**ORIGINAL PAPER**



# **Benefts of global earth observation missions for disaggregation of exposure data and earthquake loss modeling: evidence from Santiago de Chile**

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## **Abstract**

Exposure is an essential component of risk models and describes elements that are endangered by a hazard and susceptible to damage. The associated vulnerability characterizes the likelihood of experiencing damage (which can translate into losses) at a certain level of hazard intensity. Frequently, the compilation of exposure information is the costliest component (in terms of time and labor) of risk assessment procedures. Existing models often describe exposure in an aggregated manner, e.g., by relying on statistical/census data for given administrative entities. Nowadays, earth observation techniques allow the collection of spatially continuous information for large geographic areas while enabling a high geometric and temporal resolution. Consequently, we exploit measurements from the earth observation missions TanDEM-X and Sentinel-2, which collect data on a global scale, to characterize the built environment in terms of constituting morphologic properties, namely built-up density and height. Subsequently, we use this information to constrain existing exposure data in a spatial disaggregation approach. Thereby, we establish dasymetric methods for disaggregation. The results are presented for the city of Santiago de Chile, which is prone to natural hazards such as earthquakes. We present loss estimations due to seismic ground shaking and corresponding sensitivity as a function of the resolution properties of the exposure data used in the model. The experimental results underline the benefts of deploying modern earth observation technologies for refned exposure mapping and related earthquake loss estimation with enhanced accuracy properties.

**Keywords** Exposure modeling · Disaggregation techniques · Earth observation · Remote sensing · Seismic risk · Earthquake loss estimation

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## **1 Introduction**

Earthquakes represent a devastating natural hazard that caused more than 1.7 million docu-mented fatalities in the past 100 years globally (Wyss and Speiser [2022](#page-25-0)). Prospectively, the ongoing continuous increase of the world population (UN [2019](#page-24-0)) can be expected to put more people at risk in both rural (Wyss [2018\)](#page-25-1) and urban environments (Bilham [2009;](#page-22-0) Wyss et al. [2021](#page-25-2)), respectively, than ever before. For the development of mitigation strategies for these perils, detailed knowledge about afliated risks is in demand. As an important constituent element of natural hazard risk, the exposure and vulnerability need to be determined (UNISDR [2009\)](#page-24-1). In particular, it is crucial to have detailed information about the spatiotemporal distribution of population as well as about the properties of the building inventory with respect to an expected level of seismic ground shaking. Especially for loss estimation, the collection of highly resolved building inventory information normally represents the most time-consuming and expensive aspect. Traditional data collection procedures foresaw detailed in situ building-by-building analysis by, e.g., structural engineers and small-scale population surveying (e.g., Dunbar et al. [2003;](#page-22-1) Kechidi et al. [2021](#page-23-0)). This may provide very detailed and high-quality information. However, such time-demanding and cost-intensive approaches are decreasingly able to cope with the high spatiotemporal dynamics of built environments. Simultaneously, the information provided on a coarser spatial level, such as spatially aggregated census data (e.g., Corbane et al. [2017;](#page-22-2) Santa Maria et al. [2017;](#page-24-2) Yepes-Estrada et al. [2017\)](#page-25-3), hampers the consideration of small-scale hazard efects in a downstream risk model (Gomez Zapata et al. [2021;](#page-23-1) Nievas et al. [2022](#page-24-3)) and frequently shows a high level of uncertainty (Pittore et al. [2017](#page-24-4)). Moreover, recent empirical works underlined that the accuracy of damage estimates is very sensitive regarding the exposure component (Gomez-Zapata et al. [2022a](#page-23-2), [b](#page-23-3)), whereby the coarsest aggregation levels were found to be the most inaccurate (Senouci [2018](#page-24-5); Dabbeek et al. [2021](#page-22-3)).

