

230Th‑234U and 231Pa‑235U radiochronometry of hydrolyzed uranium hexafuoride gas

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Abstract

Radiochronometry analyses of three hydrolyzed UF_6 gas samples were performed using the ²³⁰Th-²³⁴U and ²³¹Pa-²³⁵U chronometers. All 230 Th- 234 U model ages are younger than, and two of the three 231 Pa- 235 U model ages overlap with, the known UF₆ gas transfer dates. The ²³⁰Th-²³⁴U discordance is caused by 8–10% ²³⁰Th loss relative to the measurement reference date, likely during alkali hydrolysis. These results confirm that $UF₆$ gas transfers effectively purify uranium from daughter progeny. Daughter progeny fractionation can occur if solutions are not kept within optimal conditions post-UF $_6$ gas transfer and hydrolysis, and discordance between the $^{230}Th^{-234}U$ and $^{231}Pa^{-235}U$ chronometers may result from the laboratory procedures used to prepare samples.

Keywords U-series radiochronometry · Nuclear forensics · Uranium hexafuoride · Isotope dilution MC-ICP-MS

Introduction

Radiochronometric dating is an important nuclear forensic tool that can be used to identify the history of an unknown nuclear material and potentially provide genetic links between diferent nuclear materials. In radiometric dating by mass spectrometry, the concentrations of radioactive parent, daughter, and in some cases, granddaughter, nuclides are measured to defne a "model age," or time that has elapsed since the latest chemical purifcation of the parent isotope from progeny nuclides. In most cases, this model age is interpreted as the date when the material was produced, although in practice this may not be the case if a material was not completely chemically purifed of progeny isotopes upon production, or if it has not existed as a closed system (i.e., no gain or loss of nuclides from the bulk material) in the ensuing time. Although it is impossible to know whether these assumptions have been fully met, the measurement of multiple chronometers in the same sample provides a strong independent avenue to assess the validity of model age assumptions.

The degree to which these assumptions are met in diverse materials produced during diferent stages in the nuclear fuel cycle is an area of active research; diferent materials that are both consistent and inconsistent with model age assumptions have been recognized [[1–](#page-8-0)[4\]](#page-8-1). Furthermore, simply because a material is discovered to have discordant model ages does not preclude gaining useful information from the radiochronometric investigation. For example, the diferent chemical behavior of actinide elements along with the difering potential for these materials to be contaminated from the ambient environment can allow for indirect knowledge to be gained about a sample's history from the discordant results. Here, we investigate the behavior of two daughter-parent radiochronometers in a common fuel cycle material to glean understanding of the meaning and signifcance of measured model ages.

Since World War II, gaseous difusion was the primary method used to produce enriched 235 U in the U.S. In this process, uranium is fluorinated to form a hexafluoride gas and propelled through a complex pressurized system of pipes and barriers to separate the uranium isotopes by mass, repeating the process hundreds if not thousands of times in an enrichment cascade to produce the desired 235 U enriched product. Other enrichment approaches utilize the gas centrifuge process, which also utilizes $UF₆$ gas as a feed

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material. UF₆ gas and related phases from both enrichment processes may be stored in pressurized cylinders at a variety of stages throughout the conversion and enrichment process. However, U-series daughter and granddaughter progeny, including Th, Pa, Ac and Ra, theoretically do not form volatile fuorides at the pressure–temperature conditions under which UF_6 is in the gas phase [\[5](#page-8-2)], so any conversion of a uranium hexafuoride gas to a diferent phase is predicted to reset the model age clock to the time the gas was converted into a form that was capable of retaining progeny nuclides, usually when converted to a solid fuoride or oxide form. Previous analysis of solid uranium hydrolysis products ("heels") extracted from emptied $UF₆$ gas cylinders found that these materials contain the bulk of daughter and granddaughter progeny produced from radioactive decay of the uranium, so that the model ages of the heels are well in excess of the known times of cylinder flling [\[3\]](#page-8-3). However, it is unknown via direct measurements of real-world nuclear fuel cycle materials whether the $UF₆$ gas in equilibrium with the heels will exhibit complete radiochronometric resetting to the date when it was extracted from the cylinder and converted to a liquid or solid form. Here we investigate this process through radiochronometric analysis of a set of solid hydrolyzed uranium samples produced from highly enriched UF_6 gas extracted from cylinders at a known time. The model ages of the cylinder heels from one of the same cylinders were determined in a previous study [[3\]](#page-8-3). The full complimentary nature of all of these analyses allow for a comprehensive understanding of the behavior of parent and progeny isotopes in UF_6 gas cylinders and provide the foundational knowledge vital towards interpretation of these signatures in similar, yet unknown, materials.

