -20 dBm received power, EVM(%) values for both downstream and upstream signals are almost the same i.e. 18%. After that, the EVMs between m-QAM signals are greatly separated EVM(%) in both transmission directions at -2 dBm received power and decreased by almost 12% for 16-QAM, 6% for 32-QAM and 2% for 64-QAM according to the given EVM(%) Eq. (20). Also, at the received optical power of -2 dBm, the measured EVM for 16-QAM is below

**Fig. 7** Proposed system of 10/10 Gbps TWDM-OFDM PON with multi-LDs based VLC outputs at single downlink transmitter stage **a** random bit sequence; **b** 16-QAM constellation; OFDM output for **c** in-phase and **d** quadrature channels; **e** OFDM modulation output, emitted spectra of 16-QAM OFDM modulation outputs over the fiber link **f** before 50 km, **g** after 50 km, downlink receiver stage photo detector as well as OFDM demodulated output for **h** in-phase and **i** quadrature channels; at receiver the received 16-QAM constellation diagram after **j** OFDM demodulator, **k** bessell filtering, **l** resampling process, **m** nonlinear and dispersion compensation, **n** an adaptive equalizer, **o** output at FEO and **p** CPE, **q** signal electrical spectrum after 16-QAM, **r** output optical spectrum of LD at 390 nm wavelength, **s** optical spectrum after 10 m VLC link and **t** BER analyser eye diagram

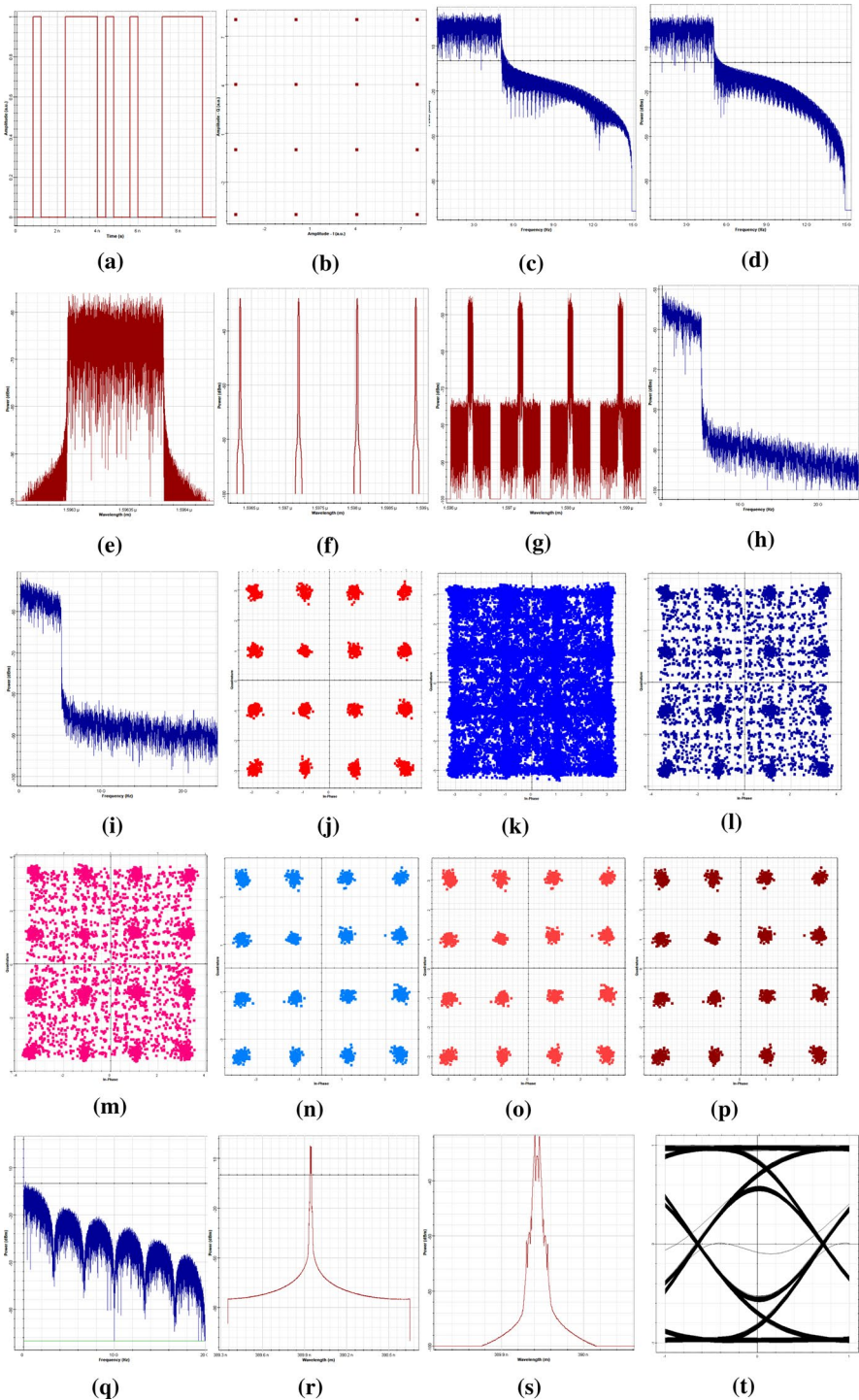
the required limit of 12.5% while for 32- and 64-QAM are above the required limits of 10% and 8% respectively with the reference of 3GPP specifications (Nguyen et al. 2019). Thus, it is observed that even at higher received power, high-order QAM modulation formats are more sensitive to noise. The minimal received optical powers required to fulfill the limits are -16 dBm and -14 dBm for 16-QAM VLC downstream and upstream signals respectively. However, for both 32- and 64-QAM VLC downstream and upstream signals, the required received power is more than -2 dBm. Thus, for the proposed link, the 16-QAM modulation format shows better performance than other formats. Influenced by issues of in-phase/quadrature-phase mismatches in the modulator/demodulator components due to gain, dc offset and phase differences, EVM shows rise in values in %age and thus, degrade the system performance. Also, illustrated in insets are the constellation diagrams depicting the high-quality data transmission of 16-QAM followed by 32- and 64-QAM modulation formats. Further, the calculated BER based on the EVMs for m-QAM are also evaluated as given in Eq. (21) (Nguyen et al. 2019):

