

Signifcance of nonlinear thermal radiation in 3D Eyring–Powell nanofuid fow with Arrhenius activation energy

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Abstract

In this paper, a mathematical analysis for three-dimensional Eyring–Powell nanofuid nonlinear thermal radiation with modifed heat plus mass fuxes is investigated. To enhance the dynamical and physical study of structure, the slip condition is introduced. A Riga plate is employed for avoiding boundary-layer separation to diminish the friction and pressure drag of submarines. To evaluate the heat transfer, the Cattaneo–Christov heat fux model is implemented via appropriate transformation. A comparison between bvp4c results and shooting technique is made. Graphical and numerical illustrations are presented for prominent parameters.

Keywords Eyring–Powell model · Nanofuid · Nonlinear thermal radiation · Activation energy · Heat and mass fuxes · 3D flow

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Introduction

In recent years, non-Newtonian fuids due to their extensive role in engineering and industrial applications have attracted the attention of a large number of researchers. These include Reiner–Philippoff fluid, Casson fluid, Carreau fluid, micropolar fuid, Prandtl fuid, power law fuid, Eyring–Powell fuid and Prandtl–Eyring fuid. Such fuids can be used in the processing of chemical; that is why, a number of researchers are investigating non-Newtonian fuids in the process of polymers and in chemical engineering. Besides, nanofuids containing small nanomaterial particles like molecules or atoms are ejected in a base fuid [\[1](#page-13-0)[–20](#page-14-0)]. Nanofuid is a fuid typical of nanomaterials coined by Choi and Eastman [\[21\]](#page-14-1). The modern convection agents have a point of view that a broad range of production and industrial characteristic plays an important role in the heat transfer in such liquids. Due to this fact, nanoparticles have been used in the past decades as attractive agents in the formation of fuids to maximize heat transfer in industrial automation. By controlling the nanoscale stage in the development of practical tools, materials and systems, they make a signifcant contribution to nanotechnology. These include inertia, Magnus brown absorption, thermophoresis, liquid precipitation and gravity. Boungiorno et al. [\[22](#page-14-2)] examined the vital role in the growth of the non-homogenous scientifc equilibrium for the convective transportation of nanoparticles with convectional boundaries. He also developed possible slipping tools for Brownian motion and thermophoresis in nanofuids. Powell and Eyring [[23\]](#page-14-3) have introduced fluid model called Eyring–Powell fuid. Patel and Timol [\[24\]](#page-14-4) developed the Eyring–Powell models more efficient and significant as compared to the power law model, but it was rather complex in nature. Simultaneously, concern was to argue that this fuid's dynamic existence is believed to be resulted from the fuids kinetic theory more than its matter-of-fact expression. The fuid model of Eyring-Powell is used to design the manufacturing in material fows. This model also reduces the viscous fluid flow of the Eyring–Powell fluid to a moveable surface at low and high shear concentrations, as investigated by Hayat et al. [[25\]](#page-14-5). Akbar et al. [\[26\]](#page-14-6) discussed Eyring–Powell magneto-fuid fow numerically past the stretching sheet by employing the fnite diference method. As various non-Newtonian fuid system equations are complex as compared to Navier–Stokes equations, obtaining the solutions of these equations is much difficult but more significant due to the simplicity and ease of Eyring–Powell model and vital in chemical engineering processes. Hayat et al. [\[27](#page-14-7)] illustrated Eyring–Powell fuid for Newtonian heat and magnetohydrodynamics, and even today, it is of great significance to improve the mathematical modeling of non-Newtonian fuids [\[28](#page-14-8)[–35](#page-14-9)]. Eldabe et al. [\[36](#page-14-10)] explored Eyring–Powell fuid for MHD within the variable viscosity efects which has been examined in [[37\]](#page-14-11). Islam et al. [\[38](#page-14-12)] reported the disturbance of the Eyring–Powell fuid. Akbar and Nadeem [[39\]](#page-14-13) argued an endoscope transfer and heating structure of Eyring–Powell fuid. Sirohi et al. [\[40\]](#page-14-14) examined the fuid flow of Eyring–Powell near a dynamic plate utilizing various techniques. Nadeem et al. [[41\]](#page-14-15) discussed the peristaltic fux of Eyring–Powell fuid. The efect of dual stratifcation by Eyring–Powell has been inspected by Jayachandra et al. [[42](#page-14-16)]. Yoon and Ghajar [\[43](#page-14-17)] offered