

# Magnetocaloric properties of $\text{La}_{0.6}\text{Ca}_{0.4}\text{MnO}_3$

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**Abstract** A theoretic work on magnetocaloric properties of the polycrystalline  $\text{La}_{0.6}\text{Ca}_{0.4}\text{MnO}_3$  system near a second-order phase transition from a ferromagnetic to a paramagnetic state is presented. The value of the magnetocaloric effect has been determined from the calculation of magnetization as a function of temperature under different external magnetic field shifts. The magnetic entropy change  $\Delta S_M$  reaches a peak of about  $3 \text{ J kg}^{-1} \text{ K}^{-1}$  at 266 K upon 1.60 KA/m applied field variation. The  $\Delta S_M$  distribution is much more uniform than that of gadolinium, which is desirable for an Ericson-cycle magnetic refrigerator, which is beneficial for the household application of active magnetic refrigerant materials.

**Keywords**  $\text{La}_{0.6}\text{Ca}_{0.4}\text{MnO}_3$  · Magnetocaloric effect · Model · Magnetic entropy change · Heat capacity change

## Introduction

The refrigeration by magnetocaloric effect (MCE) and electrocaloric effect (ECE) offer a lot of clear advantages over the conventional gas compression refrigeration technology [1–9]. These provide efficient and environment-friendly solutions for cooling. It is more efficient, inexpensive, and environmentally friendly for replacing the current refrigerators using greenhouse gases that are harmful to environment and contributing to global warming.

Characterization and application of the magnetic properties of ferromagnetic particles become increasingly

important for the level of miniaturization and reliability necessary for commercialization [10].

Perovskite manganites have attracted significant attention since the discovery of colossal magnetoresistance and several interesting properties of these compounds have been found. In recently years, there has been an increasing interest in using manganites not only as a material having colossal magnetoresistivity but also as a material with interesting magnetocaloric properties [11–13].

A large magnetocaloric effect makes manganites excellent candidates for working materials in magnetic refrigeration units especially because they are less costly than other materials, particularly those based on Gd.

In this paper, theoretic work on magnetization versus temperature in different magnetic field shifts for polycrystalline  $\text{La}_{0.6}\text{Ca}_{0.4}\text{MnO}_3$  system. It is used a phenomenological model for simulation of magnetization dependence on temperature variation to predict magnetocaloric properties such as magnetic entropy change, heat capacity change, temperature change, and relative cooling power.

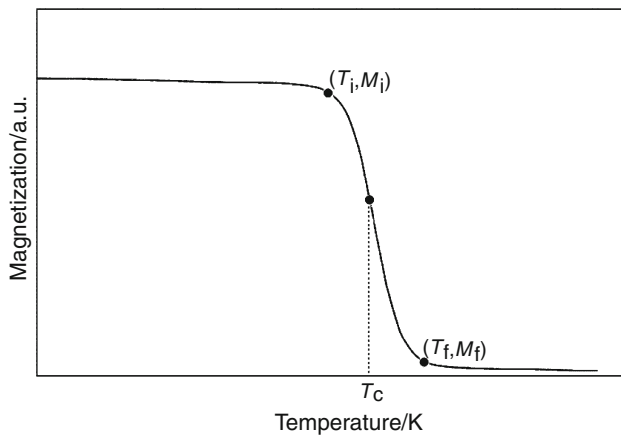
## Theoretic considerations

According to phenomenological model in Hamad [14], the dependence of magnetization on variation of temperature and Curie temperature  $T_c$  is presented by

$$M = \left( \frac{M_i - M_f}{2} \right) [\tanh(A(T_c - T))] + BT + C, \quad (1)$$

where  $M_i$  is an initial value of magnetization at ferromagnetic–paramagnetic transition and  $M_f$  is a final value of magnetization at ferromagnetic–paramagnetic transition as shown in Fig. 1.

