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Quantized output feedback stabilization for nonlinear discrete-time systems subject to saturating actuator

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Abstract The quantized output feedback stabilization problem for nonlinear discrete-time systems with saturating actuator is investigated. The nonlinearity is assumed to satisfy the local Lipschitz condition. Different from the previous results where the Lipschitz constant is predetermined, a more general case is considered, where the maximum admissible Lipschitz constant through convex optimization is obtained. In this framework, two kinds of quantizations are derived simultaneously: quantized control input and quantized output. Furthermore, sufficient conditions for the existence of static output feedback control laws are given. The desired controllers ensure that all the trajectories of the closed-loop system will converge to a minimal ellipsoid for every initial condition emanating from a large admissible domain. Finally, four illustrative examples are provided to show the effectiveness of the proposed approach.

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1 Introduction

One of the most important research areas in control theory is quantized control. Quantized feedback is found in many engineering systems including mechanical systems and networked systems. Since communication that need to transmit the feedback information from the sensor to the controller may become less reliable as the bandwidth is limited. Therefore, a number of significant results on this issue have been reported and different approaches have been proposed in the literature [\[1](#page-11-0)[–11](#page-11-1)]. Recently, some fundamental approaches for quantized control systems have been developed. For example, in [\[12\]](#page-11-2), the classical sector bound method was used to study quantized control systems with logarithmic quantizers. It should be noted that quantization errors were converted into sector bound uncertainties without conservatism. Gao et al. [\[13](#page-11-3)] proposed a quantization-dependent approach leading to less conservative results. The problem of robust H_{∞} filtering for uncertain linear systems subject to limited communication capacity was investigated in [\[14](#page-11-4)]. The logarithmic quantizer considered in [\[15](#page-11-5)] was different from the traditional quantizer used in $[12]$ and $[13]$. Liu et al. [\[16](#page-11-6)] studied the problem of observer-based stabilization for linear discrete-time systems with output measurement quantization. Compared with quantized feedback control, the robust synchronisation problem of chaotic systems via sampled-data control with stochastic sampling interval has been studied in [\[17\]](#page-11-7). In addition, the sampled data with stochastic sampling have been applied to neural networks [\[18\]](#page-11-8). Networked control systems with partly quantized information were investigated in [\[19](#page-11-9)]. The authors of [\[19](#page-11-9)] focused on the local and networked-link systems where only some of the inputs of the controller were quantized.

By exploring geometric properties of the logarithmic quantizer, a less conservative Tsypkin-type criterion for stability analysis of quantized feedback control system was proposed in [\[20\]](#page-11-10). In [\[21](#page-12-0)], a new necessary and sufficient condition was developed to guarantee the asymptotic stability of the closed system. The problem of H_{∞} filter design for a class of discrete-time systems with quantized measurements was discussed in [\[22\]](#page-12-1) and [\[23\]](#page-12-2), while [\[24\]](#page-12-3) studied the robust H_{∞} dynamic output feedback control problem for networked control systems with quantized measurements. Furthermore, measurement losses of the communicated information were also considered in [\[24](#page-12-3)]. It should be pointed out that all of the above-mentioned works were developed in the context of the logarithmic quantizer.

Moreover, actuator saturation is present in practically all control systems. Actually, linear systems with saturating inputs will change a linear system into a nonlinear one. Saturation nonlinearity may degrade system performance and even lead a stable system into an instable one. During the past years, much attention has been drawn to the problems of stability analysis and stabilization of linear systems when subject to saturating actuator. A great number of results on this topic have been reported in the literature (see, for example, [\[3,](#page-11-11)[25–](#page-12-4) [28](#page-12-5)]). One of the most popular ways to deal with saturation problem given in [\[25](#page-12-4)] was the use of polytopic differential inclusion, while in [\[3\]](#page-11-11) the quantization was converted into a form of saturation with bounded disturbances. In the context of linear systems with saturating actuator, the problem of local uniform ultimate boundedness stabilization was solved in [\[26](#page-12-6)] by using modified sector conditions. Moreover, the uniform quantizer was presented in [\[26\]](#page-12-6). However, it seems that no results on the logarithmic quantized output feedback control for discrete-time systems with saturating actuator are available in the literature.

In this paper, we consider the quantized output feedback stabilization problem for nonlinear discrete-time

systems with saturating actuator. The aim is to design quantized static output feedback controllers such that all the trajectories of the closed-loop system will converge to a minimal ellipsoid for every initial condition emanating from a large admissible domain. The nonlinearity we consider satisfies the local Lipschitz condition. However, the Lipschitz constant is not assumed to be known. Furthermore, a minimal ellipsoid, a large admissible domain and the maximum allowable Lipschitz constant are obtained by solving an optimization problem. Finally, some simulation examples are provided to demonstrate the effectiveness of the proposed method.

Notation: Throughout this brief, for symmetric matrices *X* and *Y*, the notation $X \geq Y$ (respectively, $X > Y$) means that the matrix $X - Y$ is positive semidefinite (respectively, positive definite). *I* is the identity matrix with appropriate dimension. I_n denotes the identity matrix of $n \times n$ dimensions. For a square matrix $P, P > 0$ means that *P* is symmetric and positive definite. For a matrix $P > 0$, $\varepsilon(P)$ stands for $\{x(k) \in \mathbb{R}^n \mid$ $x(k)^T P x(k) \leq 1$. For a matrix $H \in \mathbb{R}^{m \times n}$, H^T , $H_{(i)}$ and $\mathcal{L}(H, u_0)$ represent its transpose, its *i*th row and ${x(k) \in \mathbb{R}^n : ||H_{(i)}x(k)|| \leq u_{0(i)}, i = 1, ..., m},$ respectively. \star stands for symmetric blocks. For a vector $v \in \mathbb{R}^n$, $v_{(i)}$, $j = 1, \ldots, n$ denotes the *j*th component of ν.

2 Preliminaries and problem formulation

Consider the following class of discrete-time nonlinear systems with input saturation described by

$$
x(k + 1) = Ax(k) + B\text{sat}(u(k)) + f(x(k)),
$$
 (1)

$$
y(k) = Cx(k),
$$
 (2)

where $x(k) \in \mathbb{R}^n$ is the system state, $y(k) \in \mathbb{R}^s$ is the measured output, $u(k) \in \mathbb{R}^m$ is the control input. $f(\cdot): \mathbb{R}^n \to \mathbb{R}^n$ is nonlinear function and assumed to be differentiable. *A*, *B* and *C* are known real constant matrices. In this paper, the structure of the saturation function considered here is of the form

 $sat(u(k)) = [sat(u(k)_{(1)}) \dots sat(u(k)_{(m)})]^T$, (3) where $\text{sat}(u(k)_{(i)}) = \text{sign}(u(k)_{(i)}) \min\{u_{0(i)}, |u(k)_{(i)}|\}$ with $u_0 = [u_{0(1)} \dots u_{0(m)}]^T$, $u_{0(i)} > 0$, $i =$ 1,..., *m* being constants. Here we employ the static logarithmic quantizer. The signal is quantized by quantizer $q(\cdot)$ which is defined as

$$
q(v) = [q_1(v_{(1)}) q_2(v_{(2)}) \dots q_l(v_{(l)})]^{T}.
$$
 (4)

For each $q_r(v_{(r)})(1 \leq r \leq l)$, the associated set of quantization levels is expressed as

$$
Q_r = \left\{ \pm \mathcal{L}_r^{(j)} \mid \mathcal{L}_r^{(j)} = (\rho_r)^j \mathcal{L}_r^{(0)}, j = \pm 1, \pm 2, \pm 3, \dots \right\}
$$

$$
\cup \left\{ \pm \mathcal{L}_r^{(0)} \right\} \cup \{0\}, 0 < \rho_r < 1, \mathcal{L}_r^{(0)} > 0,
$$

where $\mathcal{L}_r^{(0)}$ is the initial quantization values for the *r*th sub-quantizer $q_r(v_{(r)})$ and ρ_r is the quantizer density of the *r*th sub-quantizer $q_r(v_{(r)})$. In this article, a characterization of the quantizer is given by

The quantized output feedback stabilization problem being considered in this paper can be formulated as finding the quantized feedback controller in the form of [\(7\)](#page-2-0) such that the following specification is met.