a brief description of the effect of varying large and small viscosities of shear rate by using Powell–Eyring fuid to understand the nature of fuid time range. Agbaje et al. [\[44\]](#page-14-18) investigated the incompressible nanoflow limits stage of Eyring–Powell. Gailitis and Lielausis [[45\]](#page-14-19) invented the Riga electromagnetic actuator surface, which consists of defnitely arranged magnets and electrode sets. Ahmad et al. [\[46](#page-14-20)] examined the impact of zero normal mass and heat fux on the motion of nanofuid fowing across a Riga layer. The fow problem was determined by two techniques: (1) the shooting method and (2) bvp4c. Iqbal et al. $[47]$ $[47]$ performed the analysis of nanofluid flow to a variablethick Riga plate with bioconvection, heat convection and mass fow elements within the fow region. Khan et al. [[48\]](#page-14-22) investigated Powell–Eyring MHD fuid by considering the elements of thermophysics. The stretching surface with boundary conditions flow of nanofluid is available in [[49](#page-14-23)]. Goodarzi et al. [[50](#page-14-24)] used two types of mixture model and narrow cavity channel to describe the laminar and turbulent nanofluid case flow. Riaz et al. [\[51](#page-14-25)] studied the Eyring–Powell fluid for heat and mass transfer. Three-dimensional Eyring–Powell nanofuids through the stretch sheet were proposed by Gireesha et al. [\[52\]](#page-14-26). Hayat et al. [\[53\]](#page-14-27) determined their three-dimensional previous-degree nanofuid fow instead of utilizing the stretching layer to evaluate the thermal infuence fow. Hayat et al. [\[54](#page-14-28)] reported Maxwell nanofluid with heat transfer source/sink effects for a threedimensional boundary-layer fow. Hedayati et al. [\[55](#page-14-29)] highlighted the nanofuid fow in a channel. Most of these slip systems are similar to the Fukui–Kaneko (FK) slip demarca-tion flow model [\[56](#page-14-30)], the Maxwell first-order boundary slip flow model $[57]$ $[57]$, the nominal injunction slip surface flow model [[58\]](#page-14-32) and the second command slip boundary flow method [\[59\]](#page-15-0). Kinetic theory for gases is the origin of these models. These models are used in engineering and science problems. In addition, for chemical reaction, the least required energy to reactants is the activation energy. In chemical industry, oil emulsions, water mechanics and food processing play important roles, and due to concentration, a variance in mixture-type mass transfer process happens. Geothermal reservoirs have been studied for exothermic or endothermic reactions with the aid of activation energy, where activation energy plays an important role in alternate convective flows [[60\]](#page-15-1). Techniques of numerical methods of fractional control problem were reported using the Cheby-shev polynomial technique by Zhang et al. [\[61](#page-15-2)]. Shafique et al. [[62](#page-15-3)] provided the concept of rotating viscoelastic fow by numerical approaches for chemical reactions and activation energy species for convoluted and nonlinear Fokker–Planck formula. Hemeda and Eladdad [[63\]](#page-15-4), along with an integrated scheme, provided the concept of an iterative technique. Asadollahi and Esmaeeli [\[64\]](#page-15-5) studied two-dimensional simulation of condensation liquid behavior on microobject with moving walls. They found that an increase in Weber number leads to liquid breakup and consequently this mechanism provides an efective way for removing the condensed liquid from micro-devices surfaces. Their presented results reveal the liquid evolutionary performance and breaking up over time which is ultimately a controllable situation for manipulating the walls velocity. Few useful numerical techniques can be seen in [\[65](#page-15-6)[–67](#page-15-7)]. Furthermore, Khan et al. [\[68\]](#page-15-8) inspected non-Fourier heat fux model on viscoelastic fluid. Nadeem and Muhammad [[69\]](#page-15-9) studied the flow of heat from Cattaneo–Christov model and its infuence on stratifcation saturated with porous medium. Hayat et al. [[70](#page-15-10)] discussed chemically reactive double stratifed stream via Fourier theory of heat change. Salahuddin et al. [[71\]](#page-15-11) applied the variable thicknesses of the Cattaneo–Christov experiment on Williamson fuid via stretched sheet. Recently, Cattaneo–Christov model on Powell–Eyring fuid has been discussed by Hayat et al. [[72\]](#page-15-12) with variable thermal conductivity. Powell–Eyring fuid study has not been given awide coverage. There is little literature available to support over the extended surface fow of non-Newtonian fuid from the Eyring–Powell. However, using the concept of non-Fick's

