

Comparison of heat capacity of solid explosives by DSC and group contribution methods

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Abstract The isobaric heat capacities of solid explosive materials were measured using differential scanning calorimeter. The values of C_p were determined at temperature 298.15 K and compared to theoretical data calculated using the group additivity approach. Several group contribution methods were tested, showing that certain method for some explosives provides estimation of C_p with error only 1 %. Generally, the average error limit for calculated C_p was about 11 %, which is insufficient.

Keywords Explosive material · Isobaric heat capacity · Differential scanning calorimetry · Modified stepwise method · Group contribution method

Introduction

Explosives are chemical substances or mixtures of chemical substances in metastable state. Explosives can be used in a number of ways, including explosive cladding, metal working (forming, welding and cutting) and shearing by pyrotechnics systems. However, the principal non-military use of explosives is in mining, quarrying, tunnelling, dam

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building, demolition, construction and other applications [1, 2]. Their inherent property, which makes them different from other chemicals, is ability to rapidly release chemical energy after proper initiation. The most common type of initiating event is some sort of a heat impulse (heat, flame, spark, local adiabatic compression, etc.), and it is therefore important to determine thermal stability and sensitivity of explosives. The thermal stability is important in shelf life analysis and evaluation of storage requirements, while thermal sensitivity is crucial for determination of temperature limits for safe handling and processing. Variety of methods exists and is routinely in use for evaluation of thermochemical properties of explosives [1]. Measurement of isobaric heat capacity (C_p) of explosives is not frequently published although this quantity can be used to calculate other thermodynamic properties. Moreover, $C_{\rm p}$ value is necessary for evaluation of experiments done by using accelerating rate calorimetry whose experimental results lead to most realistic approximation of real sample storage scenario (more about accelerating rate calorimetry can be found in [3–5]). However, C_p data are not so easily found in open literature.

The aim of this work is to determine the isobaric heat capacity values at 298.15 K for selected explosive materials in solid phase.

Experimental

The following explosive substances with purity over 95 % were selected: (a) standard explosives PETN, RDX, TNT, α -HMX, picric acid; (b) military explosives FOX-7, α -HNIW, ϵ -HNIW, NTO, A-IX-1, DINA, TNAZ, NQ, TEX; (c) improvised explosives DDNP (Dinol), UNi, ETN, TATP, DADP, HMTD; and (d) primary explosives MF

(mercury fulminate), GNGT (Tetrazene), LA (lead azide), LA dextrinized.

The molar heat capacities were measured using DSC Pyris 1 (PerkinElmer) with intracooler flushed with dry nitrogen at flow rate 20 cm³ min⁻¹. The temperature was calibrated to match melting point of several pure metals (Hg, Ga, In, Sn, Pb and Zn); the enthalpy was calibrated using enthalpy of fusion of indium. The metals necessary for calibration were weighted into aluminium pans. Explosive samples of mass about 10 mg were measured in sealed aluminium pans. The heat capacity measurements were repeated five times for each sample and standard material (sapphire, standard reference material 720, NIST) in the temperature range from (293 to 303) K with a heating rate 5 K min⁻¹ with isotherm 2 minutes at the beginning at 293 K and 1 minute at the end at 303 K (optimal conditions found in previous work [6]). The evaluation of C_p by so-called modified stepwise method is based on comparison between baseline, standard material and sample DSC curves and the areas under these curves, respectively (see Fig. 1). The heat capacity of studied sample can be calculated using Eq. (1), where $C_{\rm p}$ is the isobaric specific heat capacity, m is a sample mass and A is the area under relevant curve. Subscript b stands for baseline, star in superscript is used for sapphire and the values without star are for the sample.

$$C_{\rm p} = C_{\rm p}^* \left(\frac{m^* (A - A_{\rm b})}{m (A^* - A_{\rm b})} \right) \tag{1}$$

In the case of standard stepwise method (described in Ref. [7, 8]), the entire area bellow the curve (from before and after isothermal step) is used for C_p calculation. The modified stepwise method is based on integration of short temperature interval of the "step" [6]. The specific heat capacity of studied samples at the temperature 298.15 K was determined by the integration of each curve in the temperature range from 297.15 to 299.15 K as illustrated in Fig. 1b. Figure 2 shows DSC data of selected samples and sapphire as standard material. The deviation of heat capacity determined by DSC was tested using two "standard" materials (sapphire, standard reference material 720, NIST and molybdenum, reference material 781D2, NIST). The results showed deviation of C_p value under 2 % [6].