$$BER_{m-QAM} = \frac{2}{\log_2(m)} \left( 1 - \frac{1}{\sqrt{m}} \right) \cdot \text{erfc} \left( \sqrt{\frac{3}{2(m-1)} \times \frac{1}{EVM^2}} \right) \quad (21)$$

where *erfc* (.) means the complementary error function. Table 4 shows the calculated BER results for the proposed 16-, 32- and 64-QAM VLC downstream and upstream signals.

The above-reported results show that the BER values are below the 7% FEC limit (at BER = 3.08 × 10<sup>-3</sup>) for 16-QAM downstream and upstream signals. While for 32- and 64-QAM, the BER values are above the FEC limit in the bidirectional transmission. Hence, 16-QAM modulation is desirable for improving the performance of the proposed PON/VLC link.

Figure 10(a) to 10(f) present the BER versus modulation peak current of 16-, 32- and 64-QAM OFDM downstream and upstream signals over the fixed 8000 m VLC and 50 km fiber links at the transmission rate of 10 Gbps. From Fig. 10 it is found that BER value decreases with the increase of input modulation peak current up to 9 mA for downstream/upstream signals beyond which it again increases. The BER value increases before 9 mA, decrease at 9 mA and again increases after 9 mA because of the dominant under-modulation, peak-modulation and cross-modulation effects in the wireless links. Also, it can be observed that as the modulation type increases from 16- to 64-QAM, the BER of the downstream and upstream received signals for all wavelengths increases. In the downstream



