

# **Peristaltic transportation of hybrid nano‑blood through a ciliated micro‑vessel subject to heat source and Lorentz force**

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Received: 13 September 2022 / Accepted: 18 April 2023 / Published online: 29 May 2023 © Akadémiai Kiadó, Budapest, Hungary 2023

## **Abstract**

The center of interest of this research study is to unfold the phenomena in the electric double layer (EDL) adjacent to the indicted peristaltic wall and its impact on a peristaltic transport of ionized non-Newtonian blood (Jefrey liquid model) infused with hybridized copper and gold nanoparticles through a ciliated micro-vessel under the buoyancy and Lorentz forces' action. The energy equation is found with consideration of viscous dissipation and internal heat source impacts. The complicated normalized fow equations are abridged by adopting lubrication and Debye–Hückel linearization postulates. The homotopy perturbation approach is devoted to yield the optimal series solutions of the resulting equations. The amendment in the pertinent hemodynamical characteristics against the signifcant fow parameters is canvassed via plentiful graphical designs. Outcomes confess that a higher assisting the electric body force and thin EDL signifcantly opposes the blood fow nearby the ciliated micro-vessel wall. The heat exchange rate for hybrid nano-blood (26% for *Cu-Au*/blood) is greatly evaluated to nano-blood (20% for *Au*-blood and 11.4% for *Cu*-blood). The trapped bolus is expanded due to thinner EDL or longer cilia length. This simulation could help to design electro-osmotic blood pumps, diagnostic devices, pharmacological systems, etc.

**Keywords** EMHD · Peristalsis · Hybrid nano-blood · Jefrey fuid model · EDL · Ciliated micro-vessel



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*nf* Cu-blood nanoliquid *hnf Cu-Au*/blood hybrid nanoliquid

# **Introduction**

In the twenty-frst century, electro-magnetically supported transport has been gaining popularity in biomedical sciences, electromechanical systems, and bio-electrochemical engineering. It develops due to the interaction of electromagnetic felds and electrolytic fuids and generates interesting dynamical characteristics. When a charged solid surface gets into interaction with electrolyte or aqueous solutions, the positively indicted ions in the electrolytic fuids are attracted to it while the negatively charged ions repel it. As a response, an electric double layer (EDL) is produced across the charged solid area. The EDL is made up of two layers: a stationary stern layer generated near the charged solid surface and a difusive layer formed by moving positively charged ions. The positively charged EDL will migrate along imposed electric feld if it is employed parallel to the solid–fuid layer. Subsequently, the viscous drag causes the bulk liquid to be mobilized. An electro-osmotic fow (EOF) is an import of electrokinetic phenomena. It has potential biomedical and technological applications in micro- and nano-fuidic devices/systems, for example, electro-osmotic liquid pumps, pectoral fn-inspired wave energy conversion

devices, medication delivery pumps, cell culture, DNA testing, tissue scafolding, cooling chips, minimally invasive medical procedures, cellular micro-injection, bio-chip fabrication, photosynthetic-based fuel systems, corrosion mitigation, non-absorbent polymer injection systems, blood and urine diagnosis, and microbial fuel cells in carbon capture. Reuss [[1\]](#page-21-0) was the frst to explore and report the EOF in 1809. Wiedemann [[2\]](#page-21-1) later proposed a mathematical framework for EOF. Because of the rigorous requirements and benefts of EOF mechanisms, numerous scientists have concentrated their efforts over the EOF subject to various flow constraints and liquid models. The dual consequence of electro-osmosis and peristalsis is signifcant in several biological, industrial and engineering assessments. An analytical investigation to explore electro-osmosis phenomenon in biorheological micropolar fuid fow via sinusoidal wavy microchannels was presented by Chaube et al. [[3\]](#page-21-2). Their results exposed that the pumping characteristic can be altered by modifying externally imposed electric feld. Jayavel et al. [[4\]](#page-22-0) uncovered the electro-osmotic phenomena in the peristaltic fow of pseudo-plastic nanofuid via a micro-channel. In this research, it was recorded that the axial velocity of nanofuid declines near the left wall but a contrarily trend is witnessed in the zone close to the right wall for booster values of electro-osmotic term. A theoretical analysis for the EOF of double-layered fuids inside a fexible peristaltic tube was presented by Ali et al. [[5\]](#page-22-1). Their outcomes revealed that both trapping and refux can be circumvented by augmenting electrokinetic slip velocity. Noreen et al. [\[6](#page-22-2)] discovered the electro-osmotic phenomena in biofuid fow via a peristaltic micro-channel. They disclosed that the pressure gradient gets a declination for enhanced electro-osmotic parameter. For more recent researches, the readers are referred to Refs.  $[7-10]$  $[7-10]$ .

The study of mobility of ionized fluid under the interaction of electromagnetic felds is termed electro-magneto-hydrodynamic (EMHD). In this phenomenon, body forces on the stream are generated as a result of several interactions between magnetic feld, electrical charges in EDL, electric feld, and electrical currents. EMHD plays an incredible role in technological, biotechnological, biomedical, and bio-clinical felds such as biochemical engineering, developing micro-fabrication technology, targeting medications delivery system, and micro-electromechanical systems (MEMS). EMHD phenomena in peristaltic propagation have gained an amazing concern of researcher due to prospective submissions in bioengineering, bio-rheological, and medical domains. Noreen et al. [\[11](#page-22-5)] exposed the electro-osmosis regulated peristaltic propagation of magneto-nanofuid via a fexible micro-channel considering Joule heating. Their outputs revealed that the pressure gradient frstly attenuates and then amends with growing estimations of electro-osmotic

parameter or Hartmann number. The electro-magnetoosmosis in peristaltic propagation of dusty viscoelastic biofuids via micro-channel was inspected by Ramesh et al. [[12\]](#page-22-6). They disclosed that both magnetic field and electroosmotic parameter markedly suppress the velocity profle for both fuids and particles phase. Recently, Ramesh et al. [[13\]](#page-22-7) have disclosed the electro-osmotic events in the peristaltic fow of magneto-nanofuid with couple stress fuid model via a micro-channel considering the slip and convective wall conditions. Results of this paper claimed that entrapped bolus is expanded by mounted Hartmann number but compressed by elevated electro-osmotic parameter. The peristaltic transportation of a third-order non-Newtonian liquid via a micro-channel under joint action of magneto-hydrodynamics, and electro-osmosis has been examined by Tanveer et al. [[14](#page-22-8)]. The fuid velocity profle is signifcantly amended by the electro-osmotic term, while it is decremented in the core domain of the conduit but incremented nearby the walls due to an augmentation in magnetic feld. Additional related research works are found in Refs.  $[15-18]$  $[15-18]$  $[15-18]$ .

Researchers and modelers have recently shown an eagerness in peristaltic phenomena, which has a wide variety of deployments in the bio-mechanical, bioengineering, as well as biomedical felds. Continual contractions and relaxations of tube/channel/duct walls drive the fuid elements through it. This phenomenon is frequently realized in blood motion in arteries/vessels, saliva movement, spermatic material propagation and cerebrospinal fuids movement, food swallowing down the esophagus, chyme motion, and so on. This process has been smartly utilized in multi-ways, such as fnger and roller pumps, electro-pneumatics, bio-mimetic devices, embryo-cardiovascular pumps, corrosive fluid propelling, blood pump and oxygenator device, blood fltration, heart–lung machine, dialysis machine, ventilator machine, diabetic pumps delivery schemes of insulin, bio-mimetic capillary designs and glucose sensing. In order to understand the peristaltic action of non-Newtonian bio-rheological liquids, researchers have conducted several theoretical and computational investigations under a wide range of different assumptions. The peristaltic activity was initially examined by Latham [[19\]](#page-22-11). After his path-breaking work, Shapiro et al. [[20\]](#page-22-12) scrutinized the peristaltic mechanism in order to transport the liquids through a channel/duct subject to lubrication estimates. The electro-osmosisassisted peristaltic stream of non-Newtonian blood via micro-vascular tube was explored by Tripathi et al. [[21](#page-22-13)]. The MHD peristaltic pumping of non-Newtonian blood was simulated by Rashidi et al. [\[22](#page-22-14)]. They pointed out that the pressure rise per wavelength gets an augmentation for higher magnetic parameter. An inspection into the streaming of Rabinowitsch liquid inside an inclined non-uniform pipe with wall characteristics and wall slippage was made by Manjunatha et al. [[23\]](#page-22-15). In this research, they tracked out that the entrapped bolus shape infates with an elevation in rigidity and stifness parameters. Some other considerable research studies on the peristaltic drive of physiological liquids were descripted in refs. [[24–](#page-22-16)[27](#page-22-17)].

Almost all physiological materials, including mucus, synovium fuid, blood, cerebrospinal fuid, retinal humor, endobronchial discharges, and tear flm liquid, exhibit non-Newtonian viscoelastic attributes. A non-Newtonian viscoelastic fuid model called the Jefrey liquid is one of the simplest liquid models evaluated to others for understanding physiorheological properties of physiological fuids. Many scholars have conducted substantial research on peristaltic propulsion of physiological liquids using the Jefrey liquid model. The cilia driven MHD stream of Jefrey fuid in a tube was theoretically studied by Maqbool et al. [[28\]](#page-22-18). They recorded that the fuid velocity feld upsurges by incrementing the Jefrey parameter. Tripathi et al. [\[29](#page-22-19)] designed a mathematical simulation to study electro-osmosis modulated viscoelastic physiological fuid stream in a peristaltic cylindrical tube with Jefrey fuid model. Their results exposed that blood fow rate gets an enhancement with viscoelastic nature of blood and electric effects. Yasmeen et al. [[30\]](#page-22-20) implemented an analytical approach to examine viscoelastic attributes in the peristalsis of magnetized Jefrey fuid through a sinusoidal tube. They exposed that the dynamic fow profles (velocity and pressure gradients) exhibit little dependency on the Jeffrey parameter. Shaheen et al. [[31](#page-22-21)] conducted an inspection on the micro-rheological attributes of mucus propagation in a ciliary domain with the aid of Jefrey nanoliquid model. They evaluated the velocity felds for recovery and efective strokes and discovered that the efficient stroke velocity is larger than the recovery stroke velocity. Vaidya et al. [[32\]](#page-22-22) presented the peristaltic movement of magnetized Jefrey liquid with varying viscosity through an asymmetric wavy conduit. They noted that viscosity parameter uplifts the velocity profle in the core domain of the wavy channel. The MHD peristaltic propulsion of a reactive Jefrey liquid via a penetrable wavy conduit was researched by Abbas et al. [[33](#page-22-23)]. Their outcomes have exposed that pumping rate improves for higher Jefrey term in the co-pumping domain. Some additional researches on peristalsis of viscoelastic Jefrey liquid are recorded in refs. [\[34](#page-22-24)[–37\]](#page-22-25).

