

A theoretical proposal of high performance blood components biosensor based on defective 1D photonic crystal employing WS₂, MoS₂ and graphene

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Abstract

In this research, a novel confguration of 1D photonic crystal (PhC) is proposed for the detection of numerous elements present in human blood such as plasma, RBC, biotin, serum albumin. The proposed structure is envisaged with an alternate arrangement of $CaF₂$, PtSe₂ and ZnSe with a central defect layer, where the wall of the defect layer is separately coated with novel 2D materials like WS_2 , MoS₂ and graphene to enhance the sensor performance. The well-known transfer matrix method (TMM) is employed to compute the transmission spectrum and absorption spectrum by infltrating the defect layer with blood components. The cornerstone of this work is to observe the shift in the defect mode wavelength in the transmission spectrum. The geometrical parameters of the structure such as thickness of dielectric layers, defect layer, refractive index of dielectric layers and the number of period are judiciously optimized to realize efective sensor. The efect of variation in the defect layer thickness and angle of incidence on the transmission spectrum is thoroughly studied. Additionally, the number of layers of WS_2 , MoS₂ and graphene are suitably optimized for design of high performance biosensor. Various sensing characteristics such as sensitivity, signal-to-noise ratio (SNR), quality factor (QF), fgure of merit (FOM), resolution and detection limit (DL) are evaluated and compared for the proposed WS_2 , MoS₂ and graphene based sensor confgurations. Moreover, the simple structure, cost-efective fabrication methods and label-free detection of blood components make the proposed sensor a promising challenger for biosensing applications.

Keywords Defect based 1D photonic crystal · Transfer matrix method · Transmission spectrum · Biosensor · Sensing performance

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1 Introduction

Photonic crystal structures (PhCs) were frst introduced by E. Yablonovitch and S. John in early 1987, which brought a revolution in the research domain of photonics by exploring an array of novel applications (Yablanovitch [1987;](#page-18-0) John [1987;](#page-17-0) Elsayed [2018](#page-16-0); Abd El-Aziz et al. [2019a\)](#page-16-1). The PhCs are the special class of artifcial arrangements, which are envisaged as the periodic organization of low and high refractive index materials (Devashish et al. [2019;](#page-16-2) Ahmed and Mehaney [2019\)](#page-16-3). Among the various PhCs confgurations (1D/2D/3D), 1D structures have experienced a signifcant rise in demand owing to their simple structural arrangement, low loss, cost-efective fabrication techniques, compatibility with photonic integrated circuits, and extensive application area (Panda and Devi [2020](#page-17-1); Panda et al. [2018\)](#page-17-2). When electromagnetic (EM) waves are interacted with PhCs, a distinctive property is perceived known as photonic band gap (PBG), where light of certain frequency ranges are prohibited to pass through the structure (Ghasemi et al. [2019;](#page-16-4) Entezar et al. [2015\)](#page-16-5). The properties of PBG are strongly infuenced by the nature of applied material such as semiconductor, metamaterial, metal, plasma, superconductor, nano-composite materials etc. (Aly and Sayed [2020;](#page-16-6) Shi et al. [2001\)](#page-17-3). A defect can be realised in a perfect PhC by breaking its periodicity via altering the geometrical properties of a layer, introducing a diferent material into the structure or exterminating a layer from the structure (Boedecker and Henkel [2003](#page-16-7); Hattori [2002\)](#page-17-4). When the incident light frequency matches with the defect mode frequency, the photons are positioned within the band gap, which forms a resonant peak (Ghasemi et al. [2019](#page-16-4); Hemmatyar et al. [2017](#page-17-5)). The position and intensity of these resonant peaks are varied with nature of dielectric materials, nature of defect layer, thickness of the defect layer.

