



# Flexible and high heat-resistant stereocomplex PLLA-PEG-PLLA/PDLA blends prepared by melt process: effect of chain extension

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## Abstract

Stereocomplex poly(lactides) (scPLAs) are high-performance biodegradable bioplastics because they show better mechanical properties and heat-resistance than the poly(L-lactide) (PLLA). However, scPLAs retain low flexibility similar to that of PLLA. In this work, a flexible poly(L-lactide)-*b*-poly(ethylene glycol)-*b*-poly(L-lactide) (PLLA-PEG-PLLA/PDLA) was melt blended with poly(D-lactide) (PDLA) before compression molding to form scPLA films. The effect of chain extension was investigated. Stereocomplexation of PLLA-PEG-PLLA/PDLA blends improved with PDLA ratio. The thermal stability of both the blends with and without chain extension was improved by stereocomplex formation. The non-chain-extended blend films became very brittle when 40 wt% PDLA was blended. Chain extension enhanced the tensile properties of the blend films. Heat resistance of blend films was significantly improved when the PDLA ratio was increased up to 20 wt%. Dimensional stability to heat at 80 °C of the film samples confirmed the results of heat resistance. The melt-processed scPLA in this work may offer revolutionary improvements in flexible and high heat-resistant bioplastics.

**Keywords** Polylactide · Triblock copolymer · Stereocomplex · Melting blending · Tensile properties · Heat resistance

## Introduction

Poly(L-lactide) or poly(L-lactic acid) (PLLA) is an important bioplastic due to its bio-renewability, non-toxicity, biocompatibility, biodegradability and good processing properties [1–3]. PLLA has been widely investigated for use in many applications, such as tissue engineering, drug delivery and packaging [4–6]. However, its poor heat-resistance due to poor crystallizability and its brittleness due to a high glass-

transition temperature ( $T_g \approx 60$  °C) have limited some of its applications [7, 8].

The crystallization rate of PLLA was accelerated by blending with poly(D-lactide) (PDLA) form as stereocomplex poly(lactides) (scPLAs) that enhanced its heat-resistant properties [9–11]. Stronger interactions in stereocomplex crystallites of the scPLA induced higher melting temperatures ( $T_m \approx 220$ – $240$  °C) and faster crystallization speed than the PLLA [12, 13]. These properties improved the heat and hydrolysis resistance of scPLA. The scPLA with high heat-resistance is appropriate for specific applications such as heat-treatment packaging, hot-fill packaging and microwave applications. However, the scPLA was still brittle because its  $T_g$  was similar to that of PLLA.

Poly(ethylene glycol) (PEG) and poly(propylene glycol) have been used as plasticizers to improve scPLA flexibility by decreasing the  $T_g$  of scPLA [14–16]. However, the migration of plasticizers makes scPLA unstable after aging [17]. PEGs have been used as macro-initiators for synthesizing the flexible PLLA-PEG-PLLA triblock copolymers to prevent the migration effect. Triblock copolymers of PDLA-PEG-PDLA have been synthesized for solution blending with the PLLA [18–23] and PLLA-PEG-PLLA [24] to improve flexibility of obtained scPLAs. The flexible PEG middle-blocks of

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both the PLLA-PEG-PLLA and PDLA-PEG-PDLA enhanced the plasticizing effect.

In a previous work showed that high molecular-weight (M.W.) PLLA-PEG-PLLA exhibited highly extensibility by chain-extension reaction [25]. They were highly flexible bioplastics. However their heat-resistance was still poor. To the best of our knowledge, the PLLA-PEG-PLLA/PDLA blends with and without chain-extension reaction have not been reported so far. Moreover, fabrication of the scPLA by melt process is very interesting at industrial scale. It is known that the stereocomplexation of PLA strongly depended on the M.W. of both the PLLA and PDLA [26, 27]. PLLA and PDLA with low M.W. had easier chain mobility for stereocomplex formation [28, 29]. Therefore in this work, the low M.W. PDLA was selected to induce stereocomplex formation of the flexible PLLA-PEG-PLLA. The influences of blend ratio and chain extension on stereocomplexation, thermal decomposition, tensile properties and heat resistance of PLLA-PEG-PLLA/PDLA blends was investigated in this research.

## Experimental

### Materials

L-lactide (LLA) and D-lactide (DLA) monomers were synthesized from 85 wt% L-Lactic acid (L-form >95%, Purac, Thailand) and 80 wt% D-lactic acid (D-form >99%, Haihang Industry (Jinan) Co., Ltd., China) respectively, by direct polycondensation before thermal de-polymerization. The crude LLA and DLA monomers were purified by repeated re-crystallization from ethyl acetate before drying in a vacuum oven at 50 °C for 24 h. PEG (M.W. = 20,000 g/mol, Sigma-Aldrich, Switzerland) macro-initiator was dried in a vacuum oven at 50 °C for 24 h. 1-Dodecanol (98%, Fluka, Switzerland) initiator was purified by fractional distillation under reduced pressure and stored over molecular sieves at room temperature. Stannous octoate (Sn(Oct)<sub>2</sub>, Sigma-Aldrich, Switzerland) catalyst was used as supplied. Joncryl® ADR 4368 chain extender (BASF, Thailand) was used without further purification.

### Synthesis and characterization of PLLA-PEG-PLLA and PDLA

Ring-opening polymerization of PLLA-PEG-PLLA and PDLA were carried out in bulk at 165 °C under a dry nitrogen atmosphere for 6 h and 2.5 h, respectively, using 0.075 mol% and 0.01 mol% Sn(Oct)<sub>2</sub> catalyst, respectively. The PEG and 1-dodecanol were used as initiators for synthesizing the PLLA-PEG-PLLA and PDLA, respectively. PDLA with a theoretical M.W. of 5000 g/mol was synthesized using 2.8 mol%

1-dodecanol. The theoretical M.W. of PLLA-PEG-PLLA was approximately 120,000 g/mol. The obtained PLLA-PEG-PLLA and PDLA were granulated into small pieces (~5 mm) and dried in a vacuum oven at 110 °C for 3 h.

PLLA-PEG-PLLA and PDLA were characterized by gel permeation chromatography (GPC, Waters e2695 separations module) to measure number-average molecular weight ( $M_n$ ) and dispersity ( $D$ ) as well as differential scanning calorimetry (DSC, Perkin-Elmer Pyris Diamond) to observe their  $T_g$  and  $T_m$ . The characteristics of PLLA-PEG-PLLA and PDLA are summarized in Table 1.

### Preparation of PLLA-PEG-PLLA/PDLA blends

PLLA-PEG-PLLA, PDLA and Joncryl® were dried in a vacuum oven at 50 °C overnight before melt blending using an internal mixer (HAAKE PolyLab OS System) at 200 °C for 4 min. A rotor speed of 100 rpm was chosen. Blends with PLLA-PEG-PLLA/PDLA ratios of 100/0, 90/10, 80/20, 70/30 and 60/40 (w/w) were investigated. The Joncryl®-free and 4.0 phr Joncryl® blend series were prepared. The obtained blends were granulated into small pieces (~5 mm) and dried in a vacuum oven at 50 °C overnight before characterization and compression molding.

The blend films were fabricated using a compression molding machine (Auto CH Carver) at 240 °C for 1.0 min without any force followed with a 5.0 ton compression force for 1.0 min before quickly cooling. The films with 0.2–0.3 mm thickness were obtained and stored at room temperature for 24 h before characterization.