Recent assessment approaches already identifed earth observation (EO) data as a valuable source of information for exposure estimation (Geiß and Taubenböck [2013\)](#page-22-4). This is especially true for the latest generation optical sensors which enable the detection and characterization of objects of built environments within hazard-prone areas (e.g., Ehrlich and Tenerelli [2013](#page-22-5); Geiß et al. [2017a](#page-23-4)). Related studies aimed at an integrative view on vulnerability and considered numerous parameters for a holistic assessment (e.g., Taubenböck et al. [2008](#page-24-6); Ebert et al. [2009](#page-22-6)). Therefore, the derivation of a wide variety of vulnerability-related parameters from remote sensing, comprising population characteristics (e.g., Dobson et al. [2000;](#page-22-7) Aubrecht et al. [2013](#page-21-0)) and properties of the built environment (e.g., Mueller et al. [2006;](#page-24-7) French and Muthukumar [2006](#page-22-8); Sahar et al. [2010\)](#page-24-8), was explored. Given the nature of remote sensing as a tool for providing physical measurements of the earth's surface, the physical vulnerability of built environments, in particular, has been subject to increasing scientifc contemplation over the course of the last decade. Numerous approaches were postulated for seismic vulnerability assessment: Sarabandi and Kiremidjian ([2007](#page-24-9)) estimate the structural type of buildings based on remote sensing and ancillary tax assessor information for deployment in earthquake loss estimation models. Taubenböck et al.  $(2009)$ , Borzi et al.  $(2011)$ , Polli and Dell'Acqua ([2011](#page-24-11)), and Qi et al. [\(2017\)](#page-24-12) characterize the built environment with remote sensing data and retrieve specific fragility functions or damage probability matrices, respectively. In contrast to that, e.g., Borfecchia et al. ([2010](#page-22-10)), Geiß et al. ([2015a,](#page-22-11) [2017b,](#page-23-5) [2018](#page-23-6); [2014\)](#page-22-12), Liuzzi et al. [\(2019](#page-23-7)), Liu et al. [\(2019](#page-23-8)), Torres et al. [\(2019\)](#page-24-13), and An et al. [\(2021\)](#page-21-1) combined limited in situ ground truth information characterizing

the building inventory with features from remote sensing and use techniques of statistical inference for a complete labeling of the residual building inventory according to specifc vulnerability levels or more generic properties such as construction material or occupancy, respectively. Related methodological principles were also exploited by, e.g., Wieland et al. ([2012,](#page-25-4) [2016](#page-25-5)), Pittore and Wieland [\(2013\)](#page-24-14), Geiß et al. [\(2016\)](#page-23-9), Pittore et al. ([2020\)](#page-24-15), and Fan et al. [\(2021\)](#page-22-13) to assess seismic vulnerability or related parameters on a coarser spatial level to allow for the use of data with larger spatial coverage. Recently, Aravena Pelizari et al. [\(2021\)](#page-21-2) deployed street-level imagery that was extracted from the GoogleStreetView platform and classifed various seismic structural types with deep learning models to automatically compile relevant in situ data.

At the same time, data requirements for exposure modeling still hamper utilization capabilities for large areas of many approaches. This is due to data availability, monetary costs of data, and processing demand of, e.g., very high spatial resolution EO imagery and detailed in situ data. Moreover, local idiosyncrasies must not be bypassed and transfer of models cannot be carried out in a non-adaptive manner since, e.g., building structural types may feature a large variability of morphological appearance and vulnerability in diferent parts of the world. As a consequence, population data and building inventory information with afliated vulnerability characteristics are frequently still outdated, spatially discontinuous, or aggregated. Thus, afliated natural hazard risk assessment strategies do not provide a picture of risk on large scales such as nations, continents, or the entire globe, while enabling a high spatial, thematic, and temporal resolution.

In parallel, with the advent of the big earth data epoch, novel data collection mechanisms have become available on a global scale. The latest generation EO missions, which are highly relevant for characterization of built environments, such as ESA/EU's Copernicus Sentinel-2 mission (Drusch et al. [2012](#page-22-14)) and German Aerospace Center's spaceborne radar interferometer TanDEM-X (TDM) (Krieger et al. [2007\)](#page-23-10), collect planetary data with unprecedented spatial and temporal resolution properties. In particular, the Sentinel-2 satellites provide multispectral imagery with 10-m spatial resolution and high temporal coverage (i.e., 10 days at the equator with one satellite, and 5 days with 2 satellites; 2–3 days at mid-latitudes), whereas, the TDM provides a digital surface model with 12-m spatial resolution.

