



Poly (Vinyl Alcohol) Composite Membrane with Polyamidoamine Dendrimers for Efficient Separation of CO₂/H₂ and CO₂/N₂

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Abstract

Although polyvinyl alcohol (PVA) membranes are commonly used for CO₂ separation, there is still large development space in mechanical properties and high selectivity of the gas separation process. In this study, the gas separation performance and mechanical properties of the (PVA/Cu²⁺) substrate membranes were improved by introducing polyamidoamine (PAMAM). PAMAM had an important effect on the gas adsorption and separation performance of the membrane. In addition, the gas adsorption and separation properties of the PVA/Cu²⁺/PAMAM membrane (PPCm) were analyzed and studied when the inlet gas pressure and the species of mixed gases were variable. The results showed that the crystallinity and mechanical properties of the membrane with the PAMAM had been significantly improved. Young's modulus of PPCm with 30% PAMAM was 132% higher than that of the PVA/Cu²⁺ composite membrane without PAMAM. In addition, efficient separation efficiency and high selectivity of the gas separation process were observed. The separation factors of the PPCm for CO₂/H₂ and CO₂/N₂ were about three times higher than that of the PVA/Cu²⁺ substrate membranes. These results suggested that the introduction of PAMAM was promising for CO₂ separation and permeance.

Keywords PVA · PAMAM · Carrier · Crystallinity · CO₂ separation

Introduction

With the increasingly severe climate change, the separation of carbon dioxide from its emission sources has attracted global attention. Efforts have been made to find economic separation techniques to capture and separate CO₂ [1–5]. Many CO₂ capture technologies have been developed, among which membrane separation is one of the most effective technologies. Compared with the traditional method of solvent absorption, membrane separation technology has the advantages of low investment cost, compact structure and no secondary pollution [6–8]. Polyvinyl alcohol (PVA) membrane is generally used in the mixed gas separation, because it has the large amount of the hydroxyl groups on its surface, which is conducive to the formation of a large diffusion rate difference in the membrane [9–13]. Nevertheless, the separation efficiency and mechanical properties of the membrane are still poor, and it cannot be commercially applied. The in-depth study of PVA membranes found that some metal ions with PVA could form macromolecular complexes [14–19]. Therefore, the mechanical properties of the PVA based membrane were further improved by introducing Cu²⁺ into the PVA membrane [10]. But its gas separation efficiency still needs to be improved.

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Besides, there is a constraint trade-off between permeability and selectivity of commonly used polymer membranes. Polymer membranes with high permeability are usually less selective [20–23]. The promotion transfer membrane is to introduce the carrier inside the membrane, which is connected to the base membrane in the form of covalent bond. And then to promote the transfer of the component by reversible interaction between the carrier and a specific gas component in the mixed gases to be separated. Moreover, it may be mentioned that the carrier in the membrane is connected to the substrate in the form of covalent bond, which effectively solves the immobilization problem of the carrier [24, 25].

Polyamidoamine (PAMAM) is one of the most widely studied and mature tree-like molecules. It has high branching degree, symmetrical radial structure, high group density of surface amine groups. PAMAM can provide a large number of primary and secondary amine reaction active points, and has good hydrodynamic properties, easy membrane formation, good compatibility with PVA and so on [26–28].

In this work, based on the high permeability and selectivity of CO₂, PAMAM was introduced into PVA/Cu²⁺ membranes to prepare the PVA/PAMAM/Cu²⁺ promoting transfer membrane (PPCm) for further exploration. PAMAM could provide a large number of reversible reaction points with carbon dioxide. It was found that without affecting the permeability, the selection of CO₂ was highly improved. It provided a solution for the membrane to weaken the constraint trade-off between permeability and selectivity of it.

Experiment

Materials

PVA (117) was purchased from Kuraray Co.Ltd. CuSO₄·5H₂O (Analytical Reagent) was from Beijing Sinopharm Chemical Reagent Co., Ltd. Polyethersulfone (PES005) was from Beijing Vontron Technology Co., Ltd. PAMAM (zero-generation) was self-made in laboratory.