theory of mass fux and non-Fourier's theory of thermal fux, Eyring–Powell fuid over a Riga plate with nonlinear thermal energy and activation energy has not been discussed yet.

Model

Let us consider a three-dimensional Eyring–Powell nanofuid with nonlinear thermal radiation, activation energy and the non-Fourier heat transfer and non-Fick's mass fux passing over bidirectional stretching sheet as shown in Fig. [1](#page-2-0). Let the stretching velocity about *x*-direction and *y*-direction be $\tilde{u} = ax$, $\tilde{v} = by$, respectively. The region $z \ge 0$ is occupied by the fuid. Let us consider the temperature and the nanoparticle's concentration \tilde{T}_f , \tilde{C}_f are constant and assume that they are better than the ambient high temperature and the concentration \tilde{T}_{∞} , \tilde{C}_{∞} (Fig. [1](#page-2-0)).

A three-dimensional Eyring–Powell model of energy and nanoparticle's concentration with activation energy and nonlinear thermal radiation [[73](#page-15-13), [74](#page-15-14)] can be expressed by

$$
\left(\frac{\partial \tilde{u}}{\partial x} + \frac{\partial \tilde{v}}{\partial y} + \frac{\partial \tilde{w}}{\partial z}\right) = 0,\tag{1}
$$

$$
\left(\tilde{u}\frac{\partial\tilde{u}}{\partial x} + \tilde{v}\frac{\partial\tilde{u}}{\partial y} + \tilde{w}\frac{\partial\tilde{u}}{\partial z}\right) = \left(v + \frac{1}{\rho\Gamma a}\right)\frac{\partial^2\tilde{u}}{\partial z^2} - \frac{1}{2\rho\Gamma a^3} \left(\frac{\partial\tilde{u}}{\partial z}\right)^2 \frac{\partial^2\tilde{u}}{\partial z^2} \n- \frac{\sigma^* B_0^2}{\rho}\tilde{u} - \frac{v\varphi}{K^*}\tilde{u} + \frac{\pi j_0 M_0}{8\rho} \exp\left(\frac{-\pi}{\alpha_1}z\right),
$$
\n(2)

$$
\left(\tilde{u}\frac{\partial \tilde{v}}{\partial x} + \tilde{v}\frac{\partial \tilde{v}}{\partial y} + \tilde{w}\frac{\partial \tilde{v}}{\partial z}\right) = \left(v + \frac{1}{\rho T a}\right)\frac{\partial^2 \tilde{v}}{\partial z^2} \n- \frac{1}{2\rho T a^3} \left(\frac{\partial \tilde{v}}{\partial z}\right)^2 \frac{\partial^2 \tilde{v}}{\partial z^2} - \frac{\sigma B_0^2}{\rho} \tilde{v} - \frac{v\varphi}{K^*} \tilde{v},
$$
\n(3)

The Fourier and the Fick laws can be expressed as follows:

Fig. 1 Flow geometry

$$
\vec{q} + \Omega_{\rm E} \left(\frac{\partial \vec{q}}{\partial t} + \tilde{V} \cdot \nabla \vec{q} - \vec{q} \cdot \nabla \tilde{V} + (\nabla \cdot \tilde{V}) \vec{q} \right) = -k \nabla \tilde{t}, \quad (4)
$$

$$
\vec{j} + \Omega_{\rm C} \left(\frac{\partial \tilde{j}}{\partial t} + \tilde{V} \cdot \nabla \vec{j} - \vec{j} \cdot \nabla \tilde{V} + (\nabla \cdot \tilde{V}) \vec{j} \right) = -D_{\rm B} \nabla \tilde{C}, \quad (5)
$$

$$
\left(\tilde{u}\frac{\partial \tilde{T}}{\partial x} + \tilde{v}\frac{\partial \tilde{T}}{\partial y} + \tilde{w}\frac{\partial \tilde{T}}{\partial z} + \Omega_{\rm E}\phi_{\rm E}\right) = \alpha \frac{\partial^2 \tilde{T}}{\partial z^2} + \tau \left\{D_{\rm B}\frac{\partial \tilde{C}}{\partial z}\frac{\partial \tilde{T}}{\partial z} + \frac{D_{\rm T}}{T_{\infty}}\left(\frac{\partial \tilde{T}}{\partial z}\right)^2\right\} - \frac{1}{(\rho c)_{\rm p}}\frac{\partial \tilde{q}_{\rm r}}{\partial z},\tag{6}
$$

$$
\begin{split}\n\left(\tilde{u}\frac{\partial C}{\partial x} + \tilde{v}\frac{\partial \tilde{C}}{\partial y} + \tilde{w}\frac{\partial \tilde{C}}{\partial z} + \Omega_{\rm C}\phi_{\rm C}\right) \\
&= D_{\rm B}\left(\frac{\partial^2 \tilde{C}}{\partial z^2}\right) + \frac{D_{\rm T}}{T_{\infty}}\left(\frac{\partial^2 \tilde{T}}{\partial z^2}\right) \\
&- Kr^2(\tilde{C} - \tilde{C}_{\infty})\left(\frac{\tilde{T}}{\tilde{T}_{\infty}}\right)^n \exp\left(\frac{-E_{\rm a}}{K_1\tilde{T}}\right),\n\end{split} \tag{7}
$$

The associated boundary conditions can be given as follows:

$$
\tilde{u} = \tilde{u}_{w}(x) + \alpha_0 \frac{\partial \tilde{u}}{\partial z},
$$
\n
$$
w = 0, -k \frac{\partial \tilde{T}}{\partial z} = h_f [\tilde{T}_f - \tilde{T}],
$$
\n
$$
\text{at } z = 0, \tilde{v} = \tilde{v}_{w}(y) + \alpha_0 \frac{\partial \tilde{v}}{\partial z},
$$
\n(8)

$$
\tilde{u} \to 0, \tilde{v} \to 0, \tilde{T} \to \tilde{T}_{\infty}, \tilde{C} \to \tilde{C}_{\infty}, z \to \infty.
$$
\n(9)

