

Measuring Subcompositional Incoherence

Michael Greenacre

Received: 26 January 2010 / Accepted: 3 January 2011 / Published online: 24 May 2011
© International Association for Mathematical Geosciences 2011

Abstract Subcompositional coherence is a fundamental property of Aitchison's approach to compositional data analysis and is the principal justification for using ratios of components. We maintain, however, that lack of subcompositional coherence (i.e., incoherence) can be measured in an attempt to evaluate whether any given technique is close enough, for all practical purposes, to being subcompositionally coherent. This opens up the field to alternative methods that might be better suited to cope with problems such as data zeros and outliers while being only slightly incoherent. The measure that we propose is based on the distance measure between components. We show that the two-part subcompositions, which appear to be the most sensitive to subcompositional incoherence, can be used to establish a distance matrix that can be directly compared with the pairwise distances in the full composition. The closeness of these two matrices can be quantified using a stress measure that is common in multidimensional scaling, providing a measure of subcompositional incoherence. The approach is illustrated using power-transformed correspondence analysis, which has already been shown to converge to log-ratio analysis as the power transform tends to zero.

Keywords Correspondence analysis · Compositional data · Chi-square distance · Log-ratio distance · Multidimensional scaling · Stress · Subcompositional coherence

M. Greenacre (✉)
Departament d'Economia i Empresa, Universitat Pompeu Fabra, Ramon Trias Fargas, 25-27,
Barcelona 08005, Spain
e-mail: michael.greenacre@upf.edu

M. Greenacre
Barcelona Graduate School of Economics, Barcelona, Spain

1 Introduction

In his seminal paper in “*Biometrika*,” John Aitchison (1983) stated the following: “A desirable feature of any form of compositional data analysis is an ability to study subcompositions, that is subvectors rescaled to give unit sum. One important requirement is an ability to quantify the extent to which a subcomposition retains a picture of the variability of the whole composition.” The property of subcompositional coherence is indeed one of the cornerstones of Aitchison’s approach to compositional data analysis: results should be the same for components in a full composition as in any subcomposition, where the subcomposition has been closed again to give unit sum, or reclosed (Pawlowsky-Glahn et al. 2007). An example that is often given of subcompositional incoherence is that the correlation coefficient between two components in a (reclosed) subcomposition is not the same as for the same two components in the full composition (Chayes 1960). Using ratios as the basic input data for analysis solves this paradox, and the log-ratio transformation has become a standard approach to guarantee subcompositional coherence.

For ease of exposition, we shall often refer to subcompositional coherence simply as coherence. Coherence is an absolute property which a procedure either possesses or not. But if it does not (i.e., if it is incoherent), we maintain that there are levels of incoherence that can be usefully measured and exploited. For example, what if our method was close to being coherent—would that not be useful if in the process we fixed other problems, such as the treatment of zeros in the data? As a context for our investigation, we have chosen the area of visualization of compositional data in the form of maps in the style of principal component analysis (PCA) and multidimensional scaling (MDS) because these are based on the concept of distance and distance is one of the most fundamental aspects of multivariate analysis.

The log-ratio approach to PCA of compositional data originates in the papers of Aitchison (1983, 1986, 1990), which we call log-ratio analysis (LRA). Simply stated, LRA can be defined as the PCA of a matrix of strictly positive compositional data—assumed to be closed row-wise—after logarithmically transforming the data and centering each row of the log-transformed values by its respective row mean. Since the first step of the ensuing PCA is to center the columns of the table, it is said that the log-transformed table is double-centered; the dimension-reduction step is then performed using the singular value decomposition. Interestingly, even though the rows and columns are different entities (samples and components), LRA treats them totally symmetrically, and the results would be identical if the matrix were transposed. A different approach, also symmetric with respect to rows and columns, is to use correspondence analysis (CA), a method applicable to any table of non-negative numbers, as long as they are all on the same ratio-scale of measurement and hence suitable for compositional data as well, even with zeros (Greenacre 1984, 2007). In fact, it is its ability to handle zeros (even lots of zeros in very sparse tables) that has made CA so popular in environmental and archaeological research. The table is first centered with respect to the expected values based on the row and column margins of the table, a term that is borrowed from contingency table analysis. The rows and columns are weighted proportionally to these marginal values: in the case of compositional data, samples (rows) would have the same weights, but components

(columns) would be weighted proportionally to their average in the dataset. The subsequent dimension-reduction step is similar to that of PCA apart from the row and column weighting factors. For a recent account of CA, see Greenacre (2007, 2008).

Greenacre (2009) has shown that LRA and CA are actually part of a common family parameterized by a power transformation; a summary of these findings aimed at compositional data analysts is given by Greenacre (2010). Putting this result simply, if compositional data are powered up by a power α , reclosed row-wise, and then a regular CA is performed on the transformed data with a rescaling of the solution by $1/\alpha$, then this procedure converges exactly at the LRA solution as the power parameter α tends to 0. In fact, this is nothing else but the Box–Cox transformation in disguise (Box and Cox 1964); for more on the Box–Cox transformation in this context, see Greenacre (2009). This means that we can come arbitrarily close to Aitchison's LRA by performing a CA: numerically, there is hardly any difference between the CA just described using $\alpha = 0.001$, for example, and LRA. Now while LRA is coherent, CA is not. But it follows intuitively from the limiting result mentioned above, and we shall indeed show this to be true, that CA comes closer and closer to being coherent as the power parameter approaches 0. Since CA can handle zeros in a completely natural way, whereas LRA cannot, an alternative approach to the zero-value problem is to use power-transformed CA instead of LRA, coming as close as possible to coherence. This is the background necessary for the measurement of coherence and the study of its behavior in different scenarios.

In Sect. 2, the distance functions inherent in LRA and CA are defined and compared, especially with respect to their application to subcompositions. In Sect. 3, a measure of subcompositional incoherence is defined using all the two-part subcompositions of a table, quantifying how well the interpoint distances for these pairs approximate their interpoint distances in the full composition. Section 4 treats the issue of component weighting, which considerably enhances LRA since it down-weights the effect of the rare components that generally have high log-ratio variance. The subcompositional incoherence of principal component analysis (PCA) is measured in Sect. 5, and Sect. 6 concludes the paper with a discussion.

2 Log-ratio and Chi-square Distances for Compositions and Subcompositions

As intimated in the introduction, we adopt a distance-based approach where the concept of between-component distance will be fundamental. Notice that we are not interested here in between-sample distance since the property of coherence applies to the relationships between components. For our purposes, coherence will mean that distances calculated between the components in the full composition will be identical in the subcomposition. Since we will be generally concerned with Euclidean-type distances, which are embeddable in an inner product space, this distance-based property of coherence will mean that all the classical statistics (such as variance, correlation, and covariance) will also be coherent.

Suppose that the compositional data table of I samples (rows) and J components (columns) is denoted by \mathbf{X} ($I \times J$). The two equivalent definitions of what we call the log-ratio distance between two components j and j' are expressed in squared

distance form as follows

$$d_{jj'}^2 = \frac{1}{I} \sum_{i=1}^I \left[\log \left(\frac{x_{ij}}{g(\mathbf{x}_j)} \right) - \log \left(\frac{x_{ij'}}{g(\mathbf{x}_{j'})} \right) \right]^2 \tag{1}$$

(Aitchison 1983, 1986), where $g(\mathbf{x}_j)$ is the geometric mean of the j th column corresponding to the j th component (i.e., $\log(g(\mathbf{x}_j))$ is the arithmetic average of $\log(x_{ij})$, $i = 1, \dots, I$). The alternative definition is in terms of all pairwise odds-ratios across all pairs of samples

$$d_{jj'}^2 = \frac{1}{I^2} \sum_{i < i'} \sum \left[\log \left(\frac{x_{ij}x_{i'j'}}{x_{ij'}x_{i'j}} \right) \right]^2. \tag{2}$$

Notice that, compared to Aitchison’s original definition, we have averaged the squared terms over the samples, so that the distance does not depend on sample size; this form of the distance is compatible with the chi-square distance in CA, which is also averaged over samples. Although definition (1) involves centering each $\log(x_{ij})$ with respect to the average $(1/I) \sum_i \log(x_{ij})$, definition (2) shows that the distance is actually independent of this centering—this is another reason for using distance as the fundamental concept for judging and measuring coherence. Definition (2) also shows quite clearly that the log-ratio distance is coherent: if any subcomposition involving components j and j' is considered and reclosed row-wise, the ratios row-wise $x_{ij}/x_{ij'}$ remain identical, and so definition (2) remains the same.