Over the last decade, 1D PhC structures have been extensively employed for various bio-sensing applications. Aly et al. ([2020a\)](#page-16-8) reported a defect based 1D PhC with a sensitivity of 306.25 nm RIU^{-1} to detect various concentrations of creatinine present in the blood. Jahania et al. [\(2020](#page-17-6)) studied the defective PhC structure with inclusion of graphene sheets for biochemical sensing application in terahertz regime. A highly sensitive alcohol sensor is presented (Shaban et al. [2020](#page-17-7)) to detect diferent concentrations of ethanol, methanol and propanol by employing the transfer matrix method. Bouzidi et al. [\(2017](#page-16-9)) investigated the shifts in the refectance spectrum of a defect based PhC structure with respect to various glucose concentrations in blood. The reference (Abd El-Aziz et al. [2019b](#page-16-10)) proposed a defected 1D PhC biosensor for sensing protein concentrations, where the authors analysed the efect of defect layer thickness on the sensitivity. However, the authors found a maximum sensitivity of only 170 nm per RIU. Nouman et al. ([2020\)](#page-17-8) inspected the shift in resonant wavelength in a defect based 1D PhC for detection of brain lesions in a very small time. A 2D PhC with line defect is proposed (Sharma et al. [2014](#page-17-9)) to detect diferent blood components using FDTD (fnite domain time diference) approach. A PhC ring resonator structure is reported in the wavelength range 1530–1615 nm for sensing various blood components, where the authors obtained a quality factor of 262 and detection limit of 0.002 RIU−1 (Arunkumar et al. [2019](#page-16-11)). Mohammad et al. [\(2019](#page-17-10)) studied a 2D PhC with nanocavity to sense numerous blood components. But in the references (Sharma et al. [2014;](#page-17-9) Arunkumar et al. [2019;](#page-16-11) Mohammed et al. [2019\)](#page-17-10), the proposed structures are relatively complex and difficult to fabricate with high accuracy.

The performance of 1D PhC structure can be greatly enhanced by using novel materials like graphene, WS_2 and MoS_2 . So, we have included these 2D materials in our design, to enhance the sensing performance. Graphene has received enormous attention on electromagnetic applications owing to its unmatched attributes, for instance, robustness, high mobility, one atom thickness, fexibility, durability, extraordinary optical, thermal and electrical conductivity at room temperature, frequency-independent absorption of EM radiation (Falkovsky and Pershoguba [2007;](#page-16-12) Geim [2009](#page-16-13); Bonaccorso et al. [2010\)](#page-16-14). Graphene has emerged as a suitable candidate for superb conductive support for nanoparticles to realize hybrid nanocomposites (Li[u, 2018;](#page-17-11) Wei[, 2017](#page-18-1); Zang[, 2017](#page-18-2)). The conductivity of graphene can be regulated over a wide frequency range by changing the chemical potential across the graphene sheets, which can appositely alter the optical properties of photonic structures integrated with graphene. The coating of graphene can signifcantly increase the sensitivity to change in refractive index. A sort of 2D materials such as WS_2 and MoS_2 , which belong to the Transition metal dichalcogenides (TMD) group, have attracted a substantial research attention owing to their scalability property, and thickness dependent optical properties. WS₂ and MoS₂ has large band gap of 1.94 eV and 1.77 eV respectively, which is higher than the conventional semiconductor materials, thus make them feasible to manage a high temperature and voltage. With a broad work function of 5.1 eV, $MoS₂$ ofers high afnity surface area to absorb the bio-analytes and thus utilized in bio-sensing applications (Kukkar et al. 2016). WS₂ comprises a hexagonal crystal structure and shows a higher 2nd order nonlinear susceptibility and broad frequency response (Janisch[, 2015](#page-17-13)). Moreover, the high photoluminescence, nonblinking photon emission, wider PBG (visible to near-infrared wavelength range) and large surface area of WS₂, high spin orbit coupling of 420 meV, makes it a favourable material to realize biosensors (Yuan and Huang [2015](#page-18-3); Zhu et al. 2015). Recently, PtSe₂ has evolved as a gifted material for various optoelectronic applications, owing to its unmatched electrical and optical properties, and adjustable bandgap in the range 1.2 eV to 0.21 eV (Wan[g, 2015\)](#page-18-5). In addition to this, $PtSe₂$ is highly inertness towards various chemical agents and shows good resistant to toxic efect, which makes it a suitable candidate for bio sensing applications (Jia et al. [2020\)](#page-17-14).

Blood is the most important aspect of human body, as it runs the oxygen and food to each corner of the body. Blood cells are consisted of a verity of components like red blood cell (RBC), white blood cell (WBC), pallets, biotin, plasma etc. The blood appears to be red color because of presence of RBC in it, whereas the liquid part of the blood is plasma. Biotins are constituted with various types of vitamin and pallets are made up of bone marrow and help in clotting of blood. Any disorder in the blood fow in body may incur numerous diseases like lymphoma, myeloma, leukemia, anemia, malaria, haemophilia. So, it is indispensable to correctly and timely detect various concentrations of blood components to avoid any chance of fatality. Nevertheless, diferent methods of blood tests are available like kombo test, blood smear, blood count, bone marrow biopsy, fame atomic absorption spectroscopy (Wolf and Zitelli [1987\)](#page-18-6), but these tests are time consuming and require more blood samples and sophisticated laboratory facilities. Optical bio-sensing technique can be an apposite alternative for the analysis of diferent blood components as this method requires small amount of blood samples for detection and provides accurate results in less time. Mainly, two types of optical methods can be applied to test blood components such as fuorescent technique and label-free detection technique. As it is quite challenging to perform quantitative analysis of blood components using fuorescent technique, so the labelfree detection technique is widely used by the research community. In label-free detection technique, refractive index of blood components plays the most vital role to analyse the sample (Boyd and Heebner [2001;](#page-16-15) White and Fan [2008\)](#page-18-7). The refractive index based labelfree detection method greatly simplifes the sensing process by reducing the time, efort and experimental artefacts. Apart from this, the refractive index based sensors are extensively studied and practically employed for a broad bio-sensing applications (Aly et al.