Radiative heat fux can be addressed by

$$
\tilde{q}_r = -\frac{4\sigma^*}{3k^*} \frac{\partial \tilde{T}^4}{\partial z} = -\frac{16\sigma^* \tilde{T}^3}{3k^*} \frac{\partial \tilde{T}}{\partial z}.
$$
\n(10)

Substituting expression (10) (10) in Eq. (6) (6) , we get,

$$
\begin{aligned}\n\left(\tilde{u}\frac{\partial \tilde{T}}{\partial x} + \tilde{v}\frac{\partial \tilde{T}}{\partial y} + \tilde{w}\frac{\partial \tilde{T}}{\partial z} + \Omega_{\rm E}\phi_{\rm E}\right) \\
&= \alpha \frac{\partial^2 \tilde{T}}{\partial z^2} + \tau \left\{ D_{\rm B} \frac{\partial \tilde{C}}{\partial z} \frac{\partial \tilde{T}}{\partial z} + \frac{D_{\rm T}}{T_{\infty}} \left(\frac{\partial \tilde{T}}{\partial z}\right)^2 \right\} \\
&+ \frac{16\sigma^*}{3k^*(\rho c)_{\rm p}} \frac{\partial}{\partial z} \left(\tilde{T}^3 \frac{\partial \tilde{T}}{\partial z}\right),\n\end{aligned} \tag{11}
$$

where

$$
\phi_{\rm E} = \tilde{u}^2 \frac{\partial^2 \tilde{T}}{\partial x^2} + \tilde{v}^2 \frac{\partial^2 \tilde{T}}{\partial y^2} + \tilde{w}^2 \frac{\partial^2 \tilde{T}}{\partial z^2} \n+ 2\tilde{u}\tilde{v} \frac{\partial^2 \tilde{T}}{\partial x \partial y} + 2\tilde{v}\tilde{w} \frac{\partial^2 \tilde{T}}{\partial y \partial z} + 2\tilde{u}\tilde{w} \frac{\partial^2 \tilde{T}}{\partial x \partial z} \n+ \left(\tilde{u} \frac{\partial \tilde{u}}{\partial x} + \tilde{v} \frac{\partial \tilde{u}}{\partial y} \right) \frac{\partial \tilde{T}}{\partial x} \n+ \left(\tilde{u} \frac{\partial \tilde{v}}{\partial x} + \tilde{v} \frac{\partial \tilde{v}}{\partial y} + \tilde{w} \frac{\partial \tilde{v}}{\partial z} \right) \frac{\partial \tilde{T}}{\partial y} \n+ \left(\tilde{u} \frac{\partial \tilde{w}}{\partial x} + \tilde{v} \frac{\partial \tilde{w}}{\partial y} + \tilde{w} \frac{\partial \tilde{w}}{\partial z} \right) \frac{\partial \tilde{T}}{\partial z}, \tag{12}
$$

$$
\phi_{\rm C} = \tilde{u}^2 \frac{\partial^2 \tilde{C}}{\partial x^2} + \tilde{v}^2 \frac{\partial^2 \tilde{C}}{\partial y^2} + \tilde{w}^2 \frac{\partial^2 \tilde{C}}{\partial z^2} + 2 \tilde{u} \tilde{v} \frac{\partial^2 \tilde{C}}{\partial x \partial y} + 2 \tilde{v} \tilde{w} \frac{\partial^2 \tilde{C}}{\partial y \partial z} \n+ 2 \tilde{u} \tilde{w} \frac{\partial^2 \tilde{C}}{\partial x \partial z} + \left(\tilde{u} \frac{\partial \tilde{u}}{\partial x} + \tilde{v} \frac{\partial \tilde{u}}{\partial y} \right) \frac{\partial \tilde{C}}{\partial x} \n+ \left(\tilde{u} \frac{\partial \tilde{v}}{\partial x} + \tilde{v} \frac{\partial \tilde{v}}{\partial y} + \tilde{w} \frac{\partial \tilde{v}}{\partial z} \right) \frac{\partial \tilde{C}}{\partial y} + \left(\tilde{u} \frac{\partial \tilde{w}}{\partial x} + \tilde{v} \frac{\partial \tilde{w}}{\partial y} + \tilde{w} \frac{\partial \tilde{w}}{\partial z} \right) \frac{\partial \tilde{C}}{\partial z}.
$$
\n(13)

Let us introduce the following transformation:

$$
\eta = \sqrt{\frac{a}{v}z^2}, \tilde{u} = axf'(\eta), \tilde{v} = ayg'(\eta), \tilde{w} = -\sqrt{av}(f(\eta) + g(\eta)),
$$

$$
\theta(\eta) = \frac{\tilde{T} - \tilde{T}_{\infty}}{\tilde{T}_{f} - \tilde{T}_{\infty}}, \phi(\eta) = \frac{\tilde{C} - \tilde{C}_{\infty}}{\tilde{C}_{w} - \tilde{C}_{\infty}}.
$$
(14)