In CA, it is the chi-square distance that defines distance between columns. First, the column profiles are calculated by dividing the elements of each column j by their sum x_{+j} . Then, the sum of squared distances between profile elements is calculated, weighted inversely by the profile of the row sums. Since for \mathbf{X} these row sums are all equal to one, the marginal row profile has constant values $(1/I)$, and hence the squared chi-square distance between columns j and j' is

$$x_{jj'}^2 = \sum_{i=1}^I \left[\frac{x_{ij}}{x_{+j}} - \frac{x_{ij'}}{x_{+j'}} \right]^2 / (1/I) = I \sum_{i=1}^I \left[\frac{x_{ij}}{x_{+j}} - \frac{x_{ij'}}{x_{+j'}} \right]^2. \tag{3}$$

Clearly, the chi-square distance is incoherent, but from the results of Greenacre (2009, 2010) mentioned previously it follows that the chi-square distance on the power-transformed data tends to the log-ratio distance as the power parameter α tends to 0. The convergence of CA to LRA is a direct result of the Box–Cox transformation

$$f(x) = \begin{cases} (1/\alpha)(x^\alpha - 1) & \alpha > 0 \\ \log(x) & \text{otherwise} \end{cases},$$

where $(1/\alpha)(x^\alpha - 1)$ tends to $\log(x)$ as α tends to 0. To illustrate this convergence empirically in the case of the chi-square distance, Table 1 shows four versions of a subset of distances calculated on the 11 components (mostly oxides) of the 47 by 11 compositional dataset on Roman glass cups published by Baxter et al. (1990) and reproduced by Greenacre and Lewi (2009, Table 2). The chi-square distances are at

Table 1 Three sets of chi-square distances based on CAs with different power transformations, starting at the top left with power $\alpha = 1$, the regular untransformed CA, and ending at the bottom left, the log-ratio distances from LRA (read the tables clock-wise). Parts of each 11 by 11 table of distances are shown, as well as the maximum absolute difference between the distances in the full table and their corresponding log-ratio distances. The oxides are labeled by their major elements; for example, *Si* stands for silicon oxide, *SiO₂*

