EXPERIMENTAL UNIT FOR STUDYING THE PROCESSES INVOLVED IN DEFECT FORMATION IN STRIP-TYPE HIGH-TEMPERATURE SUPERCONDUCTORS

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The proposed experimental unit will make it possible to perform tests of short and long high-temperature superconductors (HTSC) in strip and wire form and to quickly evaluate their required mechanical characteristics with improved accuracy, thus giving the unit an advantage over similar existing units. The unit will also make it possible to offer a new range of services in regard to the comprehensive testing of HTSC and other new materials.

The current rate of industrial growth makes it important to develop new technologies that will reduce not only energy costs, but also the costs incurred in making, testing, and certifying products. In this context, the development of technologies for making and testing high-temperature superconductors (HTSC) is now an important problem [1, 2].

The future wide use of HTSC – materials and components – in power generation, electronics, transport, aerospace, medicine, and other sectors of the economy will create a large demand for experimental units that can be used to test them. Hundreds or thousands of such units may eventually be needed.

To meet this challenge, we have developed a unit to perform experimental studies on the identification and accumulation of damages from the bending of superconducting single- and multi-strand strips of Bi-2223/Ag. We also obtained estimates of the defect content of the specimens after loading. No small units of this type are currently made anywhere else in the world. The closest similar unit is an experimental system developed to evaluate the aging of HTSC wires made of Bi-2223 during mechanical loading. That system was designed jointly by Pirelli Cables and Systems (in Italy) and the American Superconductor Corporation (U.S.) [3]. However, this unit uses neither laser systems nor acoustic-emission techniques to evaluate the displacements and strains that occur in such wires under mechanical loads. Thus, the results obtained with it are likely to be less accurate than the results obtained from the unit being proposed here.

A basic diagram of the unit is shown in Fig. 1. The unit's load-bearing structure consists of a stationary main base 1 and a stationary auxiliary base 2 that are rigidly connected to one another by four posts 3. The small testing machine 4 of the unit is located on main base 1 along with an elastic element 5 with four extensometers 6; a special beam 7 is rigidly attached to the element, a piezoelectric element 8 with a reflector 9 being affixed to one end of the beam and two ball-bearing supports 10 being installed on the other end. The test specimen 11 is placed on the supports just mentioned. Specimen 11 is loaded by an indenter/transducer 12, which moves in the vertical direction along guides composed of a cylinder 13 and a bushing 14 with lapped surfaces. Indenter/transducer 12 is moved by the action of the lever 15, which is brought into motion by testing machine 4. The indenter/transducer is returned to its original position by a spring 16 when the load is removed. The displacement of indenter-transducer 12 is determined by the signal formed by extensometer 17.

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Fig. 1. Diagram of experimental unit.

A beam splitter 18 is secured to auxiliary base 2. The position of the splitter 18 is recorded when the unit is adjusted, and the splitter is then fixed in position by means of special spring-opposed supports 19. A radiation source 20 is mounted on the posts along with a convex lens 21. The diaphragm of three-dimensional filter 22 is located in the focus of the lens. A photodector 23 is also mounted on the posts.

Specimen 11 is mechanically loaded in a three-point loading scheme using small nonstandard testing machine 4. The specimen freely lies on both ball-bearing supports 10. The loading is done by indenter/transducer 12. Regulators provided for the switching-and-control element can be used to assign and smoothly change the rate and direction of the loading. The force that is developed is measured by means of four transducers 6, while the deflection is measured with transducer 17. The displacement is measured with a holographic interference system. Indenter/transducer 9 receives acoustic emission (AE) signals, and the parameters of those signals are analyzed by the AE block of the switching-and-control element. A matching block then converts the analyzed signals in an analog-digital converter and the output signals from the converter are subjected to final analysis in a microcomputer.

As noted above, one of the distinguishing features of the unit developed here is the use of an interference gage to measure displacement. The gage operates in the following manner: the coherent monochromatic radiation from laser 20 is converted into a divergent beam after passing through short-focus convex lens 21, the diaphgram 22 being located in the focus of this lens. One part of the beam is reflected by beam splitter 18, while the other part strikes the reflector 9 secured to piezo-electric element 8. The piezoelectric element is rigidly affixed to the elastic element 5 of the gage that measures the loading force. Beam splitter 18 and reflector 9 are adjusted so that the beams reflected from them are sent to photodetector 23. An interference pattern is formed in the plane of the photodetector in the form of rings of different inclination. The nature of this pattern is due to the interaction of the coherent, spatially coincident beams – the reference beam (formed by the splitter) and the measurement beam (formed by the reflector). The output signal of photodetector 23 is recorded and analyzed in the microcomputer. Piezoelectric element 8 is designed to establish the zero of the gage. This is done by feeding the gage a signal whose voltage has been stabilized within a 30-V range of values.

The gage incoporates design features that distinguish it favorably from standard laser interferometers. The simplicity of the overall design and the small number of optical elements make it possible to reduce losses in intensity and alleviate distortion of the wave front of the interference beams. The interference pattern is formed in the plane of the photodetector beyond the limits of the holographic photosensitive plate, on the same side as the optical axis of the light flow that is being reconstructed. This makes it possible to freely position the detector and the radiation source in space and simplifies the recording of the information. The quality and reliability of the interference measurements are improved by using a system that corrects the readings through integral recording of the intensity of the optical field of the interference pattern [4]. Use of the given method also makes it possible to check for the effects of other factors on the measurement results or to change the test conditions in general.

The interference gage being proposed here for measuring small displacements can be used to directly receive acoustic signals (such as AE signals) and analyze their spectral composition in order to study different stages of the processes involved in fracture and evaluate the damage content of structural materials and elements as they are loaded and undergo creep.

The proposed experimental unit makes it possible to test shortwave and longwave HTSC – strips and wires – and to evaluate the required mechanical characteristics faster and more reliably. This is an important advantage over existing units. The new unit can be used to offer a new range of services in regard to the systematic testing of HTSC and other new materials.

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