

# **An impact of MHD and radiation on fow of Jefrey fuid with carbon nanotubes over a stretching/shrinking sheet with Navier's slip**

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## **Abstract**

This article focuses on MHD fow and heat transfer of Jefrey fuid due to a stretching/shrinking surface with carbon nanotubes, considering the efects of thermal radiation, heat source/sink parameters, and Navier's slip. Generally, solids ofer higher thermal conductivity than fluids. To offer higher thermal conductivity, a new type of nanofluid is formed by suspending two types of carbon nanotubes (CNTs), i.e. single-wall carbon nanotubes (SWCNTs) and multi-wall carbon nanotubes (MWCNTs), which act as nanoparticles, into the base fuid, water. It is intended to enhance the thermal conductivity and mechanical properties of the base fuid. The structure of the problem is an equation of momentum and temperature, which are then converted into a set of ODEs to imitate the MHD fow of carbon nanotubes. The magnetic parameter, radiation parameter, and Navier slip efect signifcantly afect the structure of the solution to the problem. Carbon nanotubes act as nanoparticles that enhance the heat performance and mechanical properties more than the base fuid, so they have many applications in electronics and transportation. The velocity and temperature profiles, skin friction coefficient, and Nusselt number are observed and discussed through graphs. The results reveal that for stretching case, velocity profle increases with increasing the magnetic feld, while the opposite trend observed in shrinking case. We notice that the SWCNT Nanofuids are better nanofuids than the MWCNT Nanofuids. We study from these fnal results that the usage of CNTs in most cancerous therapies can be more useful than all sorts of nanoparticles.

**Keywords** CNTs · MHD · Heat source/sink · Navier slip · Jefrey fuid · Nusselt number

#### **List of symbols**





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 $\Gamma_1$ ,  $\Gamma_2$  Material parameters of Jeffrey fluid

#### **Subscripts**





## **Introduction**

The mixture of nanoparticle in a base fuid is named as nanofluid which works efficiently in cooling the system which is in high temperature range and has many thermal applications. Introduction of the MHD force will affect more on the flow due to development of Lorentz force. Magnetohydrodynamic (MHD) flow plays an important part in the production of petroleum products and processes of metallurgy. It is to note that the fnal product that is formed is dependent on the rate of cooling followed by these processes. In order to separate the metallic materials from the nonmetallic materials, this feld of magnetism is used to refne the molten metals. The carbon nanotubes (CNTs) based nanofuid as a heat transfer system. CNTs are a well-known allotrope of family of fullerene exhibiting long and hollow chemical structure compromising of graphene sheets. In a broader sense, two kinds of CNTs exist viz., single and multi-walled. The thermophysical properties of CNTs are subservient along with graphene sheets getting aligned in a sequential manner within the tube which results in this kind of materials to execute properties of metal or semiconductor. Ebaid and Sharif [\[1](#page-9-0)] investigated MHD transfer of heat and fow of CNTs-suspended nanofuids over stretching sheet (linear). The flow of MHD in such a particular case was first explored by Sarpakaya [[2\]](#page-9-1) and Mahabaleshwar [[3–](#page-9-2)[5\]](#page-10-0). Tiwari et al*.* [[6\]](#page-10-1) investigated the Marangoni convection MHD fow of CNTs through a porous medium with radiation.

Stretching sheet problems are very applicable in many industrial processes such as electronic cooling process, heat exchange between devices, and cooling of engines. Because of this reason, many researchers show an interest on stretching sheet problems. Crane [[7\]](#page-10-2) and Sakiadis [\[8](#page-10-3)] are pioneers in the investigation of stretching sheet problems. Hayat et al. [\[9\]](#page-10-4) examined stagnation point of viscous nanofuid over a nonlinear stretching surface with variable thickness.

Hamad [[10\]](#page-10-5) and Fang and Zhang [[11\]](#page-10-6) examine the MHD flow due to shrinking sheet and shrinking sheet, respectively. Vinay Kumar et al*.* [[12\]](#page-10-7) have investigated the impact of MHD and mass transpiration on the slip flow. Sneha et al. [\[13\]](#page-10-8) have examined the stagnation point flow over a Jeffrey fluid flow through a stretching/shrinking sheet. Turkyilmazoglu et al.[\[14\]](#page-10-9) examined the MHD flow, heat and mass transfer of viscoelastic fluid with slip over the stretching surface and got the multiple solutions. Recently, Reddy et al. [[15\]](#page-10-10) examine the numerical analysis of the MHD fow of CNT nanofuid over a nonlinear inclined stretching/shrinking sheet with heat generation and viscous dissipation. Norzawary et al.[\[16\]](#page-10-11) examined on the stagnation point fow in CNTs with suction/injection impacts over a stretching/shrinking sheet.