Problem 1 Design a controller [\(7\)](#page-2-0) such that all the states of the closed-loop system will converge to a minimal ellipsoid for every initial condition emanating from a large admissible domain. The corresponding domains and the maximum allowable Lipschitz constant η^* are obtained, respectively.

$$
q_r(v_{(r)}) = \begin{cases} \mathcal{L}_r^{(j)}, & \text{if } \frac{1}{1+\delta_r} \mathcal{L}_r^{(j)} < v_{(r)} \le \frac{1}{1-\delta_r} \mathcal{L}_r^{(j)}, \ v_{(r)} > 0, \ j = \pm 1, \pm 2, \pm 3, \dots, \\ 0, & \text{if } v_{(r)} = 0, \\ -q_r(-v_{(r)}), & \text{if } v_{(r)} < 0, \ r = 1, 2, 3, \dots, l, \end{cases} \tag{5}
$$

where $\delta_r = \frac{1-\rho_r}{1+\rho_r}$. It follows from [\[12](#page-11-2)] and [\[13\]](#page-11-3) that a sector bound expression can be expressed as

$$
q(v) = (I_l + \Delta(k))v,\tag{6}
$$

where the uncertainty matrix $\Delta(k) = \text{diag}\{\Delta_1(k), \Delta_2\}$ $(k), \ldots, \Delta_l(k)$ } satisfies $\Delta_r(k) \in [-\delta_r, \delta_r], r =$ 1, 2,...,*l*.

Moreover, as shown in [\[29](#page-12-7)] and [\[30](#page-12-8)], we make the following assumption on the nonlinear function in system (1) – (2) .

Assumption 1 We assume that the function $f(x)$ is locally Lipschitz with respect to *x* in a region *Q* containing the origin if $|| f(0) || = 0$ and

$$
|| f(x_1) - f(x_2)|| \le \eta ||x_1 - x_2||, \quad \forall x_1, x_2 \in \mathcal{Q},
$$

where $\|\cdot\|$ is the induced 2-norm and $\eta > 0$ is called the Lipschitz constant.

Throughout this paper, it is worth noting that the Lipschitz constant $\eta > 0$ is not fixed. The maximum allowable Lipschitz constant η^* can be determined by solving the convex optimization problem.

Now, consider two different static output feedback controllers.

• **Case 1** *quantized control input*

$$
u(k) = q(Fy(k)) = (I_m + \Delta(k))Fy(k),
$$

$$
\Delta(k) = \text{diag}\{\Delta_1(k), \Delta_2(k), \dots, \Delta_m(k)\}.
$$
 (7)

In [\(7\)](#page-2-0), the control input is quantized. Now, applying the controller (7) to the system (1) – (2) , we obtain the closed-loop system as

$$
x(k + 1) = Ax(k) + B\text{sat}((I_m + \Delta(k))FCx(k))
$$

+ $f(x(k))$. (8)

• Case 2 quantized output
\n
$$
u(k) = Fq(y(k)) = F(I_s + \Delta(k))y(k),
$$
\n
$$
\Delta(k) = \text{diag}\{\Delta_1(k), \Delta_2(k), \dots, \Delta_s(k)\}.
$$
\n(9)

In [\(9\)](#page-2-1), the measured output is quantized. Then, the resulting closed-loop system from the system (1) – (2) and the controller (9) can be written as

$$
x(k+1) = Ax(k) + B\text{sat}(F(I_s + \Delta(k))Cx(k))
$$

$$
+ f(x(k)). \tag{10}
$$

The quantized output feedback control problem can be formulated as finding the quantized feedback controller in the form of (9) such that the following requirement is met.

Problem 2 Determine a controller [\(9\)](#page-2-1) such that the closed-loop system is convergent to a minimal ellipsoid for every initial condition from an admissible domain. Simultaneously, the corresponding domains and the maximum allowable Lipschitz constant η^* are obtained.

3 Main results

This section begins by introducing some lemmas that will play important roles for the proof of our main results here. Firstly, let \mathscr{D} be the set of $m \times m$ diagonal matrices whose diagonal elements are either 1 or 0. Thus, there are 2*^m* elements in *D*. Suppose that each element of \mathscr{D} is labeled as D_i , $i = 1, 2, ..., 2^m$. Denote $D_i^- = I - D_i$. Clearly, D_i^- is also an element of \mathscr{D} if $D_i \in \mathscr{D}$.

Lemma 1 ([\[31](#page-12-9)]) *For any positive definite matrix* $P \in$ $\mathbb{R}^{n \times n}$ *and vectors x, y* $\in \mathbb{R}^n$ *, we have*

$$
f_{\rm{max}}
$$

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 $2x^T y \leq x^T P x + y^T P^{-1} y.$

Lemma 2 ([\[32](#page-12-10)]) Let A, D, S, W and F be real matri*ces of appropriate dimensions such that W* > 0 *and* $F^T F \leq I$. Then for any scalar $\varepsilon > 0$ such that $W^{-1} - \varepsilon^{-1} \mathcal{D} \mathcal{D}^T > 0$, we have

 $(\mathcal{A} + \mathcal{D}F\mathcal{S})^T \mathcal{W}(\mathcal{A} + \mathcal{D}F\mathcal{S}) \leq \mathcal{A}^T$ $(W^{-1} - \varepsilon^{-1} \mathcal{D} \mathcal{D}^T)^{-1} \mathcal{A} + \varepsilon \mathcal{S}^T \mathcal{S}.$

Lemma 3 ([\[25](#page-12-4)]) *Let* $u \in \mathbb{R}^m$ *and* $v \in \mathbb{R}^m$ *be given. If* $||v|| \leq u_0$, then sat(*u*) can be represented as sat(*u*) = Σ *m i*=1 $\eta_i(D_iu+D_i^-v)$, where $0 \leq \eta_i \leq 1$ and $\sum_{i=1}^{2^m}$ *m i*=1 $\eta_i = 1$.

Now we are in a position to present a solution to Problem [1](#page-2-2) specified above.

Theorem 1 *Consider the discrete-time nonlinear sys-tem [\(1\)](#page-1-0)* and [\(2\)](#page-1-0) and let $\beta_2 > \beta_1 > 0$ be given scalars. *For a given matrix* $M > 0$ *, there exists a static output feedback controller in the form of [\(7\)](#page-2-0) such that all solutions of the closed-loop system emanating from* $S =$ ${x(k) \in \mathbb{R}^n \mid x(k)^T P x(k) \leq 1 \text{ and } x(k)^T P_2 x(k) \geq 1}$ *converge to* $S_{\infty} = \{x(k) \in \mathbb{R}^n \mid x(k)^T P_2 x(k) \leq 1\}$ *, if there exist matrices* $P > 0$, $P_2 > 0$, F , H *and scalars* $\varepsilon_1 > 0$, $\varepsilon_2 > 0$, $\alpha > 0$ *such that the following linear matrix inequalities (LMIs) hold for i* = 1, 2, ..., 2^m :

$$
x(k + 1) = Ax(k) + B \sum_{i=1}^{2^m} \eta_i(D_i(I_m + \Delta(k))FCx(k)
$$

+
$$
D_i^- Hx(k) + f(x(k))
$$

=
$$
\sum_{i=1}^{2^m} \eta_i \{ (\tilde{A} + BD_i \Delta(k)FC)x(k) + f(x(k)) \},
$$

where $A = A + BD_i I_m FC + BD_i^- H$. The forward difference in the functional $V(k)$ along the system (1) – [\(2\)](#page-1-0) is then given by

$$
\Delta V(k) = V(k+1) - V(k)
$$

= $x(k+1)^T P x(k+1) - x(k)^T P x(k)$.