Sample description & history

The samples analyzed in this study are highly enriched (HEU) hydrolyzed uranium hexafuoride gas extracted from three 2S cylinders that originated from the Portsmouth Gaseous Difusion Plant in Pike County, Ohio. Photographs and descriptions of the sample history are presented in Fig. [1.](#page-1-0)

The UF₆ gas that produced 396HYD was stored in a 2S cylinder made of Monel while the $UF₆$ gas sources of 255HYD and 146HYD were stored in nickel cylinders. These cylinders were filled directly from the enrichment cascade at the Portsmouth Gaseous Diffusion Plant (PORTS) and were originally used as reference standards in the plant analytical laboratory. PORTS operated between 1956 and 2001, and after shuttering of the plant some of these gas cylinders containing HEU materials were shipped to Nuclear Fuel Services (NFS) in Erwin,

Fig. 1 Photos of hydrolyzed uranium sample preparation, used with permission from Materials and Chemistry Laboratory, Inc (Oak Ridge, TN). **a** the gas extraction setup showing the 2S cylinder attached to a transfer system that contains a 50 mL stainless steel gas cylinder transfer vessel and two fuoropolymer hoke P10 tubes (photo from W. Bostick). **b** hydrolyzed UF_6 solutions (photo from W.

Bostick). **c** solid hydrolyzed uranium samples under ultraviolet light exhibiting strong luminescence (photo from W. Bostick). **d** hydrolyzed UF_6 samples once converted to solids (photo from W. Bostick); samples were shipped to LLNL in these sample containers. **e** aliquoted samples before digestion at LLNL

Tennessee. Five cylinders containing various levels of ²³⁵U enrichment were reserved for further sampling and analysis because of their well-known history.

Once the cylinders were at NFS, the extractable UF_6 gas was removed via heated gas transfer and the cylinders were shipped to Materials and Chemistry Laboratories, Inc. (MCL, Inc.) in Oak Ridge, Tennessee for sampling and archival of the remaining residual uranium fluoride products ('heels'). The dates of the gas transfers are reported in Table [1](#page-2-0). After samples were received and weighed at MCL, Inc., the cylinders were attached to a gas manifold system that was new for each canister to prevent cross contamination (Fig. [1a](#page-1-0)). Non-condensable gasses hydrofluoric, nitrogen, and fluorine were removed by evacuation of the canister while under ice, followed by gentle heating in a warm water bath to sublimate UF_6 gas to two P10 tubes after a brief collection and weighing period in the transfer volume chamber. If there was excess $UF₆$ gas after filling the two P10 tubes, this material was stored in the transfer vessel for a short time before being transferred into a cleaned perfluoroalkoxy (PFA) tube. The UF₆ was converted to a liquid via hydrolysis by adding de-ionized water to the PFA tube, producing uranyl fluoride (UO_2F_2) and hydrofluoric acid (Fig. [1b](#page-1-0)). After storage for several months, the HF was removed from solutions by the addition of ammonium carbonate and dried to form bright yellow solids that are highly luminescent under UV light (Fig. [1c](#page-1-0)). These solid uranyl compounds produced by drying down neutralized hydrolyzed uranium hexafluoride gas were shipped to Lawrence Livermore National Laboratory (LLNL) and analyzed as a part of this study (Fig. [1](#page-1-0)d and e). A schematic representation of the sample history and preparation of samples investigated in this report is shown in Fig. [2](#page-3-0) (W. Bostick, personal communication).