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**Fig. 1** Temperature dependence of magnetization in constant applied field

$$A = \frac{2(B - S_c)}{M_i - M_f},$$

$B$  is magnetization sensitivity  $\frac{dM}{dT}$  at ferromagnetic state before transition,  $S_c$  is magnetization sensitivity  $\frac{dM}{dT}$  at Curie temperature  $T_C$  and

$$C = \left(\frac{M_i + M_f}{2}\right) - BT_C.$$

A magnetic entropy change of a magnetic system under adiabatic magnetic field variation from 0 to final value  $H_{\max}$  is available by

$$\Delta S_M = \left(-A \left(\frac{M_i - M_f}{2}\right) \operatorname{sech}^2(A(T_C - T)) + B\right) H_{\max}. \quad (2)$$

The foundation of large magnetic entropy change is attributed to high magnetic moment and rapid change of magnetization at  $T_C$ . A result of Eq. (2) is a maximum magnetic entropy change  $\Delta S_{\max}$  (where  $T = T_C$ ) can be evaluated as following the equation

$$\Delta S_{\max} = H_{\max} \left(-A \left(\frac{M_i - M_f}{2}\right) + B\right). \quad (3)$$

Eq. (3) is an important equation for taking into consideration of value of the magnetic entropy change to evaluate

magnetic cooling efficiency with its full-width at half-maximum.

A determination of full-width at half-maximum ( $\delta T_{\text{FWHM}}$ ) can be evaluated as follows:

$$\delta T_{\text{FWHM}} = \frac{2}{A} \cosh^{-1} \left( \sqrt{\frac{2A(M_i - M_f)}{A(M_i - M_f) + 2B}} \right). \quad (4)$$

This equation gives a full-width at half-maximum magnetic entropy change contributing for estimation of magnetic cooling efficiency as follows.

A magnetic cooling efficiency is estimated by considering magnitude of magnetic entropy change,  $\Delta S_M$  and its full-width at half-maximum ( $\delta T_{\text{FWHM}}$ ) [13]. A product of  $-\Delta S_{\max}$  and  $\delta T_{\text{FWHM}}$  is called relative cooling power (RCP) based on magnetic entropy change.

$$\begin{aligned} \text{RCP} &= -\Delta S_M(T, H_{\max}) \times \delta T_{\text{FWHM}} \\ &= \left(M_i - M_f - 2\frac{B}{A}\right) H_{\max} \\ &\quad \times \cosh^{-1} \left( \sqrt{\frac{2A(M_i - M_f)}{A(M_i - M_f) + 2B}} \right). \end{aligned} \quad (5)$$

The magnetization-related change of the specific heat is given by [13]

$$\Delta C_{P,H} = T \frac{\delta \Delta S_M}{\delta T}. \quad (6)$$

According this model [14],  $\Delta C_{P,H}$  can be rewritten as

$$\Delta C_{P,H} = -TA^2(M_i - M_f) \operatorname{sech}^2(A(T_C - T)) \tanh(A(T_C - T)) H_{\max}. \quad (7)$$