Applying similarity transformation to the governing equation, the nonlinear dimensional expressions are reduced to the following expressions:

$$
(1 + \omega - \omega f''(\eta))f'''(\eta) + (f(\eta) + g(\eta))f''(\eta)
$$

$$
-K_1 f'(\eta) - (f'(\eta))^2 + Qe^{-B\eta} = 0,
$$
(15)

$$
(1 + \omega - \omega g''(\eta))g'''(\eta) + (f(\eta) + g(\eta))g''(\eta)
$$

$$
-K_1g'(\eta) - (g'(\eta))^2 = 0,
$$
 (16)

$$
(1 + \varepsilon_1 \theta) \theta'' + \left[\frac{4}{3} N_r (1 + (\theta_w - 1) \theta)^3 \right] \theta'' + \left[\varepsilon_1 + (1 + (\theta_w - 1) \theta)^2 (4N_r (\theta_w - 1)) \theta'^2 \right] + \Pr(f(\eta) + g(\eta)) \theta'(\eta) + N_B \theta'(\eta) \phi'(\eta) + N_T (\theta'(\eta))^2 - \delta_t (f + g) (f' + g') \theta' + (f + g)^2 \theta'' = 0,
$$
(17)

$$
\phi''(\eta) + S_c(f(\eta) + g(\eta))\phi'(\eta) + \frac{N_{\rm T}}{N_{\rm B}}\theta''(\eta)
$$

$$
- S_c \sigma (1 + \delta \theta)^n \exp\left(\frac{-E_1}{1 + \delta \theta}\right) \phi(\eta)
$$

$$
- \delta_c (f + g)(f' + g')\phi(\eta) + (f + g)^2 \phi''(\eta) = 0,
$$
 (18)

(19) $f(0) = g(0) = 0, f(0) = 1 + \alpha f''(0), g'(0) = \lambda + \alpha g''(0),$

$$
f'(\eta) = 0, g'(\eta) = 0, \theta(\eta) = 0, \phi(\eta) = 0 \text{ as } \eta \to 0,
$$
 (20)

where the porosity parameter is K_1 , dimensionless constant *B*, customized Hartmann number *Q*, radiation parameter N_r , non-dimensional fluid parameter ω , Prandtl number Pr, velocity slip parameter α , Schmidt number Sc, thermophoresis number N_T , Brownian motion N_B , activation energy E_1 , chemical reaction parameter σ , heat parameter δ , Biot number γ , recreation for temperature diffusion δ_t and time relaxation for mass diffusion δ_c , which are expressed as follows:

$$
E_1 = \frac{E_a}{k_1 T_{\infty}}, \quad K_1 = \frac{\sigma^* B_0^2}{a \rho_f} + \frac{v_f \varphi}{a K^*}, \quad \Pr = \frac{v}{a},
$$

\n
$$
N_B = \frac{\tau D_B}{v} (\tilde{C}_w - \tilde{C}_\infty), \quad \alpha = \alpha_0 \left(\frac{v}{a}\right)^{-\frac{1}{2}},
$$

\n
$$
\gamma = \frac{h}{k} \sqrt{\frac{v}{a}}, \quad \lambda = \frac{b}{a}, \quad \sigma = \frac{k_r^2}{a}, \quad \delta = \frac{b^3 x^2}{2v c^2},
$$

\n
$$
\mu = v \rho, \quad N_T = \frac{\tau D_T}{v T_{\infty}} (\tilde{T}_f - \tilde{T}_\infty), \quad \omega = \frac{1}{\mu T a},
$$

\n
$$
N_r = \frac{4\sigma T_{\infty}^3}{k^* k}, \quad S_c = \frac{\alpha}{D_B}, \quad \delta_t = b \lambda_E, \quad \delta_c = b \lambda_C,
$$

\n
$$
Q = \frac{\pi M_0 J_0}{8\rho a^2 x}, \quad B = \frac{\pi}{\alpha_1} \left(\sqrt{\frac{v}{a}}\right).
$$
 (21)

To drive the skin friction coactive \tilde{C}_f , the Newton method is used. The Fourier law is implemented to fnd the value of the Nusselt number Nu_x . Also to find the value of local Sherwood number Sh_x , the Fick's laws have been utilized. Finally, the quantities of interest can be written as:

$$
C_{\text{fx}} = \frac{\tau_{\text{wx}}}{\rho U_{\text{u}}^2}, \quad C_{\text{fy}} = \frac{\tau_{\text{wy}}}{\rho U_{\text{w}}^2}, \quad \text{Nu}_{\text{x}} = \frac{xq_{\text{w}}}{k_1(\tilde{T}_{\text{w}} - \tilde{T}_{\infty})},
$$

$$
\text{Sh}_{\text{x}} = \frac{xq_{\text{m}}}{k_1(\tilde{C}_{\text{w}} - \tilde{C}_{\infty})}.
$$
(22)