Consequently, in this paper, we capitalize upon this globally existing EO data to derive constituent morphologic properties of the built environment, i.e., *built-up density* and *height*. Subsequently, we develop dasymetric disaggregation techniques to spatially allocate and eventually constrain existing exposure data from administrative entities based on the derived morphologic properties of the built environment. Finally, we align vulnerability information, i.e., fragility functions, to the exposure data and establish probabilistic seismic hazard analysis-based (PSHA) seismic loss estimations for the earthquake-prone city of Santiago de Chile. Thereby, we evaluate the loss estimation accuracies as a function of the resolution properties of the underlying exposure data. This is done to gain insights regarding how the diferent aggregation levels of the exposure data propagate into fnal loss estimates.

The remainder of the paper is organized as follows. We provide a brief description of the study site and incorporated datasets in Sect. [2.](#page-3-0) Section [3](#page-6-0) documents the developed and implemented methods for hazard assessment, disaggregation of exposure data, and loss estimation, whereas Sect. [4](#page-13-0) contains afliated results and discussion. Conclusions and future perspectives are outlined in Sect. [5](#page-19-0).

## <span id="page-3-0"></span>**2 Study site and data**

## **2.1 Santiago de Chile**

We apply the proposed methods to data that cover Santiago de Chile, the capital of Chile. The corresponding metropolitan area is inhabited by more than 7 million people and is located in close proximity to the subduction zone where the Nazca Plate subducts the South American Plate. However, the seismic hazard for Santiago de Chile is not only determined by the ofshore subduction zone, but also by shallow crust earthquakes. These events emanate from inland faults on the western fank of the Andean Cordillera, i.e., the Western Andean Thrust (Ammirati et al. [2019\)](#page-21-3). Among them is also the recently characterized San Ramon Fault. This active North–South oriented west verging fault system runs directly along the eastern border of the city (Armijo et al. [2010](#page-21-4)) and represents a likely source for damaging events (Hussain et al. [2020](#page-23-11)).

## **2.2 Data**

## **2.2.1 National exposure model for Chile**

We built upon the national exposure model for Chile which was developed in the context of the South America Risk Assessment (SARA) project (available online: [https://](https://sara.openquake.org/risk:exposure) [sara.openquake.org/risk:exposure](https://sara.openquake.org/risk:exposure)) (GEM [2014;](#page-23-12) Yepes-Estrada et al. [2017\)](#page-25-3). The exposure data were predominately generated from census data in combination with planning permission data and comprises the spatial distribution, number, and living area of residential structures, which are classifed according to 18 seismic building structural types with associated replacement costs. The information is provided on three spatial levels, i.e., *comuna* (corresponding to urban districts or municipalities), provinces, and regions. For this work, we deploy the *comuna*-level data (Fig. [1a](#page-4-0)). Thereby, the planning permission data can be considered as the most reliable data source and were compiled on *comuna* level. Consequently, we utilize this level since it provides the most favorable tradeoff between spatial resolution and reliability (Santa Maria et al. [2017;](#page-24-2) Yepes-Estrada et al. [2017\)](#page-25-3).

Additionally, we integrate population information for subsequent casualty estimates from the national exposure model for Chile. The population information for the *comuna* level was compiled from national population statistics. In particular, the data reveals the average number of dwellers per building type at the legal place of residency, i.e., the nighttime population (Yepes-Estrada et al. [2017\)](#page-25-3).

#### <span id="page-3-1"></span>**2.2.2 Earth observation data for characterization of the built environment**

To derive *built-up density* and *height*, we follow an automated workfow. First, "builtup" and "non-built-up" areas are distinguished by integrating the so-called Global Urban Footprint layer (Esch et al.  $2017$ ). We integrate this information in a tailored fltering procedure for the TDM digital surface model (DSM) data (Geiß et al. [2015b](#page-22-16)) to extract elevation information for built-up areas, i.e., a normalized DSM (nDSM) (Geiß et al. [2020a\)](#page-23-13) for Santiago de Chile (Fig. [1](#page-4-0)b). Subsequently, the intra-urban land cover is mapped under consideration of multispectral Sentinel-2 imagery. Thereby, intra-urban