[2020a;](#page-16-8) Jahania et al. [2020;](#page-17-6) Shaban et al. [2020](#page-17-7); Bouzidi et al. [2017;](#page-16-9) Abd El-Aziz et al. [2019b;](#page-16-10) Nouman et al. [2020](#page-17-8); Sharma et al. [2014](#page-17-9); Arunkumar et al. [2019](#page-16-11); Mohammed et al. [2019\)](#page-17-10).

This research proposes label-free detection of various blood components such as water, plasma, RBC, biotin and serum albumin having refractive index of 1.330, 1.350, 1.400, 1.450 and 1.470 respectively (Sharma et al. [2014](#page-17-9); Arunkumar et al. [2019](#page-16-11); Mohammed et al. [2019](#page-17-10)). For this purpose, a defect based 1D PhC structure is employed, which includes completely new combination of dielectric materials CaF_2 , $PtSe_2$ and $ZnSe$ along with other novel 2D materials like $MoS₂$, WS₂ and graphene. To the best of author's knowledge, first time we have proposed such kind of novel 1D structures to realize high performance blood components sensor. Diferent geometrical parameters like thickness of dielectric layers, thickness of defect layer, thickness of 2D materials, period of the dielectric layers, incident angle are properly optimized, which add another feather of novelty to this work. Both transmission and absorption spectrum are investigated here, which is not found in any of the research listed in the literature. Aside from this, a complete set of performance measuring parameters such as sensitivity, signal-to-noise ratio (SNR), quality factor (QF), fgure of merit (FOM), resolution (R), detection limit (DL) are computed. Moreover, with the available simple and cost efective fabrication methodologies, the authors believe that the proposed sensor can bring a remarkable advancement in the biosensing applications.

2 Proposed model and method

In this communication, a central defect based 1D PhC with the periodic arrangement of $CaF₂$, PtSe₂ and ZnSe is investigated, which is shown in Fig. [1](#page-3-0). The motivation for selecting these materials is their large refractive index diference and feeble absorption in the considered wavelength range. A defect is created at the centre, which is infltrated with blood as the analyte to detect its various components. The sidewalls of the defect layer (D) are separately coated with novel 2D materials like graphene, $MoS₂$ and $WS₂$ to efficiently

Fig. 1 Schematic view of the proposed 1D PhC sensor

absorb the analytes. Herewith, we have assayed three diferent multilayer confgurations such as $(CaF_2/PtSe_2/ZnSe)^N$ (graphene/D/graphene)(CaF₂/PtSe₂/ZnSe)^N,(CaF₂/PtSe₂/ $ZnSe$ ^N(WS₂/D/WS₂)(CaF₂/PtSe₂/ZnSe)^N and (CaF₂/PtSe₂/ZnSe)^N(MoS₂/D/MoS₂)(CaF₂/ PtSe₂/ZnSe)^N. The period (N) of the aforementioned structures is selected as N=5. A He–Ne laser source is used to generate a light of wavelength 632.8 nm, which incidents on the proposed structure. The refractive index of CaF₂ and ZnSe is taken as $n_{CaF_2} = 1.432$ and $n_{ZnSe} = 2.578$, whereas their thickness are chosen as $d_{CaF_2} = d_{ZnSe} = 300$ nm. We also analysed the transmittance spectrum for higher values of d_{CaF_2} and d_{ZnSe} , but we found that for higher thickness values, the resonant modes are more broadened and show high FWHM, which is undesired. Refractive index of PtSe₂ is selected as $n_{PtSe_2} = 3.016 + 1.673 * i$ at a thickness of $d_{PtSe_2} = 6$ nm (Guo [2020\)](#page-16-16). At the considered wavelength of 632.8 nm, refractive index of graphene is considered as 3 + 1.149 ∗ *i* (Han [2019;](#page-17-15) Keshavarz et al. [2020](#page-17-16)). Similarly, refractive index of MoS₂ and WS₂ is computed as $n_{M_0S_2} = 5.08 + 1.172 * i$ and $n_{WS_2} = 4.9 + 0.312 * i$ respectively at 632.8 nm (Han [2019;](#page-17-15) Keshavarz et al. [2020\)](#page-17-16). Thickness of graphene, MoS_2 and WS_2 is selected as $0.34*L$ nm, $0.65*L$ nm and $0.80*L$ nm respectively, where L signifies the number of layers (Han [2019;](#page-17-15) Keshavarz et al. [2020](#page-17-16)). The transfer matrix method (TMM) is manipulated to study the transmittance spectrum of the proposed structure for various blood components at defect layer thicknesses (d_D) of 400 nm and 500 nm.