On the other hand, we can obtain that

$$
\Delta V(k) - \beta_1(x(k)^T P x(k) - 1)
$$

\n
$$
-\beta_2(1 - x(k)^T P_2 x(k)) = \sum_{i=1}^{2^m} \eta_i \{x(k)^T
$$

\n
$$
[(\tilde{A} + BD_i \Delta(k) F C)^T P (\tilde{A} + BD_i \Delta(k) F C) - (1 + \beta_1) P + \beta_2 P_2] x(k)
$$

\n
$$
+ 2x(k)^T (\tilde{A} + BD_i \Delta(k) F C)^T P f (x(k))
$$

\n
$$
+ f (x(k))^T P f (x(k)) + \beta_1 - \beta_2.
$$
 (14)

Let $W = \varepsilon_1 I - P$. Applying Lemma [1,](#page-2-3) we obtain

$$
\begin{bmatrix}\n-(1+\beta_1)P + \beta_2 P_2 & I & A^T + C^T F^T I_m D_i B^T + H^T D_i^- B^T & C^T F^T & 0 \\
\star & -\alpha I & 0 & 0 & 0 \\
\star & \star & B D_i \Delta \varepsilon_2 \Delta D_i B^T - 2M + M P M & 0 & I < 0, \\
\star & \star & \star & \star & -\varepsilon_2 I & 0 \\
\star & \star & \star & \star & -\varepsilon_1 I\n\end{bmatrix}\n< 0,\n\tag{11}
$$
\n
$$
\begin{bmatrix}\nu_{0(p)} I & H_{(p)} \\
\star & \nu_{0(p)} P \\
\star & \nu_{0(p)} P\n\end{bmatrix}\n\geq 0, \quad p = 1, 2, \ldots, m,\n\tag{12}
$$
\n
$$
P_2 - P \geq 0.
$$

Proof Choose a Lyapunov function candidate as follows: $V(k) = x(k)^T P x(k)$. Along a similar line as in the proof of [\[25](#page-12-4)], $\varepsilon(P) \subset \mathcal{L}(H, u_0)$ is equivalent to $H_{(p)}P^{-1}H_{(p)}^T \leq u_{0(p)}^2$. And also by the Schur complement equivalence, (12) can be contained. Now taking into account [\(13\)](#page-3-0), it follows that $\varepsilon(P)$ contains $\varepsilon(P_2)$. Using Lemma [3,](#page-3-1) we have

$$
2x(k)^{T}(\tilde{A} + BD_{i}\Delta(k)FC)^{T}Pf(x(k))
$$

+ $f(x(k))^{T}Pf(x(k))$
= $2x(k)^{T}(\tilde{A} + BD_{i}\Delta(k)FC)^{T}Pf(x(k))$
 $-f(x(k))^{T}Wf(x(k)) + \varepsilon_{1}f(x(k))^{T}f(x(k))$
 $\leq x(k)^{T}(\tilde{A} + BD_{i}\Delta(k)FC)^{T}PW^{-1}$
 $P(\tilde{A} + BD_{i}\Delta(k)FC)x(k) + \varepsilon_{1}\eta^{2}x(k)^{T}x(k).$

Next, we shall show that

$$
\Pi \triangleq (\tilde{A} + BD_i \Delta(k)FC)^T P(\tilde{A} + BD_i \Delta(k)FC)
$$

\n
$$
- (1 + \beta_1)P + \beta_2 P_2
$$

\n
$$
+ (\tilde{A} + BD_i \Delta(k)FC)^T
$$

\n
$$
PW^{-1} P(\tilde{A} + BD_i \Delta(k)FC) + \varepsilon_1 \eta^2
$$

\n
$$
= (P\tilde{A} + PBD_i \Delta(k)FC)^T (P^{-1} + W^{-1})
$$

\n
$$
(P\tilde{A} + PBD_i \Delta(k)FC) - (1 + \beta_1)P
$$

\n
$$
+ \beta_2 P_2 + \varepsilon_1 \eta^2.
$$
 (15)

Now, set $\Delta = \text{diag}\{\delta_1, \delta_2, \ldots, \delta_m\}$ with $\delta_r(r)$ $1, 2, \ldots, m$ the defined as in [\(6\)](#page-2-4). From (6), it is easy to show that $\Delta(k)^T \Delta(k) \leq \text{diag}\{\delta_1^2, \delta_2^2, \ldots, \delta_m^2\} = \Delta^2$. Using Lemma [2,](#page-3-2) it can be verified that

$$
(P\tilde{A} + PBD_i \Delta(k)FC)^T
$$

\n
$$
(P^{-1} + W^{-1})(P\tilde{A} + PBD_i \Delta(k)FC)
$$

\n
$$
\leq \tilde{A}^T P[(P^{-1} + W^{-1})^{-1} - \varepsilon_2 PBD_i \Delta \Delta^T D_i B^T P]^{-1}
$$

\n
$$
P\tilde{A} + \varepsilon_2^{-1} C^T F^T F C.
$$
\n(16)

Then, by the matrix inversion lemma, it follows that

$$
(P^{-1} + W^{-1})^{-1} = P - P(W + P)^{-1}P = P - P\varepsilon_1^{-1}P.
$$

By using the Schur complement equivalence to (11) , one has

Setting $\alpha^{-1} = \varepsilon_1 \eta^2$ and using the Schur complement equivalence again, we have

$$
\tilde{A}^T P[(P^{-1} + W^{-1})^{-1} - P B D_i \Delta \varepsilon_2 \Delta^T D_i B^T P]^{-1}
$$

\n
$$
P\tilde{A} + \varepsilon_2^{-1} C^T F^T F C - (1 + \beta_1) P + \beta_2 P_2
$$

\n
$$
+ \varepsilon_1 \eta^2 < 0.
$$
\n(20)

It is easy to show that (20) implies that $\Pi < 0$. Noting $\beta_1 - \beta_2$ < 0, this together with inequality Π < 0 implies $V(k + 1) - V(k) < 0$ for $x(k)$ such that $x(k)^T P x(k) \le 1$ and $x(k)^T P_2 x(k) \ge 1$. This completes the proof. pletes the proof. 

Inspired in the work of $[26]$ $[26]$, the corresponding domains and the maximum allowable Lipschitz constant η^* can be determined by solving the following convex optimization problem

$$
\inf_{P,P_2,F,H,\varepsilon_1,\varepsilon_2,\alpha} \lambda(\alpha+\varepsilon_1) + (1-\lambda)(\text{trace}(R) + \mu)
$$
\ns. t. (a)(11), (12) and (13),\n
\n(b)
$$
\begin{bmatrix} P_2 & -I \\ \star & R \end{bmatrix} \ge 0 \text{ and } \begin{bmatrix} \mu I & P \\ \star & P \end{bmatrix} \ge 0,
$$
\n(21)

where $0 < \lambda < 1$. Then, the maximum allowable Lipschitz constant is $\eta^* = \frac{1}{\sqrt{\alpha \varepsilon_1}}$.

The static output feedback reduces to a state feedback, we have the controller

$$
u(k) = q(Kx(k)).
$$
\n(22)

$$
\begin{bmatrix}\n-(1+\beta_1)P + \beta_2 P_2 & I & A^T + C^T F^T I_m D_i B^T + H^T D_i^- B^T & C^T F^T \\
\star & -\alpha I & 0 & 0 \\
\star & \star & B D_i \Delta \varepsilon_2 \Delta D_i B^T - 2M + M P M + \varepsilon_1^{-1} I & 0 \\
\star & \star & \star & -\varepsilon_2 I\n\end{bmatrix} < 0.
$$
\n(17)

Noting that $-P^{-1} \le -2M + MPM$ (see [\[33](#page-12-11)]), the matrix inequality [\(17\)](#page-4-0) implies

The result on a state feedback controller design for system [\(1\)](#page-1-0) is provided in the following corollary.

$$
\begin{bmatrix}\n-(1+\beta_1)P + \beta_2 P_2 + C^T F^T \varepsilon_2^{-1} F C & I & \tilde{A}^T \\
\star & -\alpha I & 0 \\
\star & B D_i \Delta \varepsilon_2 \Delta D_i B^T - P^{-1} + \varepsilon_1^{-1} I\n\end{bmatrix} < 0.
$$
\n(18)