To make sure that the DSC will not be endangered in tested temperature range, all samples were first evaluated by explosion proof differential thermal analysis in DTA Ex550 (OZM Research). The decomposition temperatures were determined for all samples prior to heat capacity measurements. The calibration of DTA was done using indium (melting point). The sample mass varied based on the type of substance measured. Thermal decomposition of



Fig. 1 Heat flow dependence on time (a), or temperature (b) for baseline, sapphire and PETN for heat capacity determination by modified stepwise method. The temperature range for integration is emphasized, and the symbols of evaluation correspond to Eq. 1



Fig. 2 Dependence of heat flow on temperature for selected samples

primary explosives is quite violent, and they were therefore tested in amount of 5 mg. Less violently decomposing secondary explosives were measured in amount of 50 mg. All samples were measured at linear heating rate 5 K min⁻¹ in glass micro-test tubes under static air atmosphere.

Results and discussion

Explosive materials included in this study were selected to represent major types of explosives including both primary and secondary explosives. Commercially available materials and improvised explosives are included. Heat capacities (C_p) are available for some of the commercially available secondary explosives, and those were used for verification of our results. Data presented in this article for primary and improvised explosives are, to our best knowledge, not available in open literature.

DTA curves were used to characterize all the samples. The endothermic peaks were phase transition such as melting of the sample; the exothermic effects were always decompositions. The illustration of obtained DTA signals is given in Fig. 3. The temperatures of all endothermal and exothermal processes are summarized in Table 1, where symbol S stands for start and O for onset of the effect. In the cases of RDX, A-IX-1, TEX and UNi, endothermic effects overlap with exothermic one; thus, only the temperature of the maximum (max) of exothermic effect is given.

The isobaric heat capacity was measured by modified stepwise method using DSC. Values of the specific heat capacity calculated according Eq. 1 are summarized in Table 1 for all studied samples alongside with the literature data. The experimental results obtained by authors are in



Fig. 3 Temperature dependence of DTA signals of selected samples

good agreement with published values. The published values were in some cases obtained under different experimental conditions and therefore are not directly comparable with our results (data with note in Table 1).

Mercury fulminate (MF) and lead azide (LA) exhibit the lowest values of C_p (see Table 1). This may be due to their inorganic-like structure. Higher values of C_p but still below 1 J g⁻¹ K⁻¹ were determined for TEX and both forms of HNIW, which are substances with complicated caged structure. The rest of the samples are aliphatic substances and heterocycles without any systematic difference in C_p . Measured values were for all of the samples in these two groups close to 1.1 J g⁻¹ K⁻¹. The highest value of C_p was obtained for the two organic peroxides—DADP and TATP. This may be related to the high oxygen content in their molecules.

The precise experimental measurement of C_p is quite time-consuming and experimentally demanding [19]. Methodologies enabling estimation of C_p with reasonable accuracy were therefore proposed in the past. Generally, the methods can be divided into two groups; the first one is based on quantum–mechanical calculations and the second one on composition/structure of the substance (group contribution methods).

Sallamie and Shaw [20] developed a predictive technique employing density functional theory combined with the Debye–Einstein model to compute solid state C_p . It should be noted that this method is computationally intensive [20, 21]. On the contrary, the group contribution methods are easy to use, and the numerical treatment is very simple. These methods are used for estimation of the heat capacities in this paper. It should, however, be noted that these methods suffer from a limited number of group values that have been evaluated.

The group contribution methods assume that various groups (or only elements) of the molecule contribute to the total molar heat capacity. The application of majority of these methods is limited to narrow temperature ranges, and in most cases, they have been designed for specific groups of organic compounds (e.g. very precise method by Domalski and Hearing [22] is only for hydrocarbons at 298.15 K).

