

Computational study on the efects of variable viscosity of micropolar liquids on heat transfer in a channel

Shahid Rafq¹ [·](http://orcid.org/0000-0002-2562-4595) Zaheer Abbas1 · Muhammad Nawaz2 · Sayer Obaid Alharbi3

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Abstract

A numerical model is developed to study the efects of temperature-dependent viscosity on heat transfer in magnetohydrodynamic fow of micropolar fuid in a channel with stretching walls. The governing equations for linear and angular momenta and energy are transformed to a set of nonlinear ordinary diferential equations by using similarity variables, and resulting problems are solved numerically by quasi-linearization. The efects of the various physical parameters on velocity, microrotation and temperature profles are presented graphically and numerically. Finally, the efects of pertinent parameters on local skin-friction coefficient and local Nusselt number are also presented graphically. Some important observations regarding the efect of vortex viscosity parameter, microinertia density parameter, spin gradient viscosity parameter and couple stress on fow felds are noted and displayed. Numerical values of shear stress, couple stress and heat fux are computed and tabulated. The viscosity variation parameter enhances the shear stress and the couple stress. However, the heat transfer exhibits an opposite trend. The viscosity parameter is the most infuential on thermal distribution. The magnetic feld acts as a retarding force which reduces the normal and streamwise velocities as well as the microrotation distribution

Keywords Variable viscosity · Magnetohydrodynamics (MHD) · Non-Newtonian · Viscous dissipation · Order reduction

List of symbols

μ_0	Characteristic viscosity (kg m ⁻¹ s ⁻¹)
σ	Electric conductivity $(s m^{-1})$
ρ	Fluid density (kg m^{-3})
\boldsymbol{p}	Fluid pressure (kg m ⁻¹ s ⁻²)
$T_{\rm f}$	Fluid temperature (K)
$q_{\rm w}$	Heat flux (kg s^{-3})
\mathbf{v}	Kinematic viscosity ($m^2 s^{-1}$)
B_0	Magnetic field intensity $(m^{-1} A)$
\dot{i}	Microinertia per unit mass $(m2)$
	Microrotation component (s^{-1})
K	Porous permeability (m^2)
T_1, T_2	Reference fluid temperatures (K)

 \boxtimes Shahid Rafiq sheenshahid@gmail.com

- ² Department of Applied Mathematics and Statistics, Institute of Space Technology Islamabad, Islamabad, Pakistan
- ³ Department of Mathematics, College of Science Al-Zulfi, Majmaah University, Al Majma'ah 11952, Saudi Arabia
- τ_w Shear stress (kg m⁻¹ s⁻²)
- c_p Specific heat (J kg⁻¹ K⁻¹)
- *b* Stretching rate (m)
- k_0 Thermal conductivity (W m⁻¹ K⁻¹)
- κ Vortex viscosity (Pa s)
- 2*c* Width of channel (m)
- $u, v \, x$ and *y* component of velocity (m s⁻¹)

Non‑dimensional quantities

- $C_{\rm g}$ Couple stress coefficient
- Ec Eckert number
- *M* Magnetic feld parameter
- *g* Microrotation
- *f* Normal velocity
- *f* ′ Stream velocity,
- θ Temperature
- Nu Nusselt number
- *N*₂ Parameter for microinertia density
- *N*₃ Parameter for skin gradient viscosity
- *N*₁ Parameter for vortex viscosity
- Pr Prandtl number,
- Re Reynolds number
- *n* Similarity variable
- C_f Skin friction coefficient
- *γ* Spin gradient viscosity