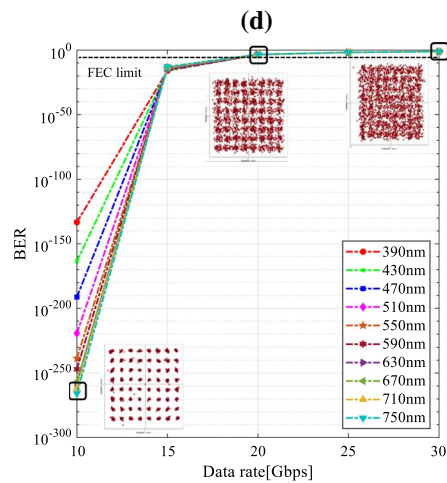
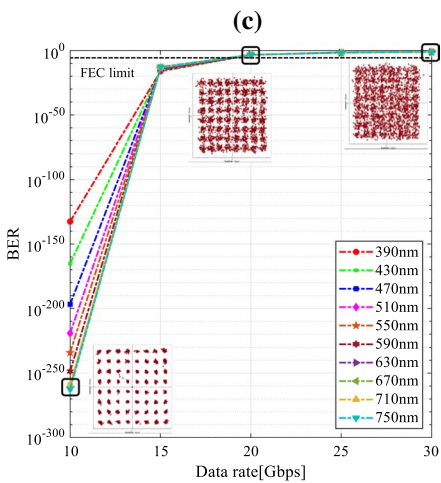
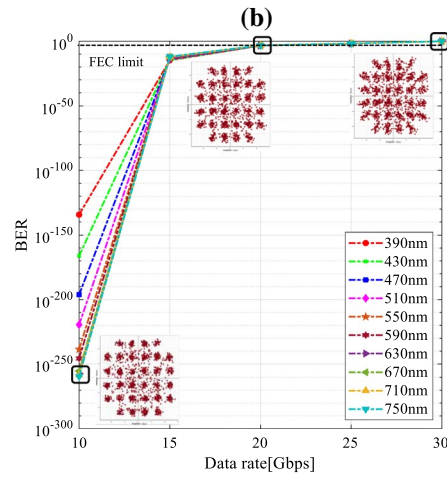
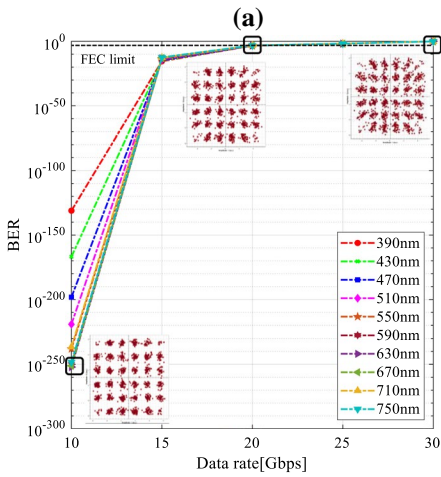
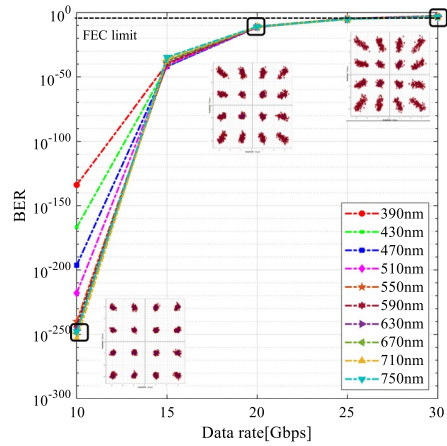
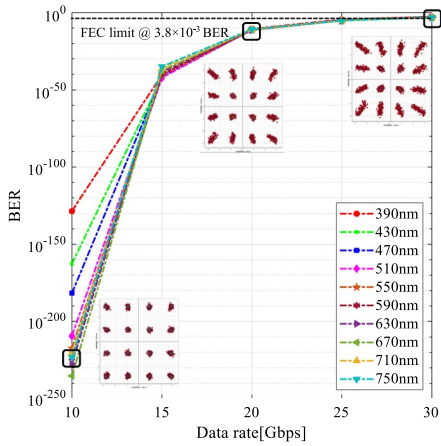
**Fig. 8** BER versus data rate of different wavelengths VLC signals for **a** downstream 16-QAM, **b** upstream 16-QAM, **c** downstream 32-QAM, **d** upstream 32-QAM, **e** downstream 64-QAM and **f** upstream 64-QAM modulation formats. Insets show the corresponding constellation diagram at different data rates