### Characterization of PLLA-PEG-PLLA/PDLA blends

The thermal transitions of the blends were observed by means of DSC using a Perkin-Elmer Pyris Diamond DSC. For DSC heating scan, samples of 3–5 mg in weight were held at 250 °C for 2 min under a nitrogen flow to eliminate their thermal history. Then, the samples were quenched to 0 °C before heating at 10 °C/min over a temperature range of 0 to 250 °C in order to observe their  $T_g$ ,  $T_m$  and cold-crystallization temperature ( $T_{cc}$ ). For DSC cooling scan, the

**Table 1** Characteristics of PLLA-PEG-PLLA and PDLA

Sample	$M_n^a$ (g/mol)	$D^a$	$T_g^b$ (°C)	$T_m^b$ (°C)
PLLA-PEG-PLLA	89,900	2.1	34	172
PDLA	5700	1.9	47	160

<sup>a</sup> determined from GPC using tetrahydrofuran as the eluent at 40 °C

<sup>b</sup> determined from DSC (samples were held at 200 °C for 2 min and quenched to 0 °C before heating from 0 to 200 °C at 10 °C/min under a nitrogen atmosphere)

sample was held at 250 °C for 2 min to remove thermal history before cooling to 0 °C at a rate of 10 °C/min to observe their crystallization temperatures ( $T_c$ ).

The degree of crystallinity from DSC ( $X_{c,DSC}$ ) for homo-crystallites ( $hc-X_{c,DSC}$ ) (Eq. 1) of the PLLA-PEG-PLLA was calculated from the enthalpy of melting for homo-crystallites ( $\Delta H_{m,hc}$ ) and enthalpy of cold crystallization ( $\Delta H_{cc}$ ).

$$hc-X_{c,DSC} (\%) = [(\Delta H_{m,hc} - \Delta H_{cc}) / (93 \times W_{PLLA})] \times 100 \quad (1)$$

where the  $\Delta H_{m,hc}$  for 100%  $hc-X_{c,DSC}$  was 93 J/g [30]. The weight fraction of the PLLA ( $W_{PLLA}$ ) determined from  $^1H$ -NMR and was 0.83 for the PLLA-PEG-PLLA [25].

The  $X_{c,DSC}$  for stereocomplex crystallites ( $sc-X_{c,DSC}$ ) (Eq. 2) of the PLLA-PEG-PLLA/PDLA blends was calculated from the enthalpy of melting for stereocomplex-crystallites ( $\Delta H_{m,sc}$ ).

$$sc-X_{c,DSC} (\%) = [(\Delta H_{m,sc}) / (142 \times W_{PLA})] \times 100 \quad (2)$$

where the  $\Delta H_{m,sc}$  for 100%  $sc-X_{c,DSC}$  was 142 J/g [30]. The weight fractions of the PLLA and PDLA ( $W_{PLA}$ ) were 0.847,

0.864, 0.881 and 0.898 for the 90/10, 80/20, 70/30 and 60/40 PLLA-PEG-PLLA/PDLA blends, respectively.

The thermal decomposition behavior of the blends was determined by thermogravimetric analysis (TGA) using a TA-Instrument SDT Q600 TGA. For TGA, 5–10 mg of the sample was heated at 20 °C/min from 50 to 600 °C under a nitrogen flow.

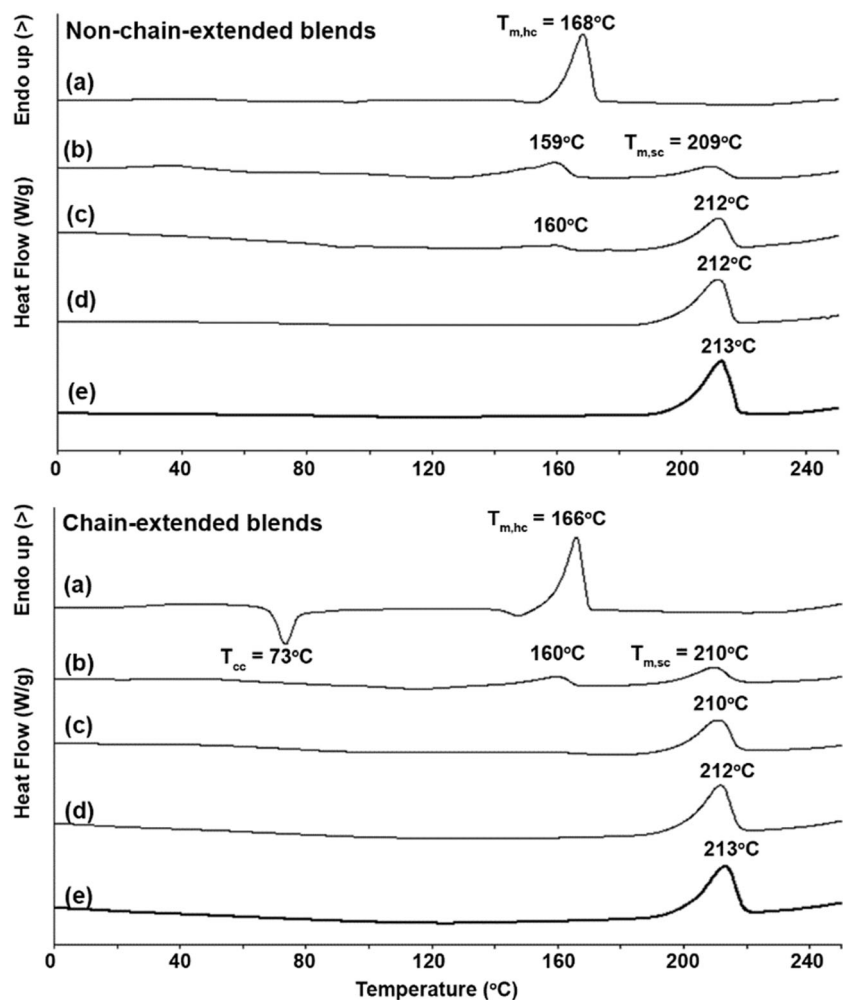
The crystalline structure of the film samples was determined by wide-angle X-ray diffractometry (XRD) using a Bruker D8 Advance XRD at 25 °C operated at 40 kV and 40 mA  $CuK\alpha$  radiation. For XRD, the film samples were recorded in a  $2\theta$  range 5° to 30° at a scan rate of 3°/min. The crystallinity from XRD ( $X_{c,XRD}$ ) for homo-crystallites ( $hc-X_{c,XRD}$ ) (Eq. 3) and stereocomplex crystallites ( $sc-X_{c,XRD}$ ) (Eq. 4) of the film samples were calculated [31].

$$hc-X_{c,XRD} (\%) = S_{hc} / (S_{hc} + S_{sc} + S_a) \times 100 \quad (3)$$

$$sc-X_{c,XRD} (\%) = S_{sc} / (S_{hc} + S_{sc} + S_a) \times 100 \quad (4)$$

where  $S_{hc}$  and  $S_{sc}$  are the integrated intensity peaks for homo-crystallites and stereocomplex crystallites, respectively.  $S_a$  is the integrated intensity of the amorphous halo.