With a tremendous advancement in technology, the authors are confdent that the proposed 1D structure can be easily fabricated. Diferent layers of dielectric materials like $CaF₂$ and ZnSe can be precisely fabricated on a glass substrate by several accepted methods such as sol–gel method (Ilinykh and Matyushkin [2016\)](#page-17-17), magnetron sputtering (Schürmann et al. [2006](#page-17-18)), spin coating (Wang et al. [2008\)](#page-17-19), and chemical vapour deposition (CVD) (Chen et al. [2008\)](#page-16-17). Moreover, recently Zahid et al. ([2020\)](#page-18-8) and Mittal et al. ([2017\)](#page-17-20) experimentally fabricated a thin film of $CaF₂$ and ZnSe. Apart from this Qi et al. ([2018\)](#page-17-21), reported the detail fabrication process for realization of various 2D TMDs materials like graphene, $MoS₂$ and WS₂, PtSe₂ by using different methods like physical vapour transport (PVT), molecular beam epitaxy (MBE), chemical vapour deposition (CVD), and mechanical exfoliation. With the aforementioned fabrication techniques, the authors believe that it is feasible to realize the proposed sensor.

3 Mathematical analysis

Transfer matrix method (TMM) is employed for efective analysis of band gap characteristics through computation of transmission spectra of the proposed layered 1D PhC (Aly et al. [2020a](#page-16-8); Abd El-Aziz et al. [2019b\)](#page-16-10). Each layer is represented in the form of its own matrix and the overall transfer matrix of the entire structure is computed through multiplication of all the discrete layer matrices. As shown in Fig. [1,](#page-3-0) the EM waves incident on the proposed structure at angle θ_i and propagate along the x direction, which confirm that the electric fields (E_m) and magnetic fields (H_m) propagate in y–z plane. The electric field and magnetic field in air i.e. E_0 and H_0 can be computed by solving the following matrix equation,

$$
\begin{bmatrix} E_0 \\ H_0 \end{bmatrix} = M_1, M_2, M_3, \dots M_N \begin{bmatrix} E_m \\ H_m \end{bmatrix}
$$
 (1)

where N represents the total number of layers with inclusion of the defect layer, M specifes the characteristics matrix. The characteristics matrix of the *p*th layer can be expressed as,

$$
M_p = \begin{bmatrix} \cos \delta_p & \left(-\frac{i}{\varphi_p} \right) \sin \delta_p \\ -i \varphi_p \sin \delta_p & \cos \delta_p \end{bmatrix}
$$
 (2)

where

$$
\delta_p = \frac{2\pi}{\lambda} d_p n_p \cos \theta_p \tag{3}
$$

where λ denotes the incident wavelength, n_p is the refractive index and d_p is the thickness of the *p*th layer. Here, θ_p is the incident angle in the *p*th layer. Further, φ_p can be written as,

$$
\varphi_p = \sqrt{\frac{\epsilon_0}{\mu_0}} n_p \cos \theta_p \quad \text{for TE mode} \tag{4a}
$$

$$
\varphi_p = \sqrt{\frac{\varepsilon_0}{\mu_0}} \frac{n_p}{\cos \theta_p} \quad \text{for TM mode} \tag{4b}
$$

where μ_0 and ϵ_0 denote the free space permeability and permittivity respectively. The characteristic matrix for the entire structure can be expressed as,

$$
M = \begin{bmatrix} M_{11} & M_{12} \\ M_{21} & M_{22} \end{bmatrix} = \left(M_A M_B M_C \right)^N M_{2D} M_{Defect} M_{2D} \left(M_A M_G M_B M_G \right)^N \tag{5}
$$