Pre-multiplying and post-multiplying both sides of inequality [\(18\)](#page-4-1) by diag{*I*, *I*, *P*}, respectively, and then applying the Schur complement equivalence, we can obtain

Corollary 1 *Given scalars* β_1 *and* β_2 *satisfying* β_2 > $\beta_1 > 0$. Suppose there exist matrices $Q > 0$, $P_2 >$ $0, K, H$ and scalars $\varepsilon_1 > 0, \varepsilon_3 > 0, \alpha > 0$ such that *the following LMIs hold for* $i = 1, 2, \ldots, 2^m$ *:*

$$
\left[\begin{array}{cc}\tilde{A}^T P(P - P\varepsilon_1^{-1}P - PBD_i\Delta\varepsilon_2\Delta^T D_i B^T P)^{-1} P\tilde{A} - (1+\beta_1)P + \beta_2 P_2 + C^T F^T \varepsilon_2^{-1} F C & I\\ \star & -\alpha I\end{array}\right] < 0. \tag{19}
$$

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$$
\begin{bmatrix}\n-(1+\beta_1)Q + \beta_2 \bar{P}_2 & Q & QA^T + \bar{K}^T I_m D_i B^T + \bar{H}^T D_i^- B^T & \bar{K}^T & 0 \\
\star & -\alpha I & 0 & 0 & 0 \\
\star & \star & B D_i \Delta \varepsilon_3 \Delta D_i B^T - Q & 0 & I \\
\star & \star & \star & -\varepsilon_3 I & 0 \\
\star & \star & \star & \star & -\varepsilon_1 I\n\end{bmatrix} < 0,\n\tag{23}
$$

$$
\begin{bmatrix} u_{0(p)}I & \bar{H}_{(p)} \\ \star & u_{0(p)}Q \end{bmatrix} \ge 0, \quad p = 1, 2, \dots, m,
$$
 (24)

$$
\bar{P}_2 - Q \ge 0.
$$
 (25)

Then, all solutions of the closed-loop system are convergent to $S_{\infty} = \{x(k) \in \mathbb{R}^n \mid x(k)^T Q^{-1} \overline{P}_2 Q^{-1} x(k)$ ≤ 1} *for every initial condition from* $S = \{x(k) \in \mathbb{R}^n \mid$ $x(k)^T Q^{-1} x(k) \leq 1$ *and* $x(k)^T Q^{-1} \overline{P}_2 Q^{-1} x(k) \geq 1$ *}. Moreover, a suitable state feedback controller can be chosen as* $u(k) = q(Kx(k))$ *with* $K = \bar{K}Q^{-1}$.

Proof Applying the controller $u(k) = q(Kx(k))$ to the system (1) and then using Lemma [3,](#page-3-1) the resulting closed-loop system can be written as

$$
x(k+1) = \sum_{i=1}^{2^m} \eta_i \{ (\tilde{A} + BD_i \Delta(k)K)x(k) + f(x(k)) \},\tag{26}
$$

where $A = A + BD_i I_m K + BD_i^- H$. Now, define the Lyapunov functional cadidate as $V(k) = x(k)^T P x(k)$, where $P > 0$. The forward difference in the functional $V(k)$ along the system (26) is then given by

$$
\Delta V(k) = V(k+1) - V(k)
$$

=
$$
\sum_{i=1}^{2^m} \eta_i \{ [(\tilde{A} + BD_i \Delta(k)K)x(k) + f(x(k))]^T P
$$

$$
\times [(\tilde{A} + BD_i \Delta(k)K)x(k) + f(x(k))]
$$

$$
-x(k)^T P x(k) \}.
$$

$$
\Delta V(k) - \beta_1(x(k)^T P x(k) - 1) - \beta_2(1 - x(k)^T P_2 x(k))
$$

\n
$$
= \sum_{i=1}^{2^m} \eta_i \{x(k)^T [(\tilde{A} + BD_i \Delta(k)K)^T P
$$

\n
$$
\times (\tilde{A} + BD_i \Delta(k)K) - (1 + \beta_1)P + \beta_2 P_2]x(k)
$$

\n
$$
+ 2x(k)^T (\tilde{A} + BD_i \Delta(k)K)^T P f (x(k))\}
$$

\n
$$
+ f (x(k))^T P f (x(k)) + \beta_1 - \beta_2
$$

\n
$$
\leq \sum_{i=1}^{2^m} \eta_i \{x(k)^T [(\tilde{A} + BD_i \Delta(k)K)^T (P + PW^{-1} P)
$$

\n
$$
\times (\tilde{A} + BD_i \Delta(k)K) - (1 + \beta_1)P + \beta_2 P_2 + \varepsilon_1 \eta^2]
$$

\n
$$
\times x(k)\} + \beta_1 - \beta_2
$$

\n
$$
\leq \sum_{i=1}^{2^m} \eta_i \{x(k)^T [\tilde{A}^T P ((P^{-1} + W^{-1})^{-1}
$$

\n
$$
- \varepsilon_3 P BD_i \Delta \Delta D_i B^T P)^{-1} P \tilde{A} + \varepsilon_3^{-1} K^T K
$$

\n
$$
- (1 + \beta_1)P + \beta_2 P_2 + \varepsilon_1 \eta^2]x(k)\} + \beta_1 - \beta_2
$$

\n
$$
= \sum_{i=1}^{2^m} \eta_i \{x(k)^T \Xi x(k) + \beta_1 - \beta_2\}, \qquad (27)
$$

where $\mathbf{E} = \tilde{A}^T P((P^{-1} + W^{-1})^{-1} - \varepsilon_3 P B D_i \Delta \Delta D_i)$ $B^T P$)⁻¹ $P \tilde{A} + \varepsilon_3^{-1} K^T K - (1 + \beta_1) P + \beta_2 P_2 + \varepsilon_1 \eta^2$. By using the Schur complement equivalence to (23) , it follows that

$$
\begin{bmatrix}\n-(1+\beta_1)Q + \beta_2 \bar{P}_2 & Q & QA^T + \bar{K}^T I_m D_i B^T + \bar{H}^T D_i^- B^T & \bar{K}^T \\
\star & -\alpha I & 0 & 0 \\
\star & \star & B D_i \Delta \varepsilon_3 \Delta D_i B^T - Q + \varepsilon_1^{-1} I & 0 \\
\star & \star & \star & -\varepsilon_3 I\n\end{bmatrix} < 0.
$$
\n(28)

Let $Q = P^{-1}$, $P_2 = Q^{-1} \bar{P}_2 Q^{-1}$, $K = \bar{K} Q^{-1}$, $H = \bar{H} Q^{-1}$, $W = \varepsilon_1 I - P$, $\Delta = \text{diag}\{\delta_1, \delta_2, \ldots, \delta_m\}.$ Following the same argument as in the proof of Theorem [1,](#page-3-3) we assert that

Pre-multiplying and post-multiplying both sides of inequality [\(28\)](#page-5-2) by diag $\{P, I, P, I\}$, we obtain

$$
\begin{bmatrix}\n\varepsilon_3^{-1} K^T K - (1 + \beta_1) P + \beta_2 P_2 & I & \tilde{A}^T P \\
\star & -\alpha I & 0 \\
\star & \star & P B D_i \Delta \varepsilon_3 \Delta D_i B^T P - P + P \varepsilon_1^{-1} P\n\end{bmatrix} < 0.
$$
\n
$$
(29)
$$

Next, setting $\alpha^{-1} = \varepsilon_1 \eta^2$, it follows from the matrix inequality [\(29\)](#page-6-0) and the Schur complement equivalence that Ξ < 0. The rest of the proof is similar to Theorem [1](#page-3-3) and thus omitted. This completes the proof of the corollary.