direction, the minimum obtained BER at a modulation current of 9 mA for 16-, 32- and 64-QAM modulation formats is measured as  $6.46 \times 10^{-12}$ ,  $1.13 \times 10^{-11}$  and  $4.12 \times 10^{-9}$  respectively. Also, in the upstream direction, the minimum obtained BER at a modulation peak current of 9 mA for all three modulation formats is measured as  $4.36 \times 10^{-10}$ ,  $4.58 \times 10^{-10}$  and  $5.63 \times 10^{-8}$  respectively. Thus, the obtained results demonstrate the best performance of the proposed TWDM-PON employing 16-QAM modulation format followed by 32- and 64-QAM modulation formats at 9 mA modulation current set for individual wavelength LDs in the VLC system.

Table 5 illustrates that the previously work done in the literature deploy 4-, 16-, 32- and 64-QAM modulation formats capable of transferring data only up to highest of 3.6 km wireless and 50 km SMF range at the transmission rate of 80 Gbps. Whereas higher data rate of 120 Gbps over long-reach wired-wireless links per channel of 8 km wireless and 50 km wired is obtained by using m-QAM OFDM modulation format and multi-color LDs based VLC system than previous work under BER of  $10^{-3}$ . Further, the power budget (PB) with receiver sensitivity at 10 dBm input power of the proposed system for 8000 m VLC link using the following Eq. (22) is calculated in Table 6.

$$PB = LaunchPower - RS \quad (22)$$

In Table 7 the proposed system shows that the previously reported works deploy 4-, 16- and 64-QAM modulation formats are capable of sending information only up to 3600 m wireless and 50 km fiber link range at the transmission rate of 80 Gbps with low/medium deployment cost. While the high information rate over fiber/VLC links per channel than previous work is received by using 16-, 32- and 64-QAM OFDM modulation format and multi-color LDs based VLC system in the proposed PON/VLC link at medium deployment cost. It shows that the proposed TWDM PON system offers high data rate, efficient bandwidth utilization by supporting the large number of customers with cost-effectiveness, reliable, scalable, flexible and easy upgradeable features.



(a)

(b)

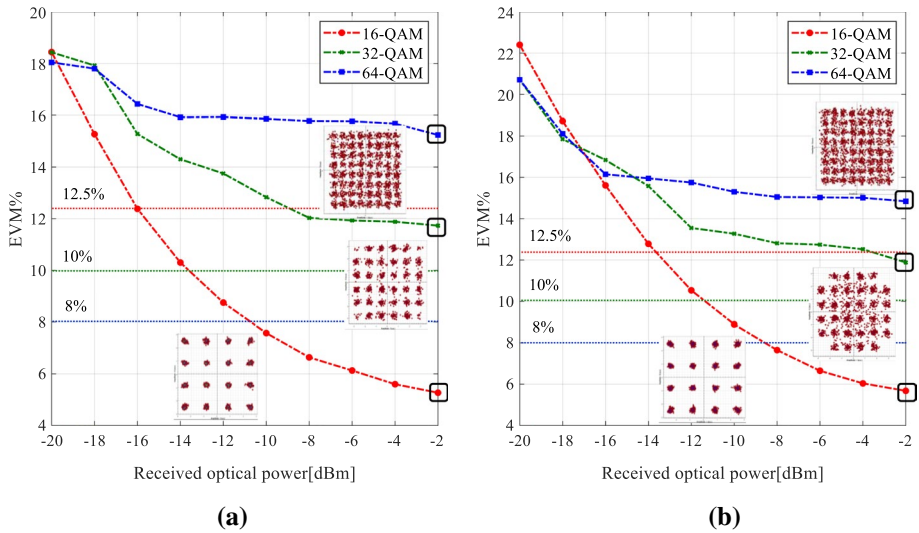
(c)

(d)

(e)

(f)