 1 Department of Mathematics, The Islamia University of Bahawalpur, Bahawalpur 63100, Pakistan

- *δ* Viscosity variation constant
- ϵ Viscosity variation parameter

Introduction

Heat transfer in fuid occurs in industrial applications. The efficiency of thermal and cooling system involves heat transfer in fuid that depends upon the thermal conductivity of fuids. Therefore, thermal enhancement has been studied in many recent investigations. For instance, Sheikholeslami [[1\]](#page-9-0) performed a computational analysis for an enhancement of heat transfer in fuid by suspension of nanoparticles. Sheikholeslami et al. [[2](#page-9-1)] did an experimental study for the application of nano-refrigerant for boiling of heat transfer in fuid fows. Sheikholeslami et al. [\[3](#page-9-2)] investigated an enhancement of heat transfer in fuid in a heat storage unit containing nanoparticles and cooling fn. Sheikholeslami and Ghasemi [[4\]](#page-9-3) performed heat transfer simulations in the presence of thermal radiation via fnite element method (FEM). Sheikholeslami and Seyednezhed [[5\]](#page-9-4) analyzed the impact of suspension of nano-structures on transport of heat energy in convective transport of momentum in fuid immersed in porous medium. Sheikholeslami and Rashid [\[6](#page-9-5)] analyzed heat transfer in Ferro fluid exposed to variable magnetic feld. Dogonchi et al. [[7\]](#page-9-6) performed numerical analysis of thermal performance of nanoparticles on transport of heat transfer in fuid flled in a cavity. Dogonchi et al. [\[8\]](#page-9-7) discussed natural convection on square enclosure with wavy circular heater exposed to magnetic feld. Hashemi-Tilehnoee [\[9](#page-9-8)] studied factors afecting entropy generation in fuid exposed to magnetic feld. By considering various shapes for nanoparticles, Sheikholeslami [\[10](#page-9-9)] investigated the infuence of magnetic feld on fow in a permeable cavity. MHD flow of Al_2O_3 -water nanofluid inside a permeable medium also studied by Sheikholeslami [\[11](#page-9-10)]. Selimefendigil et al. [\[12](#page-9-11)] investigated MHD *CuO*-water fow of nanofuid with forced convection in channel. Selimefendigil and Hakan [[13](#page-9-12)] studied mixed convection corrugation type effects through vented cavity for fuid-solid interaction. Turkyilmazoglu [[14\]](#page-9-13) presented a numerical study, in which he discussed laminar (MHD) flow of an electrically conducting fluid on a stretchable disk. Hayat $[15]$ $[15]$ analytically presented heat transfer for two-dimensional MHD flow of Maxwell fuid (with viscosity and relaxation time depending upon the pressure. A comprehensive literature review on exact solutions of Navier–Stokes equations were studied by Aristov et al. [[16](#page-9-15)]. Malik et al. [[17\]](#page-9-16) investigated two-dimensional MHD flow of the Carreau fluid over a stretching sheet with a variable thickness. The problem (MHD) steady fow and heat transfer of an incompressible (non-Newtonian fuid)

that are macromolecular in nature and their resemblance with an elastic solid were solved numerically by Misra [\[18](#page-9-17)].

Many researchers are familiar by the practical applications of the non-Newtonian fuids. In industry, non-Newtonian fuids got much importance due to their usage in modern technology but on the other hand such fuids must be investigated to get the desired results. Due to complexity of these fuids, many models have been anticipated. Among them, micropolar model is the prominent. Blood, polymers and many industrial liquids containing crystals and microsolid structures are examples of micropolar fuid. For the modeling of heat transfer one additional law, the law of conservation of angular momentum is used along with a usual conservation laws. Micro-rotation in micro-polar fuid is due to couple stress. Further, vortex viscosity and spin gradient viscosities are also signifcant in such fuid. Due to its diversity from other fuids, many researchers have discussed various aspects of this rheology. For example, Fabula and Hoyt [[19\]](#page-9-18) claimed that micropolar fuid cannot be explained and characterized by those fuids that cannot be explained and characterized by Newtonian relationship they could be explained by micro-polar model which was later introduced by Eringen [\[20](#page-9-19)] was frst to introduce set of balance laws of micropolar fuid. Laminar incompressible fow of a micropolar fuid between two disks was studied by Kamal [\[21](#page-9-20)]. Magnetohydrodynamics (MHD) flow and heat transfer characteristics of a viscous incompressible electrically conducting micropolar fuid in a channel with stretching walls was studied by Ashraf et al. [\[22\]](#page-9-21). The characteristics of melting heat transfer in a boundary layer fow of the Jefrey fuid near the stagnation point on a stretching sheet subject to an applied magnetic feld was discussed by Nawaz et al. [\[23](#page-9-22)]. Some new strategies for the exact solutions for three-dimensional thermal difusion equations are introduced, and several cases were discussed in a most recent studies by Aristov and Prosviryakov [[24\]](#page-9-23) and new classes of exact solutions of Euler equations derived by Aristov and Polyanin [[25\]](#page-9-24).

Despite the fact of importance of exact solution, here numerical method is used; exact solution is not possible to fnd. Most of the studies on transport mechanism deal with constant viscosity. This assumption is valid to some rare cases. However, in general, viscosity does not remain constant in fuid fowing in the pressure of thermal changes. In view of this, several investigations have been published [[26–](#page-9-25)[31\]](#page-10-0). Further, these studies confirmed that the effect on the fow characteristics might change drastically in comparison with the constant viscosity assumption.