Mahabaleshwar et al.[\[17](#page-10-12)] made the article on the MHD flow with carbon nanotubes by considering the effect of mass transpiration and radiation on it. Mahabaleshwar et al.  $[18]$  $[18]$  $[18]$  investigates the MHD flow and mass transfer due to porous media. Turkyilmazoglu [[19\]](#page-10-14) studied on exact solution for fow of Jefrey fuid. The Novelty of the present research is to examine the MHD fow and heat transfer of Jefrey fuid due to a stretching/shrinking surface with CNTs considering the efects of thermal radiation and Navier's slip. And the motivation is to add the efects CNTs and slips to previous works of momentum and energy with constant and linear wall temperature. Secondly, to provide an analytic solution of the resulting nonlinear system is novel. Moreover, the infuence for various physical features as magnetic parameter, mass transpiration, radiation and Prandtl number parameter are presented on the feld of fow and analysed thereafter. Investigate the important physical parameters Nusselt number and skin friction (Fig. [1\)](#page-1-0).



<span id="page-1-0"></span>**Fig. 1** Schematic diagram of the fow problem

#### **Physical model and explanations**

The steady MHD flow and heat transfer of Jeffrey fluid with CNTs due to a stretching/shrinking surface moving with deforming wall velocity  $u_w(x)$  is examined and the phenomena of heat transfer with thermal radiation are investigated. The magnetic field of strength  $B_0$  is applied perpendicular to the fuid fow. The fuid fow is along *x*-axis and *y*-axis is perpendicular to it. The sheet is stretched/shrinked with the velocity which is proportional to the distance from the origin *c*. The momentum and temperature governing equations can be modelled as Saif et al. [[20](#page-10-15)], Rao et al. [[21](#page-10-16)], and Maranna et al. [\[22\]](#page-10-17).

$$
\frac{\partial u}{\partial x} + \frac{\partial u}{\partial y} = 0,\tag{1}
$$

$$
\rho_{n\text{f}}\left(u\frac{\partial u}{\partial x} + v\frac{\partial u}{\partial y}\right) = \rho_{n\text{f}}u_{\text{e}}\frac{\partial u_{\text{e}}}{\partial x} + \frac{\mu_{\text{f}}}{1+\Gamma_{1}}
$$
\n
$$
\left[\frac{\partial^{2} u}{\partial y^{2}} + \Gamma_{2}\left(u\frac{\partial^{3} u}{\partial x \partial y^{2}} - \frac{\partial u}{\partial x}\frac{\partial^{2} u}{\partial y^{2}} + \frac{\partial u}{\partial y}\frac{\partial^{2} u}{\partial x \partial y} + v\frac{\partial^{3} u}{\partial y^{3}}\right)\right]
$$
\n
$$
-\frac{\sigma_{n\text{f}}B_{0}^{2}}{\rho_{n\text{f}}}(u - u_{\text{e}})
$$
\n(2)

$$
u\frac{\partial T}{\partial x} + v\frac{\partial T}{\partial y} = \frac{\kappa_{\rm nf}}{\left(\rho c_p\right)_{\rm nf}}\frac{\partial^2 T}{\partial y^2} - \frac{1}{\left(\rho c_p\right)_{\rm nf}}\frac{\partial q_r}{\partial y},\tag{3}
$$

with B.Cs as follows:

$$
u = dcx + A\frac{\partial u}{\partial y}, \quad v = v_w, \quad T = T_w(x) \quad y = 0
$$
  

$$
u \to u_e(x) = ax, \quad \frac{\partial u}{\partial y} \to 0, \quad T \to T_\infty \quad y \to \infty
$$
 (4)

here,  $u_e(x) = ax$  is the potential flow and wall temperature field  $T_w(x)$  is either kept at constant  $T_w$  or linearly proportional with *x* as follows:  $T_w(x) = T_w + bx$ ,  $v_w = -\left(\frac{cv_f}{(1+\omega_1)}\right)$  $\int_0^{\frac{1}{2}} S$ is wall transpiration, where  $v_w < 0$  for suction and  $v_w > 0$ for injection.  $\Gamma_1$  and  $\Gamma_2$  are material parameters of Jeffrey fluid.