 τ_{wx} , τ_{wy} are the barrage shear stress next to *x*-axis and *y*-axis, respectively, which are defned as:

$$
\tau_{\rm wx} = \mu \left(\frac{\delta \tilde{u}}{\delta z} + \frac{\delta \tilde{w}}{\delta x} \right)_{z=0}, \ \ \tau_{\rm wy} = \mu \left(\frac{\delta \tilde{v}}{\delta z} + \frac{\delta \tilde{w}}{\delta y} \right)_{z=0}, \tag{23}
$$

where

$$
h_{\rm m} = -D_{\rm B} \left(\frac{\delta \tilde{C}}{\delta z} \right)_{z=0}, \quad h_{\rm m} = -k \left(\frac{\delta \tilde{T}}{\delta z} \right)_{z=0}.
$$
 (24)

Substituting (22) (22) to (24) (24) , we get

$$
C_{fx} \text{Re}_{x}^{0.5} = -f''(0), \quad C_{fy} \text{Re}_{y}^{0.5} = -g''(0),
$$

\n
$$
\frac{\text{Nu}_{x}}{\text{Re}_{x}^{0.5}} = -\theta'(0), \quad \frac{\text{Sh}_{x}}{\text{Re}_{x}^{0.5}} = -\phi'(0).
$$

\n(25)

Here, the local Reynolds number on relied stretching velocity, local Sherwood number and local Nusselt number are denoted, respectively, as Re_x , Re_y , Sh_x , Nu_x .

Numerical procedure

The set of nonlinear coupled diferential equations with dimensionless boundaries as described in (14) (14) (14) – (19) (19) have been solved to fnd numerical results for velocity, high temperature and concentration by utilizing Lobatto IIIa fnite diference shooting method bvp4c via computational software MATLAB.

Let us consider

$$
f = l_1, \frac{df}{d\eta} = l_2, \frac{d^2f}{d\eta^2} = l_3, \frac{d^3f}{d\eta^3} = l'_3, g = l_4,
$$

\n
$$
\frac{dg}{d\eta} = l_5, \frac{d^2g}{d\eta^2} = l_6, \frac{d^3g}{d\eta^3} = l'_6, \theta = l_7, \frac{d\theta}{d\eta} = l_8,
$$

\n
$$
\frac{d^2\theta}{d\eta^2} = l'_8, \phi = l_9, \phi' = l_{10}, \phi'' = l'_{10},
$$

\n
$$
l'_3 = \frac{1}{(1 + \omega - \omega l_3)} - ((l_1 + l_4)l_3 + K_1l_2 + l_2^2 + Qe^{-B\eta}),
$$

\n
$$
l'_6 = \frac{1}{(1 + \omega - \omega l_6)}((l_1 + l_4)l_6 + k_1l_5 + l_5^2),
$$

\n
$$
l'_8 = \frac{1}{(1 + \varepsilon_1 l_7 + (l_1 + l_4)^2) \left(\frac{4}{3} \left(N_r(1 + (\theta_w - 1) + l_7)\right)^3\right)} \left[\begin{matrix} -\varepsilon_1 - (1 + (\theta_w - 1)l_7)^2 (4N_r(\theta_w - 1))l_8^2\\ -P_r[(l_1 + l_4)l_8] - N_{\text{B}}l_8l_{10} - N_{\text{T}}l_8^2 \end{matrix}\right],
$$

\n
$$
l'_{10} = \frac{1}{(1 + (l_1 + l_4)^2)} \left(-S_c(l_1 + l_4)l_{10} - \frac{N_r}{N_\text{B}}l'_8 + S_c\sigma(1 + \delta l_7)^n \exp\left(\frac{-E_1}{1 + \delta l_7}\right)l_9 + \delta_c(l_1 + l_4)(l_2 + l_5)l_9\right),
$$

\n
$$
l_1(0) = l_4(0) = 0, l(0) = 1 + \alpha l_3(0), l_5(0) = \lambda + \alpha l_6(0),
$$

\n
$$
l_8(0) = -\gamma(1 - l_7(0)), l_9(0) = 1, \text{ at } z = 0
$$

Discussion

The 3D Eyring–Powell fuid through a stretching slip with activation energy and velocity slip for diferent parameters is sketched in Figs. [2–](#page-5-0)[32](#page-11-0). Figure [2](#page-5-0) demonstrates the combined effects of porosity and magnetic parameter K_1 on f' . It is seen that velocity decreases with higher K_1 . Actually, by enhancing the magnetic parameter, the Lorentz forces or struggle forces increase, and due to this reason, the flow of fluid slows down or components of velocity profile decline in fluid. Figure [3](#page-5-1) illustrates the effects of K_1 on g' . It is experiential that with the higher values of K_1 , velocity component g' reduces. In Fig. [4,](#page-6-0) the effect of K_1 on temperature distribution θ' is shown. It is noted that temperature distribution θ' boosts up when K_1 is increased. In Fig. [5](#page-6-1), the exploration impacts of K_1 on volumetric concentration ϕ' are depicted. The volumetric concentration ϕ' increases with higher K_1 . Figure [6](#page-6-2) shows the impacts of velocity profile f' on modifed Hartmann number *Q*. It is seen that the velocity is enhanced by higher values of *Q*. Physically, increasing modifed Hartmann number *Q* leads to the conficting