<p>$\alpha = 1$ (untransformed CA)</p> <table border="1"> <thead> <tr> <th></th> <th><i>Si</i></th> <th><i>Al</i></th> <th><i>Fe</i></th> <th><i>Mg</i></th> <th><i>Ca</i></th> <th>...</th> </tr> </thead> <tbody> <tr> <td><i>Si</i></td> <td>0.0000</td> <td>0.0920</td> <td>0.2259</td> <td>0.1850</td> <td>0.1241</td> <td>...</td> </tr> <tr> <td><i>Al</i></td> <td>0.0920</td> <td>0.0000</td> <td>0.1441</td> <td>0.1261</td> <td>0.0855</td> <td>...</td> </tr> <tr> <td><i>Fe</i></td> <td>0.2259</td> <td>0.1441</td> <td>0.0000</td> <td>0.1280</td> <td>0.1472</td> <td>...</td> </tr> <tr> <td><i>Mg</i></td> <td>0.1850</td> <td>0.1261</td> <td>0.1280</td> <td>0.0000</td> <td>0.1387</td> <td>...</td> </tr> <tr> <td><i>Ca</i></td> <td>0.1241</td> <td>0.0855</td> <td>0.1472</td> <td>0.1387</td> <td>0.0000</td> <td>...</td> </tr> <tr> <td>.</td> <td>.</td> <td>.</td> <td>.</td> <td>.</td> <td>.</td> <td>...</td> </tr> <tr> <td>.</td> <td>.</td> <td>.</td> <td>.</td> <td>.</td> <td>.</td> <td>...</td> </tr> <tr> <td>.</td> <td>.</td> <td>.</td> <td>.</td> <td>.</td> <td>.</td> <td>...</td> </tr> </tbody> </table> <p>Max abs diff = 0.0797</p>							<i>Si</i>	<i>Al</i>	<i>Fe</i>	<i>Mg</i>	<i>Ca</i>	...	<i>Si</i>	0.0000	0.0920	0.2259	0.1850	0.1241	...	<i>Al</i>	0.0920	0.0000	0.1441	0.1261	0.0855	...	<i>Fe</i>	0.2259	0.1441	0.0000	0.1280	0.1472	...	<i>Mg</i>	0.1850	0.1261	0.1280	0.0000	0.1387	...	<i>Ca</i>	0.1241	0.0855	0.1472	0.1387	0.0000	<p>$\alpha = 0.25$</p> <table border="1"> <thead> <tr> <th></th> <th><i>Si</i></th> <th><i>Al</i></th> <th><i>Fe</i></th> <th><i>Mg</i></th> <th><i>Ca</i></th> <th>...</th> </tr> </thead> <tbody> <tr> <td><i>Si</i></td> <td>0.0000</td> <td>0.0909</td> <td>0.2207</td> <td>0.1878</td> <td>0.1209</td> <td>...</td> </tr> <tr> <td><i>Al</i></td> <td>0.0909</td> <td>0.0000</td> <td>0.1404</td> <td>0.1282</td> <td>0.0850</td> <td>...</td> </tr> <tr> <td><i>Fe</i></td> <td>0.2207</td> <td>0.1404</td> <td>0.0000</td> <td>0.1190</td> <td>0.1468</td> <td>...</td> </tr> <tr> <td><i>Mg</i></td> <td>0.1878</td> <td>0.1282</td> <td>0.1190</td> <td>0.0000</td> <td>0.1404</td> <td>...</td> </tr> <tr> <td><i>Ca</i></td> <td>0.1209</td> <td>0.0850</td> <td>0.1468</td> <td>0.1404</td> <td>0.0000</td> <td>...</td> </tr> <tr> <td>.</td> <td>.</td> <td>.</td> <td>.</td> <td>.</td> <td>.</td> <td>...</td> </tr> <tr> <td>.</td> <td>.</td> <td>.</td> <td>.</td> <td>.</td> <td>.</td> <td>...</td> </tr> <tr> <td>.</td> <td>.</td> <td>.</td> <td>.</td> <td>.</td> <td>.</td> <td>...</td> </tr> </tbody> </table> <p>Max abs diff = 0.0142</p>							<i>Si</i>	<i>Al</i>	<i>Fe</i>	<i>Mg</i>	<i>Ca</i>	...	<i>Si</i>	0.0000	0.0909	0.2207	0.1878	0.1209	...	<i>Al</i>	0.0909	0.0000	0.1404	0.1282	0.0850	...	<i>Fe</i>	0.2207	0.1404	0.0000	0.1190	0.1468	...	<i>Mg</i>	0.1878	0.1282	0.1190	0.0000	0.1404	...	<i>Ca</i>	0.1209	0.0850	0.1468	0.1404	0.0000
	<i>Si</i>	<i>Al</i>	<i>Fe</i>	<i>Mg</i>	<i>Ca</i>	...																																																																																																																																			
<i>Si</i>	0.0000	0.0920	0.2259	0.1850	0.1241	...																																																																																																																																			
<i>Al</i>	0.0920	0.0000	0.1441	0.1261	0.0855	...																																																																																																																																			
<i>Fe</i>	0.2259	0.1441	0.0000	0.1280	0.1472	...																																																																																																																																			
<i>Mg</i>	0.1850	0.1261	0.1280	0.0000	0.1387	...																																																																																																																																			
<i>Ca</i>	0.1241	0.0855	0.1472	0.1387	0.0000	...																																																																																																																																			
.																																																																																																																																			
.																																																																																																																																			
.																																																																																																																																			
	<i>Si</i>	<i>Al</i>	<i>Fe</i>	<i>Mg</i>	<i>Ca</i>	...																																																																																																																																			
<i>Si</i>	0.0000	0.0909	0.2207	0.1878	0.1209	...																																																																																																																																			
<i>Al</i>	0.0909	0.0000	0.1404	0.1282	0.0850	...																																																																																																																																			
<i>Fe</i>	0.2207	0.1404	0.0000	0.1190	0.1468	...																																																																																																																																			
<i>Mg</i>	0.1878	0.1282	0.1190	0.0000	0.1404	...																																																																																																																																			
<i>Ca</i>	0.1209	0.0850	0.1468	0.1404	0.0000	...																																																																																																																																			
.																																																																																																																																			
.																																																																																																																																			
.																																																																																																																																			
<p>$\alpha = 0$ (LRA)</p> <table border="1"> <thead> <tr> <th></th> <th><i>Si</i></th> <th><i>Al</i></th> <th><i>Fe</i></th> <th><i>Mg</i></th> <th><i>Ca</i></th> <th>...</th> </tr> </thead> <tbody> <tr> <td><i>Si</i></td> <td>0.0000</td> <td>0.0913</td> <td>0.2209</td> <td>0.1882</td> <td>0.1213</td> <td>...</td> </tr> <tr> <td><i>Al</i></td> <td>0.0913</td> <td>0.0000</td> <td>0.1403</td> <td>0.1279</td> <td>0.0849</td> <td>...</td> </tr> <tr> <td><i>Fe</i></td> <td>0.2209</td> <td>0.1403</td> <td>0.0000</td> <td>0.1168</td> <td>0.1471</td> <td>...</td> </tr> <tr> <td><i>Mg</i></td> <td>0.1882</td> <td>0.1279</td> <td>0.1168</td> <td>0.0000</td> <td>0.1404</td> <td>...</td> </tr> <tr> <td><i>Ca</i></td> <td>0.1213</td> <td>0.0849</td> <td>0.1471</td> <td>0.1404</td> <td>0.0000</td> <td>...</td> </tr> <tr> <td>.</td> <td>.</td> <td>.</td> <td>.</td> <td>.</td> <td>.</td> <td>...</td> </tr> <tr> <td>.</td> <td>.</td> <td>.</td> <td>.</td> <td>.</td> <td>.</td> <td>...</td> </tr> <tr> <td>.</td> <td>.</td> <td>.</td> <td>.</td> <td>.</td> <td>.</td> <td>...</td> </tr> </tbody> </table> <p>Max abs diff = 0</p>							<i>Si</i>	<i>Al</i>	<i>Fe</i>	<i>Mg</i>	<i>Ca</i>	...	<i>Si</i>	0.0000	0.0913	0.2209	0.1882	0.1213	...	<i>Al</i>	0.0913	0.0000	0.1403	0.1279	0.0849	...	<i>Fe</i>	0.2209	0.1403	0.0000	0.1168	0.1471	...	<i>Mg</i>	0.1882	0.1279	0.1168	0.0000	0.1404	...	<i>Ca</i>	0.1213	0.0849	0.1471	0.1404	0.0000	<p>$\alpha = 0.001$</p> <table border="1"> <thead> <tr> <th></th> <th><i>Si</i></th> <th><i>Al</i></th> <th><i>Fe</i></th> <th><i>Mg</i></th> <th><i>Ca</i></th> <th>...</th> </tr> </thead> <tbody> <tr> <td><i>Si</i></td> <td>0.0000</td> <td>0.0913</td> <td>0.2209</td> <td>0.1882</td> <td>0.1213</td> <td>...</td> </tr> <tr> <td><i>Al</i></td> <td>0.0913</td> <td>0.0000</td> <td>0.1403</td> <td>0.1280</td> <td>0.0849</td> <td>...</td> </tr> <tr> <td><i>Fe</i></td> <td>0.2209</td> <td>0.1403</td> <td>0.0000</td> <td>0.1168</td> <td>0.1471</td> <td>...</td> </tr> <tr> <td><i>Mg</i></td> <td>0.1882</td> <td>0.1280</td> <td>0.1168</td> <td>0.0000</td> <td>0.1404</td> <td>...</td> </tr> <tr> <td><i>Ca</i></td> <td>0.1213</td> <td>0.0849</td> <td>0.1471</td> <td>0.1404</td> <td>0.0000</td> <td>...</td> </tr> <tr> <td>.</td> <td>.</td> <td>.</td> <td>.</td> <td>.</td> <td>.</td> <td>...</td> </tr> <tr> <td>.</td> <td>.</td> <td>.</td> <td>.</td> <td>.</td> <td>.</td> <td>...</td> </tr> <tr> <td>.</td> <td>.</td> <td>.</td> <td>.</td> <td>.</td> <td>.</td> <td>...</td> </tr> </tbody> </table> <p>Max abs diff = 0.000042</p>							<i>Si</i>	<i>Al</i>	<i>Fe</i>	<i>Mg</i>	<i>Ca</i>	...	<i>Si</i>	0.0000	0.0913	0.2209	0.1882	0.1213	...	<i>Al</i>	0.0913	0.0000	0.1403	0.1280	0.0849	...	<i>Fe</i>	0.2209	0.1403	0.0000	0.1168	0.1471	...	<i>Mg</i>	0.1882	0.1280	0.1168	0.0000	0.1404	...	<i>Ca</i>	0.1213	0.0849	0.1471	0.1404	0.0000
	<i>Si</i>	<i>Al</i>	<i>Fe</i>	<i>Mg</i>	<i>Ca</i>	...																																																																																																																																			
<i>Si</i>	0.0000	0.0913	0.2209	0.1882	0.1213	...																																																																																																																																			
<i>Al</i>	0.0913	0.0000	0.1403	0.1279	0.0849	...																																																																																																																																			
<i>Fe</i>	0.2209	0.1403	0.0000	0.1168	0.1471	...																																																																																																																																			
<i>Mg</i>	0.1882	0.1279	0.1168	0.0000	0.1404	...																																																																																																																																			
<i>Ca</i>	0.1213	0.0849	0.1471	0.1404	0.0000	...																																																																																																																																			
.																																																																																																																																			
.																																																																																																																																			
.																																																																																																																																			
	<i>Si</i>	<i>Al</i>	<i>Fe</i>	<i>Mg</i>	<i>Ca</i>	...																																																																																																																																			
<i>Si</i>	0.0000	0.0913	0.2209	0.1882	0.1213	...																																																																																																																																			
<i>Al</i>	0.0913	0.0000	0.1403	0.1280	0.0849	...																																																																																																																																			
<i>Fe</i>	0.2209	0.1403	0.0000	0.1168	0.1471	...																																																																																																																																			
<i>Mg</i>	0.1882	0.1280	0.1168	0.0000	0.1404	...																																																																																																																																			
<i>Ca</i>	0.1213	0.0849	0.1471	0.1404	0.0000	...																																																																																																																																			
.																																																																																																																																			
.																																																																																																																																			
.																																																																																																																																			

Maximum absolute difference between chi-square and logratio distances

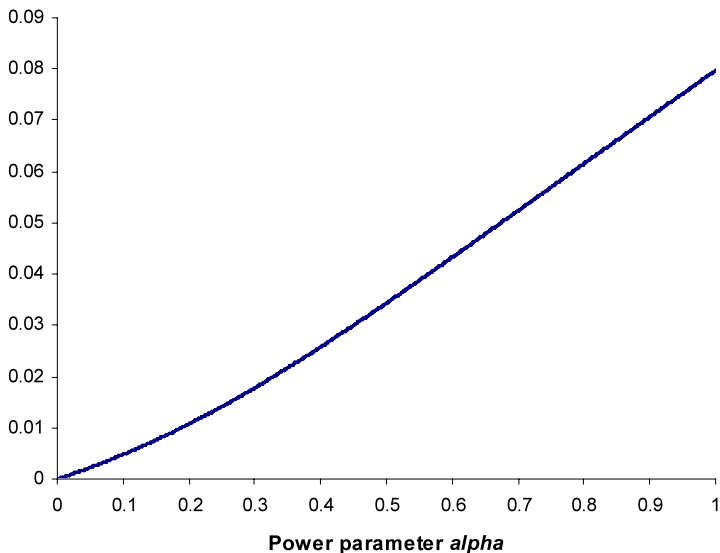


Fig. 1 Rate of convergence of chi-square distances in power-transformed CA to log-ratio distances, for powers from 1 to 0.001 (calculations made for 1000 values of the power $\alpha = 1, 0.999, 0.998, \dots, 0.001$). The vertical axis is in units of maximum absolute difference between the two sets of distances