Preparation of the PPCm

PVA aqueous solution with solid content of 5% was prepared. Then different contents of PAMAM were added into PVA solution by stirring 4 h at room temperature. The calculation formula of PAMAM content (w_{PAMAM}) is as follows:

$$w_{\text{PAMAM}} = \frac{m_{\text{PAMAM}} \times 100\%}{m_{\text{pamam}} + m_{\text{PVA}} + m_{\text{Cu}^{2+}}}$$

The m_{PAMAM} , m_{PVA} , $m_{\text{Cu}^{2+}}$ are the mass of PAMAM, PVA, Cu²⁺.

Whereafter, 5% Cu²⁺ was added into PVA/PAMAM solution by stirring 2 h at room temperature. Then the solution was allowed to stand for a period of time to remove the bubbles. The PVA/PAMAM/Cu²⁺ membrane-forming solution was poured horizontally into the glass mold to get the PVA/PAMAM/Cu²⁺ promoting transfer membrane (PPCm). Finally, the PPCm was dried at 60 °C for 24 h.

Characterization

The structure of the PPCm was determined by Fourier transform infrared spectrometer (FTIR). The infrared scanning test was carried out by potassium bromide pressing method and Nicolet iN10MX (Thermo Electron, US) infrared tester. The scanning range was 4000–500 cm⁻¹.

The structure of dried PPCm was observed and photographed with scanning electron microscope (SEM) (Quanta FEG-250, FEI Nanoports, US) operating at an acceleration voltage of 10 kV.

The dried samples were tested with Different Scanning Calorimetry (DSC) (Q2500 TA Instruments) in the N₂ atmosphere. And the sample weight was about 5–10 mg.

The mechanical properties test, the splines were placed 24 h before testing. And it tested by the tensile speed of 50 mm/min at room temperature. During the experiment, each group of samples was tested 5 times, and the average value was taken.

Gas permeability and separation performance test: effective sample size: Φ97 mm, transmission area: 38.48 cm² and gas test pressure: 0.5 MPa for the single gases CO₂, N₂ and H₂. Effective transmission area: 19.26 cm² and gas test pressure: 0.1 MPa–0.5 MPa for mixed gases CO₂/N₂ with a volume ratio of 85/15 and CO₂/H₂ with a volume ratio of 50/50. The adsorption separation chamber was sealed with a sealing ring to ensure that the gas on the permeance side did not diffuse with the air during the test.

2. Results and Discussion

Figure 1 illustrated the schematic for the preparation of the PVA/Cu²⁺/PAMAM membranes (PPCm) and the process of gases separation. PAMAM has high concentrations of amine groups which can enable the membrane to increase the selectivity of CO₂. Therefore, PAMAM was introduced into the PVA/Cu²⁺ membranes. Cu²⁺ and PAMAM complexed with PVA polymer chains to form the PPCm with significantly enhanced mechanical properties and separation efficiency [7, 8]. Generally, small molecular gases such as CO₂, N₂ and H₂ permeated through the membrane by the physical solution-diffusion mechanism. However, when PAMAM was introduced into the membrane, the amine groups in PAMAM