Moreover, it is desired to make $S_{\infty} = \{x(k) \in$ \mathbb{R}^n | $x(k)^T Q^{-1} \bar{P}_2 Q^{-1} x(k) \leq 1$ } as small as possible and $S = \{x(k) \in \mathbb{R}^n \mid x(k)^T Q^{-1} x(k) \leq 1\}$ as large as possible when designing state feedback controllers. Therefore, the corresponding domains and the maximum allowable Lipschitz constant η^* can be determined by solving the following convex optimization problem

$$
\inf_{Q, \bar{P}_2, \bar{K}, \bar{H}, \varepsilon_1, \varepsilon_3, \alpha} \lambda(\alpha + \varepsilon_1) + (1 - \lambda)(\text{trace}(R) + \mu)
$$
\ns. t. (a)(23), (24) and (25),\n
\n(b)
$$
\begin{bmatrix} \bar{P}_2 & -Q \\ \star & R \end{bmatrix} \ge 0 \text{ and } \begin{bmatrix} \mu I & I \\ \star & Q \end{bmatrix} \ge 0, \quad (30)
$$

where $0 < \lambda < 1$ and $\eta^* = \frac{1}{\sqrt{\alpha \varepsilon_1}}$.

Now, we are in a position to present the output quantization result for discrete-time nonlinear systems. In this sense, we obtain the sufficient condition for the solvability of Problem [2](#page-2-5) in the following theorem.

Theorem 2 *Consider the discrete-time nonlinear sys-tem [\(1\)](#page-1-0)* and [\(2\)](#page-1-0). For given scalars $\beta_2 > \beta_1 > 0$ and *a* matrix $M > 0$, if there exist matrices $P > 0$, $P_2 >$ 0, *F*, *H* and scalars $\varepsilon_1 > 0$, $\varepsilon_4 > 0$, $\alpha > 0$ such that *the following LMIs hold for* $i = 1, 2, \ldots, 2^m$ *:*

Then there exists a static output feedback controller in the form of [\(9\)](#page-2-1) such that all solutions of the closedloop system emanating from $S = \{x(k) \in \mathbb{R}^n \mid$ $x(k)^T P x(k) \leq 1$ *and* $x(k)^T P_2 x(k) \geq 1$ } *converge to* $S_{\infty} = \{x(k) \in \mathbb{R}^n \mid x(k)^T P_2 x(k) \leq 1\}.$

Proof Applying the controller [\(9\)](#page-2-1) to the system [\(1\)](#page-1-0)– [\(2\)](#page-1-0), we obtain the resulting closed-loop system as

$$
x(k + 1) = \sum_{i=1}^{2^{m}} \eta_i \{ (\hat{A} + BD_i F \Delta(k) C) x(k) + f(x(k)) \},
$$
\n(34)

where $A = A + BD_iFI_sC + BD_i^-H$. Let $\Delta =$ diag{ $\delta_1, \delta_2, \ldots, \delta_s$ } and $W = \varepsilon_1 I - P$. Now, define the following Lyapunov function candidate for the sys-tem in [\(34\)](#page-6-1): $V(k) = x(k)^T P x(k)$. By Lemma [1](#page-2-3) and Lemma [2,](#page-3-2) it can be shown that

$$
V(k + 1) - V(k) - \beta_1(x(k)^T P x(k) - 1)
$$

\n
$$
-\beta_2(1 - x(k)^T P_2 x(k))
$$

\n
$$
= \sum_{i=1}^{2^m} \eta_i \{x(k)^T [(\hat{A} + BD_i F \Delta(k)C)^T
$$

\n
$$
\times P(\hat{A} + BD_i F \Delta(k)C) - (1 + \beta_1)P + \beta_2 P_2]x(k)
$$

\n
$$
+ 2x(k)^T (\hat{A} + BD_i F \Delta(k)C)^T P f (x(k))
$$

\n
$$
+ f (x(k))^T P f (x(k)) + \beta_1 - \beta_2
$$

\n
$$
\leq \sum_{i=1}^{2^m} \eta_i \{x(k)^T [(P\hat{A} + PBD_i F \Delta(k)C)^T
$$

\n
$$
\times (P^{-1} + W^{-1}) (P\hat{A} + PBD_i F \Delta(k)C)
$$

$$
\begin{bmatrix}\n\varepsilon_{4}C^{T}\Delta\Delta C - (1+\beta_{1})P + \beta_{2}P_{2} & I & A^{T} + C^{T}I_{r}F^{T}D_{i}B^{T} + H^{T}D_{i}^{-}B^{T} & 0 & 0 \\
\star & -\alpha I & 0 & 0 & 0 \\
\star & \star & -2M + MPM & BD_{i}F & I \\
\star & \star & \star & \star & -\varepsilon_{4}I & 0 \\
\star & \star & \star & \star & \star & -\varepsilon_{1}I\n\end{bmatrix} < 0, \quad (31)
$$
\n
$$
\begin{bmatrix}\nu_{0(p)}I & H_{(p)} \\
\star & \nu_{0(p)}P\n\end{bmatrix} \geq 0, \quad p = 1, 2, ..., m,
$$
\n
$$
P_{2} - P \geq 0.
$$
\n(33)

$$
-(1 + \beta_1)P + \beta_2 P_2 + \varepsilon_1 \eta^2 |x(k)| + \beta_1 - \beta_2
$$

\n
$$
\leq \sum_{i=1}^{2^m} \eta_i \{x(k)^T [\hat{A}^T P((P^{-1} + W^{-1})^{-1} - \varepsilon_4^{-1} P B D_i F F^T D_i B^T P)^{-1} P \hat{A} + \varepsilon_4 C^T \Delta \Delta C
$$

\n
$$
-(1 + \beta_1)P + \beta_2 P_2 + \varepsilon_1 \eta^2 |x(k)| + \beta_1 - \beta_2
$$

\n
$$
= \sum_{i=1}^{2^m} \eta_i \{x(k)^T [\hat{A}^T P(P - P \varepsilon_1^{-1} P - \varepsilon_4^{-1} P B D_i F F^T D_i B^T P)^{-1} P \hat{A} + \varepsilon_4 C^T \Delta \Delta C
$$

\n
$$
-(1 + \beta_1)P + \beta_2 P_2 + \varepsilon_1 \eta^2 |x(k)| + \beta_1 - \beta_2
$$

\n
$$
= \sum_{i=1}^{2^m} \eta_i \{x(k)^T \Pi x(k) + \beta_1 - \beta_2\}, \qquad (35)
$$

where $\Pi = \hat{A}^T P (P - P \varepsilon_1^{-1} P - \varepsilon_4^{-1} P B D_i F F^T D_i$ $B^T P$)⁻¹ $P \hat{A} + \varepsilon_4 C^T \Delta \Delta C - (1+\beta_1)P + \beta_2 P_2 + \varepsilon_1 \eta^2$. Noting $-P^{-1} \le -2M + MPM$ and using the Schur complement equivalence to (31) , it is easy to see that

V($k + 1$) − *V*(k) < 0. Moreover, by [\(32\)](#page-6-2) and [\[25](#page-12-4)], it can be seen that $\varepsilon(P) \subset \mathcal{L}(H, u_0)$. Then taking into account [\(33\)](#page-6-2), it follows that $\varepsilon(P)$ contains $\varepsilon(P_2)$. This completes the proof.

Similar to (21) , we can obtain the corresponding domains and the maximum allowable Lipschitz constant η^* by solving an optimization problem

$$
\inf_{P,P_2,F,H,\varepsilon_1,\varepsilon_4,\alpha} \lambda(\alpha+\varepsilon_1) + (1-\lambda)(\text{trace}(R) + \mu)
$$

s. t. (a)(31), (32) and (33),

(b)
$$
\begin{bmatrix} P_2 & -I \\ \star & R \end{bmatrix} \ge 0
$$
 and $\begin{bmatrix} \mu I & P \\ \star & P \end{bmatrix} \ge 0$, (38)

where $0 < \lambda < 1$. The maximum allowable Lipschitz constant is $\eta^* = \frac{1}{\sqrt{\alpha \varepsilon_1}}$.