Table 2 Two sets of chi-square distances based on CAs of subcompositions of size 5

<i>Subset 1</i>						<i>Subset 2</i>					
	<i>Si</i>	<i>Al</i>	<i>Fe</i>	<i>Mg</i>	<i>Ca</i>		<i>K</i>	<i>Ti</i>	<i>P</i>	<i>Mn</i>	<i>Sb</i>
<i>Si</i>	0.0000	0.0922	0.2264	0.1849	0.1247	<i>K</i>	0.0000	0.1562	0.1235	0.3396	0.2648
<i>Al</i>	0.0922	0.0000	0.1445	0.1256	0.0857	<i>Ti</i>	0.1562	0.0000	0.1505	0.3339	0.3152
<i>Fe</i>	0.2264	0.1445	0.0000	0.1280	0.1472	<i>P</i>	0.1235	0.1505	0.0000	0.3407	0.2527
<i>Mg</i>	0.1849	0.1256	0.1280	0.0000	0.1385	<i>Mn</i>	0.3396	0.3339	0.3407	0.0000	0.4351
<i>Ca</i>	0.1247	0.0857	0.1472	0.1385	0.0000	<i>Sb</i>	0.2648	0.3152	0.2527	0.4351	0.0000
	Max abs diff = 0.00066						Max abs diff = 0.03682				
	Stress = 0.00245						Stress = 0.06574				

the top left, then reading clockwise, the chi-square distances are based on a double square root transformation ($\alpha = \frac{1}{4}$), then a power transformation close to zero ($\alpha = 0.001$), and finally the log-ratio distances. In order to show the rate of convergence in this example, Fig. 1 shows the maximum absolute difference between the chi-square distances and the log-ratio distances for 1000 different CAs, starting with $\alpha = 1$ (untransformed CA) and descending in steps of 0.001 (i.e., 0.999, 0.998, etc., until $\alpha = 0.001$). This shows a steady, almost linear rate of convergence, and demonstrates graphically that one can get as close as one likes to the log-ratio distance, and thus to coherence, by lowering the value of α toward 0. To show the convergence to coherence, however, is more than just showing that the chi-square distance converges to the log-ratio distance—it actually concerns the behavior of subcompositions, as treated in the next section.

3 A Measure of Subcompositional Incoherence

Coherence is the invariance of the statistical procedure when applied to subsets of components that are reclosed. Since our particular interest here is in dimension reduction, we focus on the effect on the distances, since they affect all our subsequent analyses. Since CA is incoherent because the chi-square distances clearly change when computed on subcompositions, let us see the extent of its incoherence by calculating the chi-square distances for different subsets of the components of the Roman glass cup dataset. The chi-square distances for the full eleven-part composition serve as a reference to which we will compare the chi-square distances for every relevant subset of components: the $\binom{11}{2} = 55$ subsets of size 2, the $\binom{11}{3} = 165$ subsets of size 3, etc., until the $\binom{11}{10} = 11$ subsets of size 10. For example, the top left table of Table 1 shows the chi-square distances between the first five components of the full composition. If we select these five components and then reclose them to form a five-part subcomposition, the chi-square distances turn out as the first table in Table 2. This table is remarkably similar to the original chi-square distances in Table 1, and their maximum absolute difference is only 0.00066. This is because we have included in the subcomposition some of the highest components, so that the reclosure does not affect the values too much. However, if we consider the last five elements, which happen to be amongst the rarest, the second distance table in Table 2 is obtained, which is much further away from the original ones (maximum absolute difference = 0.0368).

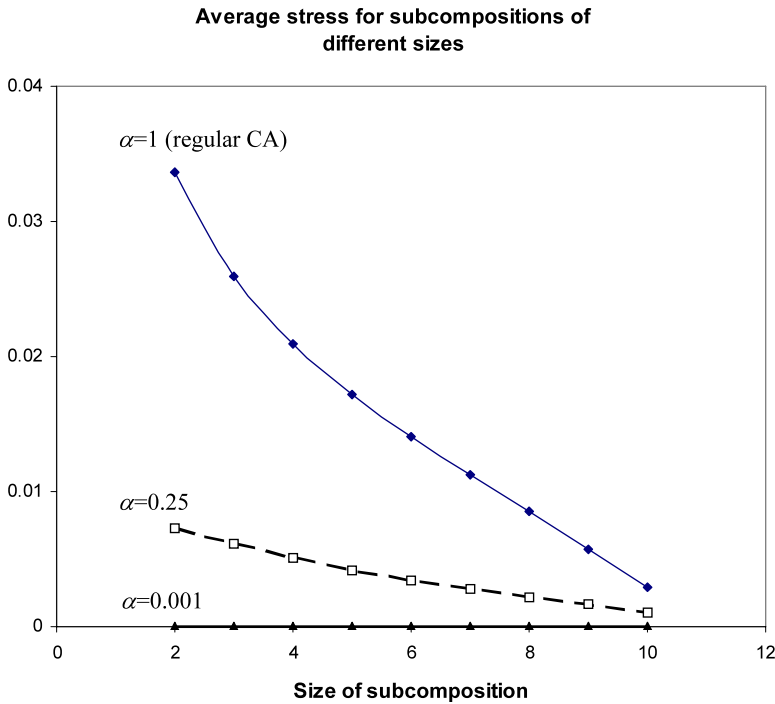


Fig. 2 Average stress (vertical axis) between chi-square distances in the full composition and corresponding chi-square distances calculated in subcompositions of different sizes (horizontal axis), for regular CA and two power-transformed CAs, $\alpha = 0.25$ and $\alpha = 0.001$. As a measure of subcompositional incoherence, stress can be interpreted as a proportion; for example, a value of 0.05 indicates a 5% difference between the two sets of distances. Subcompositions of size 2 are seen to be the worst case, while for $\alpha = 0.001$, there is almost no subcompositional incoherence

So far, to compare two distance matrices, we have used the maximum absolute difference, but this quantity depends on the scale of the distance in the particular application. In the multidimensional scaling literature, there are several well-known normalized measures for quantifying the fit of one distance matrix to another, called measures of stress. Of these, we have selected the so-called stress formula 1

$$\text{stress} = \sqrt{\frac{\sum \sum_{j < j'} (d_{jj'} - \delta_{jj'})^2}{\sum \sum_{j < j'} d_{jj'}^2}} \tag{4}$$

(Borg and Groenen 2005), where d denotes the target distances in the full composition, and δ the distances in the subcomposition. The denominator serves to normalize the sum of squared differences in the numerator, and the stress value is often multiplied by 100 and thought of as a percentage of badness of fit. For the two subcompositions analyzed in Table 2, the stress values are reported as 0.00245 (i.e., 0.245%) and 0.06574 (i.e., 6.574%). To get an idea how this deviation from coherence varies across subsets of different sizes, Fig. 2 plots the average stress against subset size (where stresses are averaged over all subcompositions of the particular size) for regular CA and repeats this for chi-square distances from two power-transformed CAs.