**Fig. 1** DSC heating curves of (above) non-chain-extended and (below) chain-extended blends of various PLLA-PEG-PLLA/PDLA compositions



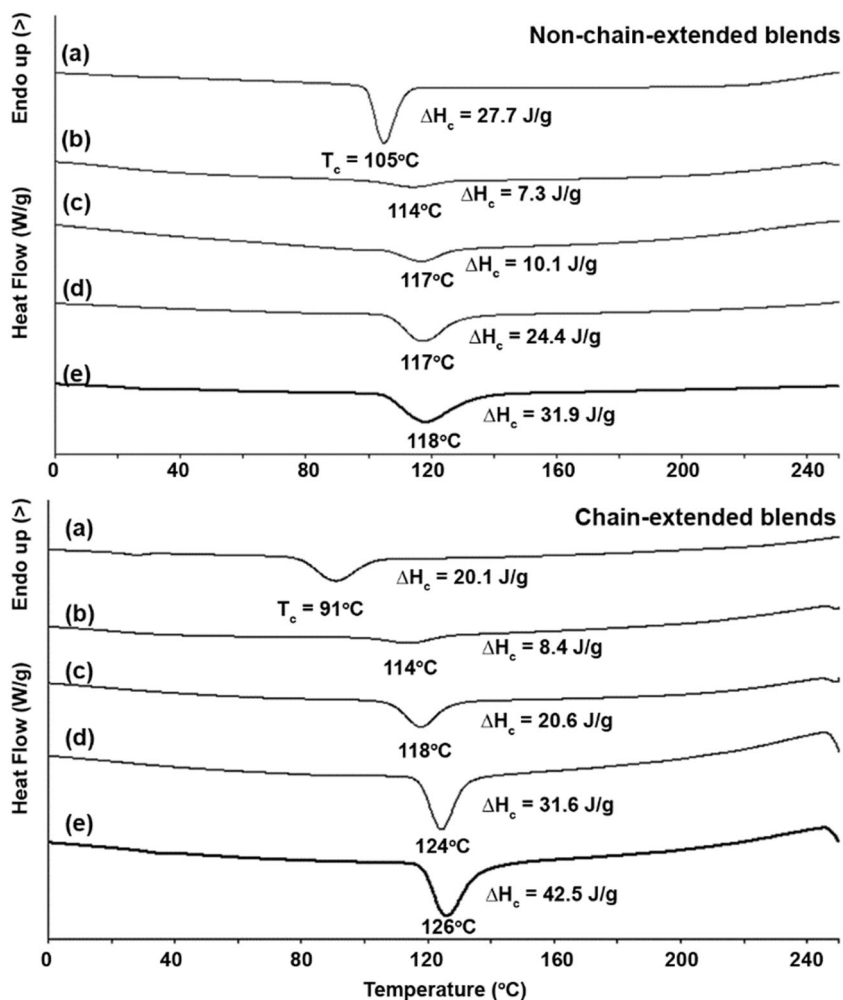
**Table 2** DSC results of PLLA-PEG-PLLA/PDLA blends

PLLA-PEG-PLLA/PDLA ratio (w/w)	$T_g$ (°C)	$\Delta H_{cc}$ (J/g)	$\Delta H_{m,hc}$ (J/g)	$\Delta H_{m,sc}$ (J/g)	hc- $X_c$ ,DSC (%)	sc- $X_c$ ,DSC (%)
Non-chain-extended						
100/0	31	–	43.8	–	56.7	–
90/10	32	–	19.3	12.5	24.5	10.4
80/20	31	–	4.5	28.6	5.6	23.3
70/30	–	–	–	45.1	–	36.0
60/40	–	–	–	50.3	–	39.4
Chain-extended						
100/0	33	15.4	39.5	–	31.2	–
90/10	32	–	10.0	16.0	12.7	13.3
80/20	32	–	1.7	31.8	2.1	25.9
70/30	–	–	–	42.6	–	34.0
60/40	–	–	–	46.0	–	38.8

The tensile properties of the film samples were analysed using a Lloyds LRX+ Universal Testing Machine at 25 °C. The film samples (100 × 10 mm) were determined with an initial distance between the grips of 50 mm at an extension speed of 50 mm/min according to ASTM D882. Each film sample was evaluated in at least five replicate experiments.

The thermo-mechanical properties of the film samples (5 × 20 × 0.2 mm) were measured by dynamic mechanical analysis (DMA) using a TA Instrument Q800 DMA under a tensile mode with the scan amplitude of 10 μm and the scanning frequency of 1 Hz from 40 to 140 °C at a heating rate of 2 °C/min.

**Fig. 2** DSC cooling curves of (above) non-chain-extended and (below) chain-extended blends of various PLLA-PEG-PLLA/PDLA compositions



The dimensional stability to heat of film samples with 0.2 mm thickness was observed by hanging the sample in an air oven at 80 °C for 30 s under a 200 g weight attached. Initial gauge length of film samples was 20 mm. The dimensional stability was calculated from the Eq. 5 [32].

Dimensional stability to heat (%)

$$= [\text{initial length (mm)}/\text{final length (mm)}] \times 100 \quad (5)$$

## Results and discussion

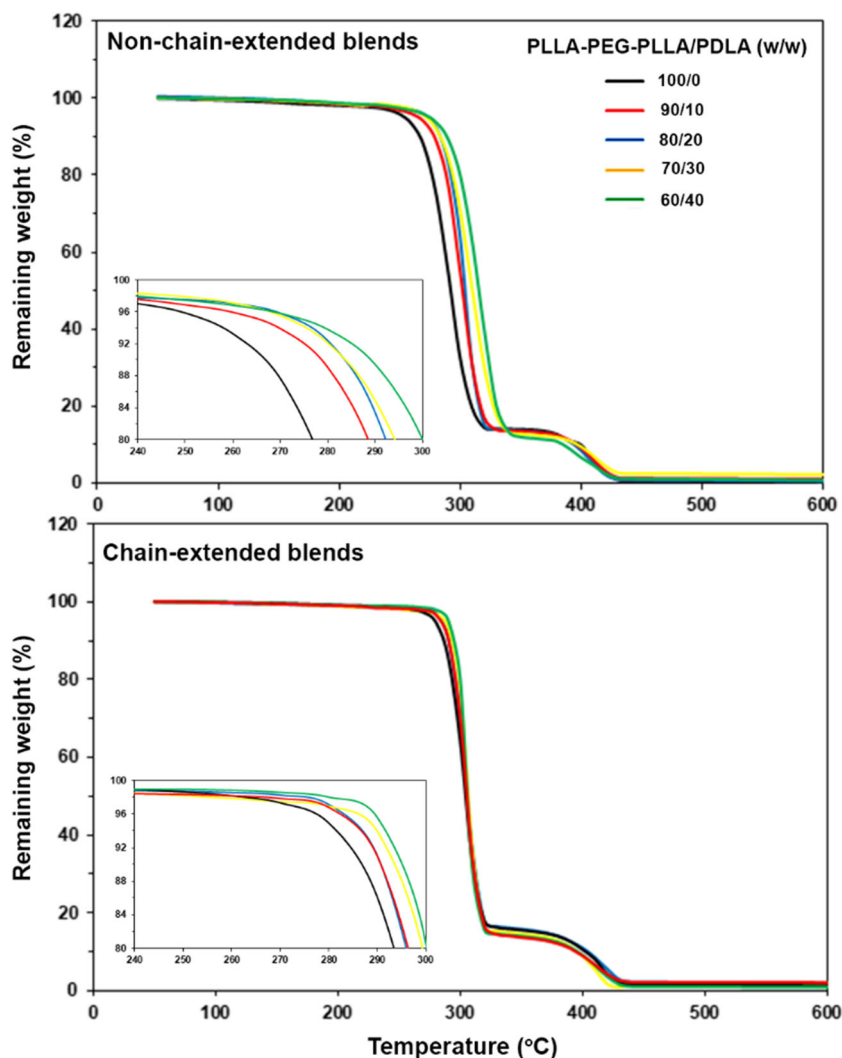
### Thermal transitions

Figure 1 shows DSC heating curves of PLLA-PEG-PLLA and blends. The corresponding DSC data are reported in Table 2. The  $T_g$  of PLLA-PEG-PLLA and blends was in the range 31–33 °C and were lower than values for the PLLA [56 °C, see Fig. S1 (a)]. This is due to flexible