Here, M_A , M_B , M_C and, M_{Defect} denote the characteristics matrix of CaF₂, PtSe₂, ZnSe and defect layer respectively. M_{2D} is the characteristics matrix of the WS₂ / MoS₂ / graphene layer. The elements of the matrix obtained in the above equations can be used to compute transmittance coefficient and reflection coefficient (Panda and Pukhrambam 2021), which can be specifed as,

$$
t = \frac{2\Psi_0}{\left(M_{11} + M_{12}\Psi_1\right)\Psi_0 + \left(M_{21} + M_{22}\Psi_1\right)}\tag{6}
$$

$$
r = \frac{(M_{11} + M_{12}\Psi_1)\Psi_0 - (M_{21} + M_{22}\Psi_1)}{(M_{11} + M_{12}\Psi_1)\Psi_0 + (M_{21} + M_{22}\Psi_1)}
$$
(7)

where $\Psi_0 = \sqrt{\mu_0/\epsilon_0} n_0 cos\theta_0$ and $\Psi_s = \sqrt{\mu_0/\epsilon_0} n_s cos\theta_s$. Here, n_0 and n_s are the refractive index of the air and substrate respectively.

Finally, transmittance (T) and reflectance (R) of the entire structure are computes as,

$$
T = \frac{\Psi_1}{\Psi_0} \left| t^2 \right| \quad and \quad R = |r|^2 \tag{8}
$$

Absorption (A) of the multilayer structure can be given as,

$$
A = 1 - T - R \tag{9}
$$

As, we observed that the refractive index plays a vital role in the computation of the transfer matrix of each layer. The refractive index of diferent dielectric layers can be obtained from the Sellmeier equations ([https://refractiveindex.info/?shelf=main&book=](https://refractiveindex.info/?shelf=main&book=CaF2&page=Malitson) [CaF2&page=Malitson](https://refractiveindex.info/?shelf=main&book=CaF2&page=Malitson); [https://refractiveindex.info/?shelf=main&book=ZnSe&page=](https://refractiveindex.info/?shelf=main&book=ZnSe&page=Marple) [Marple](https://refractiveindex.info/?shelf=main&book=ZnSe&page=Marple)), which are stated as follows,

$$
n_{\text{CaF2}}^2 = 1 + \frac{0.5675888\lambda^2}{\lambda^2 - 0.0050263605^2} + \frac{0.4710914\lambda^2}{\lambda^2 - 0.1003909^2} + \frac{3.8484723\lambda^2}{\lambda^2 - 34.649040^2} \tag{10}
$$

$$
n_{\text{ZnSe}}^2 = 4 + \frac{1.90\lambda^2}{\lambda^2 - 0.113} \tag{11}
$$

The dielectric function of monolayer of $MoS₂$ and $WS₂$ can be obtained by fitting with multi-Lorentzian function, which is given as (Gan[, 2019\)](#page-16-18),

$$
\varepsilon(E) = 1 + \sum_{i=1}^{N} \frac{f_i}{E_i^2 - E^2 - jE\rho_i}
$$
 (12)

where E signifies the energy of the photon particle, which is given as $(eV) = \frac{1.2398}{\lambda(\mu m)}$, the model parameters f_i , E_i and ρ_i represent the oscillation strength, resonance energy and spectral width of *i*th oscillation respectively. The value of f_i , E_i and ρ_i can be determined from the experimental data presented in the reference (Kravets[, 2017\)](#page-17-23).

The wavelength dependent refractive index of graphene nanolayer can be computed as given below (Lin and Chen [2019](#page-17-24)),

$$
n_{graphene} = 3 + i\left(\frac{C_1}{3}\right) \times \lambda \tag{13}
$$

where C_1 is constant, which is nearly equal to 5.446 μ m⁻¹ and λ denotes the wavelength of the incident light.

3.1 Sensor performance

Sensitivity (S) is the vital parameter to evaluate the sensor performance. Sensitivity is defned as the ratio of change in resonant wavelength (Δ*𝜆res*) to the change in RI (Δ*n*) between diferent blood components, and can be expressed as (Panda et al. [2021](#page-17-25)),

$$
S(nm/RIU) = \frac{\Delta \lambda_{res}}{\Delta n}
$$
 (14)