Motile cilia-regulated peristaltic transport appears signifcantly during cells' motion or adjacent materials fowing over cell surface. This phenomenon can be observed in vast physiological transit mechanisms such as feeding, breathing, reproduction, locomotion, circulation and respiration. In our body, cilia are very minuscule hair-like appendages that are usually existing on the eukaryotic cell surfaces, for example, kidneys, eye retina, ears, etc., and some physiological vessel/ tube/tract like respiratory tract, digestive tract, reproductive and nervous systems. Like oars, they smash back and forth strikes in synchronism to generate a commensurate patterns of traveling wave along the area, recognized as metachronal wave. Cilia-generated metachronal waves are primarily utilized to control fow continuity and improve fuid propulsion. Dust and mucus are dispelled from the airways by ciliary motion in the respiratory tract surface [[38\]](#page-22-26). The cilia in our kidneys operate as a sensory-antenna for our body. They collect signals from the adjacent urinary bladder and respond to cell warnings about the flow of urine in the surrounding area. As food moves via the digestive tract, the cilia beating helps to keep it moving [[39\]](#page-23-0). Ghazal et al. [[40\]](#page-23-1) have recorded the movement of egg and sperm swimming in the oviduct liquids via the oviducts. Cilia in male eferent ductules [\[41](#page-23-2)] are liable for mixing and dispersing sperms so that they can easily reach their ultimate destination without aggregation and blockage. Farooq et al. [[42](#page-23-3)] addressed a cilia-endorsed MHD transport of viscoelastic Jefrey liquid through a porous channel considering the cumulative impact pf chemical reaction, and external heat source. They exhibited that semen is a viscoelastic liquid with a lower volumetric flow rate than Newtonian liquid under related conditions. Sadaf et al. [\[43](#page-23-4)] analyzed the cilia-aided convection of a viscoelastic Jefrey liquid in a tube with ciliated sinusoidal wall. Shaheen et al. [[44\]](#page-23-5) reproduced a mathematical model for viscoelastic mucus fow in an axisymmetric ciliated duct. They considered the upper convected Maxwell (UCM) fuid model to explain the rheology of mucus which attributes a relaxation time, and precisely describes normal stress production in shear fows. Their outcomes explored that pressure rise is evidenced to boost signifcantly by increasing cilia length and relaxation time, while axial velocity is remarkably declined. The two-layered cilia-generated propulsion of Phan–Thien–Tanner (PTT) liquid in attendance of thermal and concentration impact has been investigated by Maqbool et al. [[45\]](#page-23-6). In this search, the two-layered design approach is attributed to the prevalence of the airway ciliary layer (ACL) and peri-ciliary liquid layer (PCL) on the epithelial tissue in the inner wall of trachea. Maqbool et al. [\[46](#page-23-7)] have explored the impact of buoyancy force in mixed convective ciliary movement of magnetized mucus with Carreau fuid model inside a channel. The cilia-assisted magneto-electro-osmotic transport of non-Newtonian liquid via a ciliated conduit with wall slip have been explored by Munawar [[47\]](#page-23-8). According to his fndings, as cilia length and cilia structure eccentricity improve, the shear stress of the ciliary wall uplifts. Shaheen et al. [[48\]](#page-23-9) have reported the electro-osmosis endorsed transport of radiated viscoelastic Jefrey fuids via a ciliary channel with heat generation/ absorption. In order to emphasize ciliary transport importance in physiology and biomedicine disciplines, several signifcant fndings were explored for engaged readers [[49–](#page-23-10)[52](#page-23-11)].

Nanotechnology has recently gained great attention. Scientists examined the efficiency of this research area in various applications such as heat exchangers, photovoltaic, photocatalysts, and biomedical engineering. Nanomaterials perform an important function in industry by controlling the heat mechanism and improving system efficiency. Recent development in bio-nanotechnology has disclosed a large array of benefts for nanomaterials (nanoparticles (*NPs*), nanofibers, nanotubes, etc.) in medical science. According to the new mechanism advanced by nanofuid dynamics, drugs can be delivered to various organs in human bodies in a uniform manner. Nanofuids are made by scattering nano-sized particles (dimension *<* 100 nm) in conventional liquids like water, lubricants, engine oil, emulsions, ethylene glycol, biofuids, and blood. This concept was frst presented by Choi [[53](#page-23-12)] to upsurge the thermal efficiency of working base fluids. The inspection of operating nanofuids in diverse geometrical aspects is carried out in many researches [\[54](#page-23-13)[–63](#page-23-14)]. Hybrid nanofuids refer to the dispersion of two or more diferent nanomaterials in the same operating fuids. There are numerous applications for these nanofuids in the felds of medical and bioengineering, for instance, disease diagnostics, preventive medicine, orthopedic lubrications, therapeutics, arthritis, antibacterial and anticancer drugs, versatile vaccines, etc. Almost all of the drugs are composed in the form of hybrid nano-liquids, and blood is utilized as a base liquid for testing the chemical reactions of these materials in the blood stream. Due to various applications in medical science, blood-based hybrid nanofuids have been extensively scrutinized via numerous researchers. The physical signifcance of hybrid nano-blood (*CuO-Cu*/blood) in a narrow stenosed artery was examined by Ijaz et al. [[64\]](#page-23-15). They recorded that hybrid *NPs* are more suitable as compared to mono nano-blood to reduce hemodynamic efect of stenosed artery. Saleem et al. [\[65](#page-23-16)] demonstrated peristaltic streaming of blood infused with hybridized nanoparticles via a curved tube with ciliated wall. They revealed that a rapid increment in pressure gradient in hybrid nano-blood (*Ag–Cu*/blood) is recorded as evaluated to *Cu*-blood. Das et al. [\[66\]](#page-23-17) presented an electromagnetic fow of blood suspended with hybridized nanoparticles inside an endoscopic conduit with peristaltic wave. They recorded that the concentration of nanoparticles in hybrid nano-blood  $(Ag-Al_2O_3/b$ lood) has a potential to modulate heat-conducting behaviors in fow conduit. The cilia-assisted flow of non-Newtonian blood diffused with copper and gold nanoparticle in a ciliary tube under consideration of entropy and heat generation has been anatomized by Ali et al. [\[67](#page-23-18)]. The entropy generation for hybrid nano-blood is higher than for nano-blood. With an electromagnetic feld along through Hall currents, Das et al. [\[68](#page-23-19)] have studied the hemodynamical properties of blood suspended with copper and gold nanoparticles in a non-uniform endoscopic annulus through wall slip. According to their fndings, the inclusion of gold and copper nanoparticles in blood possesses higher temperature

than copper nanoparticles. Ali et al. [[69\]](#page-23-20) recently explored electromagnetic phenomena in a cilia-modulated hybridized nano-blood fow. In this research, they found that the blood is emphasized on being cooled by enlarging hybrid *NPs* volume fractions. Some more related articles on peristalsis of blood via the suspension of hybridized *NPs* are loaded in Refs. [\[70–](#page-23-21)[72](#page-24-0)].

After a critical literary review, it is believed that no mathematical model has been documented yet in order to simulate the electro-magneto-hydrodynamic flow of ionized blood suspended with nanoparticles via ciliated arterial/vessel systems. In the current era, nanomaterials are extremely utilized in advanced medical science, such as bio-nano-polymer coatings for medical devices, administration of nanodrug in cardiovascular healing, smart bio-mimetic electroosmotic nanofuid pumps in ocular analysis, etc. Inspired by the aforementioned new things, here we plan to develop a new mathematical model for EOF of ionized non-Newtonian blood carrying dissimilar copper and gold nanoparticles via a vertical ciliated peristaltic micro-vessel under an electromagnetic feld environment. The Jefrey viscoelastic liquid model is invoked to mimic non-Newtonian features of blood mixed with hybridized copper and gold nanoparticles (*Au-Cu*/blood). The modeled formulae are shortened based on lubrication and Debye–Hückel linearization estimations. The sophisticated homotopy perturbation technique is opted to track out the optimal series solution for outcoming coupled nonlinear equations. A comparison between the hybrid nano-blood (*Au-Cu*/blood) model and the *Cu*-blood model is executed. The novelty of the proposed research work is the exploration of EDL's phenomena and its critical role in streaming ionized blood infused with magnetized copper and gold nanoparticles via ciliated micro-vessel with peristaltic wall.

For further clarifcation, the novel objectivities of this simulation are itemized in the following bullets:

- Exploration of electric double-layer (EDL) phenomena and its impact on the electro-magneto-hydrodynamic flow of non-Newtonian blood suspended with hybridized nanoparticles (copper and gold) due to the metachronal beating of cilia tips inside micro-vessel
- Fitting of Jeffrey liquid model in order to explain the non-Newtonian rheology of blood
- Integration of ionic blood (electrolyte solution), magnetic hybridized nanoparticles, electromagnetic force (Lorentz force), and buoyancy force
- Derivation of optimal series solutions by opting the homotopy perturbation method (HPM).

# **Modeling**

#### **Physical scheme**

Consider the two-dimensional laminar electro-magnetohydrodynamic (EMHD) of ionized non-Newtonian blood via a vertical micro-vessel with a ciliated wall. The wall of the micro-vessel wall is furnished with cilia and outer wall is negatively charged. The blood motion is induced by the cilia beating as well as electro-osmotic body force. The hybrid nano-blood is prepared as a homogeneous scattering of *Cu-Au* nano-powders into the blood. A cylindrical coordinate system  $(\tilde{R}, \tilde{Z})$  is considered to devise the current modeled problem, where  $\tilde{Z}$  is the axial coordinate, and  $\tilde{R}$  radial coordinate. The geometry of the modeled problem is displayed in Fig. [1](#page-5-0). A magnetic field is anticipated along the  $\tilde{R}$  direction. An external electric feld is applied along the *Z̃* direction, which induces the EMHD inside the ciliated micro-vessel. The electrokinetic body force is  $\rho_e E = \rho_e(E_{\tilde{R}}, E_{\tilde{Z}})$ . The micro-vessel wall is sustained with the uniform temperature  $T_0$ .

The envelopes of the cilia tips can be defned mathematically as [\[64](#page-23-15)]:

<span id="page-4-0"></span>
$$
\tilde{R} = \tilde{H} = \tilde{F}(\tilde{Z}, \tilde{t}) = \tilde{a} + \delta \tilde{a} \cos \frac{2\pi}{\lambda} (\tilde{Z} - c\tilde{t}),
$$
\n(1)

<span id="page-4-1"></span>
$$
\tilde{Z} = \tilde{G}(\tilde{Z}, \tilde{Z}_0, \tilde{t}) = \tilde{a} + \delta \tilde{a} \alpha \sin \frac{2\pi}{\lambda} (\tilde{Z} - c\tilde{t}),
$$
\n(2)

where  $\delta$  represents the dimensionless the cilia length,  $\tilde{a}$  the mean radius of the ciliated pipe, *c* metachronal wave speed,  $\alpha$  the eccentricity due to elliptical motion,  $\lambda$  the metachronal wavelength, and  $\tilde{Z}_0$  the reference particle position. The large number of cilia merges and exhibits a beating model over the inner wall of the ciliated pipe. This beating pattern produces a continuous chain of waves that acts similar to a sinusoidal or peristaltic wave at the wall of the pipe. Equations  $(1-2)$  $(1-2)$ describe the geometry of cilia movement in the form of elliptical shape.