Table 3 Inter-component chi-square distances for the regular CA and two power-transformed CAs ($\alpha = 0.25$ and 0.001), showing on the left the distances computed in the full composition and on the right the corresponding distances obtained by forming each two-part subcomposition corresponding to the row-column pairs. Only the last five components are shown, but the maximum absolute differences and the stress values are computed for the whole 11 by 11 matrix of distances in each case

<p>Full composition, untransformed CA ($\alpha = 1$)</p> <table border="1"> <thead> <tr> <th></th> <th><i>K</i></th> <th><i>Ti</i></th> <th><i>P</i></th> <th><i>Mn</i></th> <th><i>Sb</i></th> </tr> </thead> <tbody> <tr> <td><i>K</i> ...</td> <td>0.0000</td> <td>0.1573</td> <td>0.1217</td> <td>0.3704</td> <td>0.2611</td> </tr> <tr> <td><i>Ti</i> ...</td> <td>0.1573</td> <td>0.0000</td> <td>0.1615</td> <td>0.3500</td> <td>0.3191</td> </tr> <tr> <td><i>P</i> ...</td> <td>0.1217</td> <td>0.1615</td> <td>0.0000</td> <td>0.3739</td> <td>0.2407</td> </tr> <tr> <td><i>Mn</i> ...</td> <td>0.3704</td> <td>0.3500</td> <td>0.3739</td> <td>0.0000</td> <td>0.4719</td> </tr> <tr> <td><i>Sb</i> ...</td> <td>0.2611</td> <td>0.3191</td> <td>0.2407</td> <td>0.4719</td> <td>0.0000</td> </tr> </tbody> </table>		<i>K</i>	<i>Ti</i>	<i>P</i>	<i>Mn</i>	<i>Sb</i>	<i>K</i> ...	0.0000	0.1573	0.1217	0.3704	0.2611	<i>Ti</i> ...	0.1573	0.0000	0.1615	0.3500	0.3191	<i>P</i> ...	0.1217	0.1615	0.0000	0.3739	0.2407	<i>Mn</i> ...	0.3704	0.3500	0.3739	0.0000	0.4719	<i>Sb</i> ...	0.2611	0.3191	0.2407	0.4719	0.0000	<p>Two part subcomps, untransformed CA ($\alpha = 1$)</p> <table border="1"> <thead> <tr> <th></th> <th><i>K</i></th> <th><i>Ti</i></th> <th><i>P</i></th> <th><i>Mn</i></th> <th><i>Sb</i></th> </tr> </thead> <tbody> <tr> <td><i>K</i> ...</td> <td>0.0000</td> <td>0.1586</td> <td>0.1274</td> <td>0.3358</td> <td>0.2647</td> </tr> <tr> <td><i>Ti</i> ...</td> <td>0.1586</td> <td>0.0000</td> <td>0.1527</td> <td>0.3030</td> <td>0.3182</td> </tr> <tr> <td><i>P</i> ...</td> <td>0.1274</td> <td>0.1527</td> <td>0.0000</td> <td>0.3095</td> <td>0.2677</td> </tr> <tr> <td><i>Mn</i> ...</td> <td>0.3358</td> <td>0.3030</td> <td>0.3095</td> <td>0.0000</td> <td>0.4196</td> </tr> <tr> <td><i>Sb</i> ...</td> <td>0.2647</td> <td>0.3182</td> <td>0.2677</td> <td>0.4196</td> <td>0.0000</td> </tr> </tbody> </table> <p>Max abs diff = 0.07415 Stress = 0.06441</p>		<i>K</i>	<i>Ti</i>	<i>P</i>	<i>Mn</i>	<i>Sb</i>	<i>K</i> ...	0.0000	0.1586	0.1274	0.3358	0.2647	<i>Ti</i> ...	0.1586	0.0000	0.1527	0.3030	0.3182	<i>P</i> ...	0.1274	0.1527	0.0000	0.3095	0.2677	<i>Mn</i> ...	0.3358	0.3030	0.3095	0.0000	0.4196	<i>Sb</i> ...	0.2647	0.3182	0.2677	0.4196	0.0000
	<i>K</i>	<i>Ti</i>	<i>P</i>	<i>Mn</i>	<i>Sb</i>																																																																				
<i>K</i> ...	0.0000	0.1573	0.1217	0.3704	0.2611																																																																				
<i>Ti</i> ...	0.1573	0.0000	0.1615	0.3500	0.3191																																																																				
<i>P</i> ...	0.1217	0.1615	0.0000	0.3739	0.2407																																																																				
<i>Mn</i> ...	0.3704	0.3500	0.3739	0.0000	0.4719																																																																				
<i>Sb</i> ...	0.2611	0.3191	0.2407	0.4719	0.0000																																																																				
	<i>K</i>	<i>Ti</i>	<i>P</i>	<i>Mn</i>	<i>Sb</i>																																																																				
<i>K</i> ...	0.0000	0.1586	0.1274	0.3358	0.2647																																																																				
<i>Ti</i> ...	0.1586	0.0000	0.1527	0.3030	0.3182																																																																				
<i>P</i> ...	0.1274	0.1527	0.0000	0.3095	0.2677																																																																				
<i>Mn</i> ...	0.3358	0.3030	0.3095	0.0000	0.4196																																																																				
<i>Sb</i> ...	0.2647	0.3182	0.2677	0.4196	0.0000																																																																				
<p>Full composition, transformed CA ($\alpha = 0.25$)</p> <table border="1"> <thead> <tr> <th></th> <th><i>K</i></th> <th><i>Ti</i></th> <th><i>P</i></th> <th><i>Mn</i></th> <th><i>Sb</i></th> </tr> </thead> <tbody> <tr> <td><i>K</i> ...</td> <td>0.0000</td> <td>0.1534</td> <td>0.1242</td> <td>0.3072</td> <td>0.2678</td> </tr> <tr> <td><i>Ti</i> ...</td> <td>0.1534</td> <td>0.0000</td> <td>0.1543</td> <td>0.2957</td> <td>0.3206</td> </tr> <tr> <td><i>P</i> ...</td> <td>0.1242</td> <td>0.1543</td> <td>0.0000</td> <td>0.3142</td> <td>0.2531</td> </tr> <tr> <td><i>Mn</i> ...</td> <td>0.3072</td> <td>0.2957</td> <td>0.3142</td> <td>0.0000</td> <td>0.4178</td> </tr> <tr> <td><i>Sb</i> ...</td> <td>0.2678</td> <td>0.3206</td> <td>0.2531</td> <td>0.4178</td> <td>0.0000</td> </tr> </tbody> </table>		<i>K</i>	<i>Ti</i>	<i>P</i>	<i>Mn</i>	<i>Sb</i>	<i>K</i> ...	0.0000	0.1534	0.1242	0.3072	0.2678	<i>Ti</i> ...	0.1534	0.0000	0.1543	0.2957	0.3206	<i>P</i> ...	0.1242	0.1543	0.0000	0.3142	0.2531	<i>Mn</i> ...	0.3072	0.2957	0.3142	0.0000	0.4178	<i>Sb</i> ...	0.2678	0.3206	0.2531	0.4178	0.0000	<p>Two part subcomps, transformed CA ($\alpha = 0.25$)</p> <table border="1"> <thead> <tr> <th></th> <th><i>K</i></th> <th><i>Ti</i></th> <th><i>P</i></th> <th><i>Mn</i></th> <th><i>Sb</i></th> </tr> </thead> <tbody> <tr> <td><i>K</i> ...</td> <td>0.0000</td> <td>0.1534</td> <td>0.1248</td> <td>0.2946</td> <td>0.2699</td> </tr> <tr> <td><i>Ti</i> ...</td> <td>0.1534</td> <td>0.0000</td> <td>0.1526</td> <td>0.2830</td> <td>0.3213</td> </tr> <tr> <td><i>P</i> ...</td> <td>0.1248</td> <td>0.1526</td> <td>0.0000</td> <td>0.2991</td> <td>0.2581</td> </tr> <tr> <td><i>Mn</i> ...</td> <td>0.2946</td> <td>0.2830</td> <td>0.2991</td> <td>0.0000</td> <td>0.4053</td> </tr> <tr> <td><i>Sb</i> ...</td> <td>0.2699</td> <td>0.3213</td> <td>0.2581</td> <td>0.4053</td> <td>0.0000</td> </tr> </tbody> </table> <p>Max abs diff = 0.01514 Stress = 0.02114</p>		<i>K</i>	<i>Ti</i>	<i>P</i>	<i>Mn</i>	<i>Sb</i>	<i>K</i> ...	0.0000	0.1534	0.1248	0.2946	0.2699	<i>Ti</i> ...	0.1534	0.0000	0.1526	0.2830	0.3213	<i>P</i> ...	0.1248	0.1526	0.0000	0.2991	0.2581	<i>Mn</i> ...	0.2946	0.2830	0.2991	0.0000	0.4053	<i>Sb</i> ...	0.2699	0.3213	0.2581	0.4053	0.0000