Moreover, MHD flow and heat transfer in viscoelastic fuid over a stretching sheet in the presence of variable viscosity and thermal conductivity are studied by Salem [[32\]](#page-10-1). Also, the problem of thermal-diffusion and diffusion thermo effects on mixed free-forced convection and mass transfer boundary layer fow of non-Newtonian fuid with temperature-dependent viscosity was studied numerically by Eldabe and Mohamed [[33](#page-10-2)], using Chebyshev fnite diference method. Moreover, Seddeek and Salama [[34\]](#page-10-3) studied the effects of variable viscosity and thermal conductivity on an unsteady two-dimensional laminar fow of viscous incompressible conducting fuid past a semi-infnite vertical porous moving plate taking into account the efect of a magnetic feld in the presence of variable suction.

Most of the studies on micropolar fuid consider viscosity of fuid to be constant. This assumption is not realistic, and imposition of this assumption of constant viscosity leads to physically unrealistic outcomes as blood and polymers do not posses constant viscosity. In general, such fuids have temperature-dependent viscosity. In view of this strong observation, authors have considered viscosity of micropolar fuid as a function of temperature of fuid itself. Further Ashraf et al. [\[22](#page-9-21)] have considered constant viscosity while analyzing heat transfer in a micropolar fuid in a channel. We have extended it the case of temperature-dependent viscosity. Hence, based on above discussion, the present work is an attempt to study the efects of variable viscosity on hydromagnetic fow and heat transfer characteristics of a micropolar non-Newtonian fuid in a channel with stretching walls. The governing equations reduced to similarity boundary layer equations by using suitable transformations. The transformed ordinary diferential equations together with the associated boundary conditions are discretized by the central fnite diferences and solved numerically. Numerical results are shown graphically for the velocity, angular velocity, temperature and concentration distributions.

Mathematical formulations

Consider heat transfer in steady two-dimensional hydromagnetic fow of micropolar fuid in a channel with stretching walls in the presence of a transverse applied magnetic feld. The induced magnetic feld is negligible as compared to the imposed magnetic feld under the assumption of small magnetic Reynolds number [\[35\]](#page-10-4). Hence, the magnetic feld will tend to relax towards a purely diffusive state, for small magnetic Reynolds numbers. Moreover, it is assumed that the electric feld vanishes as there is no applied polarization voltage. Microrotation due to solid like structures in the colloidal suspension (called micropolar fuid) is signifcant. The walls of channel of width 2*c* are located at $y = -c$ and $y = c$ as shown in Fig. [1](#page-2-0). The upper and lower walls of channel have constant temperature T_2 and T_1 respectively. Micropolar fuids exhibit Ohmic dissipation (Joule heating phenomenon) when they move under the infuence of applied magnetic feld so Joule heating efects are considered.

Fig. 1 Flow configuration and coordinates system

The unknown flow fields are

$$
\mathbf{V} = [u(x, y), v(x, y), 0], \quad \mathbf{N} = [0, 0, \phi(x, y)], \quad T_{\mathbf{f}} = T_{\mathbf{f}}(x, y)
$$
(1)

where ϕ is the component of the microrotation field normal to the *xy*-plane, whereas the microrotation is defned as the rotation of the microscopic particles in the fuid.

Laws of conservation of mass, linear momentum, angular momentum and energy ([[36](#page-10-5)[–38\]](#page-10-6)) become

$$
\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0,\tag{2}
$$

$$
u\frac{\partial u}{\partial x} + v\frac{\partial u}{\partial y} = -\frac{1}{\rho}\frac{\partial p}{\partial x} + \frac{1}{\rho}\nabla^2\left[(\mu(T_f) + \kappa)u \right] + \frac{\kappa}{\rho}\frac{\partial \phi}{\partial y} - \frac{\sigma B_0^2}{\rho}u,
$$
\n(3)

$$
u\frac{\partial v}{\partial x} + v\frac{\partial v}{\partial y} = -\frac{1}{\rho}\frac{\partial p}{\partial y} + \frac{1}{\rho}\nabla^2\left[(\mu(T_f) + \kappa)v \right] - \frac{\kappa}{\rho}\frac{\partial \phi}{\partial x},\qquad(4)
$$

$$
\rho j \left(u \frac{\partial \phi}{\partial x} + v \frac{\partial \phi}{\partial y} \right) = \gamma \nabla^2 \phi + \kappa \left(\frac{\partial v}{\partial x} - \frac{\partial u}{\partial y} \right) - 2\kappa \phi, \tag{5}
$$