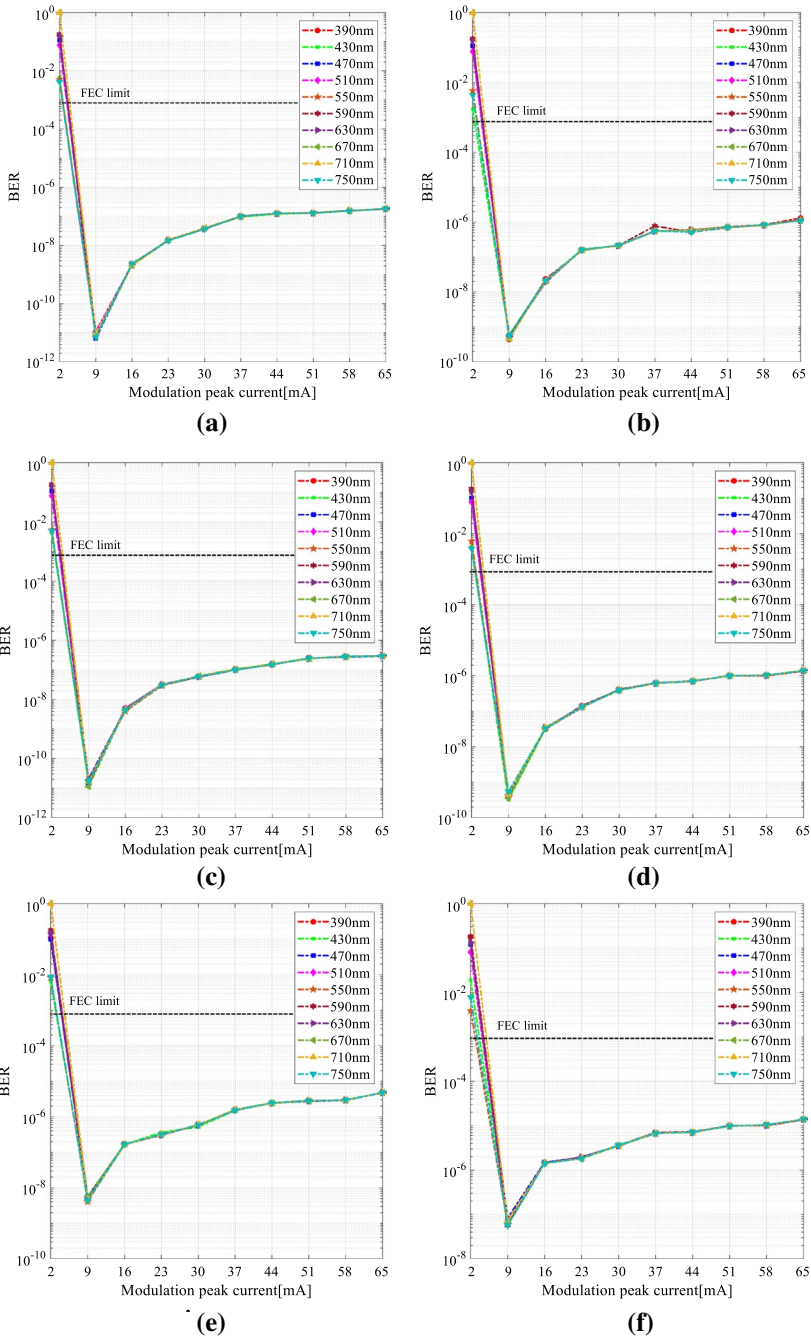




**Fig. 9** EVM versus received optical power of 750 nm wavelength VLC signal for **a** downstream 16-, 32- and 64-QAM and **b** upstream 16-, 32- and 64-QAM modulation formats. Insets show corresponding constellation diagram at -2 dBm received optical power

### 5 Conclusion

In this paper, a full-duplex  $4 \times 10$  Gbps TWDM-PON utilizing 16-, 32- and 64-QAM OFDM modulation formats with ten different colors LDs enabled VLC system has been demonstrated. From results, it is concluded that the faithful wireless range in PON/VLC link varies from 10 to 8000 m at a fixed fiber length of 50 km and 9 mA LD input modulation peak current with minimum acceptable BER of  $3.8 \times 10^{-3}$ . Also, the highest achieved transmission rates for the designed system employing m-QAM modulation with 10 m free space and 10 km fiber link range are 120 Gbps for 16-QAM, 100 Gbps for 32-QAM and 80 Gbps for 64-QAM in both downstream and upstream directions. Moreover, it is investigated that for 16-QAM modulation, the recovered downstream and upstream signals show measured EVM and calculated BER values are lower than the FEC threshold as defined by 3GPP specifications. Again, the correlated performance of the proposed system performance with the recent previous literature indicates the significant superiority for the maximum transmission length and data rate. Hence, the system can be utilized to offer economic and high-speed fiber/wireless link based applications for the 5G based applications.