The simplest method is based on element contribution to the heat capacity of the substance. Kopp [23] presented values for fundamental elements of organic compounds but without value for nitrogen. Thus, only C_p value for TATP and DADP can be calculated by this method. The value calculated for both substances (1.628 J g⁻¹ K⁻¹) is higher than experimental results.

Hurst and Harrison [23] modified Kopp's rule to be able to estimate the solid and liquid heat capacities at temperature of 298 K. They tested their method and declared that the average absolute errors for the correlations are

Table 1 Isobaric specific heat capacity values at 298.15 K, C_p values from literature, temperatures of endothermic (T_{endo}) and exothermic (T_{exo}) effects determined for selected explosive materials

Explosive	Abbreviation	CAS registry no.	$C_{\rm p}/{\rm J}~{\rm g}^{-1}~{\rm K}^{-1}$	$C_{\rm p}/{\rm J}~{\rm g}^{-1}~{\rm K}^{-1}$ references	$T_{\rm endo}/{\rm K}$	$T_{\rm exo}/{\rm K}$
SE	PETN	78-11-5	1.083	1.084 [9]	S 404.15	S 428.15
				1.086 [10]	T_{endo}/K S 404.15 O 411.15 S 333.15 O 350.15 S 466.15 O 475.15 S 475.15 O 475.15 S 475.15 O 478.15 S 391.15 O 393.15 S 391.15 O 393.15 S 434.15 O 441.15 S 480.10 O 485.15 S 318.15 O 323.15 S 332.15 O 370.15 S 537.15 O 538.15 S 422.15 O 430.15 S 314.15 S 367.15 O 369.15 S 367.15 O 370.15	O 430.30
				1.090 [11]		
	TNT	118-96-7	1.139	1.145 [10]	S 333.15	S 523.15
				1.130 [12]	O 350.15	O 560.15
				1.170 [11]		
	RDX	121-82-4	1.054	1.046 [10]	S 466.15	Max 488.15
					O 475.15	
	α-HMX	2691-41-0	1.019	1.024 [10]	S 475.15	S 518.15
				1.006 [13]	O 478.15	O 542.15
				1.017 [14]		
				1.018 [1 4] δ-HMX		
				0.908 [15] gas HMX		
	Picric acid	88-89-1	1.065	1.065 [9]	S 391.15	S 495.15
				1.060 [10]	O 393.15	O 498.15
ME	FOX-7	145,250-81-3	1.202	1.192 [16]		S 450.15
						O 475.15
	α-HNIW	135,285-90-4	0.948			S 477.15
						O 495.15
	ε-HNIW	135,285-90-4	0.931		S 434.15	S 478.15
					O 441.15	O 497.15
	NTO	932-64-9	1.065	1.088 [17]		S 524.15
						O 539.15
	A-IX-1	n/a	1.042		S 480.10	Max 497.15
					O 485.15	
	DINA	4185-47-1	1.077		S 318.15	S 414.15
					O 323.15	O 456.15
	TNAZ	97,645-24-4	1.123		S 332.15	S 454.15
					O 370.15	O 484.15
	NQ	556-88-7	1.100	1.104 [18]		S 448.15
				1.129 [10]		O 494.15
	TEX	130,919-56-1	0.894		S 537.15	Max 573.15
					O 538.15	
IE	DINOL A	4682-03-5	1.056			S 416.15
						O 432.15
	UNi	124-47-0	1.325		S 422.15	Max 437.15
					O 430.15	
	ETN	7297-25-8	1.106		S 314.15	S 417.15
					O 321.15	O 455.15
	ТАТР	17,088-37-8	1.223		S 367.15	S 414.15
					O 369.15	O 419.15
	DADP	1073-91-2	1.508		S 367.15	S 417.15
		202 55 2	1.001		O 370.15	O 420.15
	HMTD	283-66-9	1.036			S 387.15
22		(2 0.04.)	0.400			O 408.15
PE	MF	628-86-4	0.430			S 413.15
						O 427.15

Table	1	continue	d
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Explosive	Abbreviation	CAS registry no.	$C_{\rm p}/{\rm J}~{\rm g}^{-1}~{\rm K}^{-1}$	$C_{\rm p}/{\rm J~g^{-1}~K^{-1}}$ references	T _{endo} /K	$T_{\rm exo}/{\rm K}$
	GNGT	31,330-63-9	1.094			S 401.15
						O 409.15
	LA	13,424-46-9	0.499			S 581.15
						O 587.15
	LA (dextrinized)	n/a	0.469			S 663.15
						O 673.15