<span id="page-4-0"></span>**Fig. 1** Input data for the exposure mapping workfow; **a** administrative entities on *comuna* level of the national exposure model for Chile with corresponding shares of 18 diferent seismic building structural types for Santiago de Chile; **b** visualization of the normalized digital surface model (nDSM) derived from the TanDEM-X DSM which contains heights of objects which are elevated from the earth's surface such as buildings or vegetation; **c** built-up density (upper map) and height (lower map) estimation based on the TanDEM-X nDSM data and additional Sentinel-2 imagery for Santiago de Chile on grid-cell level; color coding from low to high corresponds to equally-spaced quantiles and visualizes, thus, the relative distribution of built-up density and height values, respectively; **d** visualization of the SPOT nDSM with very high spatial resolution used for validation purposes

vegetation is pruned and the residual elevated areas, i.e., elevated built-up areas, serve as the basis to compute *built-up densities* and *heights*. These two measures were combined for a morphologic characterization of the built environment for spatial entities, i.e., rectangular grid cells, with a side length of 500 m (Fig. [1c](#page-4-0)) (Geiß et al. [2019\)](#page-23-14). It is here where it can be noted that those grid-cell-level estimates can be also produced by means of supervised learning techniques, i.e., learning from an area where both TDM and Sentinel-2 are available and establishing an estimation for areas where solely Sentinel-2 is available. Despite existing globally, the TDM DSM is frequently solely accessible for up to 100 000  $km^2$  for scientific applications (Geiß et al. [2019](#page-23-14)), whereas the Sentinel-2 imagery is accessible without any restrictions. A suite of corresponding techniques was recently proposed in Geiß et al. ([2022a](#page-23-15), [b;](#page-23-16) [2020b\)](#page-23-17).

Finally, we obtained a very high resolution (VHR) DSM for validation purposes, which was derived from panchromatic tri-stereo images with a geometric resolution of 2 m acquired by the SPOT-7 satellite (d'Angelo et al. [2008](#page-22-17)). From it, also an nDSM was derived (Fig. [1d](#page-4-0)).

## **2.2.3 Fragility functions for earthquake loss estimation and empirical conversion factors for casualty estimation**

Subsequently, we align vulnerability information, i.e., existing analytical fragility functions (Villar-Vega et al. [2017](#page-24-16)), to the seismic structural types contained in the exposure model for Santiago de Chile. The fragility functions establish the likelihood of damage conditional on a certain level of ground shaking, i.e., earthquake intensity. We mainly rely on functions that were specifcally developed for the South American building inventory and local regional dataset of strong ground motion records. The structural capacity of each building class was computed from 150 single-degree-of-freedom oscillators which enable the propagation of building-to-building variabilities. In addition, the seismic demand was considered by over 300 ground motion records to account for record-to-record variabilities. The structural capacity for each building class was determined based on several existing studies, outcomes from two workshops organized in South America, and expert judgment by multiple local practitioners (GEM [2014\)](#page-23-12). Thereby, ductility levels, damage schemes, and response behaviors were considered. Finally, each fragility function was modeled as a cumulative lognormal distribution, and the representative intensity measures (PGA, SA—0.3 s, SA—1.0 s) were selected based on the correlation between ground shaking and damage distribution. Four damage states are discriminated, i.e., "slight," "moderate," "extensive," and "destroyed" (Villar-Vega et al. [2017](#page-24-16)). The set of fragility functions was completed by integrating functions from HAZUS (FEMA [2015\)](#page-22-18) for the types MCF MCF 4–5, MCF MR 4–5, and MR 4–5, respectively. The fragility functions were harmonized and aligned to the structural types of Santiago de Chile as documented in detail in Fig. [2](#page-6-1).

To anticipate the possible effects of damaging earthquakes on the exposed population, we further integrate empirical conversion factors for the building-related damage states for casualty estimation. We built upon conversion factors from HAZUS (FEMA [2015](#page-22-18)). Thereby, four degrees of injury are distinguished, which are all caused by direct consequences of an earthquake such as collapsing buildings, and falling debris (Spence and So [2021\)](#page-24-17). The degrees of injury comprise: "slightly injured," "moderately injured," "heavily injured," and "deadly injured." The degrees of injury are aligned to the damage states as documented in detail in Table [1](#page-7-0). It can be noted that the damage state "destroyed" was further distinguished according to "destroyed—with collapse" and "destroyed—without



<span id="page-6-1"></span>**Fig. 2** Deployed fragility functions which establish a relationship between the intensity of an earthquake (x-axis) and corresponding degree of damage (y-axis) for four damage states, i.e., green="slight," yellow="moderate," orange="extensive," and red="destroyed," respectively, for the seismic building structural types of Santiago de Chile

collapse." The latter describes cases where a structure faces substantial damage which prevents repairing it. However, without a collapse, the number of deadly injured inhabitants will be substantially reduced compared to a structure that faces the damage pattern "destroyed—with collapse."