After extraction of the UF_6 gas, the cylinders were cut open to extract solid hydrolysis uranium materials (i.e., the "loose heel" material) that could be poured out of the cut cylinders, and wall deposit material that was scraped from the sides of the cylinders. These materials were investigated in Rolison and Williams [[3](#page-8-3)].

Experimental

Radiochronometry analyses at LLNL use ultra-high purity acids and water purified to > 18.2 M Ω for labware cleaning and analytical dilutions. The procedure used in this study follows the method outlined in detail in Treinen et al. [[6\]](#page-8-4).

Single aliquots of each hydrolyzed uranium sample were digested by weighing approximately 200 mg of solid material into a cleaned quartz tube and dissolving with 8 M $HNO₃$ for several hours while heating. After this time there were no insoluble residues observed. Samples were then transferred into cleaned PFA vials and diluted into a fnal solution of 4 M HNO₃ + 0.05 M HF; this acid matrix has been demonstrated to stabilize uranium and progeny isotopes in solution for long periods of time [[1](#page-8-0)]. The concentration of U in these primary solutions was 9–10 mg U/g solution. Separate aliquots of the digested sample solutions were taken for isotope dilution uranium assay and uranium isotopic composition analysis. Uranium concentrations were determined by isotope dilution mass spectrometry after a series of dilutions were made to achieve optimal sample-spike ratios of ²³⁵U with a very high purity ²³³U spike (>99.9877% *n* (233) U)/n(U)) calibrated in-house using NBL CRM 112A (dilutions for uranium isotope dilution measurements had approximately 8 ng U/g solution in the analytical aliquot). The isotope dilution aliquots were spiked and equilibrated and then both the spiked and the unspiked aliquots were purifed by extraction chromatography using UTEVA resin (Eichrom Technologies Inc.).

Th and Pa concentrations were measured on the same aliquot via isotope dilution mass spectrometry. Weighed sample aliquots were spiked with a high-purity nuclear forensic reference material (NFRM) 229 Th spike [\[7](#page-8-5)] and a 233 Pa spike that is produced by separation of 233 Pa from a 20–60 mg 237 Np parent solution; the resulting 233 Pa spike is calibrated with a ²³¹Pa high purity standard [[8\]](#page-8-6) before use (see [[6\]](#page-8-4) for a more detailed discussion of 233 Pa spike production and calibration). Th and Pa are then separated using a series of anion, TEVA, and silica gel purifcations to produce analytical aliquots free of uranium (key for protactinium analyses, where the continual production of 233 U from decay of the 233Pa spike must be minimized for accurate results).

Table 1 Summary of cylinder history

| Sample | 2S Cylinder | Date of earliest PORTS sam- pling | Date of gas transfer at NFS | Initial gas transfer at MCL, Inc | Second gas transfer at MCL, fer at MCL, Inc hydrolysis Inc | Third gas trans- Date of UF_6 | | Amount of hydrolyzed $UF_6(g)$ |
|--------|-------------|---|--|--|--|---------------------------------|--------------|--------------------------------------|
| 146HYD | 30146 | 20-Jun-1977 | 22-Nov-2011 | 27-Sep-2012 | $3-Oct-2012$ | $21 - Oct-2012$ | $9-Nov-2012$ | 1.78 |
| 255HYD | 30255 | 9-Apr-1977 | 15-Dec-2011 | $31 - Aug-2012$ | $3-Sep-2012$ | N/A | 12-Sep-2012 | 2.11 |
| 396HYD | 30396 | 25-May-1982 | 22-Jan-2012 | 9-Aug-2012 | 15-Aug-2012 | $3-Sep-2012$ | unknown | 1.33 |

