# Thermal and flame retardant properties of novel intumescent flame retardant polypropylene composites

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Abstract Novel intumescent flame retardant polypropylene (PP) composites were prepared based on a char forming agent (CFA) and silica-gel microencapsulated ammonium polyphosphate (Si-MCAPP). The thermal and flame retardancy of flame retardant PP composites were investigated by limiting oxygen index, UL-94 test, cone calorimetry, thermogravimetric analysis, scanning electron micrograph, and water resistance test. The results of cone calorimetry show that the flame retardant properties of PP with 30 wt% novel intumescent flame retardants (CFA/ Si-MCAPP = 1:3) improve greatly. The peak heat release rate and total heat release decrease, respectively, from 1,140.0 to 156.8 kW m<sup>-2</sup> and from 96.0 to 29.5 MJ m<sup>-2</sup>. The PP composite with CFA/Si-MCAPP = 1:3 has the excellent water resistance, and it can still obtain a UL-94 V-0 rating after 168 h soaking in water.

**Keywords** Polypropylene · Fire retardant · Cone calorimeter · Microencapsulation · Intumescent

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#### Introduction

Polypropylene (PP) as one of the most widely used polyolefins has broad applications in many areas such as cars, architectural materials, and so on. However, as we know it is combustible and releases smoke and poisonous gas while burning. Easy combustibility restricts the range of its applying fields. Therefore, it is necessary to make this plastic flame retardant to reduce the emission of smoke, poisonous gases, and so on [1]. The halogenated organic compounds were good fire retardant additives for PP, especially synergizing with antimony trioxide. However, halogenated flame retardant PP composites have serious disadvantages such as the evolution of toxic gases and corrosive chemical fumes. Thus, more and more researchers are exploring halogen-free flame retardants. The effective halogen-free flame retardants are intumescent flame retardants (IFRs) [2, 3]. It is mainly composed of an acid source, a carbon source, and a gas source.

Among many intumescent flame retardant PP methods, a traditional and widely studied IFRs system is based on ammonium polyphosphate (APP), pentaerythritol (PER), and melamine [4–6]. Unfortunately, APP and PER are not durable due to the water solubility, so the flame retardant effect of those IFRs system is not permanent, and limits the application of IFRs in PP composites. In order to overcome poor water resistance problem, the technique of microencapsulation is a good choice. Microencapsulation protects encapsulated inner substances from some degrading reagents such as water. Microencapsulated APP has been synthesized with different materials such as PVA-melamine-formaldehyde resin, polyurethane, urea-melamine-formaldehyde resin, silica gel, and so on, and has been used in flame retardant polymer such as PP, PU, and so on [7-10]. Silica-gel microencapsulated APP (Si-MCAPP) is a kind of ammonium polyphosphate which is well microencapsulated by SiO<sub>2</sub> gel. Si-MCAPP as one of the novel microencapsulated APP with good water resistance has attracted more and more attention [7]. Due to low surface energy, silicon-containing compounds tend to migrate and concentrate on the surface of polymer materials, and can form a protective silica layer during combustion, which can protect the matrix from further thermal decomposition. Furthermore, the synergistic effect between siliconcontaining compounds and IFRs has been demonstrated and researches have shown that silicon improves the thermal stability and flame retardancy of IFR polymer composites [11–13]. So, Si-MCAPP is expected to have better flame retardancy than those of other microencapsulated APP.

Another solution to solve poor water resistance problem of flame retardants is to synthesize new carbon sources with good water resistance property. Among those new char formers, triazine derivative—CFA-containing chemical groups of hydroxyethylamino, triazine rings and ethylenediamine has been regarded as an excellent macromolecule char forming agent with excellent flame retardant properties and water resistance. Until now, CFA has been used in many polymer matrices such as PP, EVA, and so on [14–17].

In this work, CFA and Si-MCAPP were selected to form novel IFRs, and then the influence of these novel intumescent flame retardants on the thermal and flame retardant properties of PP were investigated by limiting oxygen index (LOI), UL-94 test, thermogravimetric analysis (TG), and scanning electron micrograph (SEM), especially by cone calorimetry and water resistance test. Through this research, we hope to provide an efficient intumescent flame retardant technique with excellent water resistance ability.

### Experiment

### Materials

PP (homopolymer, melt-flow rate = 2.5 g/10 min) was supplied as pellets by Yangzi Petrochemical Co. (China). CFA and Si-MCAPP were synthesized in our previous work [7, 16], and the structure of CFA is shown in Fig. 1. Si-MCAPP is a kind of ammonium polyphosphate which is well microencapsulated by SiO<sub>2</sub> gel. APP and pentaerythritol (petol) (powder, average size < 10 µm) were kindly provided by KeYan Co. (Hefei, China).