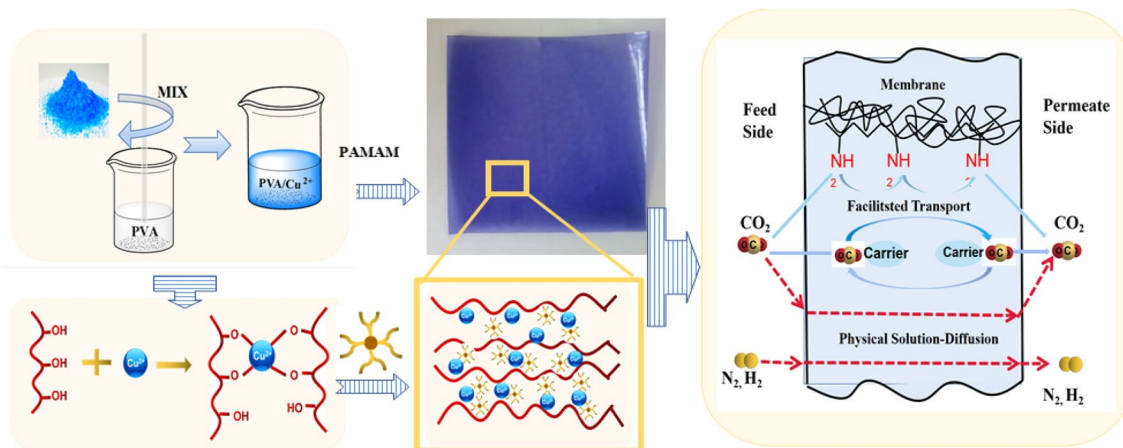


Fig. 1 The schematic for preparation of the PPCm and the process of gases separation

could react reversibly with CO_2 , so as to promote the permeance and separation of CO_2 .

Structure Characterization

Figure 2 showed the FTIR spectra of PPCm with different PAMAM contents. For the PVA/ Cu^{2+} base membranes without PAMAM, there was 3416 cm^{-1} stretching vibration attributed to $-\text{OH}$, 2919 cm^{-1} stretching vibration attributed to $-\text{C}-\text{H}$, the stretching vibration of 1434 cm^{-1} was $\text{H}-\text{C}-\text{H}$, 912 cm^{-1} and 842 cm^{-1} belonged to the stretching vibration of $\text{C}-\text{O}-\text{H}$ and $\text{C}-\text{C}$ respectively. But for the PPCm two new absorption peaks position at 1645 cm^{-1} and 1565 cm^{-1} belonged to the stretching vibration of $-\text{C}-\text{O}-$ and bending vibration of $-\text{N}-\text{H}$ in PAMAM. With the increase of PAMAM, they shifted to 1655 cm^{-1} and 1555 cm^{-1} . At this time, the peak position of $-\text{OH}$ gradually moved to a lower wave number. The shift of these functional group peaks was mainly due

to the hydrogen bond interaction between the $-\text{NH}-\text{CO}-$ group in the PAMAM and the $-\text{OH}$ group in the PVA. The strong hydrogen bonding interaction could act as physical crosslinking agents, which would enhance the mechanical performances of the matrix.

Figure 2(b) showed the surface and cross-section SEM images of PPCm with different PAMAM contents. When the content of PAMAM was 0% and 5%, the cross-section and surface of the membrane were smooth, and no obvious PAMAM agglomeration was observed. However, when the content of PAMAM exceeds 10%, it was obvious that the agglomeration phenomenon was more and more obvious on the surface, and the aggregate was also larger and larger. The cross section of the membrane was also rougher. The results showed that with the increase of PAMAM content, the surface roughness of PPCm increases, resulting in the decrease of membrane homogenization. This also led to a decrease in the tensile strength of the membrane.