**Fig. 10** Measured BER versus modulation peak current of different wavelengths VLC signals for (a) downstream 16-QAM, (b) upstream 16-QAM, (c) downstream 32-QAM, (d) upstream 32-QAM, (e) downstream 64-QAM and (f) upstream 64-QAM modulation formats

**Table 3** Comparative analysis of the proposed PON/VLC link over 10 km fiber distance with earlier works

Reference	Technique used	Modulation format	Maximum wireless range (m) @BER of $10^{-3}$	Maximum SMF length (km) @ BER of $10^{-3}$	Maximum Data rate (Gbps) @BER of $10^{-3}$
(Rahman et al. 2020)	RoF-VLC	16-QAM	3	10	2.5
(Tang et al. 2020)	OFDM in hybrid fiber – VLLC system	64- and 128-QAM	5	10	10
Proposed work		16-, 32- and 64-QAM	10	10	10

**Table 4** Calculated BER results for the proposed work at a received power of -2 dBm

m-QAM	Downstream		Upstream	
	EVM(%)	BER	EVM(%)	BER
16-QAM	5.27	$8.01 \times 10^{-18}$	5.68	$1.29 \times 10^{-15}$
32-QAM	11.73	$2.29 \times 10^{-3}$	11.88	$2.90 \times 10^{-3}$
64-QAM	15.24	$4.43 \times 10^{-2}$	14.84	$4.12 \times 10^{-2}$

**Table 5** Comparative analysis of proposed PON/VLC link over 50 km fiber distance with previous works

Reference	Technique used	Modulation format	Maximum wireless range (km) @BER of $10^{-3}$	Maximum SMF length (km) @BER of $10^{-3}$	Aggregate Maximum Data rate (Gbps) @ BER of $10^{-3}$
(Shi et al. 2018)	WDM fiber VLLC system based on OFDM/OQAM	4- and 16-QAM	0.0045	50	3.2
(Mallick et al. 2019)	OFDM-FSO system	16-QAM	0.5	50	10
(Singh and Malhotra 2019)	Hybrid MDM-OFDM-FSO syem	4-QAM	3.6	50	80
Proposed work		16-, 32- and 64-QAM	8	50	120

**Table 6** Power Budget for the proposed system for 8000 m VLC link

Channels	PB (dB)	RS (dBm)
Downstream	20	- 10
Upstream	60	- 50



**Table 7** Comparative analysis of the proposed work with earlier recent works

References	Techniques used	Modulation formats	Maximum wireless range (m) @BER of $10^{-3}$	Maximum SMF length (km) @BER of $10^{-3}$	Maximum Data rate (Gbps) @BER of $10^{-3}$	Deployment cost
(Shi et al. 2018)	OFDM/OQAM based WDM fiber VLLC system	4- and 16-QAM	4.5	50	3.2	Medium
(Wei et al. 2017)	OFDM in fiber-VLLC system	16-QAM	8	20	2.5	Medium
(He et al. 2016a)	DM-CAP-PON integration with VLLC system	16-QAM	8	30	16	Medium
(Shaddad et al. 2012)	Wireless MIMO OFDM signals over WDM PON	64-QAM	100	20	7.68	Medium
(Mallick et al. 2019)	OFDM-FSO system	16-QAM	500	50	10	Low
(Singh and Malhotra 2019)	Hybrid MDM-OFDM-FSO system	4-QAM	3600	50	80	Low
Proposed work		16-, 32- and 64-QAM	8000	50	120	Medium

**Acknowledgements** The authors are thankful to Punjabi University, Patiala, India and Guru Nanak Dev University, Amritsar, India for providing opportunity and technical support to complete the work as effective.

**Author contributions** All authors contributed to the study conception and design.

**Funding** Not applicable.

**Declarations**

**Conflicts of interest** The authors declare that they have no conflict of interest.

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