## <span id="page-6-0"></span>**3 Implemented methods**

A fowchart of the implemented methods is given in Fig. [3.](#page-8-0) First, we carry out PSHA with four probabilities of occurrence for Santiago de Chile (Sect. [3.1\)](#page-6-2). Section [3.2](#page-9-0) details the developed dasymetric disaggregation techniques to spatially disaggregate and eventually constrain the existing exposure data from the national model on *comuna* level. Finally, Sect. [3.3](#page-13-1) contains the description of implemented damage state computation and casualty estimation procedures.

## <span id="page-6-2"></span>**3.1 Probabilistic seismic hazard assessment**

For the characterization of the seismic hazard, we capitalize upon the SARA seismic hazard model according to Garcia et al. [\(2017](#page-22-19)), which follows the well-known PSHA approach (Cornell [1968](#page-22-20)). The input data for the model encompasses a database of seismically active faults, as well as seismological, geological, and geophysical information. Additionally, focal

<span id="page-7-0"></span>



The numerical values represent percentage shares of the population per building. In subsequent estimations, diferences in casualties per structural type occur, since the difer-

ent structural types have a varying probability to reach a certain damage state



<span id="page-8-0"></span>**Fig. 3** Overview of the implemented methods for hazard characterization, exposure modeling, damage state computation, and casualty estimation, respectively

mechanisms for the Nazca subduction zones are integrated along with a harmonized earthquake catalog for South America, and a selection of ground motion prediction equations (GMPEs). These input data allow for modeling of the near-surface seismic properties in South America, the subduction zones, and the processes within the continental plate. (i) The shallow seismicity is approximated by both an integrated model of distributed seismicity and crustal fault sources; (ii) the subduction interface seismicity is modeled as large 3D fault sources geometry; (iii) the subduction in-slab seismicity is considered via 3D volumes of ruptures describing the spatial location of events within the area of interest (Garcia et al. [2017\)](#page-22-19). Modeling results, in combination with the GMPEs (the epistemic uncertainty is accounted for by using a Logic Tree-based procedure), allow for a probabilistic determination of the expected earthquake intensity. For the actual seismic hazard computations for Santiago de Chile we used the OpenQuake Engine (Pagani et al. [2014\)](#page-24-18). The model reveals peak ground acceleration (PGA) and spectral acceleration  $(SA - 0.3 \text{ s}, SA - 1.0 \text{ s})$ . We consider four probabilities of occurrence to analyze a broad spectrum of events, i.e., earthquakes with a probability of occurrence of 50%, 30%, and 10% within 50 years, and an extreme event with 10% in 475 years, respectively. Lastly, we spatially refne the modeled intensity values with an exact interpolation technique, i.e., inverse distance weighting (Shepard [1968\)](#page-24-19), to obtain an intensity value every 300 m (Fig. [4](#page-9-1)).



<span id="page-9-1"></span>**Fig. 4** PGA with a probability of occurrence of **a** 50%, **b** 30%, and **c** 10% within 50 years, and **d** an extreme event with 10% in 475 years. The white contour line represents the settlement area under study of Santiago de Chile

### <span id="page-9-0"></span>**3.2 Spatial disaggregation methods for exposure estimation**

Generally, disaggregation methods establish a mapping that foresees transforming data from one set of coarse spatial units (i.e., source zone) to one set of fner spatial units (i.e., target zone) (Wu et al.  $2005$ ). We used for all disaggregation approaches exposure data from the *comuna* level as source zone and deployed EO-based datasets as target zone.

As an initial means, we implemented a linear disaggregation approach with respect to the settlement area. Thereby, the living areas per building type on *comuna* level are disaggregated proportionally regarding the settlement area on grid-cell level (Fig. [5](#page-9-2)). Consequently, the linear disaggregation corresponds to a so-called binary dasymetric mapping approach, since the redistribution of the living areas per building type is solely established according to the binary expression of a variable (i.e., presence or absence of "built-up areas"). In our application context, such a disaggregation scheme is, in particular, helpful to establish a more diferentiated consideration of the hazard intensity, since each grid cell will be assigned an individual hazard intensity value instead of solely considering one hazard intensity value per *comuna*.