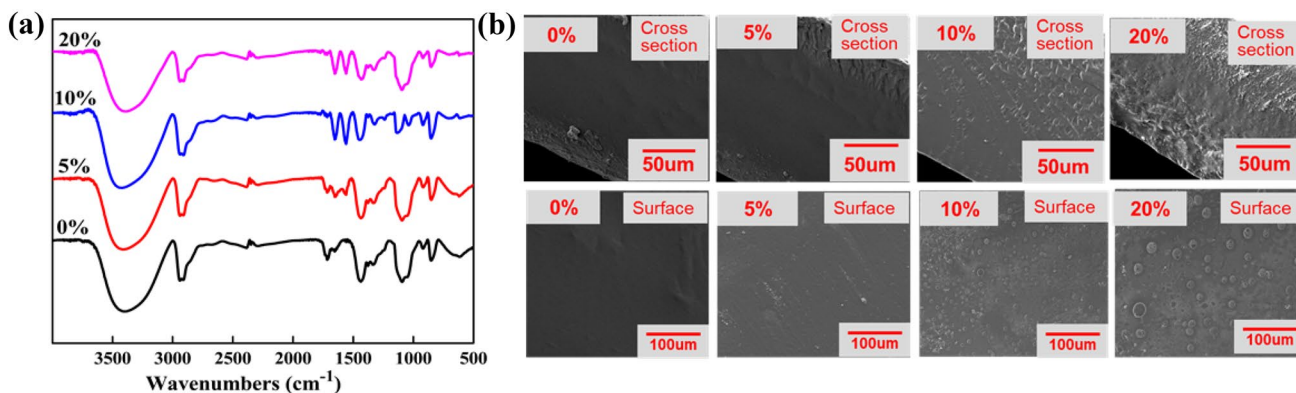


Fig. 2 a the FTIR spectra and b the surface and cross-section SEM images of PPCm with different PAMAM contents

DSC Analysis

Figure 3 showed the DSC curves and crystallinity of PPCm with different PAMAM contents. From the endothermic curves of the PPCm, PVA crystallization peak at ca. 180 °C could be observed. With the introduction of PAMAM, the crystallization onset temperature and the crystallization peak temperature decreased with the increase of PAMAM. The crystallinity of PPCm could be calculated from the follows:

$$X_c = \frac{\Delta H_c}{f \times \Delta H_0} \times 100\%$$

ΔH_0 is the melting enthalpy of the PVA membrane at 100% crystallinity; the ΔH_c is the melting enthalpy of the transfer membrane; and the f is the mass fraction of the polymer matrix.

It could be concluded that the crystallinity of PPCm was obviously higher than that of PVA/Cu²⁺ based membrane without PAMAM, as shown in Fig. 3(c). With the increase of PAMAM, the crystallinity of PPCm increased obviously. The results showed that the PAMAM with high degree of branching exhibited heterogeneous nucleation effect in the PVA matrix, which could increase the crystallinity.

Mechanical Properties

Figure 4 illustrated tensile strength, Young's modulus and elongation at break of the PPCm with different PAMAM contents. Figure 4 showed that the tensile strength of 5% PAMAM increased to the maximum. And then the tensile strength of PPCm decreased continuously with the increase of PAMAM content. PAMAM exhibited reinforcing effect in the matrix, and increased the rigidity of the membrane. With the increase of PAMAM, the Young's modulus of PPCm increased obviously. When the content of PAMAM

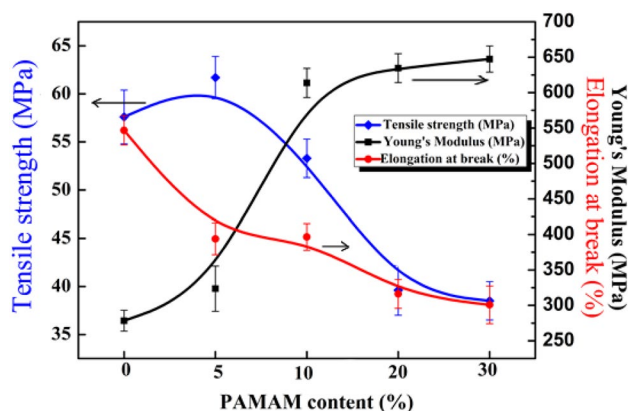


Fig. 4 Tensile strength, Young's Modulus and Elongation at break of the PPCm with different PAMAM contents

in the membrane was 30%, the Young's modulus reached 648.6 MPa. The Young's modulus of the film without PAMAM was only 279.5 MPa. The Young's modulus of the transfer promoting membrane with the 30% PAMAM content increased by 132% compared with the PVA/Cu²⁺ base membrane without PAMAM. The main reason was that the crystallinity of the membranes increased with the increasing of PAMAM. As the crystallinity of the membrane increased, its Young's modulus will increase accordingly. The fracture elongation of PPCm decreased significantly with the increase of PAMAM content. When the existence of PAMAM was too much, it destroyed the structure of the membrane, resulting in the decrease of tensile strength and elongation at break. Besides, the results of Young's modulus and tensile strength were mainly due to the increase of crystallinity of the PPCm, as well as the strong hydrogen bonding interactions. The raise of intermolecular force led to the promotion of Young's modulus and the decline of tensile strength.