$$
\rho c_p \left(u \frac{\partial T_f}{\partial x} + v \frac{\partial T_f}{\partial y} \right) = \kappa_0 \frac{\partial^2 T_f}{\partial y^2} + \sigma (B_0 u)^2, \tag{6}
$$

where κ is the vortex viscosity, ρ is the density, p is the pressure, γ is the spin gradient viscosity, B_0 is the strength of the magnetic field, *j* is the microinertia density, c_p is the specific heat at constant pressure, σ is the electrical conductivity, T_f is the temperature of the fluid and κ_0 is the thermal conductivity. The intensity of the inertial forces due to the microparticles of the fuid is known as microinertia density. Further, it is worth mentioning that for κ (vortex viscosity) is equal to zero the governing PDEs (2) (2) – (6) (6) reduce to governing PDEs for heat transfer in MHD Newtonian fuid.

The boundary conditions for the velocity, microrotation and temperature felds for the present problems are:

$$
u = bx
$$
, $v = 0$, $\phi = 0$ at $y = \pm c$
\n $T_f = T_1$ at $y = -c$
\n $T_f = T_2$ at $y = c$ (7)

 $\overline{ }$

Here, *b* is the positive constant and has dimension, reciprocal of the dimension of time.

In this stage, the following similarity variables are defned to convert the governing partial diferential Eqs. (2) (2) – (6) (6) (6) into the ordinary differential equations:

$$
u = bxf'(\eta), \quad v = -bcf(\eta), \quad \eta = \frac{y}{c},
$$

\n
$$
\phi = -\frac{b}{c}xg(\eta), \quad \theta(\eta) = \frac{T_f - T_2}{T_2 - T_1}.
$$
\n(8)

Microrotations are signifcant in micropolar liquid. Blood and other industrial fuids are examples of such fuids. It is theoretically and experimentally verifed that the viscosity of such fuid does not remain constant when thermal changes occurs. Due to this fact, the viscosity of such fuids depends on temperature. There are more than one mathematical model for temperature-dependent viscosity. Most commonly used model Ling and Dybbs [\[39](#page-10-7)] is

$$
\mu(T_{\rm f}) = \frac{\mu_o}{1 + \delta(T_{\rm f} - T_{\infty})} = \frac{\mu_o}{1 + \epsilon \theta}, \text{with } \epsilon = \delta(T_2 - T_1)
$$
\n(9)

Here ϵ is the viscosity variation parameter, μ_o is the constant dynamic viscosity, θ is the dimensionless temperature and δ is the viscosity variation constant.

Using change of variables given in Eq. [\(8\)](#page-3-0) in conservation laws (2) (2) – (7) (7) (7) and eliminating the pressure, one gets,

Newtonian case and for $\epsilon = 0$ and Ec = 0, reduces to non-Newtonian case, discussed by Ashraf et al. [[22\]](#page-9-21).

The skin friction coefficient is defined by

$$
C_{\rm f} = \frac{(\mu(T_{\rm f}) + \kappa) \frac{\partial u}{\partial y}|_{y=\pm c}}{\frac{1}{2}\rho(bx)^2}
$$

=
$$
\left(\frac{2c}{x\text{Re}}\right)\left(\frac{1}{1+\epsilon\theta(\pm 1)} + N_1\right)f''(\pm 1)
$$
 (13)

Coupled stress coefficient is defined as

$$
C_{g} = \frac{x\gamma \frac{\partial \phi}{\partial y}|_{y=\pm c}}{\frac{1}{2}\rho(bx)^{2}} = 2jN_{3}g'(\pm 1)
$$
 (14)

Similarly Nusselt number is defned as

$$
Nu = \frac{-xk_0 \frac{\partial T_f}{\partial y}|_{y=\pm c}}{k_0(T_2 - T_1)} = -\left(\frac{x}{c}\right)\theta'(\pm 1)
$$
(15)

Further, it can be noted that for $\epsilon = 0$, problem reduces to the case of constant viscosity, whereas $N_1 = 0$ is the case of Newtonian fluid. So $\epsilon = 0$, Ec = 0 is the case studied by Ashraf et al. [\[22](#page-9-21)] .