<span id="page-9-2"></span>**Fig. 5** Linear disaggregation approach for exposure estimation. The living areas per building type (pie chart) on *comuna* level are disaggregated proportionally regarding the settlement area on grid-cell level



<span id="page-10-0"></span>**Fig. 6** Disaggregation methods for exposure estimation which take the urban morphology into account: disaggregation approaches on grid-cell level with **a** absolute and **b** relative height constraints

However, to establish a more diferentiated mapping, we incorporate the derived morphologic properties of the built environment for disaggregation. Figure [6](#page-10-0) illustrates the dasymetric disaggregation approaches on grid-cell level with both absolute and relative height constraints.

First, the EO-based *built-up height* measurements are classifed into up to six distinct building height classes as defned by the height classes of the building structural types. Here, the classifcation according to absolute height thresholds (Fig. [6](#page-10-0)a) follows the number of foors of the respective height classes (Table [2](#page-11-0)), whereby we apply a value of three meters per foor. In contrast, the classifcation according to relative height thresholds (Fig. [6](#page-10-0)b) reproduces the distribution of the height classes on *comuna* level exactly. Generally, the classifcations determine which structural types can occur in a certain grid cell (i.e., one up to nine types per cell) (Table [2](#page-11-0)).



<span id="page-11-0"></span>WDNO-1–2, MATO-1–2





<span id="page-12-0"></span>**Fig. 7** Disaggregation methods for exposure estimation which take the urban morphology into account: disaggregation approaches on sub-grid-cell level with **a** absolute and **b** relative height constraints

Additionally, the living areas per building height class are summed up on *comuna* level. The sum per specifc building height class is redistributed over the grid cells which correspond to that specifc building height class while preserving the characteristic shares of individual structural types of that specifc building height class. Finally, the *built-up density* is deployed to disaggregate the living areas in a weighted manner, i.e., the living areas per building height class are redistributed proportionally regarding the corresponding *builtup densities*. For subsequent usage, we divide the mapped living area per building type by corresponding average living areas per building type (according to the numbers included in the national exposure model) to obtain the absolute number of buildings per type.

Figure [7](#page-12-0) illustrates the disaggregation approaches on sub-grid-cell level. We follow the same aforementioned methodological principles. However, here we deploy the TanDEM-X

<span id="page-13-2"></span>nDSM values of the elevated built-up areas, i.e., elevated intra-urban areas, whereby vegetation has been pruned, in order to consider all eventually existing building height classes within a grid cell. Consequently, the absolute and relative classifcation reveals a distribution of the diferent building height classes on grid-cell level. In detail, the classifcation according to absolute height thresholds (Fig. [7](#page-12-0)a) follows the number of stories per building height class (Table [2\)](#page-11-0). Analogous to the grid-cell-level approach, the classifcation according to relative height thresholds (Fig. [7](#page-12-0)b) reproduces the distribution of the building height classes on *comuna* level exactly.

In addition to that, for subsequent casualty estimation, the mapped number of buildings per type is also deployed to compute the population per building, since the *comuna*-level data also carries the average number of dwellers per building type.

#### <span id="page-13-1"></span>**3.3 Damage state computation and casualty estimation**

To assess the likely distribution of damage levels on the exposed building portfolio after the occurrence of an earthquake, the estimated ground shaking intensity is assigned to each spatial entity. Given the spatial resolution properties of the hazard assessment with an intensity value every 300 m, it is possible that multiple intensity values are located within a spatial entity of an exposure model. If this is the case, we compute the mean intensity value per spatial entity. Consequently, we can determine the intensity which afects a certain number of buildings of a certain type at a certain location. In conjunction with the typespecifc fragility functions, the overall distribution of damage states for a spatial entity can be computed. Population data per building and afliated damage states are combined with the empirical conversion factors for the building-related damage states. Finally, the numbers across the buildings are summed up to obtain the number of afected people according to the four degrees of injury per spatial entity.