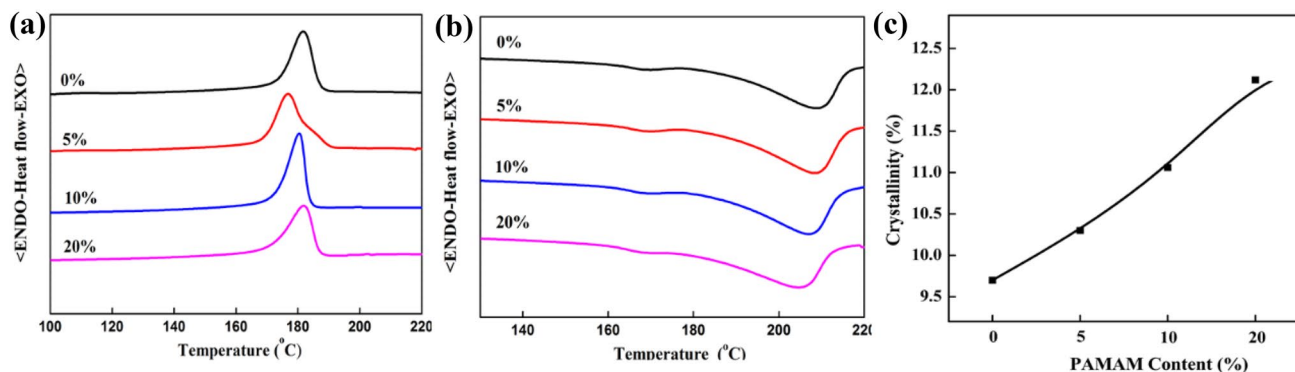


Fig. 3 DSC **a** heating curves **b** cooling curves and **c** Crystallinity of PPCm with different PAMAM contents

Gas Permeance Properties

Separation Properties for a Single Gas

The gas permeance unit (GPU) of three single gases, CO₂, H₂ and N₂, were measured, as shown in the Fig. 5. The CO₂ GPU of the PPCm increased with the increase of PAMAM. The gas permeance unit of CO₂ was as high as 120 GPU when the PAMAM concentration was 30%. It was much greater than that of N₂ and H₂. Even with the increase of PAMAM concentration, the gas permeance unit slightly decreased. The small decrease of gas permeance of N₂ and H₂ was related to the increase of PAMAM content. It was mainly due to the reduction of physical solution-diffusion in the process of gas permeance. The crystallinity of the membrane increased and the molecular chain arrangement orientation made the membrane more compact, so the small molecules that could be physically penetrated were reduced. Therefore, the physical solution-diffusion of the membrane decreased with the PAMAM content increasing. However, in the course of CO₂ permeance through PPCm with amine carriers, there was not only physical solution-diffusion mechanism, but also facilitated transport mechanism. This fully illustrated that the introduction of PAMAM would have an efficient effect on the separation of mixed gases.

Separation Properties of the Mixed Gas

As shown in Fig. 6, the gas permeance unit of CO₂/N₂ with a volume ratio of 15/85 was measured under different inlet gas pressures. The GPU of CO₂ and N₂ increased significantly with the increase of PAMAM contents. And the CO₂ and N₂ permeance unit increased at higher inlet gas pressure. When the PAMAM was 10% and the inlet gas pressure was