Fig. 2 Representation of the history of gas cylinders sampled in this study. At some time in the past (t=0), cylinders were filled with UF₆ from the Portsmouth Gaseous Difusion Plant and set aside for several years, during which time small amounts of $UF₆$ gas may have been extracted for use as a reference material. At $t=1$, here in late 2011- early 2012, the flled gas canisters were shipped to Nuclear Fuel Services (Erwin, TN) where the bulk of the UF₆ gas was extracted $(t=2)$. The canisters were then shipped to Materials and Chemistry Laboratory, Inc (Oak Ridge, TN), during which time some of the solid UF₅ sublimated to produce a small amount of UF₆ gas

All isotopic analyses were completed using a Nu Plasma HR MC-ICP-MS using CRM U010 to correct for instrumental mass bias and Faraday/ion counter gain factor; corrections were applied using the sample-standard bracketing method. CRMs U630, U850, and U930 were analyzed with samples for uranium isotopic quality control materials; all analyses were within error of certifcate values. Uranium isotope dilution samples were analyzed with ²³⁸U, ²³⁶U, ²³⁵U, ²³⁴U and ²³³U masses measured concurrently on Faraday detectors; uranium isotopic composition samples were analyzed with 236U, 234U, and 233U measured on ion counter detectors and 238U and 235U measured on Faraday detectors. Thorium isotopes were measured both using a peak jumping program where the 229 Th and 230Th beams were jumped onto the same ion counter to eliminate error introduced by relative ion counter gain factor correction on the $^{229}Th/^{230}Th$ measurement and with ^{229}Th and 230Th concurrently analyzed on separate ion counters. A second analytical aliquot was prepared and analyzed by Th isotope dilution mass spectrometry about 8 months after the original analysis to confrm the analytical results; replicate Th analyses, corrected for radioactive decay of 234U between the times of the two analytical sessions, yield 230 Th concentrations that are identical within analytical uncertainty. All protactinium isotopes are analyzed concurrently on separate ion counters as soon as possible after fnal purifcation. Uncertainties

 $(t=3)$, which was then extracted in several evacuation steps at MCL, Inc. The gas extracted at $t=4$ was reacted with water to create hydrolyzed uranium solutions. These hydrolyzed uranium solutions were stored for several months until they were reacted with ammonium carbonate to neutralize the high fluorine concentrations $(t=5)$. These solutions were dried down to form solid uranyl compounds and transferred to long-term storage containers for shipment to LLNL $(t=6)$. After all the UF_6 gas was extracted from the canisters, they were sawed open and the solid "loose heel" material was extracted and analyzed in a parallel study [[3](#page-8-3)]

on all isotope analyses are calculated following the guidelines laid out by GUM [\[9](#page-8-7)].

Total procedural blanks were below the detection limit for ²³⁰Th, 0.05 fg/g for ²³¹Pa, and 8.5 pg/g for U, respectively, and were measured in spiked blank aliquots processed alongside samples. Because these amounts of blank contribution are negligible compared to analyte in samples, no blank subtraction correction was applied to the results. Model ages are calculated by solving the Bateman equations for generalized radioactive decay assuming there were no daughter nuclides present at $t=0$ [\[10](#page-8-8)] (Eq. [1](#page-3-1)).

$$
t = \frac{1}{\lambda_{parent} - \lambda_{daughter}} ln \left[1 + \frac{N_{daughter}}{N_{parent}} \frac{\lambda_{parent} - \lambda_{daughter}}{\lambda_{parent}} \right] (1)
$$

The decay half-lives used in model age calculations are 230 Th = 75,690 ± 115 years, 234 U = 245,250 ± 490 years, $^{231}Pa = 32,760 \pm 110$ years, and $^{235}U = 7.0381 \times 10^8 \pm 4.8 \times 10^5$ [\[11](#page-8-9)[–13\]](#page-8-10).