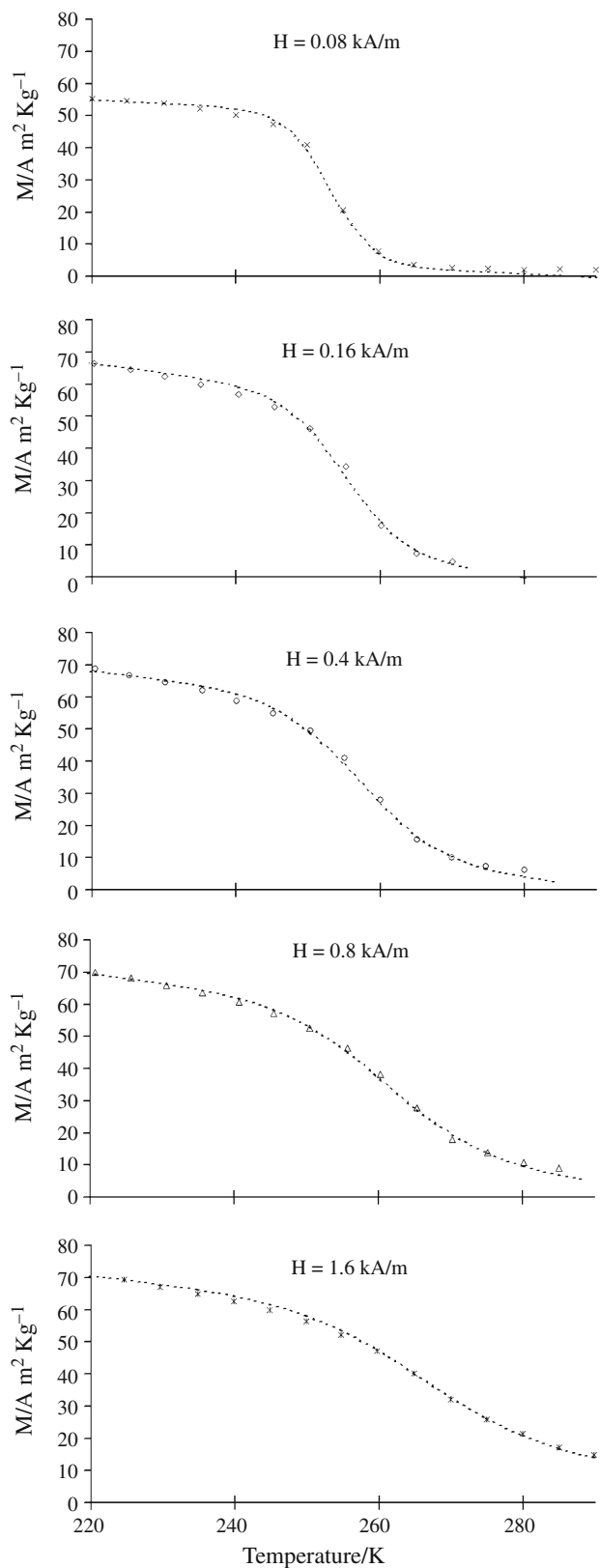
A temperature change of a magnetic system under adiabatic magnetic field variation from 0 to  $H_{\max}$  can be written in the form

$$\begin{aligned} \Delta T &= -\frac{T}{C_P} \int_0^{H_{\max}} \left(\frac{\partial M}{\partial T}\right)_E dH, \\ &= \frac{AT(M_i - M_f)}{2C_P} [\operatorname{sech}^2(A(T_C - T)) + B] H_{\max}. \end{aligned} \quad (8)$$

$C_P$  is the heat capacity per mole at constant magnetic field.

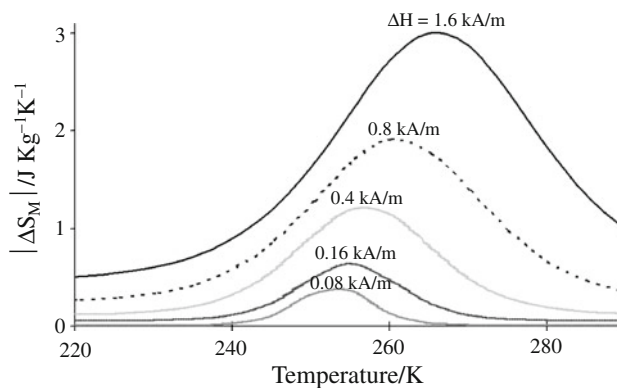
**Table 1** Model parameters for  $\text{La}_{0.6}\text{Ca}_{0.4}\text{MnO}_3$  in different applied magnetic fields

$H/\text{KA m}^{-1}$	$M_i/A \text{ m}^2 \text{ kg}^{-1}$	$M_f/A \text{ m}^2 \text{ kg}^{-1}$	$T_C/\text{K}$	$B/A \text{ m}^2 \text{ kg}^{-1} \text{ K}^{-1}$	$S_c/A \text{ m}^2 \text{ kg}^{-1} \text{ K}^{-1}$
0.08	51.25	3.65	253	-0.11	-4.08
0.16	56.30	7.00	255	-0.29	-3.22
0.40	59.50	8.50	257	-0.23	-2.45
0.80	59.80	11.00	261	-0.24	-1.91
1.60	60.10	17.10	266	-0.23	-1.50