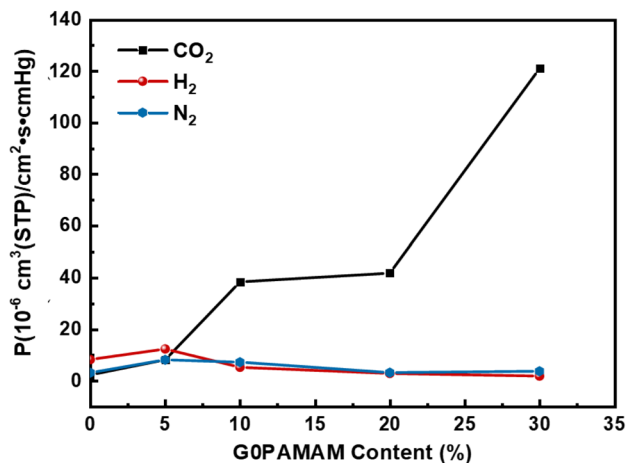


Fig. 5 The gas permeance unit of the PPCms with different PAMAM contents

0.5 MPa, the CO₂ permeance unit was 7.3 GPU and the N₂ permeance unit was 1.6 GPU, as illustrated in Fig. 6 (a, b). Separation factor was an important parameter to measure the separation ability of membranes. The separation factors for the CO₂/N₂ gas mixture of PPCm were calculated, as shown in Fig. 6(c). The separation factors of PPCm could be calculated from the follows:

$$\alpha = \frac{y_A/y_B}{X_A/X_B}$$

y_A is the volume fraction of component A in the detection gas (including permeability and purge gas); y_B is the volume fraction of component B in the detection gas (including permeability and purge gas); X_A is the volume fraction of component A in the feed gas; X_B is the volume fraction of component B in the feed gas.

As the PAMAM content increasing, the separation factor of CO₂/N₂ increased obviously. When the content of amine was too much, its steric resistance increases, resulting in the decrease of air filtration efficiency.

The permeance of small molecular gases such as CO₂ and N₂ through the membrane was the physical-diffusion mechanism. Beyond that, there was another facilitated transport mechanism for CO₂ permeance through the PPCm. Therefore, the gas permeance unit of CO₂ was obviously larger than that of the N₂. And with the increase of PAMAM contents, the separation factor increased. Because it increased the density of effective amine groups which were capable of interacting with CO₂. The CO₂ and N₂ permeance unit increased at higher inlet gas pressure, because of the coupling of two gases in the mixture. In general, the separation factors of PPCm increased with the increase of PAMAM.

The general trade-off between polymer permeability and selectivity was first quantified by Robeson when he identified 16 s in plots of $\log(P_x/P_y)$ versus $\log(P_x)$. Robeson updated all of the upper bounds in 2008 using initial data for two spirobisindane-based Polymers of Intrinsic Microporosity. Among them, the upper limit of CO₂/N₂ was updated again by McKeown et al. in 2019. Fitting parameters for the 2008 and proposed CO₂/N₂ and CO₂/H₂ upper bounds using the formula:

$$P_x = k\alpha_{xy}^n$$

where P_x is permeability of the most permeable x-gas, k is the front factor, α_{xy} is the selectivity for x/y gas pair, and n is the slope.

In Fig. 6(d), under the same 1 bar = 0.1 MPa, the comparison of the CO₂ separation performance in this work with the upper bounds in the literature [11, 20] was showed. The PCO₂/PN₂ in the work was numerically close to the upper bounds in the literatures. Therefore, as the gas separation membrane was qualified.