Results

All hydrolyzed uranium samples are highly enriched uranium (HEU) that contain the anthropogenic isotopes 236 U and 233U, indicating that reprocessed uranium was used in the feed material of the enrichment cascade (Table [2\)](#page-4-0). The samples have 91.21, 93.25, and 88.27 atom percent 235 U for samples 146HYD, 255HYD, and 396HYD, respectively.

Thorium assay and isotopic compositions are reported in Table [3](#page-4-1). As is apparent from the low overall concentrations of 232 Th (6–10 ppb), the sample preparation of the hydrolyzed $UF₆$ gas at both MCL, Inc and LLNL were very clean for Th, and it is therefore unlikely that samples are contaminated with appreciable amounts of 230 Th introduced during processing since the UF_6 gas was extracted.

231 Pa‑235U and 230Th‑234U radiochronometry results

Radiochronometry analyses were performed using 230Th- 234 U and 231 Pa- 235 U isotopic systems. The model age results measured in the dried uranyl compounds are presented in Table [4](#page-5-0) and Fig. [3](#page-6-0). These results are not corrected for initial intrinsic 229Th that existed in the samples at the time of ThID measurement from the decay of 233 U, as the amount of 233 U in the samples was so small that this correction results in a change in the Th-U model age of a few hours, negligible compared to the uncertainty of the radiochronometric measurement itself.

All ²³⁰Th-²³⁴U model ages are younger than the gas transfer dates, indicating ²³⁰Th that originated from decay of UF₆ gas since the time the cylinders were originally flled at the PORTS plant was quantitatively left behind by the extraction of UF_6 gas from the fuel cylinders (Fig. [3\)](#page-6-0). For samples 396HYD and 146HYD, the $^{231}Pa-^{235}U$ age overlaps with the date of gas transfer at MCL, Inc, while the $^{231}Pa-^{235}U$ model age of sample 255HYD plots between the gas extraction dates at NFS and MCL, Inc. If the 255HYD ²³¹Pa-²³⁵U model age is considered to be erroneously older than the gas transfer date at MCL, Inc, the amount of 231Pa that is in excess is on the order of 4×10^7 atoms, or <0.0004% of the amount measured in the PaID measurement (and less than the analytical blank); it is probable this amount of 231 Pa was inadvertently added during sample processing. There is discordance between the Th-U and Pa-U model ages, as the model ages of 230Th-234U ages are younger by several months than the Pa ages.

Discussion

The uranium isotopic compositions of the hydrolyzed $UF₆$ gas and the solid cylinder heel material are indistinguishable within error and agree with the isotopic compositions reported for this material in original documents from Portsmouth, indicating that these materials were not contaminated by extraneous U, and by extension, signifcant amounts of Th or Pa, during processing or handling. The discordance in the ages between the 230 Th- 234 U and 231 Pa- 235 U chronometers was unexpected, as the controlled $UF₆$ gas extraction was assumed to have completely purifed the parent uranium atoms from daughter progeny. Uranium hexafuoride will be sublimated starting at approximately 56.5°C at room pressure. Protactinium will not form a fuoride gas at all, while thorium requires temperatures in excess of 800–850°C to form a ThF₄ gas [[14](#page-8-11), [15](#page-8-12)]. Previous work has shown that Th and Pa are elevated above the expected concentrations for samples of their age in uranium cylinder heel material

Table 2 Uranium isotopic compositions of hydrolyzed $UF₆$ gas

Unc. $=k*u_c$, where Unc. is the expanded uncertainty, u_c is the standard uncertainty, and k, the coverage factor, is 2. Reference date for isotopic results is 5-Aug-2020

Table 3 Thorium assay of hydrolyzed $UF₆$ gas

| Sample | Th ng/g sample | Unc | 230 Th ng/g sample | Unc | 232 Th ng/g sample | Unc | 230 Th/ 232 Th | Unc |
|--------|----------------|------|----------------------------|------|----------------------------|-------|--------------------------|-------|
| 146HYD | 84.20 | 0.56 | 78.01 | 0.53 | 6.191 | 0.047 | 8.777 | 0.049 |
| 255HYD | 73.25 | 0.67 | 66.27 | 0.62 | 6.978 | 0.068 | 12.711 | 0.076 |
| 396HYD | 97.7 | 1.4 | 87.6 | 1.3 | 10.07 | 0.15 | 9.583 | 0.049 |