The preparation of samples

PP, Si-MCAPP, and CFA were dried in vacuum oven at 80 °C overnight before use. Then PP, Si-MCAPP, and CFA were melt-mixed in a twin-roller mill (XSS-300, China) for 10 min; the temperature of the mill was maintained at 175 °C and the roller speed was 60 rpm. The samples are



Fig. 1 The structure of CFA

Table 1 Formulations of the flame retardant PP composites

Sample	PP	Si-MCAPP	CFA	APP	PER	UL-94
PP0	100					Burning
PP1	70	30				Burning
PP2	70		30			Burning
PP3	70	22.5	7.5			V-0
PP4	70	20	10			V-0
PP5	70	15	15			V-0
PP6	70	10	20			Burning
PP7	75	18.75	6.25			V-0
PP8	80	15	5			V-1
PP9	70			22.5	7.5	V-0

listed in Table 1. The resulting composites were hot-pressed into sheets with suitable thickness and size for UL-94, LOI, and cone calorimeter tests.

Determination of water resistance of flame-retarded PP material

The flame-retarded PP materials were put in distilled water at 70 °C and were kept at this temperature for various time periods. The specimens were subsequently removed, dried in the vacuum oven, and evaluated by burning tests.

### Characterization

Thermogravimetric analyses were carried out using a Mettler-Toledo TGA/SDTA851e instrument from 35 to 800 °C at a linear heating rate of 20 °C min<sup>-1</sup> under an air flow rate of 50 ml min<sup>-1</sup>. Samples were measured in an alumina crucible with a mass of about 3–6 mg.

The combustion properties were evaluated using a cone calorimeter. All samples  $(100 \times 100 \times 3 \text{ mm}^3)$  were exposed to a Stanton Redcroft cone calorimeter under a heat flux of 50 kW m<sup>-2</sup> according to ISO-5660 standard procedures.

The scanning electron microscopy image of the residue after the cone calorimetry experiment was taken using a DXS-10 scanning electron microscope produced by Shanghai Electron Optical Technology Institute. The char was adhibited on the copperplate, and then coated with gold/palladium alloy ready for imaging.

LOI was measured according to ASTM D2863, and the apparatus used was an HC-2 oxygen index meter (Jiangning Analysis Instrument Company, China). The specimen dimensions used for test were  $100 \times 6.5 \times 3 \text{ mm}^3$ . The vertical burning test was carried out on a CFZ-2-type instrument (Jiangning Analysis Instrument Company, China), and the specimens used for the test are  $100 \times 13 \times 3 \text{ mm}^3$ .

## **Results and discussion**

# LOI and UL-94 analysis of flame-retarded PP composites

Figure 2 shows the LOI results for the various flame retardant PP compositions. PP is an easily combustible polymeric material, and the LOI value of PP is only 17.5 %. When CFA with 30 wt% is added in PP, the LOI value of PP composites is 24.0 %, and this PP composite is easy to burn. Si-MCAPP can increase the LOI value of the PP composites much better than that of CFA, its LOI reaches to 27.0 %. However, it still can get burned. Neither of the above samples can reach UL-94 V-0 rating. The above results show that Si-MCAPP and CFA alone have low efficiency in flame retardancy of PP. When CFA and Si-MCAPP are combined, the LOI value of PP composite is remarkably increased. The LOI value of PP/CFA/Si-MCAPP (1:1) is 34.0 % and the LOI increases with an increasing amount of Si-MCAPP. The sample of PP/CFA/ Si-MCAPP (1:3) gives the largest LOI value of 40.0 %. The results of UL-94 vertical burning rate show that all the PP/CFA/Si-MCAPP composites can pass UL-94 V-0 rating, when the mass ratio of CFA to Si-MCAPP is between



Fig. 2 The LOI results of flame retardant PP composites

Water resistance of flame retardant PP composites

Water resistance test of Sample PP3 (CFA/Si-MCAPP = 1:3) and Sample PP9 (PER/APP = 1:3) with 30 wt% as the total amount of additives is carried on. Both of the samples are treated with water at 70 °C for different times and their flame retardant properties are evaluated (Table 2). It can be found that before water treatment both the samples can pass UL-94 V-0 rating. After being soaked in water for 24 h, Sample PP8 with PER/APP = 1:3 shows a very poor water resistance. The sample looses UL-94 rating and burns seriously. The sample with CFA/Si-MCAPP = 1:3 has very excellent resistance property, after 168 h the sample can still obtain a UL-94 V-0 rating. The water resistance test demonstrates that flame retardant PP prepared based on CFA/Si-MCAPP has excellent water resistance.