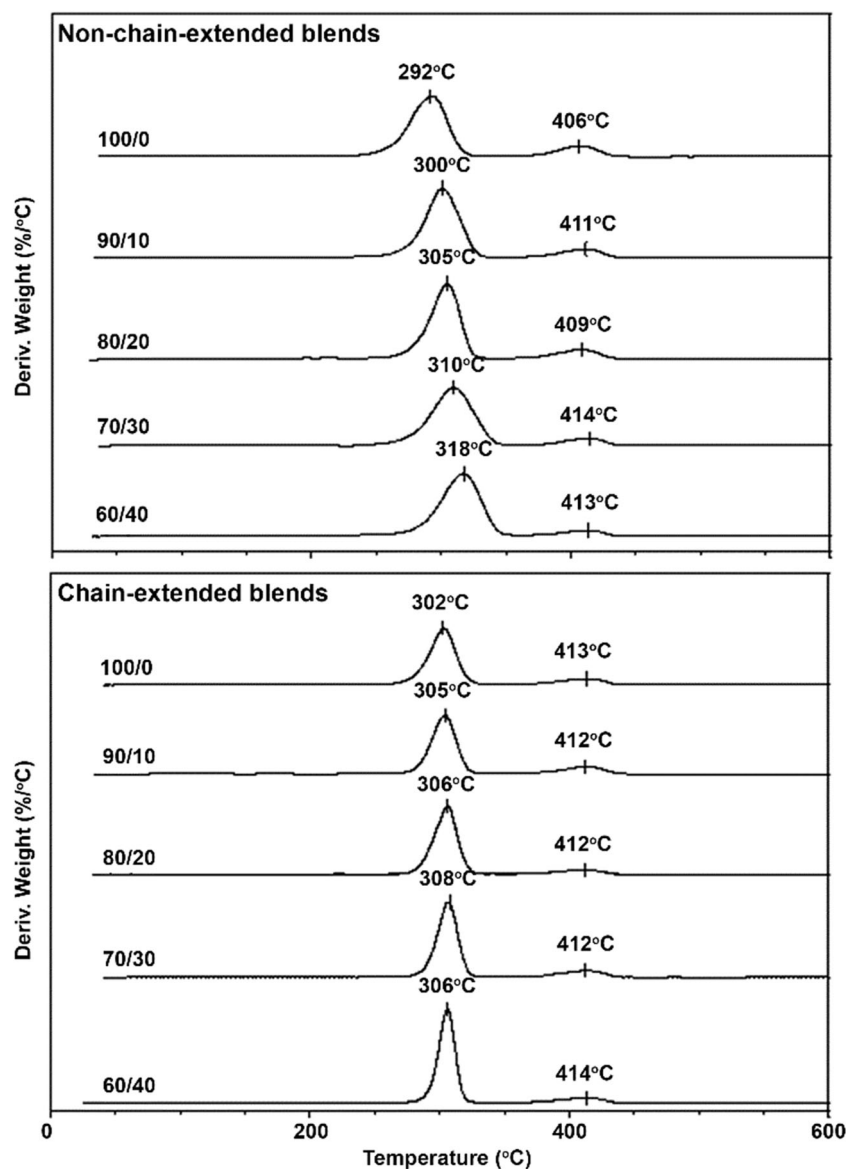
PEG middle-blocks acting as plasticizers to decreasing  $T_g$  of PLLA end-blocks [25]. The chain extension did not significantly affect the  $T_g$  of the PLLA-PEG-PLLA and blends. The  $T_m$  of PEG at 66 °C [see Fig. S1 (b)] disappeared for the PLLA-PEG-PLLA suggesting good miscibility between PEG middle-blocks and PLLA end-blocks to inhibit crystallization of PEG middle-blocks. The  $T_m$  of homo-crystallites ( $T_{m,hc}$ ) decreased and that of the stereocomplex crystallites ( $T_{m,sc}$ ) slightly increased as the PDLA ratio increased. This indicated that crystallization of the blends with larger PDLA ratio induces the integrity of the stereocomplex crystallites and their lamella thickness.

It was also found that the  $T_{m,hc}$  peaks of blends disappeared when the PDLA ratios were increased up to 30 wt% for both the non-chain-extended and chain-extended blend series. The results suggested that only the 30 wt% PDLA induced complete stereocomplexation of PLLA end-blocks. This was due to the low M.W. PDLA acting as a better stereocomplex enhancer than the high M.W. PDLA because of its easier chain diffusion and mobility for stereocomplexation [28, 29].

**Fig. 3** TG curves of (above) non-chain-extended and (below) chain-extended blends of various PLLA-PEG-PLLA/PDLA compositions



**Fig. 4** DTG curves of (above) non-chain-extended and (below) chain-extended blends of various PLLA-PEG-PLLA/PDLA compositions



The non-chain-extended PLLA-PEG-PLLA had no peak of  $T_{cc}$  as shown in Fig. 1 (above, a). The good chain-mobility of PLLA-PEG-PLLA is due to flexible PEG middle-blocks enhancing crystallization of PLLA end-blocks during the DSC quenching process. However, the chain-extended PLLA-PEG-PLLA exhibited a  $T_{cc}$  peak at 73 °C in Fig. 1 (below, a). This is due to the long-chain branched structures of chain-extended PLLA-PEG-PLLA reducing its chain diffusion and mobility for crystallization [25]. Meanwhile the  $T_{cc}$  peak did not detect all the chain-extended blends [Fig. 1 (below, b-e)]. This indicates the low M.W. PDLA accelerated crystallization of the chain-extended blend series.