	<i>K</i>	<i>Ti</i>	<i>P</i>	<i>Mn</i>	<i>Sb</i>																																																																				
<i>K</i> ...	0.0000	0.1534	0.1242	0.3072	0.2678																																																																				
<i>Ti</i> ...	0.1534	0.0000	0.1543	0.2957	0.3206																																																																				
<i>P</i> ...	0.1242	0.1543	0.0000	0.3142	0.2531																																																																				
<i>Mn</i> ...	0.3072	0.2957	0.3142	0.0000	0.4178																																																																				
<i>Sb</i> ...	0.2678	0.3206	0.2531	0.4178	0.0000																																																																				
	<i>K</i>	<i>Ti</i>	<i>P</i>	<i>Mn</i>	<i>Sb</i>																																																																				
<i>K</i> ...	0.0000	0.1534	0.1248	0.2946	0.2699																																																																				
<i>Ti</i> ...	0.1534	0.0000	0.1526	0.2830	0.3213																																																																				
<i>P</i> ...	0.1248	0.1526	0.0000	0.2991	0.2581																																																																				
<i>Mn</i> ...	0.2946	0.2830	0.2991	0.0000	0.4053																																																																				
<i>Sb</i> ...	0.2699	0.3213	0.2581	0.4053	0.0000																																																																				
<p>Full composition, transformed CA ($\alpha = 0.001$)</p> <table border="1"> <thead> <tr> <th></th> <th><i>K</i></th> <th><i>Ti</i></th> <th><i>P</i></th> <th><i>Mn</i></th> <th><i>Sb</i></th> </tr> </thead> <tbody> <tr> <td><i>K</i> ...</td> <td>0.0000</td> <td>0.1530</td> <td>0.1246</td> <td>0.2907</td> <td>0.2703</td> </tr> <tr> <td><i>Ti</i> ...</td> <td>0.1530</td> <td>0.0000</td> <td>0.1526</td> <td>0.2816</td> <td>0.3218</td> </tr> <tr> <td><i>P</i> ...</td> <td>0.1246</td> <td>0.1526</td> <td>0.0000</td> <td>0.2985</td> <td>0.2574</td> </tr> <tr> <td><i>Mn</i> ...</td> <td>0.2907</td> <td>0.2816</td> <td>0.2985</td> <td>0.0000</td> <td>0.4047</td> </tr> <tr> <td><i>Sb</i> ...</td> <td>0.2703</td> <td>0.3218</td> <td>0.2574</td> <td>0.4047</td> <td>0.0000</td> </tr> </tbody> </table>		<i>K</i>	<i>Ti</i>	<i>P</i>	<i>Mn</i>	<i>Sb</i>	<i>K</i> ...	0.0000	0.1530	0.1246	0.2907	0.2703	<i>Ti</i> ...	0.1530	0.0000	0.1526	0.2816	0.3218	<i>P</i> ...	0.1246	0.1526	0.0000	0.2985	0.2574	<i>Mn</i> ...	0.2907	0.2816	0.2985	0.0000	0.4047	<i>Sb</i> ...	0.2703	0.3218	0.2574	0.4047	0.0000	<p>Two part subcomps, transformed CA ($\alpha = 0.001$)</p> <table border="1"> <thead> <tr> <th></th> <th><i>K</i></th> <th><i>Ti</i></th> <th><i>P</i></th> <th><i>Mn</i></th> <th><i>Sb</i></th> </tr> </thead> <tbody> <tr> <td><i>K</i> ...</td> <td>0.0000</td> <td>0.1530</td> <td>0.1246</td> <td>0.2906</td> <td>0.2703</td> </tr> <tr> <td><i>Ti</i> ...</td> <td>0.1530</td> <td>0.0000</td> <td>0.1526</td> <td>0.2815</td> <td>0.3218</td> </tr> <tr> <td><i>P</i> ...</td> <td>0.1246</td> <td>0.1526</td> <td>0.0000</td> <td>0.2985</td> <td>0.2575</td> </tr> <tr> <td><i>Mn</i> ...</td> <td>0.2906</td> <td>0.2815</td> <td>0.2985</td> <td>0.0000</td> <td>0.4046</td> </tr> <tr> <td><i>Sb</i> ...</td> <td>0.2703</td> <td>0.3218</td> <td>0.2575</td> <td>0.4046</td> <td>0.0000</td> </tr> </tbody> </table> <p>Max abs diff = 0.000059 Stress = 0.000108</p>		<i>K</i>	<i>Ti</i>	<i>P</i>	<i>Mn</i>	<i>Sb</i>	<i>K</i> ...	0.0000	0.1530	0.1246	0.2906	0.2703	<i>Ti</i> ...	0.1530	0.0000	0.1526	0.2815	0.3218	<i>P</i> ...	0.1246	0.1526	0.0000	0.2985	0.2575	<i>Mn</i> ...	0.2906	0.2815	0.2985	0.0000	0.4046	<i>Sb</i> ...	0.2703	0.3218	0.2575	0.4046	0.0000
	<i>K</i>	<i>Ti</i>	<i>P</i>	<i>Mn</i>	<i>Sb</i>																																																																				
<i>K</i> ...	0.0000	0.1530	0.1246	0.2907	0.2703																																																																				
<i>Ti</i> ...	0.1530	0.0000	0.1526	0.2816	0.3218																																																																				
<i>P</i> ...	0.1246	0.1526	0.0000	0.2985	0.2574																																																																				
<i>Mn</i> ...	0.2907	0.2816	0.2985	0.0000	0.4047																																																																				
<i>Sb</i> ...	0.2703	0.3218	0.2574	0.4047	0.0000																																																																				
	<i>K</i>	<i>Ti</i>	<i>P</i>	<i>Mn</i>	<i>Sb</i>																																																																				
<i>K</i> ...	0.0000	0.1530	0.1246	0.2906	0.2703																																																																				
<i>Ti</i> ...	0.1530	0.0000	0.1526	0.2815	0.3218																																																																				
<i>P</i> ...	0.1246	0.1526	0.0000	0.2985	0.2575																																																																				
<i>Mn</i> ...	0.2906	0.2815	0.2985	0.0000	0.4046																																																																				
<i>Sb</i> ...	0.2703	0.3218	0.2575	0.4046	0.0000																																																																				