The velocity constituents of the blood fow incited due to the cilia tips are [\[64](#page-23-15)]:

<span id="page-4-2"></span>
$$
\tilde{W} = \left(\frac{\partial \tilde{Z}}{\partial \tilde{t}}\right)_{\tilde{Z}_0} = \frac{\partial \tilde{G}}{\partial \tilde{t}} + \frac{\partial \tilde{G}}{\partial \tilde{Z}} \frac{\partial \tilde{Z}}{\partial \tilde{t}} = \frac{\partial \tilde{G}}{\partial \tilde{t}} + \frac{\partial \tilde{G}}{\partial \tilde{Z}} \tilde{W}
$$
\n(3)

$$
\tilde{U} = \left(\frac{\partial \tilde{R}}{\partial \tilde{t}}\right)_{\tilde{Z}_0} = \frac{\partial \tilde{F}}{\partial \tilde{t}} + \frac{\partial \tilde{F}}{\partial \tilde{Z}} \frac{\partial \tilde{Z}}{\partial \tilde{t}} = \frac{\partial \tilde{F}}{\partial \tilde{t}} + \frac{\partial \tilde{F}}{\partial \tilde{Z}} \tilde{W}
$$
(4)

<span id="page-4-3"></span>Through Eqs.  $(1-2)$  $(1-2)$ , Eqs.  $(3-4)$  $(3-4)$  can be rewritten as:

the problem

<span id="page-5-0"></span>**Fig. 1** Geometrical structure of



$$
\tilde{W} = -\frac{\frac{2\pi}{\lambda}\delta\alpha\tilde{a}c\,\cos\,\frac{2\pi}{\lambda}(\tilde{Z}-c\tilde{t})}{1 - \frac{2\pi}{\lambda}\delta\alpha\tilde{a}\,\cos\,\frac{2\pi}{\lambda}(\tilde{Z}-c\tilde{t})}
$$
\n(5)

$$
\tilde{U} = \frac{\frac{2\pi}{\lambda} \delta a \tilde{a} c \sin \frac{2\pi}{\lambda} (\tilde{Z} - c\tilde{t})}{1 - \frac{2\pi}{\lambda} \delta a \tilde{a} \cos \frac{2\pi}{\lambda} (\tilde{Z} - c\tilde{t})}
$$
(6)

## **Jefrey liquid scheme**

To study viscoelastic attributes of hybrid nano-blood, Jeffrey fuid model is taken into consideration. In this regard, the corresponding constitutive relation for the extra-stress tensor  $\tilde{S}$  can be expressed as [[37\]](#page-22-25):

$$
\tilde{S} = \frac{1}{1 + \lambda_1^*} (\dot{\gamma} + \lambda_2 \ddot{\gamma}),\tag{7}
$$

where  $\lambda_1^*$  assigns the ratio of relaxation time to retardation time,  $\lambda_2$  the retardation time,  $\dot{\gamma}$  the shear rate, and dots (⋅) the diferentiation with respect to time.

#### **Electro‑hydrodynamics**

In electrostatics theory, the electric potential function in an electrolyte solution satisfes the Poisson–Boltzmann equation. According to it, the electric potential Φ*̃* across the EDL is expressed as follows [[15,](#page-22-9) [73](#page-24-1)]:

$$
\nabla^2 \tilde{\Phi} = -\frac{\rho_e}{\epsilon_0},\tag{8}
$$

where  $\varepsilon_0$  is the dielectric permittivity of the ionic blood (electrolyte) and  $\rho_e$  the net charge density of the ionic blood in a unit volume due to the EDL, which is given as follows  $[15]$  $[15]$ :

$$
\rho_{\rm e} = e\overline{z}(n^+ - n^-),\tag{9}
$$

*e* represents the net electronic charge (1.6 × 10<sup>−</sup>19 C), *z* is the valency for both the ions (cations and anions), and *n*<sup>−</sup> and  $n<sup>+</sup>$  are the ionic concentrations of anions and cations in the ionic blood, respectively. The Boltzmann distribution function for local ionic density is as follows [\[59](#page-23-22)]:

$$
n^{\pm} = n_0 e^{\pm \frac{e^{\pm} \Phi}{K_B T_a}},\tag{10}
$$

where  $n_0$  is the bulk density of anions and cations in the ionic blood,  $K_{\text{B}}$  the Boltzmann constant, and  $T_{\text{a}}$  the average temperature of the ionic blood. In the endoscopic conduit, there is no gradient of ionic concentration in the axial direction and hence the distribution of ionic concentration is appropriate [\[15](#page-22-9), [73,](#page-24-1) [74\]](#page-24-2). In a unit volume of the ionic blood, the electric charge density is rewritten as:

$$
\rho_{\rm e} = -2n_0 e \bar{z} \sinh\left(\frac{e \bar{z} \tilde{\Phi}}{K_{\rm B} T_{\rm a}}\right). \tag{11}
$$

In view of (8) and (11), the simplifed Poisson–Boltzmann equation is as:

$$
\nabla^2 \tilde{\Phi} = \frac{2n_0 e\overline{z}}{\epsilon_0} \sinh\left(\frac{e\overline{z}\tilde{\Phi}}{K_{\rm B}T_a}\right).
$$
 (12)

For very low zeta potential (*<* 25*mV*) for a wide range of PH of the electrolytic blood solutions across EDL, the Poisson–Boltzmann Eq. ([12\)](#page-6-0) can be simplified by adopting  $\sinh\left(\frac{e\overline{z}\tilde{\Phi}}{K_{\text{B}}T_{\text{a}}} \right)$  $\sum \limits_{K_B T_a} \exp\left(-\frac{e^{\frac{r}{2}}}{K_B T_a}\right)$  ander the *Debye* − *Hückel* linearization approximation and takes the form:

$$
\nabla^2 \tilde{\Phi} = \frac{2n_0 (e\overline{z})^2}{\epsilon_0 K_\text{B} T_\text{a}} \tilde{\Phi}.
$$
\n(13)

### **Governing equations**

The governing equations in the laboratory frame for the proposed EMHD of ionized blood with hybridized nanoparticles' suspension via a ciliated micro-vessel with peristaltic wall under the above-mentioned suppositions and employing Boussinesq approximation are [[75,](#page-24-3) [76](#page-24-4)]:

$$
\frac{\partial \tilde{U}}{\partial \tilde{R}} + \frac{\tilde{U}}{\tilde{R}} + \frac{\partial \tilde{W}}{\partial \tilde{Z}} = 0,
$$
\n(14)

$$
\rho_{\rm hnf}\left(\frac{\partial \tilde{U}}{\partial \tilde{t}} + \tilde{U}\frac{\partial \tilde{U}}{\partial \tilde{R}} + \tilde{W}\frac{\partial \tilde{U}}{\partial \tilde{Z}}\right) = -\frac{\partial \tilde{P}}{\partial \tilde{R}} + \frac{1}{\tilde{R}}\frac{\partial}{\partial \tilde{R}}(\tilde{R}\tilde{S}_{\tilde{R}\tilde{R}}) + \frac{\partial}{\partial \tilde{Z}}(\tilde{S}_{\tilde{R}\tilde{Z}}),\tag{15}
$$

$$
\rho_{\rm hnf} \left( \frac{\partial \tilde{W}}{\partial \tilde{t}} + \tilde{U} \frac{\partial \tilde{W}}{\partial \tilde{R}} + \tilde{W} \frac{\partial \tilde{W}}{\partial \tilde{Z}} \right) = -\frac{\partial \tilde{P}}{\partial \tilde{Z}} + \frac{1}{\tilde{R}} \frac{\partial}{\partial \tilde{R}} (\tilde{R}\tilde{S}_{\tilde{R}\tilde{Z}}) + \frac{\partial}{\partial \tilde{Z}} (\tilde{S}_{\tilde{Z}\tilde{Z}}) + (\rho \beta_{\tilde{T}})_{\rm hnf} g(\tilde{T} - \tilde{T}_0)
$$

$$
-\sigma_{\text{hnf}}B_0^2 \tilde{W} + \rho_e E_{\tilde{Z}},\tag{16}
$$

<span id="page-6-3"></span><span id="page-6-0"></span>
$$
(\rho c_{\rm p})_{\rm hnf} \left( \frac{\partial \tilde{T}}{\partial \tilde{t}} + \tilde{U} \frac{\partial \tilde{T}}{\partial \tilde{R}} + \tilde{W} \frac{\partial \tilde{T}}{\partial \tilde{Z}} \right)
$$
  
=  $\tilde{S}_{\tilde{R}\tilde{R}} \frac{\partial \tilde{U}}{\partial \tilde{R}} + \tilde{S}_{\tilde{R}\tilde{Z}} \frac{\partial \tilde{W}}{\partial \tilde{R}} + \tilde{S}_{\tilde{Z}\tilde{R}} \frac{\partial \tilde{U}}{\partial \tilde{Z}} + \tilde{S}_{\tilde{Z}\tilde{Z}} \frac{\partial \tilde{W}}{\partial \tilde{Z}} + k_{\rm hnf} \left( \frac{\partial^2 \tilde{T}}{\partial \tilde{R}^2} + \frac{1}{\tilde{R}} \frac{\partial \tilde{T}}{\partial \tilde{R}} + \frac{\partial^2 \tilde{T}}{\partial \tilde{Z}^2} \right) + Q_0, \tag{17}$ 

<span id="page-6-2"></span>where  $\tilde{P}$  denotes the blood pressure,  $\tilde{W}$ ,  $\tilde{U}$  the respective axially and radially velocity components of *Cu-Au* /blood in the fixed frame,  $E_{\tilde{Z}}$  the axially applied electric field,  $\tilde{T}$ the  $Cu$ -Au/blood temperature,  $k_{\text{hnf}}$  the thermal conductivity of *Cu-Au/blood,*  $\rho_{\text{hnf}}$  the density of *Cu-Au/blood,*  $(c_p)_{\text{hnf}}$  the specific heat of  $Cu$ -Au/blood at constant pressure, and  $Q_0$  the internal heat source coefficient.

In the fxed (laboratory) frame, the worthy boundary con-ditions for the flow configuration are proposed as [[64\]](#page-23-15):

<span id="page-6-1"></span>

<span id="page-7-0"></span>**Table 2** Thermophysical properties of blood, copper, and gold *NPs* [[68](#page-23-19)]

	<b>Blood</b>	Copper	Au
$\rho$ /kg m <sup>-3</sup>	1063	8933	19,320
$c_p / J kg^{-2} K^{-1}$	3594	385	129
$k / Wm^{-1} K^{-1}$	0.492	401	314
$\beta \times 10^{-6} / K^{-1}$	1.8	16.7	14
$\sigma$ /S m <sup>-1</sup>	$6.67 \times 10^{-1}$	$59.6 \times 10^{6}$	$4.10 \times 10^{7}$

$$
\frac{\partial \tilde{W}}{\partial \tilde{R}} = 0, \ \frac{\partial \tilde{T}}{\partial \tilde{R}} = 0, \ \frac{\partial \tilde{\Phi}}{\partial \tilde{R}} = 0 \ \text{at } \tilde{R} = 0,
$$

$$
\tilde{W} = -\frac{\frac{2\pi}{\lambda}\delta\alpha\tilde{a}c\,\cos\left(\frac{2\pi}{\lambda}(\tilde{Z}-c\tilde{t})\right)}{1 - \frac{2\pi}{\lambda}\delta\alpha\tilde{a}\,\cos\left(\frac{2\pi}{\lambda}(\tilde{Z}-c\tilde{t})\right)}, \tilde{T} = \tilde{T}_0, \tilde{\Phi} = \tilde{\Phi}_0
$$
\nat  $\tilde{R} = \tilde{H} = \tilde{a} + \delta\tilde{a}\cos\left(\frac{2\pi}{\lambda}(\tilde{Z}-c\tilde{t})\right),$ \n(18)

#### **Empirical relations and thermophysical properties**

The empirical relations and thermophysical properties of *Au NPs*, blood, and *Cu NPs* are provided in Tables [1](#page-6-1) and [2.](#page-7-0) where  $\phi_1$  and  $\phi_2$  denote the solid volume fractions of *Cu* and gold *NPs*, respectively. The suffices  $s_1$ ,  $s_2$ ,  $f$ ,  $h$ *nf*, and *nf* signify solid *Cu NPs*, solid Au *NPs*, base liquid (blood), hybrid nano-blood (*Cu-Au*/blood), and nano-blood (*Cu*-blood), respectively. The case  $\phi_1 = \phi_2 = 0$  (with no suspension of *NPs*) corresponds to the pure-blood. The thermophysical properties are specifed in Table [2.](#page-7-0)

#### **Flow scrutiny in moving frame of reference**

Here flow problem is considered unsteady. For this in the fixed frame into the steady state in the wave frame  $(\tilde{r}, \tilde{z})$ , developing via the same wave speed c, the linear transformations are established as [[64,](#page-23-15) [73\]](#page-24-1):

$$
\tilde{r} = \tilde{R}, \ \tilde{z} = \tilde{Z} - c\tilde{t}, \ \tilde{u} = \tilde{U}, \ \tilde{w} = \tilde{W} - c, \ \tilde{h}(\tilde{z}, \tilde{t})
$$

$$
= \tilde{H}(\tilde{Z}, \tilde{t}), \ \tilde{p}(\tilde{z}, \tilde{r}, \tilde{t})
$$

$$
\tilde{P}(\tilde{Z}, \tilde{R}, \tilde{t}), \ \tilde{T}(\tilde{z}, \tilde{r}, \tilde{t}) = \tilde{T}(\tilde{Z}, \tilde{R}, \tilde{t}), \tag{19}
$$