Fig. 2 Profile of $f'(\eta)$ against K_1

Fig. 3 Profile of $g'(\eta)$ against K_1

Fig. 4 Profile of $\theta(\eta)$ against K_1

Fig. 5 Profile of $\phi(\eta)$ against K_1

Fig. 6 Profile of $f'(\eta)$ against *Q*

behavior with the magnetic parameter as observed previously. Higher modifed Hartmann number *Q* values raise the magnetization fanked by the plates, which ultimately assist in accelerating the fow, i.e., the reverse infuence to Lorentz

Fig. 7 Profile of $f'(\eta)$ against α

Fig. 8 Profile of $g'(\eta)$ against α

magnetic pull force connected with the magnetic feld. This characteristic is exclusively linked with Riga plates. Therefore, velocities are decreased for the situation where the modifed Hartmann number *Q* disappears, and the Riga plate becomes a straight plate in this situation. Figure [7](#page-6-3) illustrates the velocity profile for slip parameter α . The velocity profile f' decreases for higher value of α . In Fig. [8,](#page-6-4) the consequence of α on velocity component g' is depicted. It is noticed that the velocity component g' decreases when α is increased. In Fig. [9](#page-7-0), the effects of α on temperature θ are shown in which an increase in α causes a rise in θ . Figure [10](#page-7-1) illustrates the effects of α on volumetric concentration ϕ . It is clearly seen that an increase in α causes a reduction in ϕ . Figure [11](#page-7-2) shows the stretching parameter β on velocity report f' where reduction in velocity f' is observed with increasing β . Figure 12 reveals the variations of g' for altering principles of β . Augmentation in stretching parameter β leads to a faster pressure group which causes an increase in velocity. Fig-ure [13](#page-7-4) represents the graph of stretching parameter β against heat distribution θ . It is exposed that θ decreases with higher

Fig. 9 Profile of $\theta(\eta)$ against α

Fig. 10 Profile of $\phi(\eta)$ against α

Fig. 11 Profile of $f'(\eta)$ against β

 β . Figure [14](#page-8-0) represents the volume friction ϕ' via stretching parameter β in which volume friction ϕ' reduces by increasing β . Figures [15](#page-8-1) and [16](#page-8-2) illustrate the effect of Biot number

Fig. 12 Profile of $g'(\eta)$ against β

Fig. 13 Profile of $\theta(\eta)$ against β

 (γ) on the temperature distribution θ and volumetric concentration profile φ , respectively. It is seen that Biot number γ is directly proportional to the temperature and volumetric concentration profle. Figure [17](#page-8-3) shows the witness that thermal distribution increases when one increased the radiation parameter. Physically, one can say that the radiation parameter increases the heat energy between the particles of fuid. It charges them up. Thus, the heat boosts up with the addition of radiation. In Fig. [18](#page-8-4), we see that the radiationparameter N_r has direct influence on concentration ϕ . It clearly reveals that the enhancement in radiation parameter N_r enhances its volume friction ϕ . Obviously, the phenomenon in which fuid particles get thermal heat energy has a prominent impact on temperature and volume friction. Fig-ure [19](#page-8-5) demonstrates Prandtl Pr for temperature coefficient. It is perceived that temperature behavior has an opposite trend with increasing Pr. Physically, a rise in Prandtl Pr causes low heat penetration, which causes a decrease in the thickness of thermal boundary layer. Figure [20](#page-9-0) displays the part

Fig. 14 Profile of $\phi(\eta)$ against β

Fig. 15 Profile of $\theta(\eta)$ against γ

Fig. 16 Profile of $\phi(\eta)$ against γ

of Pr on concentration; here, Pr is inversely proportional to the concentration trend , which suggests that concentration decreases with increasing Pr. Figures [21](#page-9-1) and [22](#page-9-2) reveal the

Fig. 17 Profile of $\theta(\eta)$ against N_r

Fig. 18 Profile of $\phi(\eta)$ against N_r

Fig. 19 Profle of *θ*(*η*) against Pr

consequence of thermophoresis number N_t for temperature distribution θ as well as volume friction of nanoparticles ϕ , respectively. It is detected that a rise in the aspect of

Fig. 20 Profile of $\phi(\eta)$ against Pr

Fig. 21 Profile of $\theta(\eta)$ against N_T

Fig. 22 Profile of $\phi(\eta)$ against N_T

Fig. 23 Profile of $\theta(\eta)$ against θ_n

Fig. 24 Profile of $\phi(\eta)$ against S_c

Fig. 25 Profile of $\theta(\eta)$ against δ_t

thermophoresis number N_t results in the rise in temperature and volume friction. Figure [23](#page-9-3) visualizes the efect of temperature ratio parameter θ_n on temperature sharing

 θ in which temperature distribution is boosted up with an increment in temperature relative amount of parameter θ_n . Figure [24](#page-9-4) shows the blow of Schmidt number S_c over ϕ in