Unc. $=k^*u_c$, where Unc. is the expanded uncertainty, u_c is the standard uncertainty, and k, the coverage factor, is 2. Reference date for isotopic results is 23-July-2020

The model purifcation date for Certifed Reference Material CRM U630 is June 6, 1989 with an uncertainty of 190 days. These analyses were prepated and analyzed~2 months after the hydro-

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lyzed UF₆ samples in this study u

lyzed UF $_6$ samples in this study using the same methods, calibrations, and spikes

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1518 Journal of Radioanalytical and Nuclear Chemistry (2021) 329:1513–1521 because Th and Pa do not form fuoride gasses under the conditions that UF_6 gas is extracted from cylinders, and are

therefore quantitatively retained in the solid cylinder heel

material while UF_6 gas is evacuated [[3\]](#page-8-3). The discordance of the 230 Th- 234 U chronometer with the known gas transfer dates represents an age bias of <10% at the time of measurement and indicates that there may have been some additional loss of ²³⁰Th after the time the UF₆ was hydrolyzed; this could have occurred during reaction of the solutions with ammonium carbonate, storage in solution form, or processing at LLNL. It is unlikely that the uranium isotopes extracted from the UF_6 cylinder would be fractionated by mass, as the fractionation factor of UF_5 sublimating at <100°C are so small that no measurable fractionation would occur. Furthermore, the uranium isotopic composi tion between the hydrolyzed uranium samples studied here and the cylinder heels analyzed elsewhere agrees to less than 1% relative standard deviation on all isotopes, suggesting isotopic fractionation is negligible. Therefore, the likely sce nario is loss of a small amount of 230 Th during preparation of these samples.

The deficit in 230 Th in the hydrolyzed uranium samples is equivalent to 6–8 months, or approximately 31–40 ng of ²³⁰Th per gram of U (Table [5\)](#page-6-1). It is apparent that 230 Th is very sensitive to environmental conditions and laboratory processing post UF_6 gas extraction, effects that are exacerbated by the fact that most of the investigated materials were dated relatively soon after extractions of the UF_6 gas (i.e., young 230 Th- 234 U ages). For the hydrolyzed uranium samples, it is likely that the sample processing method post UF₆ hydrolyzation resulted in the loss of $< 10\%$ ²³⁰Th from the solutions. This percentage is calculated based on the theoretical amount of 230 Th that should be present in samples based on radioactive decay equations and the time elapsed between the known gas extraction age and the reference date when samples were measured. We explore the possible mechanisms for this below.

When the cylinders were received at MCL, Inc, they were weighed, photographed, and drained of all remaining UF_6 gas through a gentle heated gaseous transfer on a manifold extraction system. Samples collected were stored in PFA tubes until they were hydrolyzed soon after by the addi tion of water to the frozen UF_6 gas. This step produces a vigorous reaction resulting in aqueous uranyl fuoride and hydrofluoric acid. The resulting solutions had a pH \approx 2 and a high free fuoride ion concentration, optimal for keeping trace actinides in solution. Uranium hydrolysis proceeds by the generalized reaction [\[16](#page-8-13)]:

 $UF_6 + 2H_2O = UO_2F_2 + 4HF$

Samples were stored in these low-pH and high fuorine concentration solutions for approximately 1.6–1.8 years. **Fig. 3** Radiochronometry results of hydrolyzed UF_6 gas; diamonds are the $^{231}Pa - ^{235}U$ age and circles are the 230 Th-
 234 U age. Error bars indicate the combined and expanded uncertainty $(k=2)$. The NFS bulk UF_6 gas removal for the cylinders is labeled, and the other dashed lines indicate the frst, second, third (if applicable) gas transfer dates at MCL, Inc, and the date the gas was hydrolyzed, if known. Also shown for reference is the date that the ammonium carbonate was added to samples, followed by immediate dry down