Using these dimensionless variables:

$$
r = \frac{\tilde{r}}{\tilde{a}}, z = \frac{\tilde{z}}{\lambda}, w = \frac{\tilde{w}}{c}, u = \frac{\lambda \tilde{u}}{\tilde{a}c}, p = \frac{\tilde{a}^2 \tilde{p}}{c \lambda \mu_f},
$$
  
\n
$$
\theta = \frac{\tilde{T} - \tilde{T}_0}{\tilde{T}_0}, \Phi = \frac{\tilde{\Phi}}{\Phi_0}, \Phi_0 = \frac{K_B T_a}{e \tilde{z}}, t = \frac{c \tilde{t}}{\lambda},
$$
  
\n
$$
\beta = \frac{\tilde{a}}{\lambda}, \lambda_1 = \frac{c \lambda_1^*}{\tilde{a}}, Re = \frac{c \tilde{a} \rho_f}{\mu_f}, M^2 = \frac{\sigma_f B_0^2 \tilde{a}^2}{\mu_f},
$$
  
\n
$$
\kappa = b_0 e \tilde{z} \sqrt{\frac{2n_0}{\epsilon_0 K_B T_a}} = \frac{b_0}{\lambda_D}, U_{\text{hs}} = -\frac{\epsilon_0 \zeta E_{\tilde{z}}}{c \mu_f},
$$
  
\n
$$
Gr = \frac{g \tilde{a}^2 \tilde{T}_0 \rho_f (\beta_T)_f}{c \mu_f}, Br = \frac{c^2 \mu_f}{(c_p)_f \tilde{T}_0},
$$
  
\n
$$
S_{ij} = \frac{\tilde{a} \tilde{S}_{ij}}{c \mu_f}, h = \frac{\tilde{h}}{\tilde{a}}, \xi = \frac{Q_0 \tilde{a}^2}{k_f \tilde{T}_0},
$$

where  $Re$  is the Reynolds number,  $M^2$  the magnetic field term,  $\lambda_1$  the Jeffrey parameter,  $U_{\text{hs}}$  the Helmholtz–Smoluchowski velocity (maximum electro-osmotic velocity,  $\kappa$  the electro-osmotic term, *Gr* the thermal Grashof number, *Br* the Brinkman number, and  $\xi$  the internal heat source term.

In pursuance of (7), (19–20), and the lubrication estimations, Eqs.  $(13-17)$  $(13-17)$  $(13-17)$  related to the viscoelastic hybrid nanoblood can be put in the dimensionless form as:

<span id="page-7-1"></span>
$$
\frac{1}{r}\frac{\partial}{\partial r}\left(r\frac{\partial \Phi}{\partial r}\right) = \kappa^2 \Phi,
$$
\n(21)

$$
\frac{\partial p}{\partial r} = 0,\tag{22}
$$

<span id="page-7-3"></span>
$$
-\frac{\partial p}{\partial z} + \frac{x_1}{1 + \lambda_1} \frac{1}{r} \frac{\partial}{\partial r} \left( r \frac{\partial w}{\partial r} \right) + x_2 Gr \theta + \kappa^2 U_{\text{hs}} \Phi - x_3 M^2 (w + 1) = 0,
$$
\n(23)

<span id="page-7-4"></span>
$$
\frac{x_4}{r}\frac{\partial}{\partial r}\left(r\frac{\partial\theta}{\partial r}\right) + \frac{x_1Br}{1+\lambda_1}\left(\frac{\partial w}{\partial r}\right)^2 + \xi = 0,
$$
\n(24)

where  $x_1 = \frac{\mu_{\text{hnf}}}{\mu_f}$ ,  $x_2 = \frac{(\rho \beta)_{\text{hnf}}}{(\rho \beta)_{f}}$ ,  $x_3 = \frac{\sigma_{\text{hnf}}}{\sigma_f}$ ,  $x_4 = \frac{k_{\text{hnf}}}{k_f}$ .

The non-dimensional form of the physical boundary conditions (*BCs*) becomes

$$
\frac{\partial w}{\partial r} = 0, \ \frac{\partial \theta}{\partial r} = 0, \ \frac{\partial \Phi}{\partial r} = 0 \text{ at } r = 0,
$$
  

$$
\frac{\partial w}{\partial r} = 0, \ \frac{\partial \theta}{\partial r} = 0, \ \frac{\partial \Phi}{\partial r} = 0 \text{ at } r = 0,
$$
  

$$
w = -1 - \frac{2\pi \delta \alpha \beta \cos 2\pi z}{1 - 2\pi \delta \alpha \beta \cos 2\pi z}, \ \theta = 0, \ \Phi = 1
$$
 (25)  
at  $r = h(z) = 1 + \delta \cos 2\pi z$ ,

<span id="page-7-2"></span>where  $\beta$  is the wave number.

Solution of Poisson–Boltzmann Eq. ([21\)](#page-7-1) subject to boundary conditions [\(25](#page-7-2)) can be easily derived by using Mathematica software and given by

$$
\Phi(r,z) = \frac{I_0(\kappa r)}{I_0(\kappa h)},
$$
\n(26)

where  $I_0$  designates the zero<sup>th</sup> order modified Bessel function of frst kind.

## **HPM solution**

Equations  $(23-24)$  $(23-24)$  $(23-24)$  $(23-24)$  $(23-24)$  are highly coupled nonlinear, and it is complex to resolve it analytically. Thus, series solution or numerical scheme is the only one opportunity to handle this coupled nonlinear equations. Recently, He [[74\]](#page-24-2) proposed the homotopy perturbation method (HPM). In several engineering, mechanical and liquid dynamical branches, HPM has been employed to extort more precise solution or estimation in series scheme through high convergence precision of linear and nonlinear modeled equations. A homotopy is selected and built through  $\hat{q} \in [0, 1][0, 1]$  embedding term considered to be small quantity [\[75\]](#page-24-3) in this technique.

After inserting  $(26)$  $(26)$  $(26)$  in  $(23)$  $(23)$  $(23)$ , Eqs.  $(23-24)$  $(23-24)$  $(23-24)$  become:

$$
\frac{1}{r}\frac{\partial}{\partial r}\left(r\frac{\partial w}{\partial r}\right) + a_0I_0(\kappa r) + a_1\theta - a_2(w+1) - a_3 = 0,\tag{27}
$$

$$
\frac{1}{r}\frac{\partial}{\partial r}\left(r\frac{\partial \theta}{\partial r}\right) + a_4\left(\frac{\partial w}{\partial r}\right)^2 + a_5 = 0,\tag{28}
$$

where

$$
a_0 = \frac{\kappa^2 (1 + \lambda_1) U_{\text{hs}}}{x_1 I_0(\kappa h)}, \quad a_1 = \frac{x_2}{x_1} (1 + \lambda_1) \text{ Gr}, \quad a_2 = \frac{x_3}{x_1} (1 + \lambda_1) M^2,
$$
\n
$$
a_3 = \frac{1 + \lambda_1}{x_1} \frac{dp}{dz}, \quad a_4 = \frac{x_1 Br}{x_4 (1 + \lambda_1)}, \quad a_5 = \frac{\xi}{x_4}.
$$
\n
$$
(29)
$$

In order to solve Eqs.  $(27–28)$  $(27–28)$  $(27–28)$  $(27–28)$ , we construct a homotopy  $\hat{h}(r, \hat{q}) : \Omega \times [0, 1] \rightarrow \Re$  which assures

$$
(1 - \hat{q})[\hat{L}(\hat{w}) - \hat{L}(\hat{w}_0)] + \hat{q}[\hat{L}(\hat{w})
$$
  
+ $a_0I_0(\kappa r) + a_1\hat{\theta} - a_2(\hat{w} + 1) - a_3] = 0$  (30)

$$
(1 - \hat{q})[\hat{L}(\hat{\theta}) - \hat{L}(\hat{\theta}_0)] + \hat{q}[\hat{L}(\hat{\theta}) + a_4 \left(\frac{\partial \hat{w}}{\partial r}\right)^2 + a_5] = 0, (31)
$$

where  $\hat{L} = \frac{1}{r}$  $\partial$ *r*  $\left(r\frac{\partial}{\partial r}\right)$ ) .Supposing the initial guess for the linear operator has the form

$$
\hat{w}_0(r,z) = X + \frac{1}{4}(1 + \lambda_1)(r^2 - h^2)\frac{dp}{dz}, \quad \hat{\theta}_0(r,z) = \frac{1}{4}(r^2 - h^2).
$$
\n(32)

In view of HPM, the estimated solutions  $\hat{w}(r, z)$  and  $\hat{\theta}(r, z)$ have been supposed in the these forms of power series:

<span id="page-8-0"></span>
$$
\hat{w}(r, z) = \hat{w}_0 + \hat{w}_1 \hat{q} + \hat{w}_2 \hat{q}^2 + \cdots, \n\hat{\theta}(r, z) = \hat{\theta}_0 + \hat{\theta}_1 \hat{q} + \hat{\theta}_2 \hat{q}^2 + \cdots
$$
\n(33)

Presently, including Eqs.  $(30-31)$  $(30-31)$  $(30-31)$  in Eqs.  $(28-29)$  $(28-29)$  $(28-29)$  $(28-29)$  and comparing the powers of  $\hat{q}$ , the linear equations scheme can be achieved. On view of homotopy perturbation scheme, taking  $\hat{q} = 1$ , one has

$$
w(r, z) = \hat{w}(r, z) = \hat{w}_0 + \hat{w}_1 + \hat{w}_2 + \cdots
$$
 (34)

$$
\theta(r,z) = \hat{\theta}(r,z) = \hat{\theta}_0 + \hat{\theta}_1 + \hat{\theta}_2 + \cdots
$$
\n(35)

The fnal expressions for blood temperature and velocity feld are:

$$
w(r, z) = A_1 + A_2(r^2 - h^2) + A_3(r^4 - h^4) + A_4(r^6 - h^6) + A_5I_0(\kappa r),
$$
\n(36)

$$
\theta(r,z) = A_6(r^2 - h^2) + A_7(r^4 - h^4) + A_8(r^6 - h^6) + A_9[2I_0(h\kappa) - h\kappa I_1(h\kappa) - 2I_0(\kappa r) + \kappa r I_1(\kappa r)],
$$
\n(37)

where  $I_1$  designates the first order modified Bessel function of first kind and the constants  $A_1$ ,  $A_2$ ,  $A_3$ ,  $A_4$ ,  $A_5$ ,  $A_6$ ,  $A_7$ ,  $A_8$ and  $A_9$  are given in Appendix A.

## <span id="page-8-2"></span><span id="page-8-1"></span>**Stream function, fow rate, wall shear stress and heat transport coefficient**

The volume flow rate  $Q$  is computed as

$$
Q = 2\pi \int_0^h r w(z, r) dr,
$$
\n(38)

with this, the pressure gradient is

<span id="page-8-5"></span>
$$
\frac{\mathrm{d}p}{\mathrm{d}z} = \frac{1}{2B_1} \{ B_2 - (B_2^2 - 4B_1 B_3)^{1/2} \},\tag{39}
$$

where  $B_1$ ,  $B_2$ , and  $B_3$  are given in Appendix A.