## <span id="page-13-0"></span>**4 Experimental results and discussion**

#### **4.1 Exposure data**

The results of the fve diferent disaggregation techniques along with the *comuna*-level data regarding the number of buildings per type are visualized in Fig. [8](#page-13-2)a, b. Additionally, to establish a reference mapping, we deploy the VHR nDSM (which can be considered as a proper measurement) on sub-grid-cell level while reproducing the building height class distributions on *comuna* level, since this confguration corresponds to the highest level of prior knowledge deployment. Moreover, the building types are ordered according to their frequency, i.e., "MR 1–2" corresponds to the most frequent type in Santiago de Chile, whereas "CR 25–40" represents the least frequent type.

From these fgures, it can be frst noted that distributions of buildings per type within a *comuna* are less uniform for the grid-cell-level methods compared to the sub-grid-cell





#### building type

number of buildings per grid cell

**Fig. 8** (continued)



reference

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<span id="page-16-0"></span>**Fig. 9** Scatter plots for estimated **a** number of buildings and **b** corresponding living area  $(m^2)$  for the different disaggregation techniques, i.e., linear, grid-cell-level-absolute, grid-cell-level-relative, sub-grid-celllevel-absolute, and sub-grid-cell-level-relative, respectively

reference

reference

reference

methods. This is intrinsically related to the fact that solely a single building height class per grid cell can be inferred on grid-cell level for disaggregation. However, also the estimates at the sub-grid-level allocate the diferent building types to specifc parts of the *comunas*. These mappings refect the reference spatial distributions frequently very well. This underlines the importance of spatially refned mappings compared to linear disaggregations, which solely provide uniform estimates within a *comuna*.

To study the accuracy properties of the diferent disaggregation methods in detail in this empirical setup, scatter plots (Fig. [9\)](#page-16-0) provide a comparison per grid cell for both the number of buildings and the living area (since it varies per building type). Notably, grid-cell-level and sub-grid-cell-level estimates, which are based on relative height constraints, allow obtaining consistently moderate to high positive levels of agreement  $(R>0.6)$  for both the number of buildings and living area. These estimates are substantially better aligned than linear allocations. In contrast, the methods that build upon absolute height thresholds are hardly capable of reproducing the reference mapping. This stresses the necessity to extract proper distributions of building height classes from the initial exposure model since those can hardly be estimated directly with the presented data and without further prior knowledge.

As mentioned in Sect. [2.2.2,](#page-3-1) the grid-cell-level estimates can be also produced by means of supervised learning techniques, i.e., learning from an area where both TDM and Sentinel-2 are available and establishing an estimation for areas where solely Sentinel-2 is available. Consequently, the accuracy diference of the grid-cell level and sub-grid-cell level can be interpreted as an error cost related to the integration of both TDM DSM data and Sentinel-2 imagery compared to the ubiquitously available Sentinel-2 imagery.

Additionally, Fig. [10](#page-17-0) provides median absolute errors (MAEs) both in terms of the number of buildings per grid cell and living area  $(m<sup>2</sup>)$  per grid cell for the different building types. Analogous to previous observations, the grid-cell-level estimates based on absolute height thresholds (light blue) do not provide superior accuracy properties compared to linear allocations (black). In contrast, both grid-cell-level-relative (dark blue) and sub-gridcell-level-absolute (light red) estimates provide substantial benefts for buildings of the lowest building height class (which corresponds to the vast majority of buildings in this empirical setting, i.e., 99.0% of the number and 68.6% of the living area). Moreover, the

reference



#### (a) median absolute error - number of buildings per grid-cell

(b) median absolute error - living area (m<sup>2</sup>) per grid-cell



<span id="page-17-0"></span>**Fig. 10** Median absolute errors for **a** the number of buildings per grid-cell and **b** the living area  $(m^2)$  per grid-cell regarding the diferent disaggregation techniques and seismic building structural types, respectively

sub-grid-cell-level-relative approach (dark red) allows the establishment of more accurate estimates for each building type compared to a linear disaggregation which unambiguously underlines the usefulness of the presented data and methods.