Table 5 ²³⁰Th deficit and

Then, in order to mitigate the hazardous hydrofuoric acid concentrations and low pH of these solutions, ammonium carbonate was added to samples in amounts assumed to fully react with the quantity of HF present in the hydrolyzed uranium solutions (here approximately 8 mol ammonium carbonate for every one mole of uranium). This reaction results in a basic solution (pH \approx 9) of dissolved ammonium fluoride salt, water, and eventual formation and release of gaseous carbon dioxide after the formation of an intermediate carbonic acid. The generalized reaction is:

$$
(NH_4)_2CO_3 + 2HF = 2(NH_4)F + H_2O + CO_2
$$

After this step, no precipitate was observed in these solutions, which were transferred to glass containers for drying down on a hot plate. The PFA tube was rinsed once with deionized water and added to the solutions drying down. Excess ammonium carbonate will break down upon heating and be fumed from the solution as a mixture of carbon dioxide, ammonia, and water; similarly, excess HF will be fumed off as a gas. Once fully dry, the solid materials were transferred to a TFE container for shipment to LLNL.

Uranium assay values of the fnal dried solid are low compared to what would be expected for a pure uranyl fuoride $(UO₂F₂·H₂O, 0.73 g U/g sample)$, and is instead much closer to the stoichiometric assay of ammonium uranyl carbonate (56 wt $\%$ U) and ammonium uranyl fluoride (62 wt $\%$ U; see Table [6\)](#page-7-0). Ammonium uranyl carbonate and ammonium uranyl fluoride are highly fluorescent while UO_2F_2 is not; the hydrolyzed uranium samples analyzed here are highly fuorescent (see Fig. [2\)](#page-3-0). The U assay values suggest that uranyl fuoride produced by the hydrolysis of UF_6 gas was quantitatively converted to ammonium uranyl carbonate by the alkali hydrolysis.

Therefore, the entire sample chemical processing can be described by the generalized equation [[17](#page-8-14)]:

Table 6 U assay measured by IDMS

| Sample | g U/ g sample | Unc | |
|--------|---------------|---------|--|
| 146HYD | 0.55407 | 0.00049 | |
| 255HYD | 0.55528 | 0.00051 | |
| 396HYD | 0.55851 | 0.00048 | |

Unc. $=k^*u_c$, where Unc. is the expanded uncertainty, u_c is the standard uncertainty, and k, the coverage factor, is 2

point there was an incomplete reaction of thorium that left a small 10% amount of the total 230Th as a thorium fuoride hydrate stuck to the PFA tube walls, or as a small amount of thorium hydrolysis products that stuck to the PFA tube wall; targeted experiments could test which scenario is the most likely mechanism for thorium loss.

Conversely, in concentrated solutions of hydrofluoric acid, protactinium exists in the $Pa⁵⁺$ oxidation state as incredibly stable PaF_7^{2-} anions [[22\]](#page-8-19). There would therefore have been excellent stability of the protactinium in solu-

There are several potential areas for loss of thorium during this preparation. Hydrolysis of uranium hexafuoride is sometimes accomplished by reaction of the UF_6 with pure water as it was here, and other times it is reacted with low molarity nitric acid solutions. Thorium is predominately in the $4⁺$ oxidation state when it is in solution, and is very stable in solutions of nitrate, chloride, sulphate, and perchloric acids [[18](#page-8-15)]. When uranium hydrolysis is carried out with nitric acid solutions, the resulting thorium compound is the highly soluble $Th(NO₃)₄$.6H₂O. However, in very strong solutions of hydrofuoric acid, thorium will form insoluble fuorides that are pure if dried down multiple times in the presence of NH4F, otherwise it is a white, gelatinous precipitate of Th F_4 hydrate that is actually a mix of $ThF₄ + ThO₂ + ThOF₂$ [[19,](#page-8-16) [20\]](#page-8-17). This step may be a possible candidate for the fractionation of thorium from protactinium because protactinium is very stable in strong complexing acids such as hydrofuoric and sulfuric acids [[21,](#page-8-18) [22\]](#page-8-19). However, if the formation of thorium fuoride was quantitative as the thorium grew from uranium decay and left behind as a gelatinous precipitate on the PFA walls when the solution was transferred, it would have resulted in a complete resetting of the 230 Th- 234 U age to the age of the alkaline hydrolysis and dry down rather than only losing ~ 10% of the 230 Th that should have decayed between the known gas transfer date and the measurement reference date. Therefore, it is likely most of the thorium fuoride precipitate was transferred with the solution and rinse to the fnal sample dry-down container.