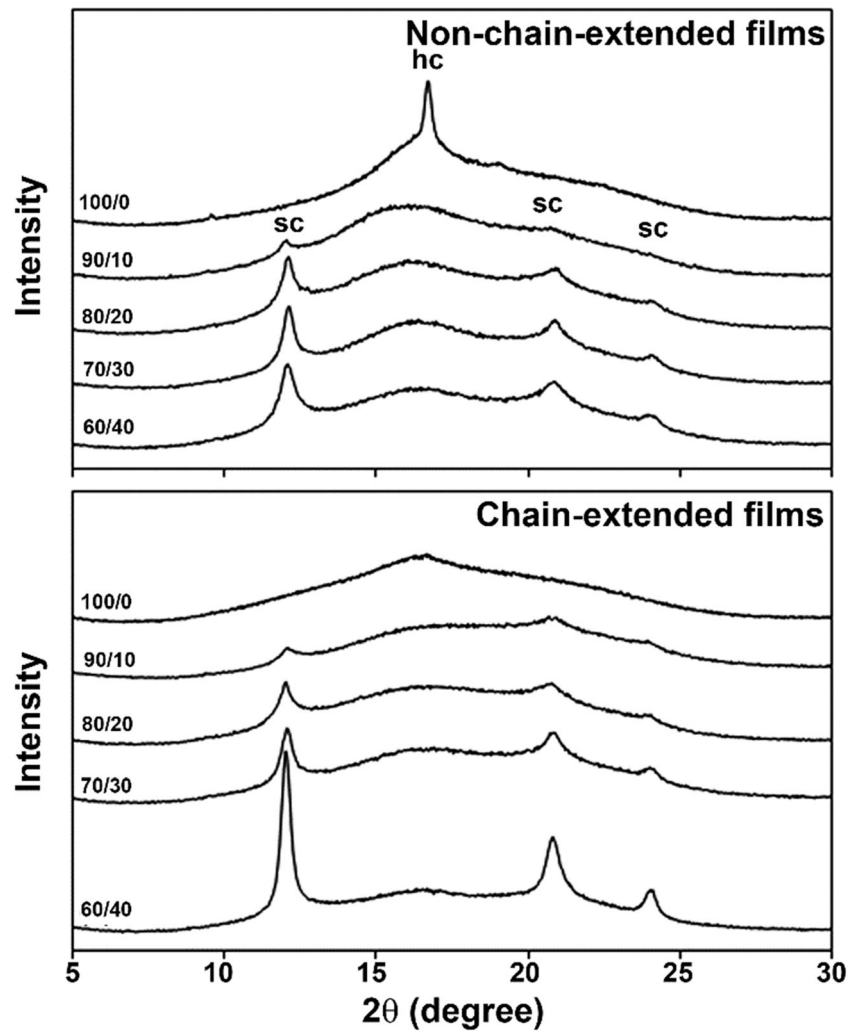
For  $X_{c,DSC}$ , the  $hc-X_{c,DSC}$  largely decreased and  $sc-X_{c,DSC}$  steadily increased as the PDLA ratio increased. The chain-extended blends had lower  $hc-X_{c,DSC}$  than the non-chain-extended blends for the same blend ratio. It has been reported

that the long-chain branched structures of chain-extended PLLA suppressed its homo-crystallization [33]. However, the  $sc-X_{c,DSC}$  of the blends did not change significantly by chain extension for the same blend ratio.

Crystallization behavior of the samples was investigated from DSC cooling curves as illustrated in Fig. 2. The  $T_c$  and enthalpy of crystallization ( $\Delta H_c$ ) of non-chain-extended PLLA-PEG-PLLA (105 °C and 27.7 J/g, respectively) were higher than that of the chain-extended PLLA-PEG-PLLA (91 °C and 20.1 J/g, respectively) suggested that chain extension suppressed crystallizability of homo-crystallites of PLLA-PEG-PLLA during DSC cooling scan. This supports the conclusion that branched structures of chain-extended PLLA-PEG-PLLA inhibited homo-crystallization of PLLA end-blocks as described above.

The  $T_c$  peaks of the  $scPLA$  from DSC cooling scan included crystallization of both the homo- and stereocomplex

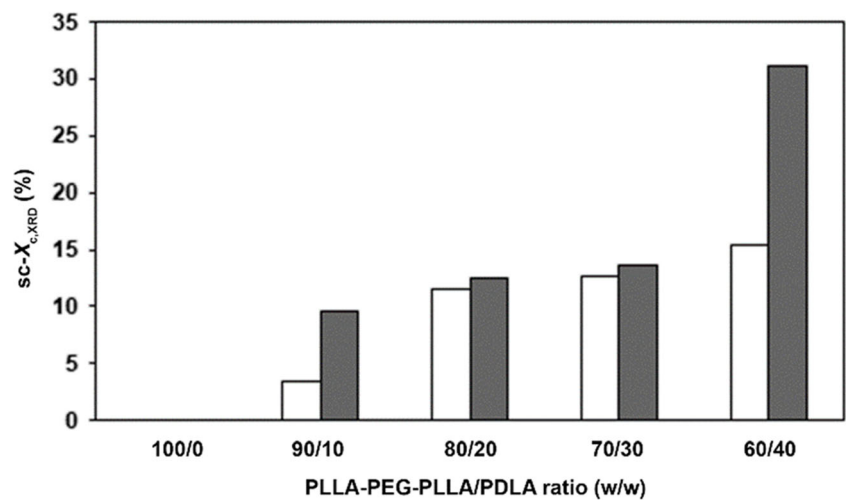
**Fig. 5** XRD patterns of (above) non-chain-extended and (below) chain-extended blend films of various PLLA-PEG-PLLA/PDLA compositions



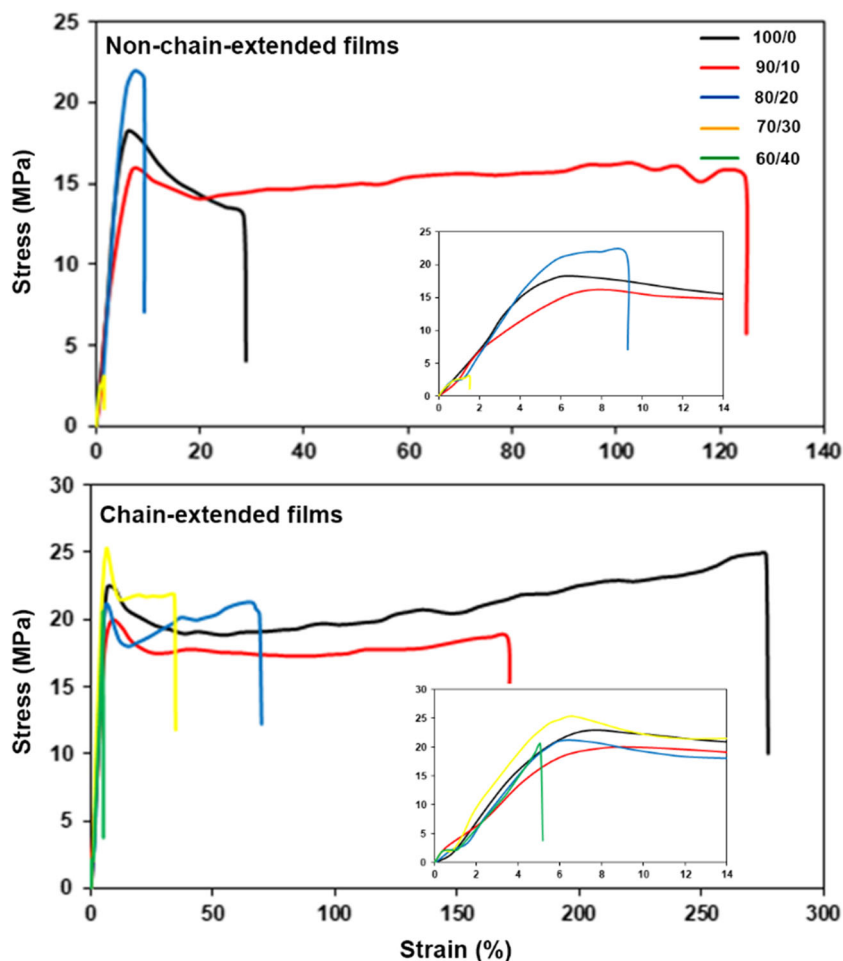
crystallites [29]. In this work, the 90/10 and 80/20 (w/w) blends with and without chain extension showed smaller  $T_c$  peaks (lower  $\Delta H_c$ ) significantly different from those of PLLA-PEG-PLLA. This may be due to the  $\Delta H_c$  of homo-

crystallization dropping considerably when the PDLA ratios were 10 and 20 wt% while little stereocomplex crystallization occurred at these PDLA ratios [18]. For both the non-chain-extended and chain-extended blend series, the  $T_c$  peaks shifted

**Fig. 6**  $sc-X_{c,XRD}$  of (□) non-chain-extended and (■) chain-extended blend films of various PLLA-PEG-PLLA/PDLA compositions



**Fig. 7** Tensile curves of (above) non-chain-extended and (below) chain-extended blend films of various PLLA-PEG-PLLA/PDLA compositions



to higher temperatures and  $\Delta H_c$  values steadily increased as the PDLA ratio increased because of increasing content of stereocomplex crystallites. The crystallization speed of stereocomplex crystallites was faster.