SNR is defined as the ratio of shift in resonant peak wavelength $(\Delta \lambda_{res})$ to the spectral half-width of the transmission dip $(\Delta \lambda_{1/2})$. Detection limit is signified as the smallest refractive index variation that can be accurately detected by the sensor, whereas resolution of a sensor is defned as the smallest spectral shift, which can be quantifed with high accuracy. FOM is the capability of the sensor to sense any small variations in the resonance peak. The aforesaid sensing parameters can be expressed numerically as below (Aly et al. [2020a;](#page-16-8) Nouman et al. [2020](#page-17-8); Panda and Pukhrambam [2021](#page-17-22)),

$$
SNR = \frac{\Delta \lambda_{res}}{\Delta \lambda_{1/2}}\tag{15}
$$

$$
FOM = \frac{S}{\Delta \lambda_{1/2}}\tag{16}
$$

$$
Quality factor = \frac{\lambda_{res}}{FWHM}
$$
 (17)

$$
R = \frac{\Delta \lambda_{1/2}}{1.5 \times SNR^{1/4}}
$$
 (18)

$$
DL = \frac{R}{S}.\tag{19}
$$

4 Results and discussions

The keystone of the present research is the study of transmission spectrum of the proposed defective 1D structure by employing TMM technique. The resonant modes or defect modes, formed within the PBG, are investigated for diferent components of blood like plasma, RBC, biotin, serum albumin. We discretely investigated the shift in resonant mode wavelength by separately coating the wall of the defect layer with graphene, $MoS₂$ and $WS₂$. The structure parameters like defect layer thickness (d_D) and angle of incidence (θ_i) are properly optimized. The transmittance characteristic is analysed for $d_D = 400$ nm and 500 nm, whereas θ_i is selected as 20° and 40°. For higher values of d_D and θ_i , it is observed that more than one defect modes are formed within the PBG and the intensity of the defect modes are decreased, which makes the analysis difficult and bestows poor performance. So, we restricted our analysis only to $d_D = 400$ nm and 500 nm, and $\theta_i = 20°$ and 40°.

Figure [2](#page-8-0) depicts the transmission spectra of the proposed 1D structure by infltrating the defect layer with various blood components at diferent defect layer thickness of 400 nm and 500 nm. This analysis is performed separately by coating the structure with novel 2D materials like WS_2 , MoS_2 and graphene. Here, it is observed that, with an increase in refractive index of the blood components, the resonant peak formed within the transmission spectrum is shifted towards higher wavelength. This red-shift phenomenon of defect mode wavelength takes place according to the standing wave condition (Zeng et al. [2014\)](#page-18-9),

$$
\sigma = m\lambda = n_{\text{eff}}\rho \tag{20}
$$

where σ and ρ represent the optical path difference and geometrical path difference respectively, λ denotes the wavelength of the incident light, m is an integer and n_{eff} is the effective refractive index of the proposed structure. Upon infltrating the defect layer with diferent blood components, n_{eff} of the defect layer increases, which leads to red-shift in the wavelength, such that σ remains fixed. Additionally, it is perceived that for an increase in defect layer thickness, the resonant peak is red shifted within the PBG. Further, we observed that in case of graphene based sensor confguration, resonant peaks are envisaged at higher wavelengths as compared to WS_2 and MoS_2 based sensor configuration.

Fig. 2 Transmission spectra of the proposed sensor at $\theta_i = 0^\circ$. **a** WS₂. **b** MoS₂. **c** graphene

We investigated the nature of variation in the wavelength of the resonant peaks of different blood components for all the three shorts of proposed confgurations. The position of resonant mode or defect mode depends upon the defect layer thickness and refractive index of the analyte. In Fig. [3,](#page-9-0) shift in the resonant wavelength is plotted along the primary vertical axis for $d_D = 400$ nm, whereas the same for $d_D = 500$ nm is plotted along the secondary vertical axis in the reverse order. From this fgure it is evident that with an increase in the refractive index of the blood components, resonant wavelength increases linearly. Also, it can be observed that for $d_D = 500$ nm, resonant mode is attained at high wavelengths as compared to the case for $d_D = 400$ nm in all the three proposed configurations. It is revealed that for the graphene based structure, resonant modes are formed at higher wavelengths than WS_2 and MoS_2 based structures.

Sensitivity of diferent blood components at defect layer thickness of 400 nm and 500 nm is inspected for all the proposed confgurations, which is shown in Fig. [4.](#page-9-1) It can be observed that the sensor shows higher sensitivity at $d_D = 500$ nm for both WS₂ and MoS₂ based structure, whereas a deviation is noticed at graphene based proposed sensor. As it can be seen, for graphene based 1D structure, high sensitivity is attained at $d_D = 400$ nm than $d_D = 500$ nm. On comparing the aforementioned three types of structure configurations, it is perceived that optimum sensitivity of 1100.23 nm/RIU is achieved for WS_2 based sensor configuration at $d_D = 500$ nm.