Solution procedure

The governing boundary value problems (10) (10) – (12) (12) (12) are solved numerically by employing a computational meth-

$$
(1+N_1)f'''' - N_1g'' = 2\left(\frac{\epsilon}{1+\epsilon\theta}\right)^2(\theta')^2f'' - \left(\frac{\epsilon}{1+\epsilon\theta}\right)\theta''f'' + \text{Re}\{f'f'' - ff'''\} + Mf'',
$$

$$
f(1) = 0, \quad f'(1) = 1, \quad f(-1) = 0, \quad f'(-1) = 1.
$$
 (10)

$$
N_3 g'' + N_1 N_2(f'' - 2g) = f'g - fg',
$$

$$
g(1) = 0, \quad g(-1) = 0.
$$
 (11)

$$
\theta'' + \Pr(\text{Re}f\theta' + M\text{Ec}(f')^{2}) = 0,\n\theta(1) = 0, \quad \theta(-1) = 1.
$$
\n(12)

where $N_1 = \frac{\kappa}{\mu_0}$ is the vortex viscosity parameter, $N_2 = \frac{\mu_0}{\rho_j b}$ is the microinertia density parameter, $N_3 = \frac{\gamma}{\rho j c^2 b}$ is the spin gradient viscosity parameter, Re = $\frac{\rho c^2 b}{\mu_0} > 0$ is the stretching Reynolds number, Pr = $\frac{\mu_0 c_p}{\kappa_0}$ is the Prandtl number, $M = \frac{c^2 \sigma B_0^2}{b^2 x_0^{\frac{\mu_0}{2}}}$
is the magnetic parameter and Eckert number Ec = $\frac{b^2 x_0^{\frac{\mu_0}{2}}}{c_p(T_2 - T_1)}$ defined as Gopal et al. [[40](#page-10-8)]. For $\epsilon = 0$ and $N_1 = 0$, the boundary value problem given in Eqs. (10) (10) – (12) (12) reduces to

odology based on order reduction and fnite diference discretization used by Ashraf et al. [\[22\]](#page-9-21), which is elaborated for the fourth order system as follows:

Let for a function G_f , we write

$$
G_{\rm f}(f, f', f'', f''', f'''')
$$

= $(1 + N_1)f'''' - N_1g'' - 2\left(\frac{\epsilon}{1 + \epsilon\theta}\right)^2(\theta')^2f''$
+ $\left(\frac{\epsilon}{1 + \epsilon\theta}\right)\theta''f'' - Mf'' - \text{Re}\{f'f'' - ff''' \},$

We now suppose that *F* be the solution of the ODE, then

$$
G_{\rm f}(F,F',F'',F''',F'''')=0.
$$

or can be written in another form as

$$
G_{\rm f}(f + (F - f), f' + (F' - f'), f'' + (F'' - f''),
$$

$$
f''' + (F''' - f'''), f'''' + (F'''' - f'''')) = 0.
$$

which on using frst-order Taylor series expansion, yields

$$
G_{\rm f}(f, f', f'', f''', f''') + (F - f)\frac{\partial G}{\partial f} + (F' - f')\frac{\partial G}{\partial f'}
$$

$$
+ (F'' - f'')\frac{\partial G}{\partial f''}
$$

$$
+ (F''' - f''')\frac{\partial G}{\partial f'''} + (F'''' - f'''')\frac{\partial G}{\partial f''''} = 0,
$$

or

$$
(1 + N_1)F'''' + (\text{Re}f)F''' + -2\left(\frac{\epsilon}{1 + \epsilon\theta}\right)^2(\theta')^2f''
$$

$$
+ \left(\frac{\epsilon}{1 + \epsilon\theta} - M - \text{Re}f''\right)F''(-\text{Re}f'')F' + (\text{Re}f'')F
$$

$$
= N_1g'' - \text{Re}f'f'' + \text{Re}ff'''.
$$

This equation may be used to set iterative process as

$$
(1 + N_1)F^{(k+1)''''} + (\text{Re}f)F^{(k+1)'''} + (-2\left(\frac{\epsilon}{1 + \epsilon\theta}\right)^2(\theta')^2f'' + \left(\frac{\epsilon}{1 + \epsilon\theta} - M - \text{Re}f''\right)F^{(k+1)''} - (\text{Re}f'')F^{(k+1)''} + (\text{Re}f'')F^{(k+1)'} + \text{Re}f^{(k+1)''} - Ref^{(k+1)'}f^{(k+1)''} + \text{Re}f^{(k+1)''}.
$$
\n(16)

Similar process may be adopted for the rest of the equations. Finally, the iterative procedure can be summarized as follows:

- An initial guess satisfying the corresponding boundary conditions is provided for *f*, *g* and θ
- A new approximation of *f* is obtained for solving Eq. (16)
- The updated *f* is then used to find the modified *g* and θ .
- Above-mentioned procedure is repeated until no signifcant iterative improvement is noted for *f*, *g* and θ

Results and discussion

In order to get physical insight into the problem, velocity felds (linear and angular), shear and couple stresses are examined for various values of physical parameters. Numerical values of shear, couple stresses and heat fuxes at the channel wall for various values of Reynolds number, Prandtl number, viscosity parameter and Eckert number are tabulated in Tables $1-5$. As the problem is inherently symmetric, numerical values of shear and couple stresses and heat fux for various values of the parameters are given at one channel wall only. Infuence of the external magnetic

Table 1 Magnetic fields effects on shear, couple stresses and heat transfer rate when $N_1 = 4$, $N_2 = 0.3$, $N_3 = 0.6$, Pr = 21, Re = 1, Ec = 0.01 and $\epsilon = 2$

M	$\left(\frac{1}{1+\epsilon\theta(\pm 1))} + N_1\right) f''(-1) \quad \left(\frac{N_3}{2}\right) g'(-1)$		$\theta'(-1)$
Ω	-2.8638	-1.6146	-1.1945
	-2.9002	-1.6166	-0.9423
\mathcal{D}	-2.9218	-1.6186	-0.2014
3	-2.9185	-1.6195	1.0240
$\overline{4}$	-2.8871	-1.6191	2.7505

Table 2 Efects of magnetic feld on shear, couple stresses and heat transfer rate with $N_1 = 4$, $N_2 = 0.8$, $N_3 = 0.2$, Pr = 1.5, Re = 40, Ec = 0.01 and $\epsilon = 2$

Table 3 Effects of Prandtl	Pr	$\theta'(1)$	$\theta'(-1)$
number on heat fluxes at channel walls when $N_1 = 4$, N_2 $= 0.3, N_3 = 0.6, M = 1, \epsilon = 2,$ $Ec = 0.01$ and $Re = 1$	0.05 0.10 1.00 1.50 2.00 2.50	-0.5019 -0.5037 -0.5381 -0.5799 -0.5782 -0.5991	-0.5016 -0.5032 -0.5319 -0.5481 -0.5643 -0.5806
	5.00 10.0	-0.7118 -0.9817	-0.6626 -0.8164

Table 4 Effects of temperature-dependent viscosity parameter on wall shear and couple stresses and wall heat transfer rate when N_1 = $4, N_2 = 0.3, N_3 = 0.6, Pr = 21, M = 1, Ec = 0.01$ and Re = 1

feld on the three physical quantities is also observed from Table [1.](#page-4-0) It is easy to note that the magnetic parameter M has a signifcant impact on the shear stress. Heat fux at the walls **Table 5** Efects of Eckert number on heat fuxes at channel walls when $N_1 = 4$, N_2 $= 0.3, N_3 = 0.6, M = 1, \epsilon = 2,$ $Pr = 5$ and $Re = 5$

Fig. 2 Comparison of results for normal velocity: Curves with flled circles represent Newtonian fluid for $N_1 = 0$ and curves without circles represent non-Newtonian fluid for $N_1 = 1$ when $N_2 = 0.3$, $N_3 = 0.6$, $Pr = 21$, $\epsilon = 2$, $R = 1$, $Ec = 0.01$

of channel increases with an increase in the Prandtl number (see Table [3\)](#page-4-1). Efect of the viscosity variation parameter on the physical quantities is evident from Table [4](#page-4-2). The shear stress and the couple stress are increased by increasing the viscosity parameter. However, the heat transfer exhibits an opposite trend. Behavior of heat fux with the variation of Eckert number is tabulated in Table [5](#page-5-0).

The behavior of streamwise and normal velocities is dis-played in Figs. [2](#page-5-1)[–8](#page-6-0) when $N_1 = 4$, $N_2 = 0.3$, $N_3 = 0.6$, Pr $= 21, M = 1$, $Ec = 0.01$ and $Re = 1$. Impact of viscosity parameter ϵ on the normal velocity of the fluid within the channel for Newtonian $(N_1 = 0)$ fluid and non-Newtonian $(N_1 = 1)$ fluid displayed in Fig. [2.](#page-5-1) It is observed that normal velocity of the fuid is enormously lower in the context of non-Newtonian fluid $(N_1 = 1)$ then Newtonian fluid $(N_1 = 0)$ with variation of ϵ . In addition, normal velocity of both Newtonian and non-Newtonian fuid increases with the increase in viscosity variation parameter. In Fig. [3](#page-5-2) , normal velocity increases with the increase in magnetic feld due to the presence of temperature-dependent viscosity and Joule