The results in Theorem [2](#page-6-3) are now employed to design a state feedback control law for the system [\(1\)](#page-1-0). We represent a state feedback controller in the following form:

$$
u(k) = Kq(x(k)).
$$
\n(39)

$$
\begin{bmatrix}\n\varepsilon_4 C^T \Delta \Delta C - (1 + \beta_1)P + \beta_2 P_2 & I & \hat{A}^T & 0 \\
\star & -\alpha I & 0 & 0 \\
\star & \star & -P^{-1} + \varepsilon_1^{-1} I & B D_i F \\
\star & \star & \star & -\varepsilon_4 I\n\end{bmatrix} < 0.
$$
\n(36)

On the other hand, pre-multiplying and post-multiplying [\(36\)](#page-7-0) by diag{*I*, *I*, *P*, *I*} result in

Then, from Theorem [2,](#page-6-3) we have the following quantized state feedback controller design result for the discrete-time nonlinear system [\(1\)](#page-1-0).

$$
\begin{bmatrix}\n\varepsilon_4 C^T \Delta \Delta C - (1 + \beta_1)P + \beta_2 P_2 & I & \hat{A}^T P \\
\star & -\alpha I & 0 & 0 \\
\star & \star & -P + P \varepsilon_1^{-1} P + \varepsilon_4^{-1} P B D_i F F^T D_i B^T P\n\end{bmatrix} < 0,\tag{37}
$$

which, by the Schur complement equivalence, implies that Π < 0 with $\alpha^{-1} = \varepsilon_1 \eta^2$. This together with $\beta_1 - \beta_2$ < 0 implies that for all $x(k)$ such that $x(k)^T P x(k) \le 1$ and $x(k)^T P_2 x(k) \ge 1$, we have

Corollary 2 *Given scalars* β_1 *and* β_2 *satisfying* β_2 > β_1 > 0. Suppose there exist matrices $P > 0, P_2 >$ 0, *K*, *H* and scalars $\varepsilon_1 > 0$, $\varepsilon_5 > 0$, $\alpha > 0$ such that *the following LMIs hold for i* = 1, 2, ..., 2^m *:*

$$
\begin{bmatrix}\n\varepsilon_{5}\Delta\Delta - (1+\beta_{1})P + \beta_{2}P_{2} & I & A^{T} + K^{T}D_{i}B^{T} + H^{T}D_{i}^{-}B^{T} & 0 & 0 \\
\star & -\alpha I & 0 & 0 & 0 \\
\star & \star & -2M + MPM & BD_{i}K & I \\
\star & \star & \star & \star & -\varepsilon_{5}I & 0 \\
\star & \star & \star & \star & \star & -\varepsilon_{1}I\n\end{bmatrix} < 0, \quad (40)
$$
\n
$$
\begin{bmatrix}\nu_{0(p)}I & H_{(p)} \\
\star & \nu_{0(p)}P\n\end{bmatrix} \geq 0, \quad p = 1, 2, ..., m,
$$
\n(41)\n
$$
P_{2} - P \geq 0.
$$

Then, the closed-loop system obtained by applying the quantized state feedback controller in [\(39\)](#page-7-1) to system [\(1\)](#page-1-0) is convergent to $S_{\infty} = \{x(k) \in \mathbb{R}^n \mid$ $x(k)^T P_2x(k) \leq 1$ *for all initial condition from* $S =$ ${x(k) \in \mathbb{R}^n \mid x(k)^T P x(k) \leq 1 \text{ and } x(k)^T P_2 x(k) \geq 1}$ 1}*.*

Proof Applying the controller [\(39\)](#page-7-1) to the system [\(1\)](#page-1-0), we obtain the following closed-loop system

$$
x(k+1) = \sum_{i=1}^{2^m} \eta_i \{ (\hat{A} + BD_i K \Delta(k)) x(k) + f(x(k)) \},
$$
\n(43)

where $A = A + BD_i K I_n + BD_i^- H = A + BD_i K +$ BD_i^-H . Firstly, we set $\Delta = \text{diag}\{\delta_1, \delta_2, \ldots, \delta_n\}$ and $W = \varepsilon_1 I - P$. Next, we define the Lyapunov function candidate as $V(k) = x(k)^T P x(k)$. Taking the difference between the Lyapunov function candidates for two consecutive time instants yields

$$
\Delta V(k) = V(k+1) - V(k)
$$

=
$$
\sum_{i=1}^{2^m} \eta_i \{x(k)^T [(\hat{A} + BD_i K \Delta(k))^T
$$

$$
\times P(\hat{A} + BD_i K \Delta(k)) - P]x(k)
$$

+
$$
2x(k)^T (\hat{A} + BD_i K \Delta(k))^T P f(x(k))
$$

+
$$
f(x(k))^T P f(x(k))\}.
$$

Then, similar to the proof of Theorem [2,](#page-6-3) we can obtain

$$
\Delta V(k) - \beta_1(x(k)^T P_X(k) - 1) - \beta_2(1 - x(k)^T P_2x(k))
$$

\n
$$
= \sum_{i=1}^{2^m} \eta_i \{x(k)^T [(\hat{A} + BD_i K \Delta(k))^T
$$

\n
$$
\times P(\hat{A} + BD_i K \Delta(k)) - (1 + \beta_1)P + \beta_2 P_2]x(k)
$$

\n
$$
+ 2x(k)^T (\hat{A} + BD_i K \Delta(k))^T P f(x(k)) + f(x(k))^T
$$

\n
$$
\times P f(x(k))\} + \beta_1 - \beta_2
$$

\n
$$
\leq \sum_{i=1}^{2^m} \eta_i \{x(k)^T [(P\hat{A} + PBD_i K \Delta(k))^T (P^{-1} + W^{-1})
$$

\n
$$
\times (P\hat{A} + PBD_i K \Delta(k))
$$

\n
$$
- (1 + \beta_1)P + \beta_2 P_2 + \varepsilon_1 \eta^2]x(k)\} + \beta_1 - \beta_2
$$

\n
$$
\leq \sum_{i=1}^{2^m} \eta_i \{x(k)^T [\hat{A}^T P((P^{-1} + W^{-1})^{-1}]
$$

\n
$$
- \varepsilon_5^{-1} PBD_i K K^T D_i B^T P)^{-1} P \hat{A} + \varepsilon_5 \Delta \Delta
$$

\n
$$
- (1 + \beta_1)P + \beta_2 P_2 + \varepsilon_1 \eta^2]x(k)\} + \beta_1 - \beta_2
$$

\n
$$
= \sum_{i=1}^{2^m} \eta_i \{x(k)^T \Theta x(k) + \beta_1 - \beta_2\}, \qquad (44)
$$

where $\Theta = \hat{A}^T P ((P^{-1} + W^{-1})^{-1} - \varepsilon_5^{-1} P B D_i K K^T$ $D_i B^T P$ ⁻¹ $P \hat{A} + \varepsilon_5 \Delta \Delta - (1 + \beta_1)P + \beta_2 P_2 + \varepsilon_1 n^2$. Then, by the Schur complement equivalence it follows from (40) that

$$
\begin{bmatrix}\n\varepsilon_5 \Delta \Delta - (1 + \beta_1)P + \beta_2 P_2 & I & \tilde{A}^T P & 0 \\
\star & -\alpha I & 0 & 0 \\
\star & \star & P\varepsilon_1^{-1}P - P & PBD_iK \\
\star & \star & \star & -\varepsilon_5 I\n\end{bmatrix} < 0,
$$
\n(45)

Noting $(P^{-1} + W^{-1})^{-1} = P - Pe_1^{-1}P$, the matrix inequality [\(45\)](#page-8-0) implies that $\Theta < 0$ with $\alpha^{-1} = \varepsilon_1 \eta^2$. The rest of the proof can be carried out by following a similar line as in the proof of Theorem [2](#page-6-3) and thus is omitted. This completes the proof. 

Similar to (21) , the corresponding domains and the maximum allowable Lipschitz constant η^* can be obtained by solving the following optimization problem

$$
\inf_{P, P_2, K, H, \varepsilon_1, \varepsilon_5, \alpha} \lambda(\alpha + \varepsilon_1) + (1 - \lambda)(\text{trace}(R) + \mu)
$$
\ns. t. (a)(40), (41) and (42),\n
\n(b) $\begin{bmatrix} P_2 & -I \\ \star & R \end{bmatrix} \ge 0$ and $\begin{bmatrix} \mu I & P \\ \star & P \end{bmatrix} \ge 0$, (46)

 $< 1.$ The maximum allowable Lipschitz constant is $\eta^* = \frac{1}{\sqrt{\alpha \varepsilon_1}}$.