SE standard explosive, ME military explosive, IE improvised explosive, PE primary explosive, S start temperature of DTA effect, O onset temperature of DTA effect

Table 2 Isobaric specific heat capacity values at 298.15 K calculated using elements contribution method by Hurst and Harrison [23], C_p^{Hur} , the group contributions by Chickos et al. [27], C_p^{Chi} and by Goodman et al. [28], C_p^{Goo}

Abbreviation	$C_{\rm p}^{\rm Hur}/{ m J}~{ m g}^{-1}~{ m K}^{-1}$	$(C_{\rm p}^{\rm Hur} - C_{\rm p})/C_{\rm p}/\%$	$C_{\rm p}^{\rm Chi}/{ m J}~{ m g}^{-1}~{ m K}^{-1}$	$(C_{\rm p}^{\rm Chi} - C_{\rm p})/C_{\rm p}/\%$	$C_{\rm p}^{\rm Goo}/{\rm J}~{\rm g}^{-1}~{\rm K}^{-1}$	$(C_{\rm p}^{\rm Goo} - C_{\rm p})/C_{\rm p}/\%$
PETN	1.110	2.5	1.665	53.7	1.282	18.4
TNT	1.104	3.1	1.206	5.9	1.071	6.0
RDX	1.220	15.8	1.106	5.0	1.065	1.0
α-HMX	1.220	19.7	1.106	8.6	1.143	12.2
Picric acid	1.040	2.4	1.138	6.9	0.962	9.6
FOX-7	1.220	1.5	1.164	3.2	1.029	14.4
α-HNIW	1.133	19.6	0.945	0.3	0.945	0.3
ε-HNIW		21.7		1.5		1.5
NTO	1.169	9.8	1.144	7.4	0.860	19.3
DINA	1.193	10.7	1.361	26.4	1.205	11.8
TNAZ	1.137	1.2	1.113	0.9	1.034	8.0
NQ	1.373	24.8	0.928	15.6	1.262	14.7
TEX	1.118	25.1	0.853	4.5	0.781	12.6
DINOL A	1.059	0.3	_	_	_	_
UNi	1.288	2.8	_	-	-	_
ETN	1.076	2.8	1.640	48.3	1.176	6.4
TATP	1.496	22.3	1.408	15.2	1.693	38.5
DADP	1.496	0.8	1.408	6.6	1.548	2.7
HMTD	1.317	27.1	1.001	3.4	1.179	13.8
MF	0.400	6.9	_	_	-	_
GNGT	1.504	37.5	-	-	_	_
LA	0.494	0.9	_	_	-	_

The difference between experimental and calculated value relates to experimental C_p is given in percentage

9.6 % for solid. The values calculated for substances studied in this work are summarized in Table 2. It can be seen that the values are within 10 % error from experimental results for 12 substances, from 20 to 25 % for 5 substances and over this limit for 2 substances. There does not seem to be correlation between the structure of the substance and the level of error of estimated C_p . Although the highest errors were estimated for substances with complicated cyclic structure where nitrogen or oxygen is situated into the cycle, there are exceptions—TNAZ with error of only 1.2 % where nitrogen is in the cycle. The

estimations for aromatic substances (TNT, picric acid, DINOL A) exhibit low error limits. Generally, the average error limit of all estimated C_p values is 11.8 % using Hurst and Harrison method.