The second candidate for loss of 230 Th is the alkaline hydrolysis of the solutions before the fnal dry down. Typically, when the pH of a solution containing Th^{4+} is elevated to a pH above 3.5, the thorium will be hydrolyzed to form a $Th(OH)₄$ gelatinous precipitate $[20, 23, 24]$ $[20, 23, 24]$ $[20, 23, 24]$ $[20, 23, 24]$ $[20, 23, 24]$ $[20, 23, 24]$. However, this reaction will not occur if there is excess carbonate in the solution to complex with the thorium as would have been the case with the addition of so much ammonium carbonate. In an excess of carbonate, thorium will be precipitate as (NH_4) ₂Th(CO₃)₃·6H₂O [\[20\]](#page-8-17). It is possible that at some

tion during UF_6 hydrolyzation and subsequent storage as low pH, high F− molarity solutions. When solutions of protactinium in hydrofuoric acid are dried down, the result is readily soluble $Pa₂OF₅$ salts [\[25\]](#page-8-22). Similarly, alkali hydrolysis and carbonate precipitation will result in the precipitation of protactinium that will not undergo a reverse reaction to re-dissolve in the solution [\[21](#page-8-18)]. There is, consequently, conservation of all the protactinium in the system. It should be noted that even though protactinium is notoriously sticky to glassware, the strong complexation of the protactinium with fuorine, followed possibly by carbonate, resulted in the complete conservation of protactinium in this system [[21,](#page-8-18) [25\]](#page-8-22). It is unknown whether the fnal solid product of protactinium was a fuoride or carbonate compound.

The coherence of the chemistry of these samples is supported by the fact that all three samples exhibited very similar losses of thorium; each hydrolyzed uranium sample lost between 7.8 and 9.9% of the amount of ²³⁰Th that is predicted based on the time elapsed between the date of $UF₆$ gas extraction and the measurement reference date. This suggests that the process that resulted in the loss of 230 Th is reproducible within 2%, which appears systematic rather than random. Overall, there is agreement that the extraction of $UF₆$ gas from a fuel cylinder separates the parent isotope uranium from daughter progeny during low-temperature controlled releases of gas, even in materials in real-world use. Furthermore, if conservation of daughter progeny is desired in the resulting hydrolyzed uranium, the solutions should be dried down immediately to prevent fractionation in the 230Th-234U chronometer.

Conclusion

The results found in this study support the hypothesis that the removal of UF_6 gas from the cylinder effectively purifes the uranium from daughter progeny quantitatively as only the uranium parent atoms form a hexafuoride gas that is extractable by low-temperature gaseous transfer. This

scenario satisfes the underlying assumptions of radiochronometry model ages, and the 230 Th- 234 U and 231 Pa- 235 U model ages should record the date of $UF₆$ gas transfer if care is taken to ensure progeny nuclides are conserved in the subsequent prepared UF_6 hydrolyzed solution. However, the fractionation of daughter progeny can easily occur if solutions are not kept under optimal conditions, and discordance between the 230 Th- 234 U and 231 Pa- 235 U radiochronometers in hydrolyzed uranium samples may indicate such steps occurred during sample processing.

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