Further, the effect of number of layers (L) of the proposed 2D materials (WS_2, MoS_2) , graphene) on the transmission characteristics is thoroughly scrutinized at $d_D = 500$ nm by considering plasma $(n=1.35)$ $(n=1.35)$ $(n=1.35)$ in the defect layer, which is delineated in Fig. 5. Interestingly, it is realized that with an increase in number of layers, the position of the defect mode is red-shifted (i.e. moves towards higher wavelengths), whereas the intensity of the resonant mode decreases drastically. With increase in the value of L, the overall thickness

Fig. 3 Shift in the resonant wavelength of the proposed structures at different defect layer thickness. **a** WS₂. **c** graphene

Fig. 4 Sensitivity at different defect layer thickness at $\theta_i = 0^\circ$. **a** WS₂. **b** MoS₂. **c** graphene configurations

Fig. 5 Transmission spectra of the proposed structure confgurations for diferent number of layers of 2D materials. **a** WS₂. **b** MoS₂. **c** graphene at $d_D = 500$ nm, n=1.35

of the 1D PhC structure increases as explained in the Sect. [2,](#page-3-1) which leads to increase in the geometrical path difference (ρ) . So, according to Eq. [\(20\)](#page-7-0), with increase in ρ , the wavelength shifts towards longer wavelength (i.e. red-shift) at a constant m and n_{eff} . Moreover, it is envisaged that for higher number of layers, the FWHM (full width half maximum) of the resonant mode increases, which will reduce the sensor performance, i.e. high value of FWHM leads to reduction in signal-to-noise ratio, fgure of merit and quality factor. Thus, to achieve high performance we selected monolayer $(L=1)$ of WS₂, MoS₂ and graphene in all the analysis presented in this research.

As we observed a high sensitivity at defect layer thickness of 500 nm, so we fxed this thickness value and investigated the transmittance spectrum under variable incidence angles $(\theta_i = 20^\circ, 40^\circ)$ of the EM signal, which is depicted in Fig. [6.](#page-10-0) The defect mode properties such as spectral position, FWHM and intensity undergo considerable change with change in the incidence angle. In particular, it is observed that the defect mode position is blue-shifted (i.e. moved towards lower wavelengths) for increase in θ_i . The main cause for this blue-shift in wavelength can be explained by the Bragg condition, which is given as (Aly et al. [2020b\)](#page-16-19),

$$
m\lambda_{res} = 2N\sqrt{n_{eff}^2 - sin^2\theta_i}
$$
 (21)

where λ_{res} is the defect mode wavelength, m represents the constructive diffraction order, θ_i denotes the angle of incidence, n_{eff} indicates effective refractive index of the multilayers, and N signifies the period of dielectric layers. So, with an increase in θ_i , the defect mode wavelength is blue-shifted, to satisfy Bragg condition. Also, the aforementioned behavior is observed in the researches cited in the literature (Aly et al. [2020a](#page-16-8); Jahania et al. [2020;](#page-17-6) Shaban et al. [2020;](#page-17-7) Bouzidi et al. [2017](#page-16-9); Abd El-Aziz et al. [2019b;](#page-16-10) Nouman et al. [2020\)](#page-17-8).

Fig. 6 Transmittance spectrum of the proposed sensors at different angles of incidence for **a**, **b** WS₂, **c**, **d** MoS₂, **e**, **f** graphene

Fig. 7 Sensitivity of the proposed structures at different incident angles of $\theta_i = 20^\circ$, 40°

Fig. 8 Absorption spectrum of the proposed structures for blood components at $d_D = 500$ nm and $\theta_i = 0°$

We also numerically studied the sensitivity of the proposed structures at diferent incident angles of 20° and 40° at d_D = 500 nm, which is shown in Fig. [7](#page-11-0). It is found that the variation in the sensitivity for diferent blood components shows a nonlinear trend. If we compare the sensitivity for different incident angles $(\theta_i = 0^{\circ}, 20^{\circ}, 40^{\circ})$, it can be clearly observed that the proposed structures show maximum sensitivity at $\theta_i = 0^\circ$ (shown in Fig. 4).

The absorption spectrum for all the three proposed configurations is shown in Fig. [8](#page-11-1). From Fig. [2](#page-8-0), we have already verifed that intensity of transmission spectra are above 95% for diferent blood components. So, here in Fig. [8,](#page-11-1) it is apparent that intensity of the absorption spectra are very small, less than 5%. Further, it is observed that intensity of the absorption spectra are decreased and red-shifted with increase in the refractive index of diferent blood components.

We also studied the absorption spectrum of the WS_2 based sensor configuration by considering plasma as the infltrated blood component at diferent angles of incidence at $d_D = 500$ nm, which is delineated in Fig. [9](#page-12-0). Here, it is perceived that absorption spectrum is blue-shifted with increase in the angle of incidence and the intensity of absorption is relatively more at higher incident angle.