Fig. 3 Comparison of results for normal velocity: Curves with flled circles represent results by Ashraf et al. [\[22\]](#page-9-21) for $\epsilon = 0$, Ec = 0 and curves without circles are present results for $\epsilon = 2$, $Ec = 0.01$ when $N_1 = 4$, $N_2 = 0.3$, $N_3 = 0.6$, $Pr = 1.5$, $R = 40$, $Ec = 0.01$

Fig. 4 Normal velocity profile when $N_1 = 4$, $N_2 = 0.3$, $N_3 = 0.6$, Pr $= 21, M = 1, R = 1, Ec = 0.01$

heating, while it decreases in the absence of both parameters. Moreover, both Figs. [2](#page-5-1) and [3](#page-5-2) show the comparison of present result with the existing literature Ashraf et al. [[22\]](#page-9-21). The streamwise velocity decreases when the viscosity parameter is increased (see Fig. [4\)](#page-5-3). The magnitude of streamwise velocity of micropolar fuid with constant viscosity is high as compared to the velocity of micropolar fuid of temperature-dependent viscosity. Therefore, it is concluded that the streamwise velocity of blood in vessels lower when its viscosity varies with respect to the temperature as compared to the case when viscosity of blood is constant. However, monotonic behavior for normal velocity is observed (see Fig. [5](#page-6-1)).

Fig. 5 Streamwise velocity profile for $N_1 = 4$, $N_2 = 0.3$, $N_3 = 0.6$, Pr $= 21, M = 1, R = 1, Ec = 0.01$

Fig. 6 Microrotation profile when $N_1 = 4$, $N_2 = 0.3$, $N_3 = 0.6$, Pr = 21, $M = 1, R = 1$, $Ec = 0.01$

It can be noted from Fig. [6](#page-6-2) that angular motion of blood in vessels is greatly afected by the variation of viscosity of blood. This variation of micro-motion of blood in the vessels is simulated in Fig. [6](#page-6-2). The temperature of blood (micropolar liquid) in the vessel increases when the viscosity of the blood is increased by increasing the temperature.

The behavior of temperature of blood for various values of viscosity parameter is shown in Fig. [7](#page-6-3). The efect of magnetic feld on the normal velocity is shown in Fig. [8.](#page-6-0) It is obvious from Fig. [8](#page-6-0) that normal velocity decreases when the intensity of the magnetic feld is increased. This shows that fow of micropolar liquid is decelerated by the opposing Lorentz force. The streamwise velocity profles are extended to the boundaries (channel walls), and in the central region of the channel,

Fig. 7 Temperature profile when $N_1 = 4$, $N_2 = 0.3$, $N_3 = 0.6$, Pr = 21, $M = 1$, $R = 1$, $Ec = 0.01$

Fig. 8 Normal velocity profile when $N_1 = 4$, $N_2 = 0.3$, $N_3 = 0.6$, Pr $= 21, \epsilon = 2, R = 1, Ec = 0.01$

velocity becomes decreases because of damping efects from the magnetic feld, shown in Fig. [9.](#page-7-0) The Reynolds number is the ratio of viscous force to the inertial force. The magnitude of the angular velocity of the micropolar liquid decreases with an increase in the Reynolds number. It means an increase in the viscous force or a decrease in the inertial force results to slow down the micro-motion of the micropolar liquid in the channel (see Fig.[10](#page-7-1)). The efect of the magnetic feld on the temperature of the micropolar liquid in the channel is shown in Fig. [11.](#page-7-2) It can be noted from Fig. [11](#page-7-2) that the temperature of micropolar fuid increases near the lower wall of the channel, whereas the opposite trend is noted for upper half of the channel. The magnitude of the normal velocity of the fuid decreases when Reynolds number of the fuid is increased

Fig. 9 Streamwise velocity profile when $N_1 = 4$, $N_2 = 0.3$, $N_3 = 0.6$, $Pr = 21, \epsilon = 2, R = 1, Ec = 0.01$