The suitable similarity transformations [[19](#page-10-14)] are as follows:

$$
\eta = \left(\frac{c(1+\Gamma_1)}{v_f}\right)^{\frac{1}{2}} y, \ u = cx\frac{\partial f}{\partial \eta},
$$
  

$$
v = -\left(\frac{cv_f}{(1+\Gamma_1)}\right)^{\frac{1}{2}} f(\eta), \ \theta(\eta) = \frac{T-T_{\infty}}{T_w - T_{\infty}}
$$
\n(5a)

The radiative heat flux  $q_r$  is obtained by using the approximation of Rosseland for radiation as in [\[23–](#page-10-18)[26](#page-10-19)],

$$
q_{\rm r} = -\frac{4\sigma^*}{3k^*} \frac{\partial T^4}{\partial y} \tag{5b}
$$

T is implicit that the temperature varies within the flow, where the term  $T^4$  is the linear function of the temperature. Therefore, on using Taylor series expansion to the term  $T^4$  about  $T_{\infty}$  and on ignoring the higher order terms to get,

$$
T^4 \cong 4T_{\infty}^3 T - 3T_{\infty}^4
$$

<span id="page-2-3"></span>Then, Eq.  $(3)$  $(3)$  reduces to

$$
u\frac{\partial T}{\partial x} + v\frac{\partial T}{\partial y} = \frac{\kappa_{\rm nf}}{\left(\rho c_{\rm p}\right)_{\rm nf}}\frac{\partial^2 T}{\partial y^2} - \frac{1}{\left(\rho c_{\rm p}\right)_{\rm nf}}\frac{16\sigma^* T_{\infty}^3}{3k^*} \frac{\partial^2 T}{\partial y^2},\quad (5c)
$$

<span id="page-2-2"></span>On the implementation of similarity transformations (5a) and Eq.  $(5b)$  $(5b)$  to governing Eqs.  $(2)$  $(2)$  and  $(3)$  $(3)$ , we obtain,

$$
\frac{C_2}{C_1} \frac{\partial^3 f}{\partial \eta^3} + f(\eta) \frac{\partial^2 f}{\partial \eta^2} - \left(\frac{\partial f}{\partial \eta}\right)^2 + \beta \frac{C_2}{C_1} \left[ \left(\frac{\partial^2 f}{\partial \eta^2}\right)^2 - f(\eta) \frac{\partial^4 f}{\partial \eta^4} \right] - M \left(\frac{\partial f}{\partial \eta} - \lambda\right) \frac{C_3}{C_1} + \lambda^2 = 0,
$$
\n(6)

<span id="page-2-4"></span><span id="page-2-0"></span>
$$
(C_5 + N_{\rm R})\frac{\partial^2 \theta}{\partial \eta^2} + \Pr C_4 f \frac{\partial \theta}{\partial \eta} = 0, \text{ (for } T_{\rm w}(x) = T_{\rm w}) \tag{7}
$$

$$
(C_5 + N_{\rm R})\frac{\partial^2 \theta}{\partial \eta^2} + \Pr C_4 \left( f \frac{\partial \theta}{\partial \eta} - \frac{\partial f}{\partial \eta} \theta \right) = 0, \quad \text{(for } T_{\rm w}(x) = T_{\rm w} + bx)
$$
\n(8)

also B.Cs are as follows:

$$
f(\eta) = V_c, \frac{\partial f}{\partial \eta} = d + L_1 \frac{\partial^2 f}{\partial \eta^2}, \ \theta(\eta) = 1 \text{ at } \eta = 0
$$
  

$$
\frac{\partial f}{\partial \eta} = \lambda, \qquad \frac{\partial^2 f}{\partial \eta^2} = 0, \qquad \theta(\eta) = 0 \text{ as } \eta \to \infty
$$
 (9)

here,  $\beta = \Gamma_2 c$  is Deborah number,  $\lambda = \frac{a}{c}$  is stagnation/ strength parameter,  $M = \frac{\sigma_f B_0^2}{\rho_f c}$  is magnetic parameter,  $C_1 = \frac{\rho_{\text{nl}}}{\rho_f c}$ and  $C_2 = \frac{\mu_{\text{nf}}}{\mu_f}, C_3 = \frac{\sigma_{\text{nf}}}{\sigma_f}, C_4 = \frac{(\rho c_p)_{\text{nf}}}{(\rho c_p)_f}, C_5 = \frac{\kappa_{\text{nf}}}{\kappa_f}. P_r = \frac{\nu_f}{\alpha_f}$  is Prandtl number.  $V_c$  is mass transpiration parameter, for suc-