Rihani and Doraiswamy [24] published group contributions method with ring formation corrections (their method is based on data for cycloalkane and alkene rings). Unfortunately, the published groups correspond to simpler structures without contributions of oxygen and nitrogen. The C_p values calculated by this method could therefore be determined only for 5 of the studied samples—TNT, picric acid (aromatic) and PETN, ETN, DINA (aliphatic). The estimated C_p values

Abbreviation	$C_{\rm p}^{\rm Rih}/{ m J}~{ m g}^{-1}~{ m K}^{-1}$	$(C_{\rm p}^{\rm Rih} - C_{\rm p})/C_{\rm p}/\%$	$C_{\rm p}^{\rm Sat}$ /J g ⁻¹ K ⁻¹	$(C_{\rm p}^{\rm Sat} - C_{\rm p})/C_{\rm p}/\%$
PETN	0.919	15.1	1.083	0
TNT	0.811	28.8	0.976	14.3
RDX	0.783	25.7	1.139	8.1
α-HMX	0.818	19.7	1.139	11.8
Picric acid	0.807	24.2	0.907	14.8
FOX-7	-	_	0.991	17.6
α-HNIW	-	-	1.021	7.7
ε-HNIW				9.7
DINA	0.955	11.3	1.157	7.4
TNAZ	0.783	30.3	1.040	7.4
NQ	1.054	4.2	_	-
TEX	-	_	1.064	19.0
ETN	0.867	21.6	1.048	5.2
TATP	1.157	5.4	1.449	18.5
DADP	1.144	24.1	1.449	3.9
HMTD	0.903	12.8	1.380	33.2

Table 3 Isobaric specific heat capacity values at 298.15 K calculated using the group contribution method by Rihani and Doraiswamy [24], C_p^{Rih} , and by Satoh [25, 26], C_p^{Sat}

The difference between experimental and calculated value relates to experimental $C_{\rm p}$ is given in percentage

are lower than the experimental ones, and the difference is higher for aromatic substances than for aliphatic. The values of C_p for other substances as given in Table 3 are only rough estimation with simplification (e.g. correction to 6-membered ring instead of 8-membered for α -HMX), and obtained values are in all cases lower then experimental results. The Rihani and Doraiswamy method can provide only rough estimation of C_p value with the average error limit of 18.6 % for our type of substances.

Krevelen and Nijenhuis [25] in their work emphasized contribution method developed by Satoh [26] bases on group contributions without corrections for ring formation. The limiting for his method is the absence of values for some important groups: -COO-, -CONH-, -SO2- and -F. Nevertheless, Satoh's method allows calculation of C_p for majority of substances studied in this work (see Table 3). The agreement with experimental values is better for Satoh's method and then for method proposed by Rihani and Doraiswamy, but the average error is 12.8 %.

Chickos et al. [27] published the group contribution method for heat capacity estimation of the condensed phase substances at 298 K with accuracy within 26.9 J mol⁻¹ K⁻¹ on data set containing 446 solids. The authors claimed that the standard error of estimation using their approach is almost the same as was a typical experimental uncertainty of their studied solids. The calculated values of C_p for studied samples as summarized in Table 2 give the average error of 13.2 %, but two substances, PETN and ETN, have error close to 50 %, and the calculated values are in both cases higher than the experimental ones. These results show that the error is in general higher than the Chickos et al. [27] declared in their work.

Goodman et al. [28] presented two methods for the estimation of C_p of solid organic compounds applicable to two temperature regions higher than 50 K. The power-law method utilizes empirical temperature dependence, while the partition function method is based on the Einstein-Debye partition function for crystals with a modified frequency distribution function. Both methods have fixed temperature functionality but utilize group contributions to obtain the compound-specific constants in the predictive equations. Tests on the methods' extrapolation capabilities suggest that at 298 K they have comparable accuracy to Domalski and Hearing [22] method or method of Hurst and Harrison [23]. The power-law method was used to calculate the $C_{\rm p}$ values for studied samples, and the results are summarized in Table 2. This method provides results without any extreme value as was obtained in previous case by method of Chickos et al. [27], and the average error is 11.2 %.

The comparison of all methods for estimation of C_p leads us to conclusion that the most accurate results were obtained using Hurst and Harrison [23] method and Goodman et al. [28] method.

Conclusions

The isobaric heat capacity of selected explosive materials was measured using differential scanning calorimeter. The heat capacity at 298.15 K was determined for 24 explosive materials in solid state, where for 16 of them the heat capacity data were not presented in open literature up to now. Several group contribution methods were used to estimate C_p values for studied samples. The comparison with experimental results shows that the average error limit of estimated C_p is not lower than 11 %, which is insufficient when heat capacity data should be used for other calculations.

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