Fig. 10 Microrotation profile when $N_1 = 4$, $N_2 = 0.3$, $N_3 = 0.6$, Pr = $21, \epsilon = 2, R = 1, Ec = 0.01$

as shown in Fig. [12.](#page-7-3) An increase in the Reynolds number is due to the decrease in inertial force or an increase in the viscous force. The behavior of streamwise velocity due to an increase in the Reynolds number is depicted in Fig. [13](#page-8-0). From this Fig. [13](#page-8-0), one can easily notice that the streamwise velocity increase near the channel walls. However, opposite trend can be noted in the center of the channel. From Fig. [14,](#page-8-1) we observe that Joule heating due to magnetic feld has immense efect on the temperatures and consequently increases the temperature with the increase in Eckert number. Figure [15](#page-8-2) is the comparison of the present result for temperature profle with Ashraf et al. [[22\]](#page-9-21). Finally, Fig. [16](#page-8-3) illustrates the variation in the heat transfer rate within the channel. This fgure shows that the rate of heat transfer increases with the increase in magnetic

Fig. 11 Temperature profile when $N_1 = 4$, $N_2 = 0.3$, $N_3 = 0.6$, Pr = $21, \epsilon = 2, R = 1, Ec = 0.01$

Fig. 12 Normal velocity profile when $N_1 = 4$, $N_2 = 0.3$, $N_3 = 0.6$, Pr $= 5, \epsilon = 2, M = 1, \text{Ec} = 0.01$

parameter which is exactly because of the fact that, frstly, heat is transmitted from the one end of the wall toward the fuid within the channel, and then, it is transferred from fuid toward the other end of the wall.

The results of special case are compared with already published work. The outcomes related this validation are recorded in Figs. [2](#page-5-1), [3](#page-5-2) and [15](#page-8-2). A good agreement between present results and already published is noted (see Figs. [2](#page-5-1), [3,](#page-5-2) [15](#page-8-2)).

Applications and further directions

The constitutive equations of micropolar fuid represents the rheology of blood and other biofuid (synovial fuid). Therefore, micropolar fuid model [\[8](#page-9-7), [9\]](#page-9-8) is frequently used to

Fig. 13 Streamwise velocity profile when $N_1 = 4$, $N_2 = 0.3$, $N_3 = 0.6$, Pr = 5, $\epsilon = 2$, $M = 1$, Ec = 0.01

Fig. 14 Temperature profile when $N_1 = 4$, $N_2 = 0.3$, $N_3 = 0.6$, Pr = $5, \epsilon = 2, M = 1$

study the dynamics of blood and other biofuids. The results presented may predict hemodynamic fow of blood in the cardiovascular system when subjected to an external magnetic feld. Further, arteries like cardiac vascular artery are channel like structures. Therefore, present analysis is carried out to get insight into the problem in order to give some predictions about blood fow in cardiac vascular. The results of the study are supposed to be of profound importance to medical surgeons in their endeavor to regulate blood fow during surgery. The latest advancement on an enhancement of thermal performance has proved that suspension of nano-sized particles in fuid of temperature viscosity plays a signifcant role in the improvement of thermal efficiency of working

Fig. 15 Comparison of results for temperature profle: Curves with filled circles represent results by Ashraf et al. $[22]$ $[22]$ $[22]$.) for $\epsilon = 0$, Ec = 0 and curves without circles are present results when $\epsilon = 2$, Ec = 0.01, $N_1 = 4$, $N_2 = 0.3$, $N_3 = 0.6$, $Pr = 1$, $M = 1$

Fig. 16 Nusselt number profle for diferent values of *M*

fluid. So, for efficient thermal systems, suspension of hybrid nanoparticles is recommended. Although consideration of such phenomenon leads to complex mathematical problems, such consideration provides information about behavior of thermal system under dispersion of hybrid nanoparticles.

Conclusions

A numerical study is carried out to investigate the efects of temperature-dependent viscosity on heat transfer in fow of magnetohydrodynamic (MHD) micropolar fuid in a channel with stretching walls. The powerful tool of similarity transformation has been employed to convert the governing equations into a set of nonlinear ordinary diferential equations. The analysis is summarized as follows:

- The magnetic parameter has a profound impact on the shear stress as compared to the couple stress and the heat transfer.
- An increase in Prandtl number causes the heat transfer rate at the channel walls.
- The viscosity variation parameter enhances the shear stress and the couple stress. However, the heat transfer exhibits an opposite trend.
- The viscosity variation parameter is the most influential for the thermal distribution.
- The magnetic field acts as a retarding force which reduces the normal and streamwise velocities as well as the microrotation distribution
- The Reynolds number affects the velocity and microrotation in the same way as the intensity of magnetic parameter is increased.

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