<span id="page-8-3"></span>The mean volume flow rate via one period of the peristaltic wave is:

$$
F = Q + \frac{1}{2} \left( \frac{\delta^2}{2} + 1 \right),\tag{40}
$$

<span id="page-8-4"></span>The non-dimensional pressure rise Δ*p* toward one period of wavelength can be articulated as

$$
\Delta p = \int_0^1 \frac{\mathrm{d}p}{\mathrm{d}z} \mathrm{d}z,\tag{41}
$$

To assess the numerical estimations of the pressure rise  $\Delta p$ , Mathematica built-in function N Integrate is deployed.

The speed components are articulated in terms of the stream function and are defned as

$$
u = -\frac{1}{r}\frac{\partial \psi}{\partial r}, \ w = \frac{1}{r}\frac{\partial \psi}{\partial r}
$$
 (42)

To acquire the stream function  $\psi$ , we integrate  $w = \frac{1}{r}$  $\partial \psi$ *𝜕r* through  $\psi = 0$  at  $r = 0$ , and then the stream function is specifed as

$$
\psi = r^2 \left[ \frac{A_1}{2} - \frac{1}{2} h^2 (A_2 + A_3 h^2 + A_4 h^4) \right] + \frac{A_2}{4} r^4
$$
  
+ 
$$
\frac{A_3}{6} r^6 + \frac{A_4}{8} r^8 + \frac{A_5}{\kappa} r I_1(\kappa r),
$$
 (43)

The stream function denotes the volumetric flow rate via the cross section bounded through the ciliated tube wall.

The wall shear at the tube wall is estimated by utilizing the following equation:

$$
S_{rz} = \frac{\mu_{\text{hnf}}}{\mu_{\text{f}}} \left( \frac{\partial w}{\partial r} \right)_{r=h}
$$
  
=  $x_1 [2A_2 h + 4A_3 h^3 + 6A_4 h^5 + A_5 \kappa I_1(h\kappa)].$  (44)

The heat transport coefficient at the wall of ciliated pipe is calculated as:



<span id="page-9-0"></span>**Fig. 2** Profiles of velocity and temperature through  $Br = 0$ ,  $\alpha = 0.1$ ,  $\beta = 0.2$ ,  $M^2 = 1$ ,  $\xi = 1$ ,  $\delta = 0.1$ ,  $F = 0.5$ ,  $Gr = 2$ ,  $\kappa = 1$ ,  $\lambda_1 = 0.6$ ,  $U_{\text{hs}} = -2$ ,  $z = 0.75$ ,  $\phi_1 = \phi_2 = 0.02$ 

$$
Z^* = \frac{k_{\text{hnf}}}{k_{\text{f}}} \frac{dh}{dz} \left(\frac{\partial \theta}{\partial r}\right)_{r=h}
$$
  
=  $-2\pi \delta hx_4 [2A_6 + 4A_7h^2 + 6A_8h^4 + A_9\kappa^2 I_2(h\kappa)] \sin 2\pi z,$  (45)

where  $I_2$  designates the second-order modified Bessel function of frst kind.

# **Code validation**

To testify the authenticity of our semi-analytical resolutions, we have supposed a particular cases. The current model moderates to the model studied via [\[76\]](#page-24-4) by deputizing  $\kappa = \xi = \phi_1 = \phi_2 = 0$ . Furthermore, in Fig. [2a](#page-9-0)-b, the graphical comparison of the present model in the absence of viscous dissipation have been carried out for exact solution and semi-analytical homotopic perturbation approach. These figures affirm that our computed homotopic solution for the limiting case is very close to the results of exact solution. Furthermore, a numeric contrast in Table [3](#page-9-1) is performed in the constraining case and reported excellent correlation with Nadeem and Sadaf [[79\]](#page-24-5). These establish the authenticity of the present solutions.

## **Outcomes and discussion**

In this segment, the physical explorations of graphical demonstration for various relevant terms over the pertinent hybrid nano-blood fow characteristics are explicated. The signifcant fuctuation in the dimensionless velocity and temperature evolutions, pumping characteristics (Axial pressure gradient and pressure rise per wavelength), mean

<span id="page-9-1"></span>**Table 3** Comparison of velocity profile for when varying  $\phi_1 = 0.02$ ,  $\alpha = 0.02, \quad \beta = 0.11, \quad z = 0.08, \quad \xi = 0.17, \quad \delta = 0.05, \quad F = 0.16,$  $\lambda_1 = M^2 = Br = \phi_2 = \kappa = 0$ 

w(r, z)		
r	[79]	Current work
0.1	$-1.000000$	$-1.000001$
0.17	$-0.717905$	$-0.717904$
0.24	$-0.559157$	$-0.559156$
0.31	$-0.465615$	$-0.465615$
0.45	$-0.396313$	$-0.396314$
0.52	$-0.403151$	$-0.403152$
0.66	$-0.478546$	$-0.478547$
0.73	$-0.542343$	$-0.542344$
0.80	$-0.621371$	$-0.621372$
0.94	$-0.820638$	$-0.820639$
1.04382	$-1.00061$	$-1.00062$

<span id="page-10-0"></span>**Fig. 3** Evolution of  $w(r, z)$  for various physical terms  $\alpha = 0.1$ ,  $\beta = 0.2$ ,  $z = 0.75$ ,  $Br = 0.1$ ,  $\xi = 1.0$ , and **a**  $\lambda_1 = 0.6, \kappa = 2.0,$  $U_{\text{hs}} = -2.0, \delta = 0.1, F = 0.5,$  $Gr = 2.0, \phi_1 = \phi_2 = 0.02,$ **b**  $M^2 = 1.0, \kappa = 3.0,$  $U_{\text{hs}} = -2.0, \delta = 0.1, F = 0.5,$  $Gr = 2.0, \phi_1 = \phi_2 = 0.02$ **c**  $M^2 = 1.0$ ,  $\lambda_1 = 0.6$ ,  $U_{\text{hs}} = -2.0, \delta = 0.1, F = 0.5,$  $Gr = 2.0, \phi_1 = \phi_2 = 0.02$  $d M^2 = 1.0, \lambda_1 = 0.6,$  $\kappa = 2.0, \delta = 0.1, F = 0.5,$  $Gr = 2.0, \phi_1 = \phi_2 = 0.02,$ **e**  $M^2 = 1.0$ ,  $\lambda_1 = 0.6$ ,  $\kappa = 2.0, U_{\text{hs}} = -2.0, F = 0.5,$  $Gr = 2.0, \phi_1 = \phi_2 = 0.02$ **f**  $M^2 = 1.0$ ,  $\lambda_1 = 0.6$ ,  $\kappa = 2.0, U_{\text{hs}} = -2.0, \delta = 0.1,$  $Gr = 2.0, \phi_1 = \phi_2 = 0.02, g$  $M^2 = 1.0$ ,  $\lambda_1 = 0.6$ ,  $\kappa = 3.0$ ,  $U_{hs} = -2.0, \delta = 0.1, F = 0.5,$  $\phi_1 = \phi_2 = 0.02$ , **h**  $M^2 = 3.0$ ,  $\lambda_1 = 0.6, \kappa = 2.0, U_{\text{hs}} = -2.0,$  $\delta = 0.1, F = 0.5, Gr = 1.0$ 



flow rate *F*, wall shear stress (WSS), heat transport coefficient (HTC), and streamlines for magnetic term  $M^2$ , Jeffrey term  $\lambda_1$ , electro-osmotic term  $\kappa$ , cilia length  $\delta$ , Helmholtz–Smoluchowski velocity (maximum electro-osmotic speed) *U*hs, Brinkman number *Br*, thermal Grashof number *Gr*, heat source term  $\xi$ , and *NPs* volume fractions  $\phi_1$ ,  $\phi_2$  is demonstrated in Figs. [3](#page-10-0)–[9.](#page-18-0) The graphical demonstrations are executed by taking default values/ranges of

parameters and flow constants  $[15, 64, 73]$  $[15, 64, 73]$  $[15, 64, 73]$  $[15, 64, 73]$  $[15, 64, 73]$ :  $M^2 = 0 - 2$ ,  $\kappa = 2 - 4$ ,  $U_{hs} = -4 - 2$ ,  $\lambda_1 = 0 - 0.9$ ,  $\alpha = 0.1 - 0.4$ ,  $\beta = 0.1 - 0.4$ ,  $\delta = 0.1 - 0.7$ ,  $F = 0.1 - 0.5$ ,  $Br = 0.1 - 0.5$ ,  $z = 0 - 2$ ,  $\xi = 0 - 2$ ,  $\phi_1 = 0 - 0.1$ ,  $\phi_2 = 0 - 0.1$ . In addition,  $\phi_1 = \phi_2 = 0$  corresponds to pure blood,  $\phi_1 = 0.02$ ,  $\phi_2 = 0$ for *Cu*-blood, and  $\phi_1 = 0.02$ ,  $\phi_2 = 0.02$  for *Cu-Au*/blood.

The graphical and numerical outcomes are assessed by implementing computational software *Mathematica*.

#### **Axial velocity profle**

The ascendancy of diferent elevating dynamical quantities, namely magnetic parameter  $M^2$ , Jeffrey parameter  $\lambda_1$ , cilia length *𝛿*, thermal Grashof number *Gr*, electro-osmotic term  $\kappa$ , Helmholtz–Smoluchowski velocity (maximum electroosmotic speed)  $U_{\text{hc}}$ , and *NPs* volume fractions  $\phi_1$  and  $\phi_2$  on the dimensionless axial velocity evolution  $w(r, z)$ , is explicated in Fig. [3](#page-10-0)a-h. The alternation of magnetic parameter *M*<sup>2</sup> via axial velocity feld is verifed in Fig. [3a](#page-10-0). It is evident from these curves that the axial velocity is substantially decremented at the core region of the ciliary vessel for growing *M*<sup>2</sup> for both hybrid *Au-Cu*/blood and *Cu*-blood flow. The red blood cell contains hemoglobin molecules which are formed by iron oxide. Those red cells are attracted by the strong Lorentz forces which are generated by intensifying *M*<sup>2</sup>. Hence, blood circulation is disrupted by an implication of a strong magnetic feld. Therefore, the blood fow can be infuentially controlled through choosing suitable strength of applied magnetic feld during various kinds of complex surgeries. Figure [3](#page-10-0)b is designed to disclose how Jeffrey parameter  $\lambda_1$ afects the axial velocity. The plotted fgures explore that by boosting the Jeffrey parameter  $\lambda_1$ , the axial velocity rises in the core domain of the ciliary vessel, but the overturn trend is evident in the peripheral domain. Jeffrey parameter  $\lambda_1$  designates the proportion of relaxation time to retardation time. In the scenario of physiological fuids (such as blood, mucus, semen, etc.), the retardation time is longer than the relaxation time ( $\lambda_1$  < 1). This suggests that when stress is relieved, the physiological fuids respond more quickly and get back to their normal state, which has a signifcant consequence through the pressure gradient, resulting in an increment in axial fow at the core domain of the ciliary blood vessel. The consequence of electro-osmotic term  $\kappa$  via the axially varying speed distribution is directed in Fig. [3c](#page-10-0). The axial velocity exposes an elevating trend in the core domain of ciliary blood vessels for larger  $\kappa$ , while an inverse trend is witnessed in the peripheral domain. Debye length or EDL (electric double layer) thickness is inversely linked to the electro-osmotic term, which characterizes the electro-osmosis phenomenon. An upsurge in  $\kappa$  (thinning the EDL) amplifes the electrical potential distribution which accelerates the blood pumping in the core domain of the micro-vessel and suppresses it in the peripheral domain of the vessel wall. In the EOF regime, a thin EDL plays as a stabilizing factor. It can be perceived that the electro-osmotic parameter *𝜅* (essential factor in electro-osmosis) synchronizes electric potential in the EDL and is useful for designing and developing micro-blood pumps and mixing physiological fuids

(blood, mucus, saliva, semen, etc.) with reagents (medications, nutrients, enzyme, etc.).