### Thermal decomposition

The thermal decomposition of PLLA-PEG-PLLA and blends was investigated from TG curves as shown in Fig. 3. The PLA and PEG chains showed thermal decompositions in the ranges 240–350 °C and 350–450 °C, respectively, as compared with TG curves of PLLA and PEG (see Fig. S2). The inset thermograms illustrate the initial-step of thermal decomposition. From Fig. 3 (above), it can clearly be seen that the blends showed slower thermal-decomposition than the pure PLLA-PEG-PLLA. The stronger interactions between PLLA end-blocks and PDLA chains improved its thermal stability.

The chain-extended blend series showed slower thermal decomposition than the non-chain-extended blend series. It can be seen that the blends with and without chain extension started weight loss at approximately 270 °C and 240 °C, respectively. Joncryl® has been used to maintain M.W. or build

high M.W. of PLA by formation of long-chain branching molecules during the melt process [35].

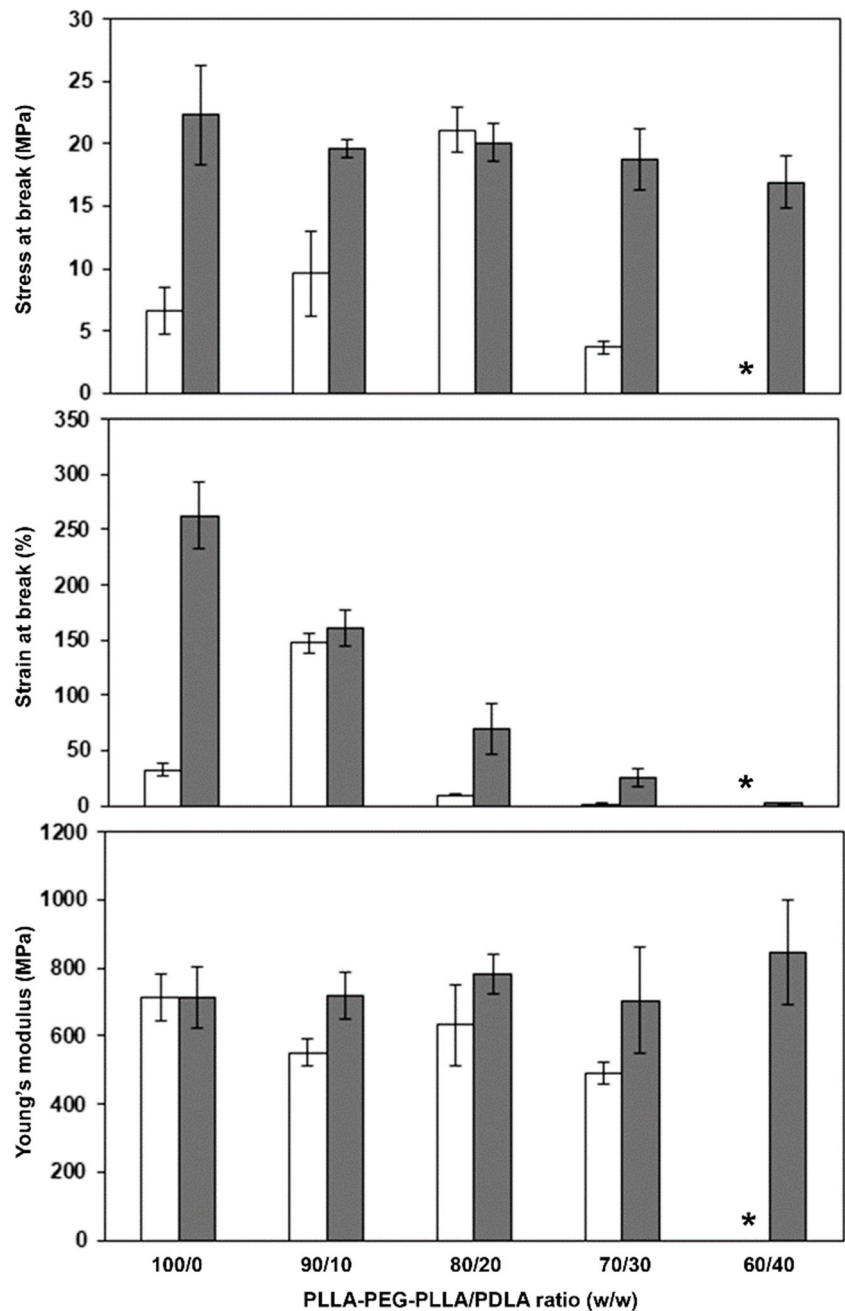
Derivative TG (DTG) thermograms in Fig. 4 were used to provide more data on thermal decomposition of the samples. Peaks of temperature of maximum decomposition-rate ( $T_{d, \max}$ ) were detected. The  $T_{d, \max}$  peaks of PLA chains were in range 292–318 °C for the non-chain-extended blend series [Fig. 4 (above)] and significantly increased with the PDLA ratio. This supports the conclusion that PLA stereocomplexation improved thermal stability of the blends. In addition, the  $T_{d, \max}$  peaks of PEG blocks of the non-chain-extended blends (409–414 °C) were also higher than the pure PLLA-PEG-PLLA (406 °C). However, the  $T_{d, \max}$  peaks of chain-extended PLA chains slightly increased from 302 °C to 305–308 °C when the PDLA was blended. The  $T_{d, \max}$  peaks of PEG blocks of the blends with chain extension were in range 412–414 °C.

### Crystalline structures

Figure 5 shows XRD patterns of film samples. For the non-chain-extended blend films in Fig. 5 (above), the PLLA-PEG-PLLA film only had a diffraction peak at 17° (hc



**Fig. 8** Tensile properties of (□) non-chain-extended and (■) chain-extended blend films of various PLLA-PEG-PLLA/PDLA compositions (\* = could not determine)