Fig. 26 Profile of $\phi(\eta)$ against δ_c

Fig. 27 Profile of $\phi(\eta)$ against N_B

Fig. 28 Profile of $\phi(\eta)$ against E_1

Fig. 29 Comparison of Pr by shooting method

Fig. 30 Comparison of N_T by shooting method

Fig. 31 Comparison of N_B by shooting method

Fig. 32 Comparison of N_r by shooting method

which a rise in S_c yields a drop in concentration. Figure 25 exhibits the effect of relaxation for heat diffusion δ_t on temperature distribution. In Fig. [25,](#page-9-5) a decrease in temperature against relaxation for heat diffusion δ_t is viewed. The sway of time is for collection diffusion δ_c versus attentiveness profile, which is shown in Fig. [26](#page-10-0). The volumetric concentration of nanomaterials is clearly decomposed with an increment in the values of point relaxation for mass diffusion δ_c . The conductivity of Brownian motion parameter on volume friction is plotted in Fig. [27.](#page-10-1) Escalating N_b results in a decrease in volume friction. Physically, N_b creates a continuous motion between the particles of fuids. This motion enhances chaotic

Table 3 Statistical shooting assessment and outcomes from bvp4c with Freidoonimehr and Rahimi $[75]$ and Wang $[76]$ for $f''(0)$, when $\gamma = M = 0$, $\delta_t = 0$, $\delta_c = 0$, $Q = 0$ also all extended parameters are zero

Parameter Ref [47] λ	$-f''(0)$	Ref [48] $-f''(0)$	Ref [49] $-f''(0)$	Shooting $-f''(0)$	BVP4C $-f''(0)$
$\overline{0}$	1.0000	1.0000	1.0000	1.0000	1.0000
0.25	1.048813		1.048813 1.048812 1.048834 1.048834		
0.5			1.093097 1.093095 1.093095 1.093105		1.093105
0.75			1.134485 1.134485 1.134485 1.134491 1.134491		
1.0	1.173720		1.173721 1.173721 1.173723		1.173723

Table 4 Statistical shooting assessment and outcomes from bvp4c with Freidoonimehr and Rahimi [\[75\]](#page-15-15) and Wang [\[76\]](#page-15-16) for −*g*^{*n*}(0) when $\gamma = M = 0$, $\delta_t = 0$, $\delta_c = 0$, $Q = 0$ also all extended parameters are zero

movements, which uplifts the kinetic energy and thus causes the devaluation in the nanoparticle's concentration profles. Figure [28](#page-10-2) elucidates the efect of the Arrhenius activation energy on volumetric concentration profile ϕ . Intensifying the value of parameter E_1 , the nanoparticle concentration

Table 2 Statistical shoot assessment and outcom from bvp4c with Hayat [[72](#page-15-12)] and Freidoonimehr Rahimi $[75]$ $[75]$ $[75]$ for $-g''(0)$ $\gamma = M = 0, \delta_{\rm t} = 0, \delta_{\rm c} =$ also all extended param are zero

are zero

 $Table$

profles rise. From Figs. [29](#page-10-3)[–32,](#page-11-0) it is perceived that on top of the dimensionless rapidity components, heat distribution and the volumetric application profle give a good agreement of shooting technique and the bvp4c technique. A dual comparison is also presented in Tables [1](#page-11-1)[–4](#page-11-2) in which frstly the values of diferent parameters against existing reported results are taken into account and secondly it has been prepared in between two diferent techniques. It can easily be seen that our applied numerical scheme has produced exactly the same results with the existing shooting technique. An excellent agreement is established when a comparison has been made between current analysis and available results [[47–](#page-14-21)[49,](#page-14-23) [72,](#page-15-12) [75](#page-15-15)]. In Tables [1](#page-11-1) and [3,](#page-11-3) the values of −*f''*(0) are provided against parameters M and λ , while Tables [2](#page-11-4) and [4](#page-11-2) give the insight into values of same parameters when produced against $-g''(0)$. Additionally, some new results of local Nusselt number and Sherwood number for diferent physical parameters are also reported in Tables [5](#page-12-0) and [6,](#page-12-1) respectively. It is analyzed that local Nusselt number $-\theta'(0)$ rises with Pr, γ , N_h , Q, but it diminishes with δ_T , δ_E , N_T . The basic purpose of Table [6](#page-12-1) is to represent the various impacts of the key parameters Pr, δ_{t} , δ_{E} , γ , N_{T} , N_{b} on Sherwood number $\phi'(0)$. As for increasing values of N_T , E , γ getting the higher variation in $\phi'(0)$, the negative behavior is observed for the cases of N_r , N_b

Conclusions

The quantitative fndings of this study are as follows:

- Velocity decreases with higher values of magnetic parameter because of Lorentz forces, whereas temperature boosts up.
- Velocity and concentration decrease with higher values of slip parameter; however, the reverse conductivity is noted for temperature distribution.
- Velocity, temperature and concentration decline with rising values of stretching parameter.
- Enhancement of radiation parameter leads to enhancement of volume friction.
- The temperature distribution decreases with relaxation heat difusion.

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