Figure [3](#page-10-0)d portends the alteration of axial velocity for Helmholtz–Smoluchowski speed (maximum electro-osmotic speed)  $U_{\text{hs}}$ . The respective figure designates that there is a suppressing behavior in the blood flow in the core area of the blood vessel and an inverse trend is manifested nearby the blood vessel wall toward changing values (from −4 to −1) of  $U_{\text{hs}}$ . Physically,  $U_{\text{hs}} < 0$  corresponds to the axial electric field orientated in the peristaltic wave way, which assists the electro-osmotic body force  $-\kappa^2 U_{\text{hs}}\Phi$ . A decrement in negative  $U_{\text{hs}}$  physically means that the strength of the axially applied electric feld is weakened which produces a slow movement of ionic species in the liquid medium. Therefore, the lowering electro-osmotic velocity exhibits declining behavior in the overall axial speed. The fuctuation in axial velocity for multiple values of cilia length  $\delta$  is delineated in Fig. [3e](#page-10-0). It is evident that the speed in the streaming domain is deteriorating as  $\delta$  increases. A longer  $\delta$  generates more resistive forces in the streaming region, leading to a declination in velocity distribution. Figure [3f](#page-10-0) is pervaded to disclose the alteration of axial speed for multiple values of fow rate term *F*. It is noted that an elevation in *F* reveals a mounting trend in the axial speed throughout the streaming area. For larger *F*, less resistive force is produced throughout the ciliary vessel, and as a outcome, the velocity feld gets an escalation.

The impact of enlarging thermal *Gr* over the velocity feld is manifested in Fig. [3g](#page-10-0). A higher *Gr* boosts up the buoyancy force which improves the axial speed profle in the main domain, but an inverse outcome is found at the peripheral area of the ciliary vessel. Figure [3h](#page-10-0) descripts the consequences of  $\phi_1$  and  $\phi_2$  over the axial velocity profile. An improvement in  $\phi_1$  and  $\phi_2$  corresponds to a denunciation in the axial speed in the principal domain of the ciliary blood vessel, and a slight augmentation nearby the ciliary microvessel wall. From Fig. [3a](#page-10-0)–g the axial velocity for *Cu-Au*/ blood accomplishes higher estimations than *Cu*-blood at the core domain but an inverse trend is found at the peripheral domain of the ciliary micro-vessel.

#### **Temperature distribution**

In this subpart, Fig. [4](#page-12-0)a–h is configured to elucidate the contribution of diferent emerging physical terms such as magnetic term  $M^2$ , Jeffrey term  $\lambda_1$ , Brinkman number *Br*, heat source parameter *ξ*, electro-osmotic term *κ*, Helmholtz–Smoluchowski speed *U*hs, and nanoparticles (*NPs*) volume fractions  $(\phi_1, \phi_2)$  over the non-dimensional temperature feld. In Fig. [4a](#page-12-0), the fuctuation of Cu-Au/blood and Cu-blood temperature for intensifying magnetic parameter *M*<sup>2</sup> is manifested. It is worthy to note that both *Cu-Au*/blood and  $Cu$ -blood temperature elevates for when  $M^2$  enlarges. It is witnessed that the peak of the temperature distribution is

<span id="page-12-0"></span>



**(d)** Temperature profile for changing ξ

**(h)** Temperature profile for different type of blood

found at the center  $(r = 0)$  of the ciliary tube. Blood flow under a magnetic feld dissipates thermal energy and as a result, the temperature for both hybrid and nano-blood upsurges. An augmentation of hybrid and nano-blood temperature due to increasing strength of magnetic feld has tremendous application in hyperthermic treatment for cancerous cells. The sway of mounting Jeffrey parameter  $\lambda_1$  on both *Cu-Au*/blood and *Cu*-blood temperature is disclosed in Fig. [4b](#page-12-0). For  $\lambda_1$  < 1 (physiological fluids), the retardation time is higher than the relaxation time. An enhancement in  $\lambda_1$  enlarges the relaxation time which enriches the visco-elasticity of blood, and as an outcome, the temperature for both *Cu-Au*/blood and *Cu*-blood gets a diminution. The upshot due to an enhancement in Brinkman number *Br* on hybrid *Cu-Au*/blood and *Cu*-blood temperature is explored in Fig. [4](#page-12-0)c. An upliftment in *Br* receives a remarked attenuation in the temperature of blood. The Brinkman number is a physical function of the proportion of thermal energy yielded by viscous debauchery and heat transport by molecular colliding. For *Br <* 1, heat transport by molecular colliding is higher than heat produced via viscous dissipation. Therefore, incrementing *Br* reduces the impact of heat transit by molecular colliding and abates the temperature of blood. Figure [4d](#page-12-0) is divulged to outline the consequence of heat source term *𝜉* on both *Cu-Au*/blood and Cu-blood temperature. It is evident from these graphs that an upliftment in  $\xi$  yields more heat energy, which dramatically raises the blood temperature. To outline the upshot of  $U_{\text{hs}}$  over temperature, Fig. [4](#page-12-0)e is presented. It is remarked that both *Cu-Au*/blood and *Cu*-blood temperature tends to a declination for changing values from  $-3.5$  to  $-2.0$  of  $U_{\text{hs}}$ . A higher negative  $U_{\text{hs}}$  strongly assists the electro-osmotic body force which develops temperature profle. In Fig. [4f](#page-12-0), the iteration of both *Cu-Au*/blood and *Cu*-blood temperature for multiple values of electro-osmotic parameter  $\kappa$  is exposed. It infers that a higher value of  $\kappa$ attenuates the thickness of EDL which has a fourishing role in the enhancement of the temperature profle. According to the kinetic theory of molecules, kinetic energy and temperature are directly related. An inhomogeneous dispersion of electric potential within the hybrid nano-blood produces kinetic energy in the blood cells and nanoparticles, which tends to uplift the temperature profile when  $\kappa$  enlarges.

The fuctuation of temperature profle for multiple values of *NPs* volume fractions ( $\phi_1$  and  $\phi_2$ ) is designed in Fig. [4g](#page-12-0). It is worthy to record that improvement in  $\phi_1$  and  $\phi_2$  leads to an attenuation in the temperature of hybrid nano-blood. It is mechanically justifed since the scattering of dissimilar *NPs* is related directly to the thermal difusivity, which is the main reason for fast heat migration from the fow regime, resulting in a crucial reduction in the blood temperature. Due to a signifcant advancement in the thermophysical behavior of blood, the hybrid *NPs* concentration is preferred over the mono *NPs* concentration. As blood goes away from the ciliated vessel wall, *NPs* at the peripheral domain of the ciliated vessel heated up, the blood circulation enriches in the central domain of the ciliary blood vessel, and the temperature of blood subsequently diminishes. The alteration in the temperature for *Cu-Au*/blood, *Cu*-blood, *Au*-blood, and pure blood is interpreted via Fig. [4h](#page-12-0). It is remarked that *Cu-Au*/blood depicts supremacy toward other nano or pure blood. Furthermore, *Au NPs* have a significantly bigger atomic number, which causes a subsequent drop in blood temperature. So, *Au NPs* have higher thermal efficiency than *Cu NPs*. In case of hyperthermic therapy for cancerous cells, this output is extremely beneficial (*Au* NPs as a drug carrier).

#### **Pumping features**

#### **Axial pressure gradient**

Figure [5a](#page-14-0)–h is suggested to demystify the consequences of magnetic term  $M^2$ , Jeffrey term  $\lambda_1$ , thermal *Gr*, electroosmosis parameter  $\kappa$ ,  $U_{\text{hs}}$ , cilia length  $\delta$ , and *NPs* volume fractions ( $\phi_1$  and  $\phi_2$ ) on the fluctuation of the pressure gradient d*p*∕d*z*. The upshot of magnetic parameter *M*<sup>2</sup> via d*p*∕d*z* is revealed in Fig. [5a](#page-14-0). An intensifying  $M^2$  leads to boost up the drag force which tends to suppress the pressure gradient. In Fig. [5b](#page-14-0), the alteration of the pressure gradient d*p*∕d*z* for increasing Jeffrey parameter  $\lambda_1$  is exposed. An upsurge in  $\lambda_1$  decreases the retardation time which attenuates the elastic property of blood and consequently, d*p*∕d*z* gets an improvement. The variation of pressure gradient *dp*∕*dz* for increasing *Gr* is demonstrated in Fig. [5](#page-14-0)c. For growing *Gr*, a strong buoyancy force is expanded in the flow domain and consequently, thriving behavior is noted in d*p*∕d*z*.

Figure [5d](#page-14-0) is divulged to perceive the sway of electroosmotic term  $\kappa$  on d $p/dz$ . It discloses that  $\kappa$  has a diminutive impact on  $dp/dz$ . For an upliftment in  $\kappa$  (thin EDL), the electro-osmotic force (EOF) is mounted, which generates a substantial deterioration in the pressure gradient. This entails that ion difusion from the charged surface has a substantial impact on pumping characteristics. Graphs of Fig. [5e](#page-14-0) disclose that mounted  $U_{\text{hs}}$  amplifies the pressure gradient d*p*∕d*z*. It is inferred that more pressure gradient is perceived for weaker the axial electric feld in fow direction. Figure [5f](#page-14-0) is illustrated to explore the impression of cilia length  $\delta$  over  $dp/dz$ . It is noteworthy to record that cilia length  $\delta$  has a subsequent accentuation in d*p*∕d*z*. The growth of *NPs* volume fractions ( $\phi_1$  and  $\phi_2$ ) outcomes in a dramatic enhancement of d*p*∕d*z*, as shown in Fig. [5g](#page-14-0). This suggests that the abundance of hybrid *NPs* can signifcantly alter the pressure gradient. The pressure gradients of *Cu-Au*/blood, *Cu*-blood, *Au*-blood, and pure blood are compared in Fig. [5h](#page-14-0). These visualizations demonstrate that the pressure gradient for *Cu-Au*/blood is greater than *Cu*-blood, *Au*-blood, and pure blood.

#### **Pressure rise per wavelength**

One of the most signifcant physiological features in the peristaltic pumping process is the pressure rise Δ*P*. Figure [6a](#page-15-0)–h is portrayed to manifest the alteration of Δ*P* against the mean volumetric fow rate *F* for multiple values of  $M^2$ ,  $\lambda_1$ ,  $Gr$ ,  $\kappa$ , Helmholtz–Smoluchowski velocity  $U_{\text{hs}}$ , cilia length  $\delta$ , and *NPs* volume fractions ( $\phi_1$  and  $\phi_2$ ). Figure [6a](#page-15-0) reveals that pressure rise  $\Delta P$  has a waning nature with amplifying  $M^2$ . An intensified magnetic field can offer a surprising response to low blood viscosity, and consequently, a commensurate decrement in Δ*P* also affirms good agreement with the existing literature [[80](#page-24-6)]. Figure [6b](#page-15-0) is outlined for exploring the infuence of  $\lambda_1$  over  $\Delta P$ . An augmentation in  $\lambda_1$  leads to an improvement in viscosity of hybrid and nano-blood in the axial direction, which encourages the pressure rise Δ*P*. The variation of the pressure rise Δ*P* for multiple values of *Gr* is designed in Fig. [6c](#page-15-0). Physically, an enlargement in *Gr* induces a strong buoyancy force in the flow area, which

<span id="page-14-0"></span>

elevates the pressure rise. Figure [6d](#page-15-0) discloses the alteration of pressure rise  $\Delta P$  due to increasing electro-osmotic parameter  $\kappa$ . Higher  $\kappa$  improves the electrical potential which attenuates the pressure rise. Figure [6](#page-15-0)e exhibits the thriving behavior in Δ*P* for changing values −3.5 to  $-2$  of  $U_{\text{hs}}$ . For an ascent in  $U_{\text{hs}}$ , the axial electric field is remarkably boosted and as a result, Δ*P* evolves. Thus, the Helmholtz–Smoluchowski velocity  $U_{\text{hs}}$  can be designed to control the pumping features of EOFs. Figure [6](#page-15-0)f explores the depleting trends in  $\Delta P$  in the region ( $0 < F \le 1$ ) and it evolves in the rest with enlarging  $\delta$ . Figure [6g](#page-15-0) delineates that  $\delta$  strongly elevates with larger values of  $NPs$ volume fractions ( $\phi_1$  and  $\phi_2$ ). From the physical point of view, to pump the hybrid nano-blood with a higher concentration, more effort is required. A higher concentration of hybrid *NPs* leads to a higher increment in the pressure rise. Furthermore, Fig. [6](#page-15-0)h exposes the comparative studies of pressure rise Δ*P* for *Cu-Au*/blood, *Cu*-blood, *Au*-blood, and pure blood. Outcomes communicate that  $\Delta p_{\text{Cu-Au/blood}} > \Delta p_{\text{Au-blood}} > \Delta p_{\text{Cu-blood}} > \Delta p_{\text{Pure-blood}}$ 

<span id="page-15-0"></span>

There is an inversely linear relationship between Δ*p* and mean flow rate  $F$ . These findings are consistent with the physical predictions of the relevant parameters.