<span id="page-2-1"></span>tion case  $V_c > 0$  and for injection case  $V_c < 0$ , *d* is stretching/ shrinking parameter, where  $d > 0$  for stretching and  $d < 0$ for shrinking, respectively.  $L_1 = A \left( \frac{c(1+\Gamma_1)}{v_c} \right)$  $V_1$  $\int_{0}^{\frac{1}{2}}$  is first order slip. And nanofuid quantities are given by,

Here,  $\varphi$  is solid volume fraction of nanofluid. The physical quantities of interest, the skin friction coefficient and local Nusselt number, respectively, given by,

$$
C_{\rm f} = \frac{v_f}{a^2 x^2} \left(\frac{\partial u}{\partial y}\right)_{y=0} = \frac{c}{a^2 x} \left(c v_{\rm f} (1 + \Gamma_1)\right)^{\frac{1}{2}} \left(\frac{\partial^2 f}{\partial \eta^2}\right)_{\eta=0},
$$
  

$$
Nu_x = -x \left(\frac{c(1 + \Gamma_1)}{v_{\rm f}}\right)^{\frac{1}{2}} \left(\frac{\partial \theta}{\partial \eta}\right)_{\eta=0}
$$
(10)

Additionally the skin friction and Nusselt number can be determined from  $-\left(\frac{\partial^2 f}{\partial \eta^2}\right)^2$  $_{\eta=0}$  and  $-\left(\frac{\partial\theta}{\partial\eta}\right)_{\eta=0}$ 

#### **Analysis of momentum equation**

The present work is related to classical Crane's [[10\]](#page-10-5) solution for the simple flow, that is for  $\lambda = S = L_1 = 0$  and  $d = 1$ . For the general case, the solution form of momentum equation is as below and to get the physical solution there is an additional constraint as  $\delta > 0$ ,

$$
f(\eta) = V_c + \lambda \eta + \frac{d - \lambda}{\delta \left(1 + L_1 \delta\right)} \left[1 - \exp(-\delta \eta)\right] \tag{11}
$$

Applying of Eq. ([11\)](#page-3-0) into Eq. ([6\)](#page-2-3) gives,  $C_1$ ,  $C_2$ ,  $C_3$ ,  $C_4$ ,  $C_5$ 

$$
(d - \lambda) \left\{ \left( 1 + L_1 \delta \right) \left[ -\frac{C_3}{C_1} M + \delta \left( \frac{C_2}{C_1} \delta - V_c + \frac{C_2}{C_1} \beta S \delta^2 \right) \right] + d \left( -1 + \frac{C_2}{C_1} \beta \delta^2 \right) - \lambda - 2\lambda L_1 \delta - \frac{C_2}{C_1} \beta \lambda \delta^2 + \eta \lambda \delta \left( 1 + L_1 \delta \right) \left( -1 + \frac{C_2}{C_1} \beta \delta^2 \right) \right\} = 0
$$
\n(12)

For the special case  $\lambda = 0$ , Eq. [\(12\)](#page-3-1) got the form as follows:

$$
d\left(-1+\frac{C_2}{C_1}\beta\delta^2\right)(1+L_1\delta) + \left[-\frac{C_3}{C_1}M + \delta\left(\frac{C_2}{C_1}\delta - V_c + \frac{C_2}{C_1}\beta S\delta^2\right)\right] = 0
$$
 (13)

#### **Analysis of heat transfer**

These momentum and temperature solutions got match with the examined work of Turkyilmazoglu [[3,](#page-9-2) [6\]](#page-10-1). In the case of linear wall concentration, Eqs.  $(8)$  $(8)$  and  $(11)$  $(11)$  can lead us to obtain an additional solution by taking the assumption,

$$
\theta(\eta) = \exp(-\delta \eta) \tag{14}
$$

Applying Eq.  $(11)$  $(11)$  and  $(14)$  $(14)$  in Eq.  $(8)$  $(8)$  will imply,

$$
C_4 \Pr{d + (1 + L_1 \delta) \delta \left[ C_4 V_c \Pr{-(C_5 + N_R) \delta} \right]} = 0, \tag{15}
$$