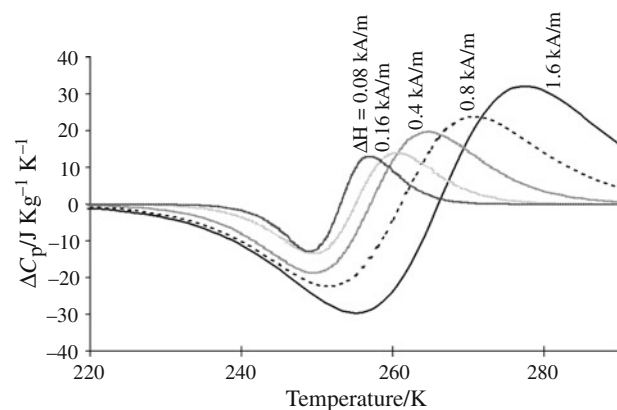


**Fig. 2** Magnetization in different applied magnetic field shifts for the  $\text{La}_{0.6}\text{Ca}_{0.4}\text{MnO}_3$  versus temperature. The *dashed curves* are modeled results and symbols represent experimental data from ref. [12]

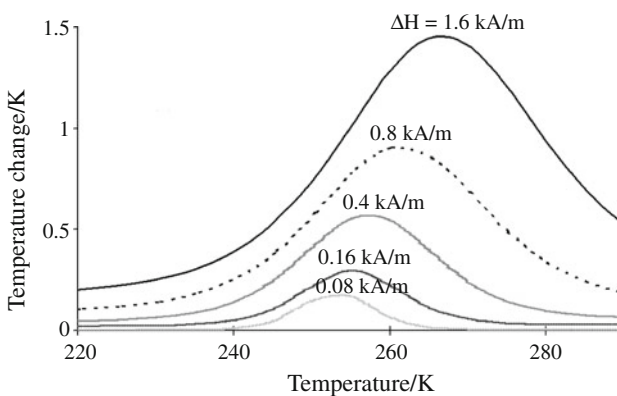
From this phenomenological model, it can easily assess the values of  $\delta T_{\text{FWHM}}$ ,  $|\Delta S|_{\text{max}}$ , RCP, and  $\Delta T$  for  $\text{La}_{0.6}\text{Ca}_{0.4}\text{MnO}_3$  under magnetic field variation.



**Fig. 3** Magnetic entropy change as function of temperature for  $\text{La}_{0.6}\text{Ca}_{0.4}\text{MnO}_3$  in different applied magnetic field shifts



**Fig. 4** Heat capacity changes as function of temperature for  $\text{La}_{0.6}\text{Ca}_{0.4}\text{MnO}_3$  in different applied magnetic field shifts



**Fig. 5** Temperature changes as function of temperature for  $\text{La}_{0.6}\text{Ca}_{0.4}\text{MnO}_3$  in different applied magnetic field shifts

**Table 2** The predicted values of applied magnetocaloric properties for  $\text{La}_{0.6}\text{Ca}_{0.4}\text{MnO}_3$  in different applied magnetic field shifts

$\Delta H/\text{KA m}^{-1}$	$-\Delta S_{\text{max}}/\text{J kg}^{-1} \text{K}^{-1}$	$\delta T_{\text{FWHM}}/\text{K}$	$\text{RCP}/\text{J kg}^{-1}$	$\Delta C_{\text{P,H(max)}}/\text{J kg}^{-1} \text{K}^{-1}$	$\Delta C_{\text{P,H(min)}}/\text{J kg}^{-1} \text{K}^{-1}$	$ \Delta T _{\text{max}}/\text{K}$
0.08	0.37	10.80	4.024	13.16	-12.75	0.17
0.16	0.65	16.04	10.37	13.98	-13.35	0.30
0.40	1.20	21.98	26.33	19.75	-18.59	0.56
0.80	1.92	28.85	55.26	23.93	-22.20	0.91
1.60	3.00	34.42	103.39	32.14	-29.59	1.45

### Theoretic work

Numerical calculations were made with parameters as displayed in Table 1. A heat capacity  $C_p = 550 \text{ J kg}^{-1} \text{ K}^{-1}$  [15, 16]. Figure 2 shows the magnetization versus temperature in different applied magnetic field shifts for  $\text{La}_{0.6}\text{Ca}_{0.4}\text{MnO}_3$  polycrystals have been prepared by a non-standard ceramic method with presintering at 1,100 °C and final sintering at 1,350 °C. The symbols represent experimental data from ref. [12], while the dashed curves represent modeled data using model parameters given in Table 1. It is seen that for the given parameters, the results of calculation are in a good agreement with the experimental results. Furthermore, Figs. 3, 4, and 5 show predicted values for changes of magnetic entropy, specific heat, and temperature versus temperature. Magnetic entropy change in  $\text{La}_{0.6}\text{Ca}_{0.4}\text{MnO}_3$  is reported in Fig. 3 and shows an increase in  $|\Delta S_M|$  with increasing  $\Delta H$ . The magnetic entropy change curves reveal the characteristics of the spin reorientation by the kinks in the  $\Delta S_M$  curve. The maxima observed in the  $\Delta S_M$  curves are associated to a spin reorientation that occurs continuously. The behavior of curves suggests how to extend the range of temperatures for use in the MCE.