## **Wall share stress (WSS)**

Figure [7a](#page-16-0)–f is sketched to demystify the consequence of  $M^2$ ,  $\lambda_1$ , *Gr*,  $\kappa$ ,  $U_{\text{hs}}$ , and  $(\phi_1, \phi_2)$  via  $S_{\text{rz}}$  at the ciliary microvessel wall. From these figures, it is clear that WSS  $S_{rz}$ has an inverse deportment as compared to the pressure

rise. WSS  $S_{rz}$  on the micro-vessel tube wall is significantly enhanced for greater values of  $M^2$ ,  $U_{\text{hs}}$ ,  $\phi_1$ , and  $\phi_2$ ; however, an inverse outcome is tracked out for increasing  $\lambda_1$ , *Gr*, and  $\kappa$ , as shown in Fig. [7](#page-16-0)a–f. Higher  $M^2$  generates larger Lorentzian drag force which retards ciliary flow pressure rise and results in boosting WSS. It is detected that WSS exhibits monotonically increasing behavior with the mean fow rate *F*. The hybrid *Cu-Au*/blood fow accomplishes comparatively higher WSS as compared to *Cu*-blood.

<span id="page-16-0"></span>



#### **Heat transport coefficient**

The fluctuation of the heat transport coefficient  $Z^*$  at the ciliary micro-vessel wall for varying values of  $M^2$ ,  $\lambda_1$ ,  $U_{\text{hs}}$ ,  $\kappa$ , *Br*,  $\xi$ ,  $\delta$ ,  $\phi$ <sub>1</sub>, and  $\phi$ <sub>2</sub> is depicted in Fig. [8a](#page-17-0)–j. The heat transfer coefficient Z<sup>\*</sup> exposes a depleting nature for escalating estimation of  $M^2$ ,  $\lambda_1$ ,  $U_{\text{hs}}$ ,  $\kappa$ , and a reverse trend is tracked out for elevating *Br*,  $\xi$ ,  $\delta$ ,  $\phi$ <sub>1</sub>, and  $\phi$ <sub>2</sub>, as sketched in Fig. [8](#page-17-0)a–i. The magnetic feld reduces the intensity of ciliary movement at the vessel wall which decreases heat transfer coefficient  $Z^*$  3.7% for hybrid nano-blood and 12.4% for *Cu* nano-blood. From the physical point of view, higher negative  $U_{\text{hs}}$  strengthens the EOFs which compensate the frictional kinetic energy loss and boost the heat transfer coefficient  $Z^*$ . On another side, a thinner EDL (higher value of  $\kappa$ ) infers a lower velocity of blood pumping near the micro-vessel wall and as a result, it possesses a lower rate of heat transport. It is also depicted that due to changes of  $\kappa$  from 2.0 to 3.5,  $Z^*$  decreases 8.2% for

*Cu-Au*/blood and 19.8% *Cu*-blood, respectively. A elevated *Br* uplifts the kinetic energy of *NPs* which upsurge the heat transfer coefficient *Z*<sup>∗</sup> 65.7% for *Cu-Au*/blood and 45.6% for *Cu* nano-blood. The ionic hybrid or nano-blood in the micro-vessel is energized with upswing heat source parameter *𝜉*, due to which *Z*<sup>∗</sup> surges 26.9% for *Cu-Au*/blood and 28.8% Cu-blood, respectively. This propensity of heat generation could be efficient in the treatment of thermal therapy. The process of heat transfer is accentuated due to higher alteration in pressure gradient by larger  $\delta$ . The *NPs* volume fractions are directly related to the thermal difusion of the hybrid or nano-blood, which assists the quick transfer process of heat from the flow domain. Consequently, an enlargement in  $\phi_1$  or  $\phi_2$  leads to upliftment in the process of heat transport. The outcomes of Fig. [8j](#page-17-0) conclude that  $Z_{\text{Pure blood}}^* < Z_{\text{Cu–blood}}^* < Z_{\text{Au–blood}}^* < Z_{\text{Cu–Au/blood}}^*$ . Due to the higher atomic number of *Au NPs* as compared to *Cu NPs, Au*-blood possesses relatively more heat





<span id="page-17-0"></span>Fig. 8 Evolution of heat transport coefficient  $Z^*$  for various physical terms  $\alpha = 0.1$ ,  $\beta = 0.2$ ,  $F = 0.5$ ,  $Gr = 2.0$ , and (a)  $\lambda_1 = 0.6, U_{\text{hs}} = -2.0, \ \kappa = 3.0, \ \text{Br} = 0.1, \ \xi = 1.0, \ \delta = 0.1, \ z = 0.3,$  $\phi_1 = \phi_2 = 0.02$ , (b)  $M^2 = 1.0$ ,  $U_{\text{hs}} = -2.0$ ,  $\kappa = 3.0$ ,  $Br = 0.1$ ,  $\xi = 1.0, \delta = 0.1, z = 0.3, \phi_1 = \phi_2 = 0.02, \text{ (c)}$   $M^2 = 1.0, \lambda_1 = 0.6,$  $\kappa = 3.0, \; Br = 0.1, \; \xi = 0.1, \; \delta = 0.1, \; z = 0.7, \; \phi_1 = \phi_2 = 0.02, \;$  (d)  $M^2 = 1.0$ ,  $\lambda_1 = 0.6$ ,  $U_{\text{hs}} = -2.0$ ,  $Br = 0.1$ ,  $\xi = 1.5$ ,  $\delta = 0.1$ ,  $z = 0.3$ ,  $\phi_1 = \phi_2 = 0.02$ , (e)  $M^2 = 1.0$ ,  $\lambda_1 = 0.6$ ,  $U_{hs} = -2.0$ ,  $\kappa = 2.0$ ,

 $\xi = 0.5, \delta = 0.1, z = 0.3, \phi_1 = \phi_2 = 0.02, (f)$   $M^2 = 1.0, \lambda_1 = 0.6,$  $U_{\text{hs}} = -2.0, \, \kappa = 3.0, \, Br = 0.1, \, \delta = 0.1, \, z = 0.3, \, \phi_1 = \phi_2 = 0.02, \, \text{(g)}$  $\overline{M^2} = 1.0, \ \lambda_1 = 0.6, \ U_{\text{hs}} = -2.0, \ \kappa = 3.0, \ Br = 0.1, \ \xi = 1.0, \ z = 0.3,$  $\phi_1 = \phi_2 = 0.02$ , (h)  $M^2 = 1.0$ ,  $\lambda_1 = 0.6$ ,  $U_{\text{hs}} = -2.0$ ,  $\kappa = 3.0$ , *Br* = 0.1,  $\xi$  = 1.0,  $\delta$  = 0.1,  $z$  = 0.35,  $\phi$ <sub>2</sub> = 0.02, (i)  $M^2$  = 1.0,  $\lambda_1 = 0.6, U_{\text{hs}} = -2.0, \ \kappa = 3.0, \ Br = 0.1, \ \xi = 1.0, \ \delta = 0.1, \ z = 0.35,$  $\phi_1 = 0.02$ , (j)  $M^2 = 1.0$ ,  $\lambda_1 = 0.6$ ,  $U_{\text{hs}} = -2.0$ ,  $\kappa = 3.0$ ,  $Br = 0.1$ ,  $\xi = 2.0, \delta = 0.1, z = 0.35$ 



(c) 
$$
\lambda_1 = 0.3
$$





<span id="page-18-0"></span>**Fig. 9** Streamlines for different physical parameters  $\alpha = 0.1$ ,  $\beta = 0.2$ ,  $F = 0.5$ ,  $Br = 0.1$ ,  $\xi = 0.5$ , and (a)&(b)  $\lambda_1 = 0.6$ ,  $Gr = 1.0$ ,  $\kappa = 2.0$ ,  $U_{hs} = -2.0, \ \delta = 0.1, \ \xi = 0.5, \ \phi_1 = \phi_2 = 0.02, \ \text{(c)}\&\text{(d)} \ \ M^2 = 1.0,$  $Gr = 1.0, \ \kappa = 2.0, \ \ U_{hs} = -2.0, \ \ \delta = 0.1, \ \ \xi = 0.5, \ \ \phi_1 = \phi_2 = 0.02,$ (e)&(f)  $M^2 = 1.0$ ,  $\lambda_1 = 0.6$ ,  $\kappa = 2.0$ ,  $U_{hs} = -2.0$ ,  $\delta = 0.1$ ,  $\xi = 0.5$ ,  $\phi_1 = \phi_2 = 0.02$ , (g)&(h)  $M^2 = 1.0$ ,  $\lambda_1 = 0.6$ ,  $Gr = 1.0$ ,  $U_{hs} = -2.0$ ,

 $\delta = 0.1, \quad \xi = 0.1, \quad \phi_1 = \phi_2 = 0.02, \quad \text{(i)}\&\text{(j)} \quad M^2 = 1.0, \quad \lambda_1 = 0.6,$ *Gr* = 1.0,  $\kappa = 3.0$ ,  $\delta = 0.1$ ,  $\xi = 0.5$ ,  $\phi_1 = \phi_2 = 0.02$ , (k)&(l)  $M^2 = 1.0$ ,  $\lambda_1 = 0.6$ ,  $Gr = 1.0$ ,  $\kappa = 2.0$ ,  $U_{hs} = -2.0$ ,  $\phi_1 = \phi_2 = 0.02$ , (m)&(n)  $M^2 = 1.0$ ,  $\lambda_1 = 0.6$ ,  $Gr = 1.0$ ,  $\kappa = 2.0$ ,  $U_{hs} = -2.0$ ,  $\delta = 0.1$ ,  $\xi = 0.5(0)$  *M*<sup>2</sup> = 1.0,  $\lambda_1 = 0.6$ , *Gr* = 1.0,  $\kappa = 2.0$ ,  $U_{hs} = -2.0$ ,  $\delta = 0.1, \xi = 0.5, \phi_1 = \phi_2 = 0.0 \phi_1 = \phi_2 = 0.0$ 



**Fig. 9** (continued)

migration than *Cu*-blood or pure blood, whereas the supreme heat transport process is observed for hybrid *Cu*-*Au*/blood.