Equation  $(13)$  $(13)$  and  $(15)$  $(15)$  gives the relations,

$$
\delta = \sqrt{\frac{(C_5 + N_{\rm R}) - \Pr \frac{C_4 C_2}{C_1} \pm \sqrt{\left((C_5 + N_{\rm R}) - \Pr \frac{C_4 C_2}{C_1}\right)^2 + 4 \Pr \beta \frac{C_2 C_3 C_4}{C_1^2} (C_5 + N_{\rm R})}}{2 \beta \frac{C_2}{C_1} (C_5 + N_{\rm R})}},
$$
\n(16)

and

<span id="page-3-0"></span>
$$
S = -\frac{d}{\delta \left(1 + L_1 \delta\right)} + \frac{\delta \left(C_5 + N_R\right)}{C_4 \text{ Pr}} \tag{17}
$$

Here,  $\delta$  and  $S$  is influenced by all used physical parameters.

And clearly for the above studied special case  $\lambda = 0$ , the velocity and concentration felds becomes,

$$
f(\eta) = V_c + \frac{d}{\delta \left(1 + L_1 \delta\right)} \left[1 - \exp(-\delta \eta)\right],\tag{18}
$$

and

<span id="page-3-2"></span>
$$
\phi(\eta) = \exp(-\delta \eta) \tag{19}
$$

Here,  $\delta > 0$  and *S* are given by Eqs. [\(16](#page-3-4)) and [\(17](#page-3-5)). For this case, skin friction and Sherwood numbers becomes,

<span id="page-3-6"></span>
$$
-\left(\frac{\partial^2 f}{\partial \eta^2}\right)_{\eta=0} = \frac{\delta d}{1 + L_1 \delta} \quad \text{and} \quad -\left(\frac{\partial \phi}{\partial \eta}\right)_{\eta=0} = \delta \tag{20}
$$

The Jefrey fuid will change to following *f* in case of  $\lambda = d = 1$ .

<span id="page-3-1"></span>
$$
f(\eta) = V_c + \eta,\tag{21}
$$

Temperature profle is given by,

$$
\theta(\eta) = \frac{\text{Erfc}\left[\sqrt{\frac{\text{Pr}C_4}{2(C_5 + N_R)}}(V_c + \eta)\right]}{\text{Erfc}\left[\sqrt{\frac{\text{Pr}C_4}{2(C_5 + N_R)}}V_c\right]},\tag{22}
$$

<span id="page-3-3"></span>The function *Erfc* denotes the complementary error function. From Eq. ([22](#page-3-6)) the Nusselt number will be obtained as follows:

$$
-\theta_{\eta}(0) = \frac{-\sqrt{\frac{2\Pr C_4}{\pi(C_5 + N_R)}} \exp\left[-\frac{Pr}{(C_5 + N_R)}\right]}{\text{Erfc}\left[\sqrt{\frac{\Pr C_4}{2(C_5 + N_R)}} V_c\right]}.
$$
(23)

# <span id="page-3-4"></span>**Result and discussion**

<span id="page-3-5"></span>The current work examine the MHD slip flow and heat transfer of Jefrey fuid due to a stretching/shrinking surface with CNTs considering the effects of thermal radiation and

<span id="page-4-0"></span>



Navier's slip. Further consider the effects of nanofluid by adding CNTs. This leads to offer higher thermal conductivity than base fuid and considered nanofuid is formed by

<span id="page-4-1"></span>**Fig. 2** The transverse velocity profile  $f(\eta)$  for various values of magnetic parameter *M* due to **a** stretching sheet and **b** shrinking sheet



Figures [2](#page-4-1) and [3,](#page-5-0) respectively, demonstrate the transverse and axial velocity for diferent entities of magnetic parameter *M*. In Fig. [2,](#page-4-1) Pr is fixed at 6.2 for base fluid water for SWCNTs and MWCNTS. It can be seen that velocity



<span id="page-5-0"></span>**Fig. 3** The axial velocity profle  $f_{\eta}(\eta)$ for various values of magnetic parameter *M* due to **a** stretching sheet and **b** shrinking sheet



profles increases with raise in *M* for stretching boundary*.* Similarly, we can also notice that velocity profles decreases with raise in *M* for shrinking boundary. Transverse velocity improves for water and kerosene oil nanofuid for SWCNT than MWCNT. If MWCNT nanofuids have higher efective velocities than the SWCNT-deferred nanofuids, and this might assist in industrial applications and medical benefts.