4 Simulation examples

In this section, we present some examples to demonstrate the applicability and effectiveness of the proposed method. Example [1](#page-8-1) and Example [2](#page-9-0) are provided to check the static logarithmic quantizer of one dimension, while Example [3](#page-10-0) and Example [4](#page-10-1) are given to show the static logarithmic quantizer of two dimensions.

Example 1 Consider the following discrete-time nonlinear system with parameters as

$$
A = \begin{bmatrix} -0.8 & 0.9 \\ 0.2 & 1.3 \end{bmatrix}, \quad B = \begin{bmatrix} 0.5 \\ 2 \end{bmatrix}, \quad C = \begin{bmatrix} 1.2 & 1 \\ 0.5 & 0 \end{bmatrix}.
$$

The tuning parameters are $\beta_1 = 10^{-3}$ and $\beta_2 =$ 0.1. Moreover, we consider that the saturation level is fixed as $u_0 = 5$. In this example, we choose $M =$ $(A^T A + I)^{-1}$, $\rho_1 = 0.6$, $\lambda = 0.3$ and $\mathcal{L}_1^{(0)} = 30$. Solving the convex optimization problem (21) by the standard convex optimization numerical software, we can obtain the maximum allowable Lipschitz constant $n^* =$

Fig. 1 State trajectories (Example [1\)](#page-8-1)

Fig. 2 Trajectory of input (Example [1\)](#page-8-1)

0.09 and the controller gain $F = [-0.5930, 1.0545]$. The nonlinear function is selected as $f(x(k)) =$ $0.08\sin(e^{-x_2(k)}) + 0.06\cos(x_1(k))$ 0.09sin(*e*−*x*1(*k*)) . The state trajectories of the closed-loop system are shown in Fig. [1.](#page-9-1) As shown in Fig. [1,](#page-9-1) the outer ellipsoid is $\{x(k) \in \mathbb{R}^n \mid$ $x(k)^T P x(k) \leq 1$ } with $P =$ $1.6158 - 0.8927$] -0.8927 1.4416 and the inner ellipsoid is $\{x(k) \in \mathbb{R}^n \mid x(k)^T P_2 x(k) \leq$ 1} with $P_2 = \begin{bmatrix} 1.6273 & -0.6880 \\ -0.6880 & 5.0837 \end{bmatrix}$. It is clearly observed from Fig. [1](#page-9-1) that some trajectories of plant states emanating from the outer ellipsoid converge to the inner ellipsoid. Figure [2](#page-9-2) shows the input trajectory

Fig. 3 State trajectories (Example [2\)](#page-9-0)

Fig. 4 Trajectory of input (Example [2\)](#page-9-0)

of the closed-loop system for initial condition given by $x(0) = \begin{bmatrix} -0.2 \\ -0.94 \end{bmatrix}$.

Example 2 Consider the system described in Example [1.](#page-8-1) Furthermore, the saturation level and the parameters β_1 , β_2 , ρ_1 , $\mathcal{L}_1^{(0)}$ are the same as those presented in Example [1.](#page-8-1) Then, by solving the optimiza-tion problem [\(30\)](#page-6-4) with $\lambda = 0.1$, we can obtain $\eta^* = 0.13$ and the state feedback gain $K =$ η^* = 0.13 and the state feedback gain $K =$ $\lceil -0.3609 - 0.4735 \rceil$. The nonlinear function is chosen $[-0.3609 - 0.4735]$. The nonlinear function is chosen as $f(x(k)) =$ $\left[0.1\sin(e^{-x_2(k)}) + 0.125\cos(x_1(k))\right]$ $0.13\sin(e^{-x_1(k)})$. Figure [3](#page-9-3) shows the state trajectories of the closedloop system and two ellipsoids. For this example, the outer ellipsoid is $\{x(k) \in \mathbb{R}^n \mid x(k)^T P x(k) < 1\}$

Fig. 5 State trajectories (Example [3\)](#page-10-0)

Fig. 6 Trajectory of input (Example [3\)](#page-10-0)

with $P = \begin{bmatrix} 1.0201 & -0.5317 \\ -0.5317 & 0.7665 \end{bmatrix}$ and the inner ellipsoid is $\{x(k) \in \mathbb{R}^n \mid x(k)^T P_2 x(k) \leq 1\}$ with $P_2 = \begin{bmatrix} 1.3669 & -0.5430 \\ -0.5430 & 2.7315 \end{bmatrix}$. The control input of the closed-loop system for initial condition given by $x(0) = \begin{bmatrix} 1.2 \\ 1.12 \end{bmatrix}$ is recorded in Fig. [4.](#page-9-4)

Example 3 Consider the discrete-time nonlinear system (1) – (2) with parameters as follows:

$$
A = \begin{bmatrix} -0.3 & 0.1 \\ 0.2 & 1.2 \end{bmatrix}, \quad B = \begin{bmatrix} 0.5 & 0.2 \\ 1.2 & 0.6 \end{bmatrix}, \quad C = \begin{bmatrix} 0.2 & 1 \\ 0.5 & 2.5 \end{bmatrix}.
$$

Now, we choose $\beta_1 = 10^{-2}$ and $\beta = 0.1$, respectively. The saturation level is selected as $u_0 = 5$. In this case, we choose $M = 10(A^T A + I)^{-1}$, $\rho_1 = 0.2$, $\rho_2 =$

0.5, $\lambda = 0.2$ and $\mathcal{L}_1^{(0)} = \mathcal{L}_2^{(0)} = 30$. Then, solving the convex optimization problem [\(38\)](#page-7-3), we can obtain the maximum allowable Lipschitz constant $\eta^* = 0.18$ and the controller gain $F = \begin{bmatrix} -0.1452 & 0.0774 \\ 0.0774 & -0.7221 \end{bmatrix}$. The nonlinear function is supposed to be $f(x(k)) =$
 $\begin{bmatrix} 0.15\sin(e^{-x_2(k)}) & 1 \end{bmatrix}$ The state tra $0.17\cos(x_1(k)) + 0.12\sin(e^{-x_1(k)})$. The state trajectories of the closed-loop system with the controller [\(9\)](#page-2-1) are shown in Fig. [5,](#page-10-2) and the control input of the closed-loop system for initial condition given by $x(0) = \begin{vmatrix} 1.5 \\ -1. \end{vmatrix}$ −1.5 is shown in Fig. 6 . As shown in these figures (Figures [1](#page-9-1)[,3](#page-9-3)[,5\)](#page-10-2), in the quantized feedback controller, the states cannot converge to the origin; however, they remain around a certain area. Furthermore, we can obtain that the outer ellipsoid is $\{x(k) \in \mathbb{R}^n \mid$ $x(k)^T P x(k) \le 1$ with $P = \begin{bmatrix} 0.1707 & 0.0224 \\ 0.0224 & 0.3104 \end{bmatrix}$ and the inner ellipsoid is $\{x(k) \in \mathbb{R}^n \mid x(k)^T P_2 x(k) \le 1\}$ with $P_2 = \begin{bmatrix} 0.5374 & -0.0410 \\ -0.0410 & 0.9256 \end{bmatrix}$.