### **Streamlines pattern**

The velocity vectors in a flow domain are mechanically coupled via streamlines. Indeed, the existence of a stagnation point causes streamlines to separate and construct an enveloping bolus of fluid. In a metachronal wave propagation, the development of bolus and the split-up of streamlines are known as trapping phenomena. Figure [9](#page-18-0)a–o explores the insight into the modifcation in the development of bolus and streamline confgurations under the variations of  $M^2$ ,  $\lambda_1$ ,  $Gr$ ,  $\kappa$ ,  $U_{\text{hs}}$ ,  $\delta$ ,  $\phi_1$ , and  $\phi_2$ . Figure [9a](#page-18-0)–b is demonstrated to unveil the streamlines pattern for  $M^2$ . With changing  $M^2$ , there is a slight change in bolus structure. To explore the impressions of Jefrey parameter  $\lambda_1$  on streamline structures, Fig. [9](#page-18-0)c–d is manifested. There is a major modifcation in size and number of entrapped boluses for a higher estimation of  $\lambda_1$ . It is attributed that a higher Jefrey parameter enlarges the size and number of trapped boluses. The impact of *Gr* on streamlines is presented in Fig. [9](#page-18-0)e–f. It is noteworthy here that with an elevation in *Gr*, the entrapped bolus is amended in size and number. The upshot of  $\kappa$  over streamlines is delineated in Fig.  $9g-h$ . An amendment in  $\kappa$  expands the entrapped bolus in size as well as in number. Figure  $9i-j$  $9i-j$ is designed to assess the variation in streamline modifcation with Helmholtz–Smoluchowski velocity  $U_{\text{hs}}$ . There is a contraction in size and number of streamlines under the changes of  $U_{\text{hs}}$  from  $-3$  to  $-2$ . The alternation of the entrapped bolus is signifcantly attenuated by increasing cilia length  $\delta$ , as shown in Fig. [9k](#page-18-0)–l. Figure [9m](#page-18-0)–o portends the comparison of captured streamlines for *Cu-Au*/ blood, *Cu*-blood, and pure blood. It is perceived that there is no signifcant alteration in streamlines for hybrid or nano-blood but a contraction in size and number of the entrapped bolus is exposed in the case of pure blood.

# **Conclusions**

In this research article, a new mathematical scheme is prepared for the electro-magneto-hydrodynamic flow of ionized non-Newtonian blood injected through *Cu–Au NPs* via a vertical ciliated micro-vessel with peristaltic waves. To capture the non-Newtonian rheological attributes of the hybrid nano-blood, Jeffrey liquid model is fitted. The mathematical representations are simplified via Debye–Hückel linearization and lubrication postulates. The analytic estimation for electric potential is tracked out in terms of Bessels functions. The estimated power series solutions of the associated nonlinear coupled flow equations are computed employing homotopy

perturbation method. The significant influences of evolving physical terms toward the axial distribution of the blood temperature and velocity, WSS, axial pressure gradient, pressure rise per wavelength, heat transport coefficient, and streamlines pattern have been evidenced and anatomized. The noteworthy outcomes turned out from this graphical illustration are epitomized as:

- A higher assisting the electro-osmotic force and thin EDL signifcantly hinder the blood motion nearby the ciliary micro-vessel wall.
- Enhancement in Jefrey parameter or Grashof number boosts up the blood velocity, whereas magnetic feld or cilia length yields a perceptible attenuation in the central area of the micro-vessel.
- The blood in the flow conduit is remarkably energized due to an elevation in heat source parameter, while reverse propensity is tracked out due to Jefrey parameter, Brinkman number, and *NPs*' volume fractions.
- The temperature of hybrid nano-blood is greater than nanoblood or pure blood.
- The pressure gradient is abated for the assisting electroosmotic force and thin EDL, while it is important through higher values of Jefrey term or cilia length.
- The heat transfer coefficient surges 26.9% for *Cu-Aul*blood and 28.8% *Cu*-blood with changing estimation of heat source term from 0.5 to 2.0.
- The heat exchange rate for hybrid nano-blood (26% for *Cu-Au*/blood) is greatly evaluated to nano-blood (20% for Au-blood and 11.4% for Cu-blood).

Outcomes obtained in this hemodynamic investigation are very productive for deeper insights into EDL phenomena in the EMHD flow of ionized blood doped with copper and gold nanoparticles via a ciliated micro-vessel. This novel model can be applicable in muco-ciliary clearance processes of respiratory systems, biomicro-electro-mechanical systems, hemodynamic therapies, simulations of chirurgical treatments, and medical engineering.

# **Appendix A:**

$$
X = -\frac{2\pi\alpha\beta\delta\cos 2\pi z}{1 - 2\pi\alpha\beta\delta\cos 2\pi z} - 1,
$$

$$
A_1 = X + \frac{a_0}{k^4} (a_2 + k^2) I_0(hk),
$$

$$
A_2 = \frac{1}{256} \left[ \frac{64}{k^2} a_0 a_2 I_0(hk) - a_1 \left\{ -16h^2 (a_2 - a_5 - 1) + a_4 \left( \frac{dp}{dz} \right)^2 h^4 (1 + \lambda_1)^2 + 64 \right\} + a_2^2 h^2 \left\{ 3 \frac{dp}{dz} h^2 (1 + \lambda_1) - 16(1 + X) \right\} - 16a_2 (a_3 h^2 - 4(1 + X)) + 64a_3 \right],
$$

$$
A_3 = \frac{1}{256} [4a_1(-a_2 + a_5 + 1)
$$
  
\n
$$
+a_2 \left\{ -a_2 \frac{dp}{dz} h^2 (1 + \lambda_1) + 4a_2 (X + 1) + 4a_3 \right\} \Big],
$$
  
\n
$$
A_4 = \frac{1}{2304} (1 + \lambda_1) \frac{dp}{dz} \left\{ a_1 a_4 \frac{dp}{dz} (1 + \lambda_1) + a_2^2 \right\},
$$
  
\n
$$
A_5 = -\frac{a_0}{k^4} (a_2 + k^2),
$$
  
\n
$$
A_6 = -\frac{a_5}{4},
$$
  
\n
$$
A_7 = \frac{1}{128} a_4 \frac{dp}{dz} (1 + \lambda_1) \Big[ 4a_1 + a_2 \frac{dp}{dz} h^2 (1 + \lambda_1) - 4a_2 (X + 1) + 2 \Big( -2a_3 + \frac{dp}{dz} (1 + \lambda_1) \Big) \Big]
$$
  
\n
$$
A_8 = -\frac{1}{576} a_2 a_4 \Big( \frac{dp}{dz} \Big)^2 (1 + \lambda_1)^2,
$$
  
\n
$$
A_9 = \frac{a_0 a_4}{k^4} \frac{dp}{dz} (1 + \lambda_1),
$$
  
\n
$$
B_1 = \frac{5}{3072} \pi a_1 a_4 h^8 (1 + \lambda_1)^2,
$$
  
\n
$$
B_2 = \frac{1}{3072 \pi_1} \pi h^4 (1 + \lambda_1) [a_2 h^2 (11a_2 h^2 x_1 - 64) + 384],
$$
  
\n
$$
B_3 = \frac{1}{8k^5} \pi a_0 h \Big[ h k \{k^2 (8 - a_2 h^2) + 8a_2 \} I_0(hk) -16(a_2 + k^2) I_1(hk) \Big]
$$
  
\n
$$
\frac{1}{48} \pi h^4 \{a_1 (h^2 (-a_2 + a_5 + 1) + 6) + a_2 (X + 1) (a_2 h^2 - 6) \} + \pi h^2 X - Q
$$

# **Appendix B: Summary of Some important formulas:**

(1) The constitutive formulas for the extra-stress tensor *S̃* in Jefrey fuid model in component form are as:

$$
\tilde{S}_{\tilde{R}\tilde{R}} = \frac{2\mu_{\text{Inf}}}{1 + \lambda_1^*} \left[ 1 + \lambda_2 \left( \tilde{U} \frac{\partial}{\partial \tilde{R}} + \tilde{W} \frac{\partial}{\partial \tilde{Z}} \right) \right] \frac{\partial \tilde{U}}{\partial \tilde{R}},
$$

$$
\tilde{S}_{\tilde{R}\tilde{Z}} = \tilde{S}_{\tilde{Z}\tilde{R}} = \frac{\mu_{\text{hnf}}}{1 + \lambda_1^*} \left[ 1 + \lambda_2 \left( \tilde{U} \frac{\partial}{\partial \tilde{R}} + \tilde{W} \frac{\partial}{\partial \tilde{Z}} \right) \right] \left( \frac{\partial \tilde{U}}{\partial \tilde{Z}} + \frac{\partial \tilde{W}}{\partial \tilde{R}} \right)
$$
\n
$$
\tilde{S}_{\tilde{\theta}\tilde{\theta}} = \frac{2\mu_{\text{hnf}}}{1 + \lambda_1^*} \left[ 1 + \lambda_2 \left( \tilde{U} \frac{\partial}{\partial \tilde{R}} + \tilde{W} \frac{\partial}{\partial \tilde{Z}} \right) \right] \left( \frac{\tilde{U}}{\tilde{R}} \right),
$$
\n
$$
\tilde{S}_{\tilde{Z}\tilde{Z}} = \frac{2\mu_{\text{hnf}}}{1 + \lambda_1^*} \left[ 1 + \lambda_2 \left( \tilde{U} \frac{\partial}{\partial \tilde{R}} + \tilde{W} \frac{\partial}{\partial \tilde{Z}} \right) \right] \frac{\partial \tilde{W}}{\partial \tilde{Z}},
$$
\n(2) The electric potential  $\tilde{\Phi}$  across the EDL is expre

pressed as follows  $[15, 70]$  $[15, 70]$  $[15, 70]$ :

$$
\nabla^2 \tilde{\Phi} = -\frac{\rho_e}{\varepsilon_0},
$$

(3) In a unit volume of the ionic blood, the electric charge density is rewritten as:

$$
\rho_{\rm e} = -2n_0 e \bar{z} \sinh\left(\frac{e \bar{z} \tilde{\Phi}}{K_{\rm B} T_{\rm a}}\right).
$$

(4) The simplifed Poisson–Boltzmann equation is as:

$$
\nabla^2 \tilde{\Phi} = \frac{2n_0 e \bar{z}}{\epsilon_0} \sinh\left(\frac{e \bar{z} \tilde{\Phi}}{K_{\rm B} T_{\rm a}}\right),\,
$$

(5) Debye–Hückel linearization approximation: When the thermal energy of the ions is greater than the electric poten- $\text{trial energy, i.e.,} |e\overline{z}\tilde{\Phi}| \ll |K_{\text{B}}T_{\text{a}}|$  $\vert$ , then  $\vert$ *ez*Φ*̃*  $\frac{\epsilon_{\rm s}\Phi}{K_{\rm B}T_{\rm a}}$ *≪* 1; accordingly  $\sinh\left(\frac{e\overline{z}\Phi}{K_{\mathrm{B}}T_{\mathrm{a}}}$  $\left( \alpha \right) \approx \frac{e\overline{z}\Phi}{K_{\textrm{B}}T_{\textrm{a}}}.$ 

(6) Adopting Debye–Hückel linearization approximation, Poisson–Boltzmann equation is:

$$
\frac{1}{\tilde{R}}\frac{\partial}{\partial}\left(\tilde{R}\frac{\partial\tilde{\Phi}}{\partial\tilde{R}}\right) + \frac{\partial^2\tilde{\Phi}}{\partial\tilde{Z}^2} = \frac{1}{\lambda_{\rm D}^2}\tilde{\Phi}.
$$

**Acknowledgements** The authors would like to thank the Deanship of Scientifc Research at Umm Al-Qura University for supporting this work via Grant Code: (22UQU4240002DSR14). The author (Alok Barman) gratefully acknowledges the funding of this research work by the University Grants Commission (UGC), India [Grant no.: Id.1245/(CSIRUGCNET2019)]. Also, we are thankful to the Editor and anonymous reviewers for their precious comments and suggestions in improving the quality of this article.

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