But axial velocity has no much diference for SWCNTs and MWCNTs. The impact of Radiation parameter  $N_R$  on axial velocity  $f_n(\eta)$  is examined in Fig. [4](#page-6-0). The axial velocity profle for SWCNTs and MWCNTs using base liquid water indicates a reduction for the behaviour of  $N_R$ . The consequence of increase of  $N_R$  on axial velocity will be, increased  $f_n(\eta)$ 

<span id="page-6-0"></span>

for stretching boundary and decreased  $f_{\eta}(\eta)$  for shrinking boundary.

Figure [5](#page-7-0)a depicts the skin friction  $C_f$  verses Prandtl number Pr for different values of *M*. The skin friction is more for SWCNTs than for MWCNTs and is negative. With the increase in *M*, the skin friction will decrease. In the similar way, the variation of skin friction  $C_f$  verses *M* for different values of *Pr* is as shown in Fig. [5b](#page-7-0). With the increase in Pr, the skin friction will decrease.  $C_f$  will increase with dense of volume fraction and decreases with Navier slip because of an increase in CNT density with solid volume fraction.

Figure [6](#page-8-0) portrays the effect of  $M$  and  $V_C$  on temperature profile  $\theta(\eta)$ . From Fig. [6](#page-8-0)a, the observations can be made

<span id="page-7-0"></span>



are, raise in *M* for both SWCNT and MWCNTs will result in decrease of thermal boundary layer thickness. For lower value of M, there is a temperature diference for SWCNTs and MWCNTs, further can be seen that on increasing *M*, the diference is negligible.

Figure [6](#page-8-0)b represents the impact of  $V_C$  on temperature profile  $\theta(\eta)$ . In both the SWCNT and MWCNT cases, temperature decreases with increase in  $V<sub>C</sub>$ . This is because of the way that fuid has a lower thermal conductivity for a comprehensive mass transpiration, which lessens

<span id="page-8-0"></span>



conduction and the thickness of the thermal boundary layer, lowering the temperature.

Figure [7](#page-9-3) depicts the effect of Pr on Nusselt number which plot versus mass transpiration  $V_C$ . It can be observed the improvement in the rate of heat transfer as *V<sub>C</sub>* increases. And also Nusselt number will be more for more value of Pr and the Nusselt number for SWCNTs is less than that for MWCNTs.

<span id="page-9-3"></span>



# **Conclusions**

The examination of MHD slip flow and heat transfer of Jefrey fuid due to a stretching/shrinking surface with CNTs considering the efects of thermal radiation and Navier's slip will result in some observations. Further consider the effects of nanofluid by adding CNTs to offer higher thermal conductivity than base fuid. The governing partial diferential equations for momentum and energy are transformed into ordinary diferential equations using a similarity transformation. These equations are solved analytically. MWCNT suspended nanofuids have evolved faster velocities than SWCNT suspended nanofuids, indicating that they may be benefcial in a few applications. Primary research has shown that MWCNT nanoparticles can reach the tumour faster than SWCNT nanoparticles in the treatment of disorder. Magnetic parameter (*M*), radiation parameter  $(N_{\rm R})$ , and Navier slip  $(L_{\rm l})$  effect significantly on the structure of solution of the problem is discussed. And investigate the important physical parameters Nusselt number and skin friction.

- Velocity profles increases with increase in magnetic feld for stretching boundary and decreases with increase in magnetic feld for shrinking boundary.
- The axial velocity profile for SWCNTs and MWCNTs using base liquid water indicates a reduction for the behaviour of radiation parameter.
- Increase of radiation parameter on axial velocity will results in, axial velocity increased for stretching boundary and decreased for shrinking boundary.
- The skin friction is more for SWCNTs than for MWCNTs and is negative.
- Increase of magnetic field or Prandtl number will decrease the skin friction.
- In both the SWCNT and MWCNT cases, temperature decreases with increase in mass transpiration.
- The rate of heat transfer will improve as mass transpiration increases. And also Nusselt number will be more for more value of Prandtl number.
- Nusselt number for SWCNTs is less than that for **MWCNTs**

A number of previous studies serve as the limiting example for this investigation.

(a)  $\lim_{M \to \infty}$  {Results of present works} $\rightarrow$  {Results of Turky- $M\rightarrow 0,$ <br>  $\phi \rightarrow 0,$  $q_\text{r}$  $\rightarrow$ 0,

ilmazoglu [[19](#page-10-14)]}.

Further extensions of the current work can be implemented incorporating new physical mechanisms, such as an external Newtonian/non-Newtonian fuid rheology with various parameter.

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