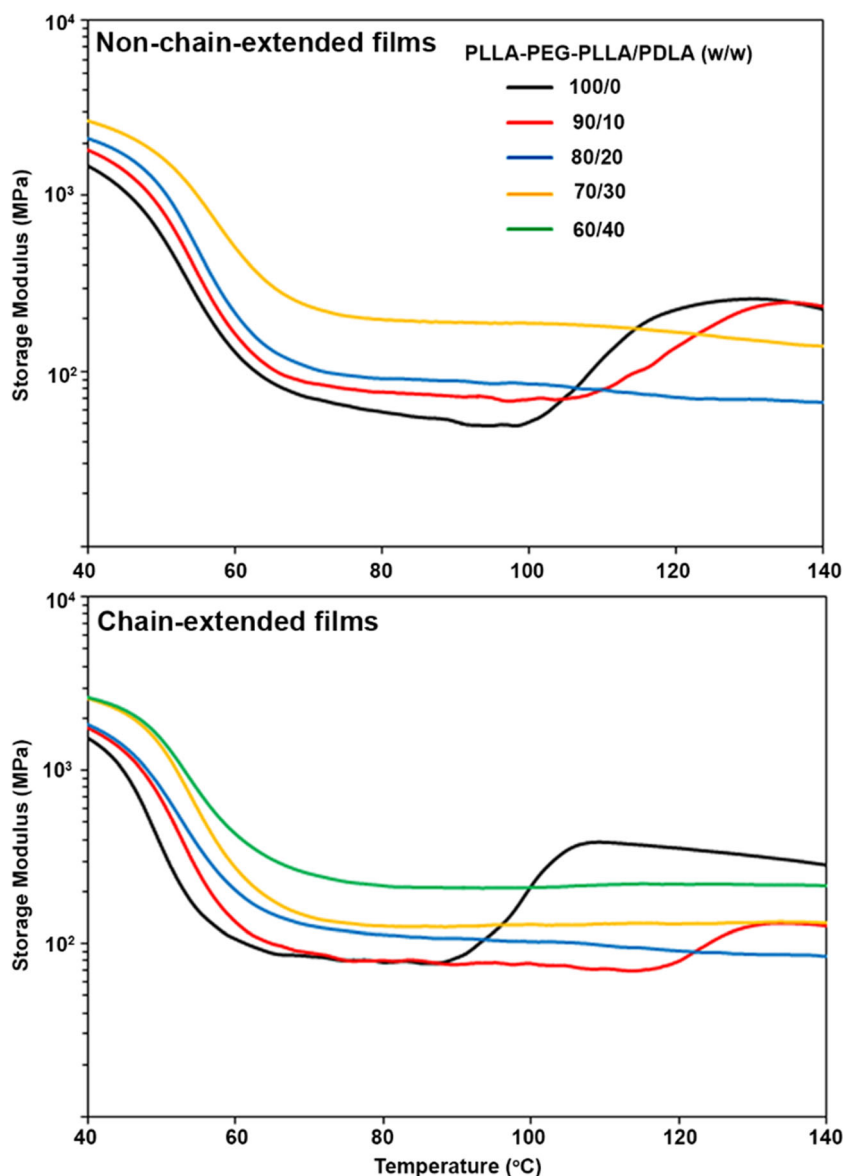


peak), attributed to the homo-crystallites of PLLA [34]. Usually the compressed PLLA films were completely amorphous. Therefore the crystallization of the PLLA end-blocks was improved by increasing their chain-mobility due to the flexible PEG middle-blocks [25]. For all the non-chain-extended blend films, the diffraction peaks assigned to homo-crystallites disappeared, and the diffraction peaks at 12°, 21° and 24° (sc peaks) ascribed to stereocomplex crystallites [34] were the only peaks observed. As PDLA ratio increased, the intensity of these diffraction peaks tended to increase. The results indicate that only stereocomplex crystallites formed in the blend films. This can be explained by

external compression-forces enhancing stereocomplexation of the blend films [36]. The chain-extended PLLA-PEG-PLLA film in Fig. 5 (below) was completely amorphous. The latter film did not have any diffraction peaks. Only sc peaks of stereocomplex crystallites were detected for all the chain-extended blend films. These diffraction peaks of stereocomplex crystallites more obvious as the PDLA ratio increased.

The  $hc-X_{c,XRD}$  and  $sc-X_{c,XRD}$  of the film samples were calculated from Eqs. (3) and (4), respectively. The non-chain-extended PLLA-PEG-PLLA film had only a hc peak ( $hc-X_{c,XRD} = 7.5\%$ ) while all the blend films had only sc

**Fig. 9** Storage modulus from DMA of (above) non-chain-extended and (below) chain-extended films of various PLLA-PEG-PLLA/PDLA compositions



peaks. The  $sc-X_{c,XRD}$  of the film samples were compared in Fig. 6. It can be seen that the  $sc-X_{c,XRD}$  of the blend films increased as the PDLA ratio increased. The  $sc-X_{c,XRD}$  values of the chain-extended blend film type were larger than the non-chain-extended blend film type for the same blend ratio.

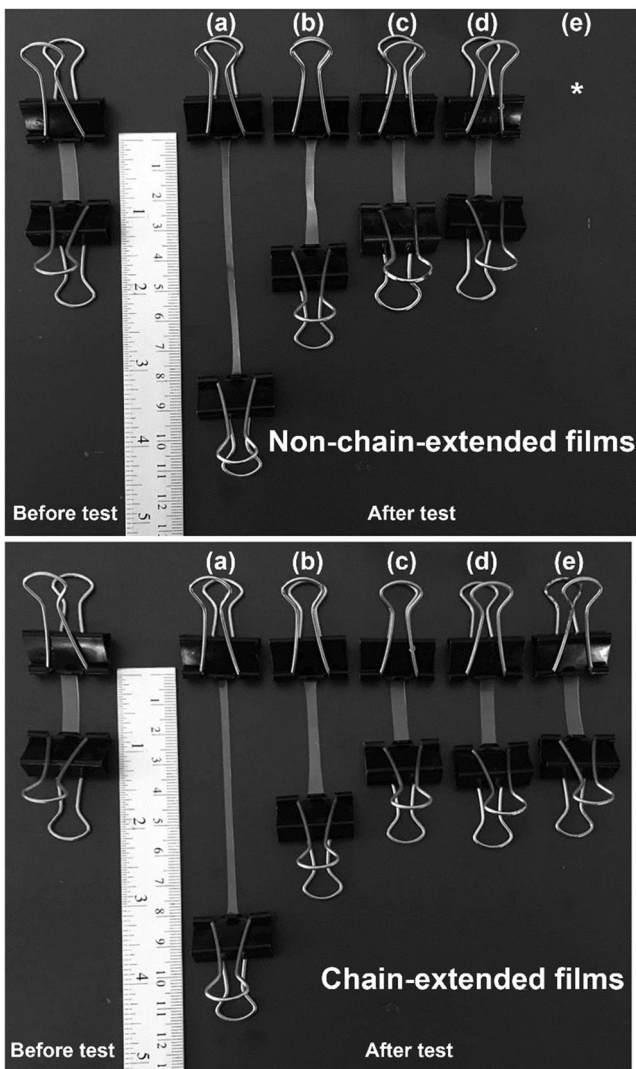
In previous work [32], the scPLA films of high M.W. PLLA/high M.W. PDLA blends with and without chain extension were prepared by melt blending before compression molding. The chain extension of stereocomplex PLLA/PDLA films suppressed stereocomplexation due to their rigid long-chain branching structures with high  $T_g$ s (54–55 °C) inhibiting crystallization. However, the chain-extended PLLA-PEG-PLLA/PDLA films in this work showed better stereocomplexation than the non-chain-extended PLLA-PEG-PLLA/PDLA films. This may be explained by the flexible long-chain branching

structures of PLLA-PEG-PLLA-based scPLA with low  $T_g$ s (31–33 °C) enhancing crystallization.