Example 4 Consider the system described in Exam-ple [3.](#page-10-0) In this case, the parameters u_0 , β_1 , β_2 , ρ_1 , ρ_2 , $\mathcal{L}_1^{(0)}$, $\mathcal{L}_2^{(0)}$ are the same as those presented in Example [3.](#page-10-0) Similarly, by solving the optimization problem [\(46\)](#page-8-2) with $\lambda = 0.1$ and $M = (A^T A + I)^{-1}$, we can obtain the following solutions $\eta^* = 0.13$, $K =$ can obtain the following solutions $\eta^* = 0.13$, $K =$ $\begin{bmatrix} 0.3337 & -0.7061 \end{bmatrix}$, $P = \begin{bmatrix} 1.6642 & 0.1904 \end{bmatrix}$ and $\begin{bmatrix} 0.3337 & -0.7061 \\ -0.7061 & -0.0879 \end{bmatrix}$, $P = \begin{bmatrix} 1.6642 & 0.1904 \\ 0.1904 & 1.2179 \end{bmatrix}$ and $P_2 = \begin{bmatrix} 1.9512 & -0.3058 \\ -0.3058 & 2.7214 \end{bmatrix}$. The nonlinear function is fixed \overline{a} as $f(x(k)) = \begin{bmatrix} 0.13\sin(e^{-x_2(k)}) \\ 0.13\cos(x_1(k)) + 0.12\sin(x_2(k)) \end{bmatrix}$ $0.13\cos(x_1(k)) + 0.12\sin(e^{-x_1(k)})$. Figure [7](#page-11-12) illustrates the trajectory of the states, and

Fig. [8](#page-11-13) shows the control input of the closed-loop system for initial condition given by $x(0) = \begin{bmatrix} 0.7 \\ -0 \end{bmatrix}$ -0.5 .

5 Conclusions

The problems of quantized output feedback stabilization for nonlinear discrete-time systems with saturating actuator have been studied. Two cases of quantized control laws are considered. The first case is the input quantization, and the other is the output quantization. Attention has been paid to the design of static output feedback controllers such that all the trajectories

Fig. 7 State trajectories (Example [4\)](#page-10-1)

Fig. 8 Trajectory of input (Example [4\)](#page-10-1)

of the closed-loop system will converge to a minimal ellipsoid for every initial condition emanating from a large admissible domain. Finally, some examples have shown the effectiveness of the proposed approach.

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References

1. Liberzon, D.: Hybrid feedback stabilization of systems with quantized signals. Automatica **39**, 1543–1554 (2003)

- 2. Ishii, H., Francis, B.A.: Quadratic stabilization of sampleddata systems with quantization. Automatica **39**, 1793–1800 (2003)
- 3. Zhang, C., Feng, G., Qiu, J., Shen, Y.: Control synthesis for a class of linear network-based systems with communication constraints. IEEE Trans. Ind. Electron. **60**, 3339–3348 (2013)
- 4. Mahmoud, M., Al-Rayyah, A., Xia, Y.: Quantised feedback stabilisation of interconnected discrete-delay systems. IET Control Theory Appl. **5**, 795–802 (2011)
- 5. Mahmoud, M.: Control of linear discrete-time systems by quantised feedback. IET Control Theory Appl. **6**, 2095– 2102 (2012)
- 6. Wu, L., Zheng, W.: Passivity-based sliding mode control of uncertain singular time-delay systems. Automatica **45**, 2120–2127 (2009)
- 7. Zheng, B., Yang, G.: Decentralized sliding mode quantized feedback control for a class of uncertain large-scale systems with dead-zone input nonlinearity. Nonlinear Dyn. **71**, 417– 427 (2013)
- 8. Zheng, B., Yang, G.: *H*² control of linear uncertain systems considering input quantization with encoder/decoder mismatch. ISA Trans. **52**, 577–582 (2013)
- 9. Zheng, B., Xue, Y.: A sliding sector approach to quantized feedback variable structure control. Int. J. Control Automation Syst. **11**, 1177–1186 (2013)
- 10. Jiang, Z., Liu, T.: Quantized nonlinear control-a survey. Acta Automatica Sinica **39**, 1820–1830 (2013)
- 11. Mera, M., Castaños, F., Poznyak, A.: Quantised and sampled output feedback for nonlinear systems. Int. J. Control **87**, 2475–2487 (2014)
- 12. Fu, M., Xie, L.: The sector bound approach to quantized feedback control. IEEE Trans. Automatic Control **50**, 1698– 1711 (2005)
- 13. Gao, H., Chen, T.: A new approach to quantised feedback control systems. Automatica **44**, 534–542 (2008)
- 14. Gao, H., Chen, T.: H_{∞} estimation for uncertain systems with limited communication capacity. IEEE Trans. Automatic Control **52**, 2070–2084 (2007)
- 15. Xia, Y., Yan, J., Shi, P., Fu, M.: Stability analysis of discretetime systems with quantized feedback and measurements. IEEE Trans. Ind. Inform. **9**, 313–324 (2013)
- 16. Liu, M., You, J.: Observer-based controller design for networked control systems with sensor quantisation and random communication delay. Int. J. Syst. Sci. **43**, 1901–1912 (2012)
- 17. Lee, T., Park, J., Lee, S., Kwon, O.: Robust synchronisation of chaotic systems with randomly occurring uncertainties via stochastic sampled-data control. Int. J. Control **86**, 107– 119 (2013)
- 18. Lee, T., Park, J., Kwon, O., Lee, S.: Stochastic sampled-data control for state estimation of time-varying delayed neural networks. Neural Netw. **46**, 99–108 (2013)
- 19. Ge, Y., Wang, J., Li, C., Zhang, L.: Robust *H*[∞] output feedback control with partly quantised information. IET Control Theory Appl. **7**, 523–536 (2013)
- 20. Zhou, B., Duan, G., Lam, J.: On the absolute stability approach to quantized feedback control. Automatica **46**, 337–346 (2010)
- 21. Zhang, J., Lam, J., Xia, Y.: Observer-based output feedback control for discrete systems with quantised inputs. IET Control Theory Appl. **5**, 478–485 (2011)
- 22. Zhou, S., Wang, L., Zheng, W.: H_{∞} filter design for nonlinear parameter-varying systems with quantized measurements. J. Frankl. Inst. **349**, 1781–1807 (2012)
- 23. Yang, W., Liu, M., Shi, P.: *H*[∞] filtering for nonlinear stochastic systems with sensor saturation, quantization and random packet losses. Signal Process. **92**, 1387–1396 (2012)
- 24. Lu, R., Zhou, X., Wu, F., Xue, A.: Quantized H_{∞} output feedback control for linear discrete-time systems. J. Frankl. Inst. **350**, 2096–2108 (2013)
- 25. Hu, T., Lin, Z.: Control Systems with Actuator Saturation: Analysis and Design. Birkhäuser, Boston (2001)
- 26. Tarbouriech, S., Gouaisbaut, F.: Control design for quantized linear systems with saturations. IEEE Trans. Automatic Control **57**, 1883–1889 (2012)
- 27. Su, H., Chen, M., Lam, J., Lin, Z.: Semi-global leaderfollowing consensus of linear multi-agent systems with input saturation via low gain feedback. IEEE Trans. Circ. Syst.-I: Regul. Pap. **60**, 1881–1889 (2013)
- 28. Su, H., Chen, M., Wang, X., Lam, J.: Semiglobal observerbased leader-following consensus with input saturation. IEEE Trans. Ind. Electron. **61**, 2842–2850 (2014)
- 29. Abbaszadeh,M.,Marquez, H.J.: LMI optimization approach to robust H_{∞} observer design and static output feedback stabilization for discrete-time nonlinear uncertain systems. Int. J. Robust Nonlinear Control **19**, 313–340 (2009)
- 30. Sayyaddelshad, S., Gustafsson, T.: *H*[∞] observer design for uncertain nonlinear discrete-time systems with time-delay: LMI optimization approach. Int. J. Robust Nonlinear Control **25**, 1514–1527 (2015)
- 31. Xu, S.: Robust H_{∞} filtering for a class of discrete-time uncertain nonlinear systems with state delay. IEEE Trans. Circ. Syst.-I: Fundam. Theory Appl. **49**, 1853–1859 (2002)
- 32. Xu, S., Chen, T.: Robust H_{∞} control for uncertain stochastic systems with state delay. IEEE Trans. Automatic Control **47**, 2089–2094 (2002)
- 33. Chen, K., Fong, I.K.: Stability analysis and output-feedback stabilisation of discrete-time systems with an interval timevarying state delay. IET Control Theory Appl. **4**, 563–572 (2010)