The values of maximum magnetic entropy change, full-width at half-maximum, and relative cooling power at different magnetic field shifts for  $\text{La}_{0.6}\text{Ca}_{0.4}\text{MnO}_3$  are calculated by Eqs. 3–5, respectively, and tabulated in Table 2. Furthermore, the maximum and minimum values of specific heat change for each sample is determined from Fig. 4.

Both  $\Delta S_M$  and  $\Delta T$  reflect a fundamental importance on the understanding of the behavior of the MCE, and these terms can be approximately estimated by Eqs. 2 and 8, respectively. As shown in Fig. 3,  $\Delta S_M$  reaches a peak of about  $3 \text{ J kg}^{-1} \text{ K}^{-1}$  at 266 K upon 1.60 KA/m applied field variation. Though the maximum  $\Delta S_M$  is  $1.92 \text{ J kg}^{-1} \text{ K}^{-1}$  upon 0.80 KA/m applied field variation which is about 70 % of that of a pure Gd metal  $2.8 \text{ J kg}^{-1} \text{ K}^{-1}$  upon 0.80 KA/m, the  $\Delta S_M$  distribution of the  $\text{La}_{0.6}\text{Ca}_{0.4}\text{MnO}_3$  is much more uniform than that of gadolinium [17, 18]. This feature is desirable for an Ericsson-cycle magnetic refrigerator [19].

Although  $\text{La}_{0.6}\text{Ca}_{0.4}\text{MnO}_3$  is very similarly to research  $\text{La}_{0.67}\text{Ca}_{0.33}\text{MnO}_3$  in Hamad [14], the magnetic entropy changes of  $\text{La}_{0.6}\text{Ca}_{0.4}\text{MnO}_3$  and  $\text{La}_{0.67}\text{Ca}_{0.33}\text{MnO}_3$  have great difference. This due to the methods and conditions of

synthesizing of two samples are different. Moreover, the former has a polycrystalline structure, while the latter has a single crystalline structure.

In general, the large magnetic entropy change in perovskite manganites has been believed to be related to the considerable variation of magnetization near  $T_C$  [20]. The spin–lattice coupling in the magnetic ordering process could play a significant role in additional magnetic entropy change [21]. Owing to the strong coupling between spin and lattice, significant lattice change accompanying magnetic transition in perovskite manganites has been observed [22, 23]. The lattice structural change in the Mn–O bond distance as well as Mn–O–Mn bond angle would, in turn, favor the spin ordering. Thereby, a more abrupt reduction of magnetization near  $T_C$  occurs and results in a significant magnetic entropy change [16, 24–26]. In this way, a conclusion might be drawn that a strong spin–lattice coupling in the magnetic transition process would lead to additional magnetic entropy change near  $T_C$ , and consequently, favors the MCE.

### Conclusions

Dependence of the magnetization on temperature variation for  $\text{La}_{0.6}\text{Ca}_{0.4}\text{MnO}_3$  upon different magnetic fields was simulated. In general, this allows the prediction of magnetocaloric properties of  $\text{La}_{0.6}\text{Ca}_{0.4}\text{MnO}_3$  such as magnetic entropy change, full-width at half-maximum, relative cooling power, and magnetic specific heat change for  $\text{La}_{0.6}\text{Ca}_{0.4}\text{MnO}_3$  upon different magnetic field shifts. Though the maximum  $\Delta S_M$  is about 70 % of that of gadolinium, the  $\Delta S_M$  distribution is much more uniform than that of gadolinium, which is desirable for an Ericsson-cycle magnetic refrigerator, which is beneficial for the household application of active magnetic refrigerant materials.

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