Figure [10](#page-12-1) shows the transmission spectrum of the proposed WS_2 based defective 1D PhC under infltrating the defect layer with plasma. To select the optimum value of N, we carried out the above said analysis for different number of period (N) i.e. $N=3$, 5, 7, 9. From Fig. [10](#page-12-1), it is evident that in case of $N=3$, the FWHM of the transmission spectrum is very large, thus the structure will show poor sensing performance. For $N = 5, 7, 9$, although the position of the resonant mode is nearly same, but intensity of the resonant mode decreases drastically with increase in the value of N. To accomplish optimum sensing performance, the intensity of the resonant mode should be high, so we selected $N = 5$, where high transmittance intensity of nearly 95% is achieved.

Fig. 9 Absorption spectrum of the WS₂ based sensor for blood plasma at $d_D = 500$ nm

Variation in SNR with respect to diferent blood components, of the proposed sensor designed with WS_2 , MoS_2 and graphene material, is represented in Fig. [11](#page-13-0). Here, the primary vertical axis shows the SNR variation for $d_D = 400$ nm, whereas the secondary vertical axis is meant for SNR variation for $d_D = 500$ nm, where data are plotted in reverse order. It can be perceived that SNR increases with increase in the refractive index of the diferent blood components. Also, it is revealed that higher value of SNR is noticed at d_D = 500 nm for WS₂ and MoS₂ based structures, but on the contrary maximum SNR is obtained at $d_D = 400$ nm for graphene based sensor configuration.

We studied the FOM of the proposed sensor confgurations at diferent defect layer thickness, which is delineated in the Fig. [12.](#page-13-1) Unlike SNR, variation in FOM for diferent blood constituents follows a nonlinear trend. A higher FOM is perceived at $d_D = 500$ nm as compared to $d_D = 400$ nm.

Variation in the quality factor (Q) of the proposed structures is shown in Fig. [13](#page-14-0) at different defect layer thickness. Here, it is asserted that quality factor in order of $10³$ is obtained, which indicates the proposed sensor delivers excellent sensing characteristics. Additionally, it is clearly observed that a higher Q value is obtained at $d_D = 500$ nm as compared to $d_D = 400$ nm.

Figure [14](#page-15-0) represents the variation in resolution and detection limit (DL) of the proposed sensors with respect to diferent blood components. Resolution in nm is plotted along the primary vertical axis, whereas DL in RIU is taken along the secondary vertical axis in reverse order. It is observed that a very low resolution is obtained for $d_D = 500$ nm for

Fig. 11 SNR of the proposed sensor for different defect layer thickness. **a** WS₂. **b** MoS₂. **c** graphene based configuration

Fig. 12 FOM of the proposed sensors at diferent defect layer thickness

diferent proposed sensor confgurations. Similarly, a very low DL in the order of 10[−]⁵ is attained for $d_D = 500$ nm. Such minimal value of resolution and DL indicate that high performance characteristics can be achieved with the proposed sensor confgurations. Finally, optimum value of sensing parameters (maximum SNR, QF, FOM and minimum R, DL) for the three diferent sensor confgurations are listed in Table [1](#page-15-1).

Fig. 13 Quality factor of the proposed structures at diferent defect layer thickness

5 Conclusions

We propose a novel 1D defective PhC, which employs completely new combination of materials like $CaF₂$, PtSe₂ and ZnSe, for real-time and label-free detection of different blood components such as plasma, RBC, biotin, serum albumin. The wall of defect layer is separately coated with novel 2D materials like WS_2 , MoS_2 and graphene, which is further infltrated with diferent blood components. TMM is manipulated in the proposed structure to analyse its transmission and absorption spectrum. Diferent geometrical parameters like thickness of dielectric layers, thickness of defect layer, thickness of 2D materials, period of the dielectric layers, incident angle are properly optimized to attain high intensity and low FWHM resonant mode, formed within the PBG in the transmission spectrum. By studying the shift in resonant mode wavelength with respect to various blood components, we evaluated diferent performance measuring parameter of the proposed sensors like sensitivity, SNR, QF, FOM, resolution and DL. From the outcomes, it is observed that all the three sensor configurations show optimum sensing performance at $d_D = 500$ nm and $\theta_i = 0°$. Moreover, with the available simple and cost efective fabrication techniques, the proposed sensors open up an avenue for future advancement in the biosensing research feld.

Fig. 14 Resolution and detection limit of the proposed sensors at diferent defect layer thickness

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Declarations

Conficts of interest There is no confict of interest.

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