<span id="page-18-0"></span>**Fig. 11** Results of the diferent mapping techniques regarding the four damage states and PSHA results. The color bars indicate the absolute number of buildings per grid cell according to a certain damage state and PSHA result, respectively

## **4.2 Damage state computation and casualty estimation**

Figure [11](#page-18-0) provides the damage states for the spatial entities according to the four considered PSHA results. It can be visually traced how the number of damaged buildings increases with increasing intensity of shaking. Thereby, large parts of the business and fnancial areas, which expand northeastwards from the city center, feature a comparatively low concentration of damaged buildings. This is more pronounced for the grid-cell-level approaches compared to the sub-grid-cell-level approaches due to a denser spatial pooling of high-rise buildings (cf. Fig. [8](#page-13-2)b). Generally, the underlying mechanism relates to the existence of high-rise buildings in the city center, which are typically compliant with seismic design provisions and thus, having low fragility. In contrast, particularly for the considered severe events, i.e., earthquakes with a probability of occurrence of 10% within 50 years and with 10% in 475 years, respectively, we observe that large areas at the fringes of the city might feature a high concentration of damaged buildings, which relates to the existence of numerous low-rise building types with a comparative higher seismic fragility (e.g., informal, non-engineered structures). Overall, diferent damage is estimated for diferent parts of the city, which allow for anticipation of the situation based on possible events.

Figure [12](#page-19-1) shows MAEs, which describe the deviation regarding the estimated number of buildings per grid cell in relation to the reference number of buildings per grid cell, for the four damage states and PSHA results. Thus, MAEs indicate the numerical deviation that relates to the majority of grid cells, i.e., area. Except for the grid-cell-level-absolute



<span id="page-19-1"></span>**Fig. 12** Median absolute errors regarding the number of buildings per grid cell for the four damage states and PSHA results

approach, the proposed disaggregation techniques all provide substantial benefts in terms of their accuracy properties compared to linear disaggregation which confrms the benefts of the presented data and methods. Thereby, the sub-grid-cell-level approaches are more favorable than the grid-cell-level-relative method, whereby the relative height constraints on the sub-grid-cell level reveal the most favorable results overall.

Finally, Figs. [13](#page-20-0) and [14](#page-20-1) provide the percentages of the population in the respective casualty state for the spatial entities according to the four PSHA results and the corresponding MAEs of the diferent disaggregation techniques, respectively. Analogous to the disaggregated damage state mappings, large parts of the center and areas in the Northeast feature a comparatively low concentration of people in the respective casualty states. In contrast, various areas arranged in a concentric manner around the core of the city represent particular hot spots for casualties. Thereby, sub-grid-level-relative estimates provide superior MAEs. The casualty estimates can serve as a metric for prioritizing rescue activities and further mitigation efforts after an earthquake.

## <span id="page-19-0"></span>**5 Conclusion and outlook**

In this paper, we established a workfow for the derivation of constituent morphologic properties of the built environment and subsequent utilization for spatial disaggregation of exposure information based on globally existing EO data, i.e., TDM DSM data and Sentinel-2 imagery. Hereby, we proposed fve diferent disaggregation techniques to allocate various seismic building structural types. Moreover, we aligned building fragility functions and conversion factors for casualty estimation and utilized the compiled data for



<span id="page-20-0"></span>**Fig. 13** Results of the diferent mapping techniques regarding the four damage states and PSHA results. The color bars indicate the percentage of the population in the respective casualty state



<span id="page-20-1"></span>**Fig. 14** Median absolute errors regarding the percentage of the population in the respective casualty state and PSHA results

PSHA-based earthquake loss estimations. The proposed disaggregation methods turned out to be benefcial for a fne-grained mapping of various seismic building structural types and refned estimates of both building damage and casualties. Based on our estimates of damage and casualties, resulting from a variety of accelerations, one may formulate an informed mitigation program.

In the future, we aim to integrate machine learning techniques (Geiß et al. [2020b](#page-23-17), [2022a,](#page-23-15) [b\)](#page-23-16) in the workfow to overcome restrictions related to the accessibility of the TDM DSM data and apply the workfow on a country scale for Chile. Thereby, it can be expected that the relevance of the proposed disaggregation techniques will be increased given that some *comunas* particularly in rural areas expand over comparatively small settlement areas, i.e., solely a minor fraction of the area of a *comuna* is covered by settlements, and, thus, fail to allow for a spatially diferentiated consideration of smallscale hazard efects. Consequently, with a refned exposure mapping, we aim to better quantitatively describe risks from various earthquakes, especially in rural areas.

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## **Declarations**

**Confict of interest** The authors have not disclosed any competing interests.

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