### Thermal stability

TG was used to investigate the thermal behavior of CFA/ Si-MCAPP systems, and the TG curves are shown in Fig. 3. It can be seen that the decomposition of CFA consists of two main steps i.e., 254–344, 344–700 °C. CFA itself has a good charring ability, and produces 59.2 % char residue at 500 °C, 39.8 % at 600 °C, and 11.0 % at 800 °C. The degradation of Si-MCAPP can be divided into two temperature regions. The first region with 5 wt% loss is at 285 °C. The volatile products in this region are mainly NH<sub>3</sub> and H<sub>2</sub>O, and a crosslinked polyphosphoric acid layer is formed in this step [7]. The second region is the main decomposition process, which occurs between 500 and 700 °C. The residue of Si-MCAPP is 80.6 % char residue at 500 °C, 73.4 % at 600 °C, and 32.4 % at 800 °C, respectively.

**Table 2** The UL-94 testing results of flame retardant PP compositesafter water treatment with a 30 wt% total loading level of additives

	PP4	PP9
24 h	V-0	Burning
48 h	V-0	Burning
72 h	V-0	Burning
96 h	V-0	Burning
168 h	V-0	Burning



Fig. 3 TG curves of CFA/Si-MCAPP systems under air atmosphere

It can be observed that CFA/Si-MCAPP (1:3) system produces, respectively, 70.3 % char residue at 500 °C, 66.0 % at 600 °C, and 40.0 % at 800 °C. But the calculated char residue of CFA/Si-MCAPP system by calculating the datum of Si-MCAPP and CFA should be 75.3 % at 500 °C, 65.5 % at 600 °C, and 27.0 % at 800 °C, respectively. At temperature higher than 600 °C, the CFA/Si-MCAPP system shows greatly improved thermal stability than that of calculated one. It demonstrates that some synergistic effects exist between CFA and Si-MCAPP due to chemical interactions between CFA and Si-MCAPP, such as the phosphorylation reaction and the stabilization of polyphosphoric acid by forming bridges or crosslinks between adjacent chains, which can inhibit the further decomposition of the system at high temperature. CFA/ Si-MCAPP (1:1) system produces, respectively, 64.9 % char residue at 500 °C, 60.6 % at 600 °C, and 22.5 % at 800 °C. Comparing between CFA/Si-MCAPP (1:1) with CFA/Si-MCAPP (1:3), it can be observed that CFA/ Si-MCAPP (1:3) is thermally stabler than CFA/Si-MCAPP (1:1).

Figure 4 shows the decomposition of flame retardant PP composites. The curve for pure PP shows one step degradation of total mass loss in the range of 230–400 °C, and has no char residue beyond the temperature of 400 °C. Compared to pure PP, the flame retardant PP composites (Fig. 4) show poorer thermal stability before 270 °C, mainly due to the decomposition of Si-MCAPP, the formation of ester mixtures between –P–OH group in Si-MCAPP and –OH group in CFA and the formation of a char layer. Above 270 °C, the flame retardant PP composites have much better thermal stability and have about 15 % char compared with almost nothing for pure PP. The ratio of CFA/Si-MCAPP affects the thermal stability of the flame retardant PP composite. Sample PP3 with the ratio of CFA/Si-MCAPP = 1/3



Fig. 4 TG curves of PP and flame retardant PP composites under air atmosphere



Fig. 5 The HRR curves of PP and flame retardant PP composites with a 30 wt% total loading level of additives



Fig. 6 The THR curves of PP and flame retardant PP composites with a 30 wt% total loading level of additives

Fig. 7 SEM photographs of flame retardant PP composites after the flame extinguished. a PP2, b PP1, c PP3, and d PP5



has 19.5 % char left at 600 °C, and has higher thermal stability than that (15.1 % char left) of sample PP5 with the ratio of CFA/Si-MCAPP = 1/1. From the above results it can be concluded that CFA/Si-MCAPP has a synergistic effect and can obviously improve the thermal stability of PP. Meanwhile, the ratio of CFA/Si-MCAPP is also very important.