This illustrates again, but in a way more directly related to the notion of coherence, how CA comes closer and closer to coherence as the power parameter decreases. In addition, this shows what might have been suspected from the start: subcompositions of size 2 appear to be the worst-case scenario for deviation from coherence, at least in this application, since they are the most affected by reclosure. In other words, if we can bring the stress of subcompositions of size 2 acceptably low enough, then we are guaranteeing that all other subcompositions will be at least less incoherent on average. This is a very convenient result, but we should stress that it is an empirical observation in this particular case and not a general result.

All the pairwise distances from two-part subcompositions can be placed in a square distance matrix, which can then be compared directly with the pairwise distances in the full composition using the same stress measure (4). Table 3 gives three examples, showing just the last five out of the eleven components, for $\alpha = 1, 0.25$ and 0.001 ; the distances on the left are computed in the full composition, and the distances on the right are those obtained by forming each subcomposition corresponding

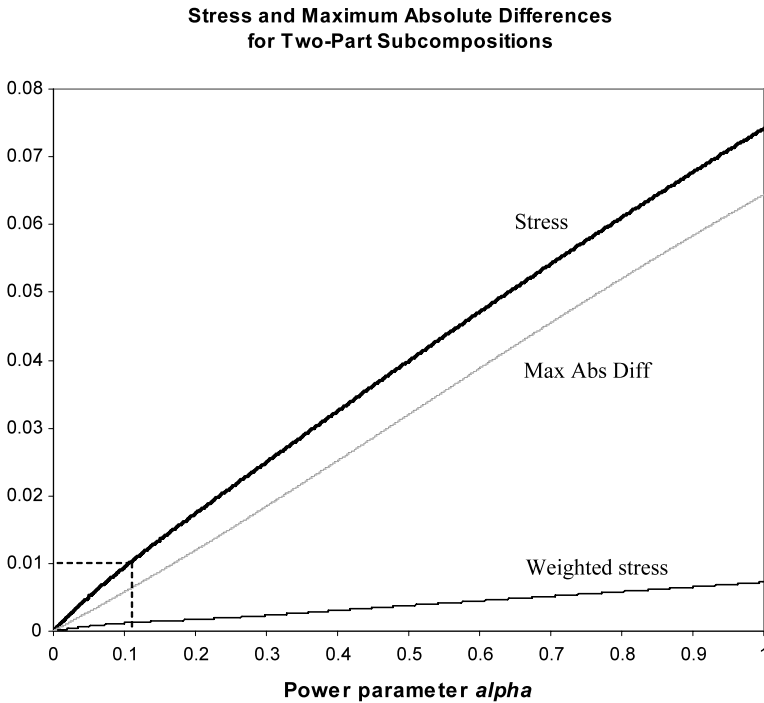


Fig. 3 Stress between chi-square distances calculated in two-part subcompositions and the corresponding chi-square distances in the full composition for the Roman glass cup data, for power transformations $\alpha = 1, 0.999, 0.998, \dots, 0.001$. The power parameter corresponding to a stress of 0.01 (1%) has value 0.106, as indicated. The weighted stress on the vertical axis takes into account the average level of the components, discussed in the text

to the row-column pairs. Again, we witness the convergence as α decreases. Figure 4 shows a continuous version of the stress as a function of α . If a 1% level of stress were acceptable as being a measure of incoherence that was low enough, then the power transform with $\alpha = 0.106$ would be appropriate.

4 To Weight or Not to Weight

So far, we have treated each component equally, as is general practice in compositional data analysis, even in the paper on log-ratio biplots by Aitchison and Greenacre (2002). However, Greenacre and Lewi (2009) have brought to attention the necessity for and benefits of weighting the components when doing LRA. Convenient weights are the so-called masses in CA, namely the marginal averages of the components, and thus a rare component with low average value in the dataset is downweighted compared to the abundant components. Although this appears to be an issue only when analyzing the data (e.g., visualizing the compositional distances in a subspace of reduced dimension), it is also an issue when measuring stress, as we now demonstrate.

We have just come to the conclusion that a power-transformed CA of the Baxter et al. (1990) data with power parameter $\alpha = 0.106$ would reduce the incoherence of CA to 1%; now we will study this 1% lack of coherence in further detail. The stress

measure is a sum of positive numbers for each cell in an 11 by 11 table; Figure 4 shows a graphical display where the contribution of each of these values is indicated by the area of a circle. It is immediately obvious that this incoherence, albeit small, is almost totally due to the oxide of the element Mn (manganese). In previous analyses of these data by Greenacre and Lewi (2009), Mn has already been singled out as a problem as it takes on only three small values (by weight): 0.03%, 0.02%, and 0.01% (i.e., 0.0003, 0.0002, and 0.0001 on a proportion scale), engendering large values on the ratio and log-ratio scale. Greenacre and Lewi (2009) proposed weighting the components in proportion to their marginal averages, which eliminates the influence of this rare component. Our stress measure of incoherence can also be easily modified to take the abundance of each component into account in the measure, in which case Mn would not feature so prominently. Then, the measure would be measuring incoherence weighted by the average level of each component, with incoherence in higher-abundance components being taken into account more than incoherence in rare components. This weighted stress measure is then

$$\text{weighted stress} = \sqrt{\frac{\sum \sum_{j < j'} c_j c_{j'} (d_{jj'} - \delta_{jj'})^2}{\sum \sum_{j < j'} c_j c_{j'} d_{jj'}^2}}, \quad (5)$$

where c_j denotes the weight of the j th component, usually taken to be equal to its marginal average proportion. The lower curve in Fig. 3 traces out weighted stress as a function of the power parameter; it is considerably lower than the unweighted curve at the top, and now even a regular, untransformed CA is seen to have less than 1% incoherence overall. Figure 5 shows the contribution-to-weighted-stress plot for a regular CA; Mn is no longer an important contributor, the highest contributions to incoherence coming from two distances involving calcium, Ca to Si (silica), and Ca to Na (sodium).

5 Comparison with Principal Component Analysis

As a comparison, we note how PCA, with or without standardization, fares on our measure of subcompositional incoherence for the present dataset. We used the Euclidean distance with and without standardization of the components. The weighted stress measures are very high (0.3442 (34.42%) and 0.1828 (18.28%), respectively); if one compares these values with those for CA shown in Fig. 3, one realizes how high these measures are and how far away from coherence PCA is. There is also a quirk in the two-part compositions in PCA due to the centering with respect to component means. Since the pair of closed values has the property $x_{ij'} = 1 - x_{ij}$, the two centered values have the property $y_{ij'} = -y_{ij}$ and thus also have the same variance (e.g., s_j). It can be easily deduced that the unstandardized Euclidean distance between components j and j' in the two-part composition is a constant multiple of the standard deviation $2\sqrt{n-1}s_j$, while the standardized Euclidean distance is a constant $2\sqrt{n-1}$ for all two-part subcompositions. The correlation between the components of any two-part subcomposition is -1 , independent of the data. It seems that PCA on unstandardized or standardized data is out of the question for compositional data analysis if one places importance on the principle of subcompositional coherence.

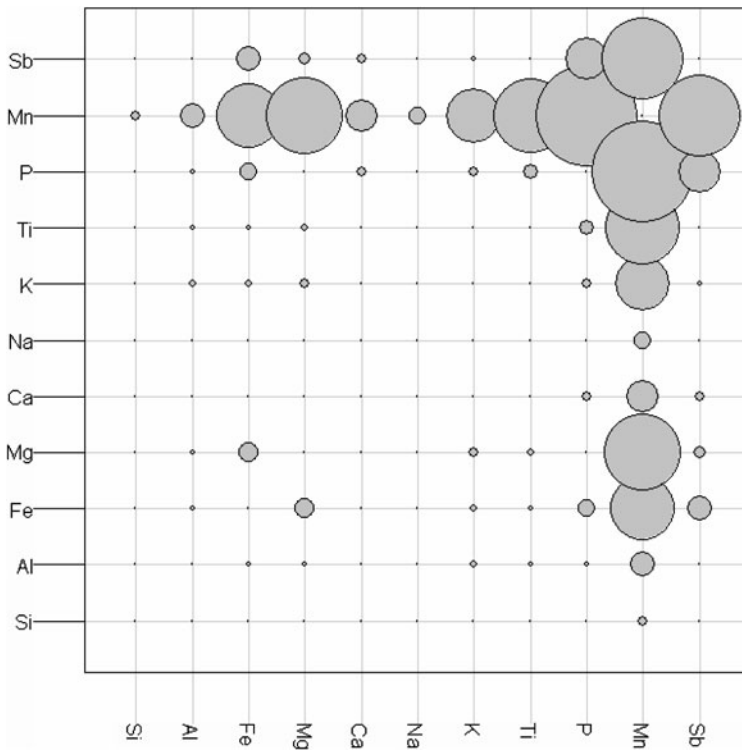


Fig. 4 Values that constitute the stress measure for measuring incoherence in the CA with power transformation $\alpha = 0.106$. The area of the circles is proportional to the contribution to stress (function `table.dist` in the R package `ade4` by Thioulouse and Dray 2007). The lack of coherence is concentrated almost entirely in the Mn (manganese) oxide component. Notice that the diagonal of the symmetric table underlying this graphic, which contains zeros, runs from bottom left to top right

In this eleven-part compositional dataset, the performance of ten-part subcompositions should be the most favorable for evaluating PCA, but the incoherence is large even for these. The average stress for all ten-part subcompositions was calculated as 0.1371 (13.71%) for unstandardized PCA and 0.0425 (4.25%) for standardized PCA. Average weighted stresses are 0.1906 (19.06%) and 0.0940 (9.40%), respectively. Compare these to regular (untransformed) CA, which, for the eleven ten-part subcompositions of these data, has average unweighted and weighted stresses of 0.0029 (0.29%) and 0.0021 (0.21%), respectively.