### Tensile properties

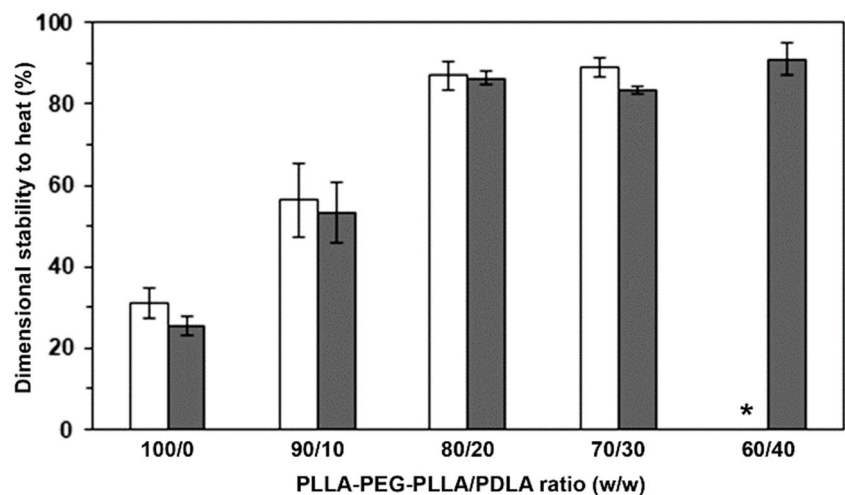
Figure 7 shows selected tensile curves of the film samples, except the 60/40 (w/w) PLLA-PEG-PLLA/PDLA blend film without chain extension because it was highly brittle. The inset tensile-curves are also presented for clarity. The blend films exhibited a yield point except for the chain-extended 60/40 blend film indicating more flexibility of these blend films.

The averaged tensile results are compared in Fig. 8. For the non-chain-extended blend films, the stress at break of the films increased until the PDLA ratio was increased up to 20 wt%. The stereocomplex crystallites



**Fig. 10** Photographs of dimensional stability to heat at 80 °C of (above) non-chain-extended and (below) chain-extended blend films with PLLA-PEG-PLLA/PDLA compositions of (a) 100/0, (b) 90/10, (c) 80/20, (d) 70/30 and (e) 60/40 (w/w) (★ = could not determine)

**Fig. 11** Dimensional stability to heat of (□) non-chain-extended and (■) chain-extended blend films of various PLLA-PEG-PLLA/PDLA compositions (★ = could not determine)



linked between the PLLA-PEG-PLLA chains acted as cross-linkers to enhance stress at break of the blend films [26, 27]. However the stress at break of the blend films dramatically dropped when the PDLA ratio was 30 wt%. The latter films became brittle because they contained a larger fraction of low M.W. PDLA. The strain at break of non-chain-extended PLLA-PEG-PLLA film increased from 33% to 148% as the PDLA ratio was 10 wt% due to the plasticizing effect of PEG middle-blocks for the film with low crystallinity ( $sc-X_{c,XRD} = 3.4\%$ ). However, the strain at break largely dropped to 10% when the PDLA ratio was 20 wt%. Brittleness was observed in the latter film.

The strain at break of the PLLA-PEG-PLLA film was largely improved with chain extension. This is due to the long-chain branching structures suppressing the homo-crystallization of the PLLA end-blocks and enhancing the plasticizing effect of the PEG middle-blocks [25]. The chain-extended blend films showed better stress and strain at break than the non-chain-extended blend films for the same blend ratio. The results may be due to the longer chains of chain-extended blend films increased tie-chain density between stereocomplex crystallites [37].

In addition, the stress and strain at break of the chain-extended blend films decreased with increasing PDLA ratio. The larger fraction of low M.W. PDLA made the film brittle. The larger PDLA ratio induced higher  $sc-X_{c,XRD}$  that also reduced the plasticizing effect of flexible PEG middle-blocks. The Young's moduli of blend films with and without chain extension were in ranges 705–846 MPa and 490–714 MPa, respectively.

### Thermo-mechanical properties

Changes of storage modulus as a function of temperature from DMA analysis have been used to investigate the heat-resistant

properties of scPLA [38, 39]. The storage modulus of amorphous PLLA with poor heat-resistance largely dropped in the  $T_g$  region before rising up again due to cold crystallization during the DMA heating scan [40]. However high crystallinity PLLA with high heat-resistance maintained its stiffness in the  $T_g$  region [8].

Figure 9 shows storage modulus of film samples from DMA. For the non-chain-extended films in Fig. 9 (above), the 100/0 and 90/10 (w/w) PLLA-PEG-PLLA/PDLA films exhibited a cold-crystallization effect at around 100 °C and 110 °C, respectively, during DMA heating. Therefore these films had poor heat-resistance. The storage modulus in the range 70–90 °C significantly increased with the PDLA ratio suggesting that the heat-resistance of films increased with increasing PDLA ratio because the higher PDLA ratio induced larger values of  $sc-X_{c,XRD}$  [see Fig. 6]. The heat-resistance of chain-extended films also improved with increasing PDLA ratio as shown in Fig. 9 (below). Their storage moduli in the temperature range 70–90 °C also increased with the PDLA ratio.

### Dimensional stability to heat

The film samples before and after testing of dimensional stability to heat are shown in Fig. 10. The dimensional stability of 60/40 (w/w) PLLA-PEG-PLLA/PDLA blend film was not determined due to its high brittleness. Both the PLLA-PEG-PLLA films with and without chain extension exhibited the largest film-extension [Fig. 10(a)] indicating they had poor heat-resistance. All the blend films after testing exhibited shorter film-extension than the PLLA-PEG-PLLA films. The results suggested that the blend films had better heat-resistance because they contained stereocomplex crystallites. The film extension significantly decreased as the PDLA ratio was increased from 10 to 20 wt%. This is due to increasing the  $sc-X_{c,XRD}$  of the blend films.

The heat resistance of the film samples was clearly compared with the dimensional stability to heat as calculated from Eq. (5). Figure 11 shows the results of dimensional stability to heat that were 26% and 31% for PLLA-PEG-PLLA films with and without chain extension, respectively. These values increased up to 56% and 53% when the PDLA ratio was 10 wt%. The results of dimensional stability to heat of blend films were in the range 83–91% for the PDLA ratios of 20–40 wt%. Thus, the heat resistances of the blend films were better than the PLLA-PEG-PLLA films, for both the non-chain-extended and chain-extended blend films. The stereocomplexation of PLA with the PDLA can improve heat resistance of the PLLA-PEG-PLLA films.

### Conclusions

The scPLA were prepared by melt blending the PLLA-PEG-PLLA with low M.W. PDLA in the absence or presence of chain extender. The DSC results showed that complete stereocomplexation was obtained when the PDLA ratio was increased up to 30 wt% for both the non-chain-extended and chain-extended blend series. In addition, the larger PDLA ratios of the blends induced faster crystallization upon the DSC cooling scan.

All the blend films fabricated by compression molding exhibited complete stereocomplexation as indicated by the XRD results. The  $sc-X_{c,XRD}$  of blend films increased steadily with the PDLA ratio. The non-chain-extended blend films became brittle when the PDLA ratio was increased up to 20 wt%. However, the chain-extension reaction can reduce film brittleness. The PDLA blending enhanced heat-resistance of both the non-chain-extended and chain-extended blend film series as seen from the results of DMA and dimensional stability to heat. High heat-resistance of blend films was obtained when the PDLA ratio was increased up to 20 wt%. In conclusion, the low M.W. PDLA has the potential to induce the stereocomplexation and heat-resistance of PLLA-PEG-PLLA/PDLA blends while the chain-extension reaction improved mechanical properties of the blend films. This work will expand the knowledge of scPLA that will provide more application potential for flexible and high heat-resistant scPLA products.

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