### Cone calorimeter test

Cone calorimetry is a small-scale test for the combustion of the materials, but it has good correlation with real fire disaster and provides a wealth of information on the combustion behavior [18, 19]. The heat release rate (HRR) and total heat release (THR) are regarded as important parameters to evaluate the developing, spreading, and intensity of fires. The HRR curves of PP and flame retardant PP composites are shown in Fig. 5. From the figure it is clear that pure PP burns intensely, with only a peak heat release rate (pHRR) of 1140.0 kW  $m^{-2}$ . With the addition of CFA or Si-MCAPP with 30 wt% in PP, the pHRR value of PP composites is 638.1 and 616.7 kW m<sup>-2</sup>, respectively. Si-MCAPP can decrease the pHRR value of the PP composites better than that of CFA. Just as LOI results demonstrate that Si-MCAPP and CFA alone have low efficiency in flame retardancy of PP. When CFA and Si-MCAPP are mixed with a certain ratio, the pHRR value of PP composite is remarkably decreased. The pHRR value of the sample with CFA/Si-MCAPP = 1:3 is the lowest (156.8 kW m<sup>-2</sup>), with 86.2 % decrease compared with that of pure PP. As the CFA:Si-MCAPP ratio increases, the pHRR value of flame retardant PP composites increases from 156.8 to 408.0 kW m<sup>-2</sup> (PP6). The reason for the decrease of the HRR value can be due to the formation of the intumescent protective char layer through etherification, dehydration, expansion, and crosslinking process, when PP composites are subjected to high temperature. The blowing agent decomposes to produce gaseous products and causes the char to swell. With the presence of the efficient protective char layer, the amount of heat and combustible gas decreases greatly, and the further degradation of inner PP is prevented, so the HRR value decreases [20, 21].

The THR curves of PP and flame retardant PP composites are shown in Fig. 6. It can be found from Fig. 6 that the THR decreases from 96 MJ m<sup>-2</sup> in PP to 93.4 and 81.7 MJ m<sup>-2</sup> in PP/CFA and PP/Si-MCAPP, finally to 89.4 MJ m<sup>-2</sup> at CFA:Si-MCAPP = 2:1 (PP6) and to 29.5 MJ m<sup>-2</sup> at CFA:Si-MCAPP = 1:3 (PP3). Obviously the ratio of CFA and Si-MCAPP effects the flame retardant behavior of flame retardant PP composites. From the result of PP3 and PP6, it can be observed only with suitable ratio, flame retardant PP composite can get the best flame retardant properties. SEM analysis of char residue after combustion

SEM (Fig. 7) also shows very different char morphology of the flame retardant PP composites obtained during LOI test. Investigation on the morphology of the char is helpful to explain the differences in the flame retardancy among the flame retardant PP composites. For PP/Si-MCAPP (PP1) without CFA (Fig. 7b), a compact charred layer is formed, but it is not able to swell and form intumescent char layer due to the lack of a carbon source. PP/CFA (PP2) without Si-MCAPP (Fig. 7a) shows a loose char layer with a lot of holes on the surface, and this kind of charred layer has poor protective effect during combustion. The intumescent charred layer of sample PP3 (Fig. 7c) is very compact and much char stacked together seemed to possess bigger thickness and less susceptible to crack, which provides a much better barrier to the transfer of the heat, combustible gases, and free radicals during a fire [22]. So, it can be concluded that when CFA and Si-MCAPP are synergized together at a certain ratio, a high quality of charred layer can be formed. It can also be found that the ratio of Si-MCAPP and CFA influence the morphology of the intumescent charred layer. For PP5 (Fig. 7d) with the CFA/Si-MCAPP ratio is 1:1, char layer is swollen and has some holes, so the flame retardant ability is not as good as that of PP3.

# Conclusions

Novel intumescent flame retardant PP composites were prepared based on CFA and Si-MCAPP. The thermal and flame retardancy of flame retardant PP composites were investigated. With the addition of 30 wt% IFRs (CFA/Si-MCAPP = 1:3), the LOI value can reach 40.0 %. When the loading of IFRs is only 25 wt% in PP, the flame retardant PP composite still obtains UL-94 V-0 rating. The results of Cone calorimetry experiments show that the pHRR and THR significantly decrease with the addition of 30 wt% IFRs (CFA/Si-MCAPP = 1:3) in PP. The pHRR and THR decrease, respectively, from 1,140.0 to 156.8 kW m<sup>-2</sup> and from 96.0 to 29.5 MJ m<sup>-2</sup>. The water resistance test proves that the PP composites with CFA/Si-MCAPP = 1:3 has the best water resistance property, and it can still pass UL-94 V-0 rating after 168 h soaking in water. SEM indicates that CFA/Si-MCAPP system can form excellent and compact char residue, which can better endure the oxidation of high temperature. From the above results, we can summarize that the combining of CFA and Si-MCAPP in PP matrix can prepare novel flame retardant PP composites with good flame retardant properties and with excellent water resistance ability.

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