6 Discussion and Conclusions

The main aim of this paper is to propose a measure of subcompositional incoherence (i.e., the lack of subcompositional coherence), defined as the stress between the inter-component distance matrix calculated using the full composition and the matrix of pairwise component distances computed from all the two-part subcompositions. Having such a measure allows different multivariate approaches to compositional

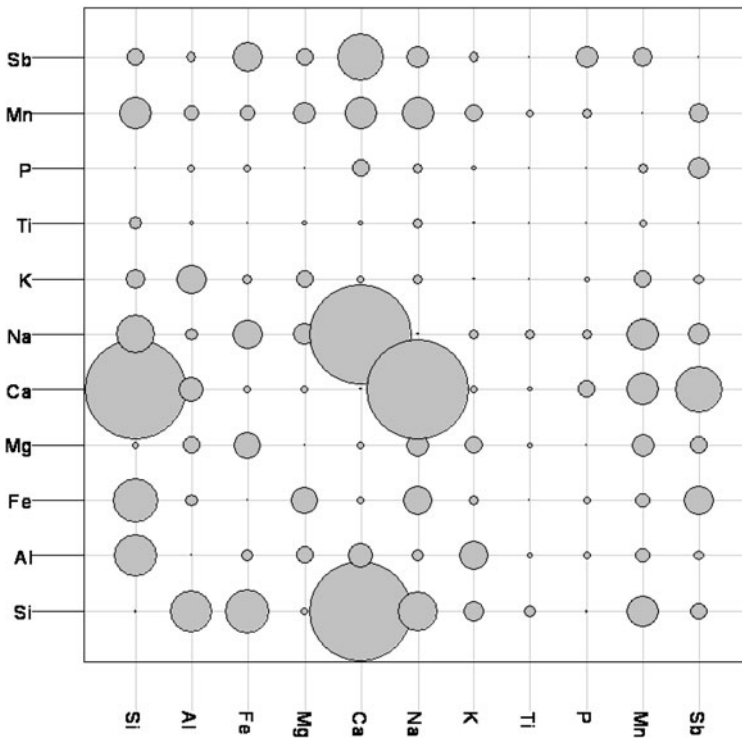


Fig. 5 Values that constitute the weighted stress measure for measuring incoherence in a regular CA. The area of the circles is proportional to the contribution to weighted stress

data analysis that rely on distance measures to be evaluated in terms of their closeness to subcompositional coherence. Our approach assumes that the two-part subcompositions are the worst case for measuring subcompositional incoherence; this has been empirically demonstrated in a specific dataset and for a specific distance function, but the general result remains an open problem.

From the results of the previous section and from the discussion of Greenacre and Lewi (2009), we strongly advise to include the weighting of the components proportional to their average value in the dataset. We have seen in the example of the Roman glass compositional dataset that regular CA, for example, owes most of its incoherence (when measured without weights) to one problematic component that is rare. Weighting eliminates this problem, and then we see that CA is, in fact, only slightly incoherent.

Application of this idea to a wider spectrum of compositional datasets will show to what extent CA, with or without power transformations, can be used as an alternative to LRA. Greenacre and Lewi (2009) have already showed that a regular CA of the Roman glass dataset and a weighted LRA gave almost the same two-dimensional biplot, so the fact that CA is almost coherent (using weighted stress) fits in with this result. It is already known that CA gives similar results to association modeling contingency tables when the variance in the data is low (Cuadras et al. 2006) and that

weighted LRA has strong theoretical similarities to association modeling (Greenacre and Lewi 2009). Here, low variance means that the observed data are close to their expected values based on the table margins. It follows that CA and weighted LRA will give similar results in such a low-variance situation where the samples are very similar to one another, which is the case in the present example and often the case in archaeological data. But when the variance is high, which is often the case for geological and geochemical data where there can be many data zeros, the power family of CAs will show greater differences across the range of power transformations.

CA has the obvious benefit of being able to cope with data zeros, and we have shown that we can reduce incoherence by applying nonzero power transformations; therefore, this holds promise for the analysis of compositional data with zeros, which is a perennial problem with the log-ratio transformation (Martín-Fernández et al. 2003). It remains to be shown whether we can use a power transformation to come acceptably close to coherence while being able to analyze zeros as actual zeros, without having to resort to replacing them artificially with some small positive number. However, at least a tool is now available to measure subcompositional incoherence in order to enable judgment of how close we are to coherence in different situations.

Acknowledgements This research was supported by the Fundación BBVA in Madrid, Spain. Partial support by the Spanish Ministry of Science, grants MTM2008-00642 and MTM2009-09063, is also hereby acknowledged. The paper has benefited considerably from the very careful reading and comments by a reviewer.

References

- Aitchison J (1983) Principal component analysis of compositional data. *Biometrika* 70:57–65
- Aitchison J (1986) The statistical analysis of compositional data. Chapman & Hall, London (reprinted in 2003 with additional material by Blackburn Press)
- Aitchison J (1990) Relative variation diagrams for describing patterns of compositional variability. *Math Geol* 22:487–511
- Aitchison J, Greenacre M (2002) Biplots for compositional data. *Appl Stat* 51:375–392
- Baxter MJ, Cool HEM, Heyworth MP (1990) Principal component and correspondence analysis of compositional data: some similarities. *J Appl Stat* 17:229–235
- Borg I, Groenen P (2005) Modern multidimensional scaling, 2nd edn. Springer, New York
- Box GEP, Cox DR (1964) An analysis of transformations (with discussion). *J R Stat Soc B* 35:473–479
- Chayes F (1960) On correlation between variables of constant sum. *J Geophys Res* 65:4185–4193
- Cuadras C, Cuadras D, Greenacre M (2006) A comparison of methods for analyzing contingency tables. *Commun Stat, Simul Comput* 35:447–459
- Greenacre M (1984) Theory and applications of correspondence analysis. Academic Press, London
- Greenacre M (2007) Correspondence analysis in practice, 2nd edn. Chapman & Hall/CRC Press, London
- Greenacre M (2008) La práctica del análisis de correspondencias. Fundación BBVA, Madrid
- Greenacre M (2009) Power transformations in correspondence analysis. *Comput Stat Data Anal* 53:3107–3116
- Greenacre M (2010) Log-ratio analysis is a limiting case of correspondence analysis. *Math Geosci* 42:129–134
- Greenacre M, Lewi P (2009) Distributional equivalence and subcompositional coherence in the analysis of compositional data, contingency tables and ratio-scale measurements. *J Classif* 26:29–54
- Martín-Fernández JA, Barceló-Vidal C, Pawłowsky-Glahn V (2003) Dealing with zeros and missing values in compositional data sets. *Math Geol* 35:253–278
- Pawłowsky-Glahn V, Egozcue J, Tolosana-Delgado R (2007) Lecture notes on compositional data analysis. <http://dugi-oc.udg.edu/handle/10256/297>. Accessed 15 May 2011
- Thioulouse J, Dray S (2007) Interactive multivariate data analysis in R with the ade4 and ade4TkGUI packages. *J Stat Soft.* <http://www.jstatsoft.org/v22/i05/paper>. Accessed 15 May 2011