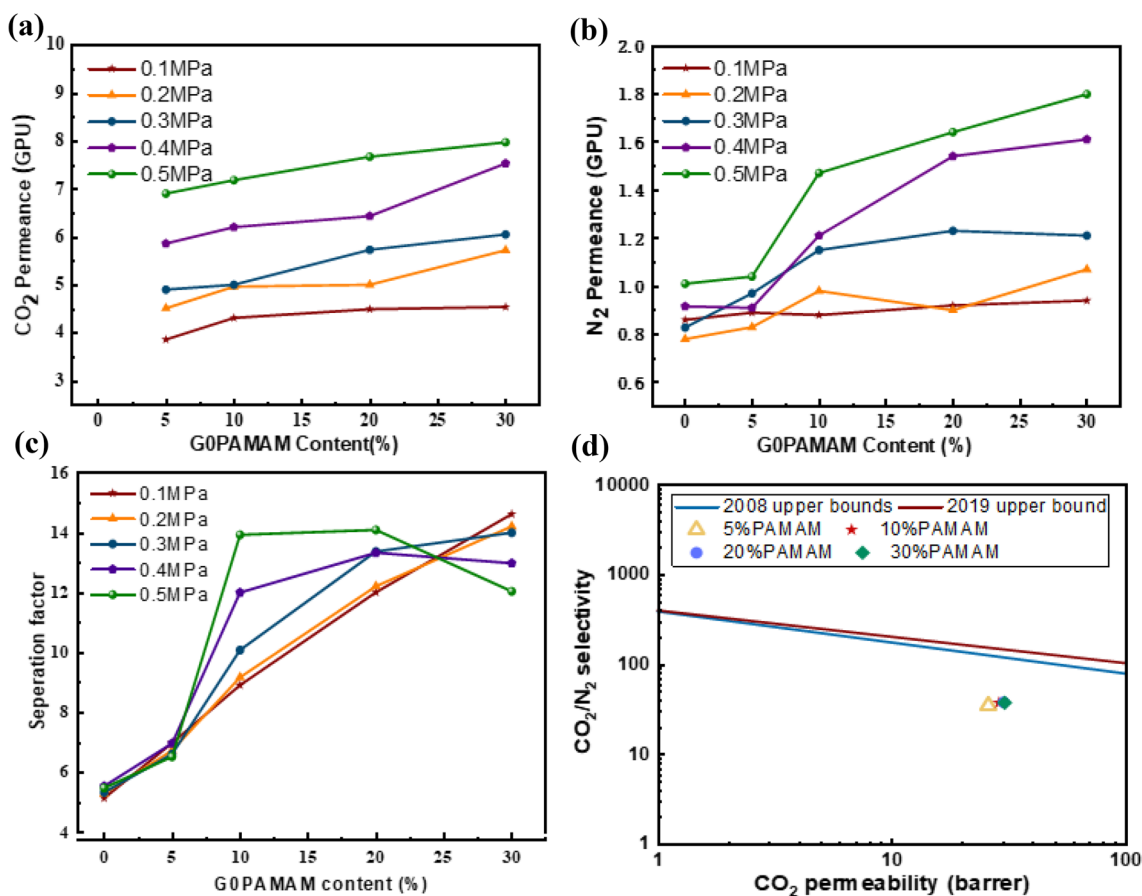


Fig. 6 CO₂/N₂ mixture separation performance of the membranes with different PAMAM concentrations. **a** CO₂ permeance, **b** N₂ permeance, and **c** the separation factors of the CO₂/N₂; **d** comparison of

the membranes with 5%, 10%, 15% and 20% PAMAM performance in this work with literature data^{11, 20} for CO₂/N₂. Feed gas: CO₂/N₂ (15/85 by volume) mixture

Under different inlet gas pressures, the gas permeance unit of CO₂/H₂ with a volume ratio of 50/50 was illustrated in Fig. 7(a, b). The CO₂ permeance unit generally decreased and then stabilized with the increase of PAMAM content, while the H₂ permeance unit generally decreased with the increase of PAMAM content. The CO₂/H₂ separation factors of the PVA/PAMAM/Cu²⁺ transfer membranes were calculated, as shown in Fig. 7(c). And when the PAMAM was 20% and the inlet gas pressure was 0.5 MPa, the separation factor of the PPCm was 1.3, reaching the maximum. It was in the upper part of diffusivity coefficient CO₂/N₂ lie between 0.9 and 1.5 proposed by McKeown et al. The separation factor of CO₂/H₂ increased steadily, with the increase of PAMAM contents. When the PAMAM content exceeded 20%, the separation factor of PPCm for CO₂/H₂ decreased.

Since the dynamic diameter of the H₂ molecule is smaller than that of the CO₂ molecule [29]. The small size of H₂ molecule was easier to permeate through the membrane than CO₂ and N₂ molecules by the dissolution-diffusion mechanism, when the PAMAM content increased, the tightness of the membrane increased, resulting in the decline of H₂

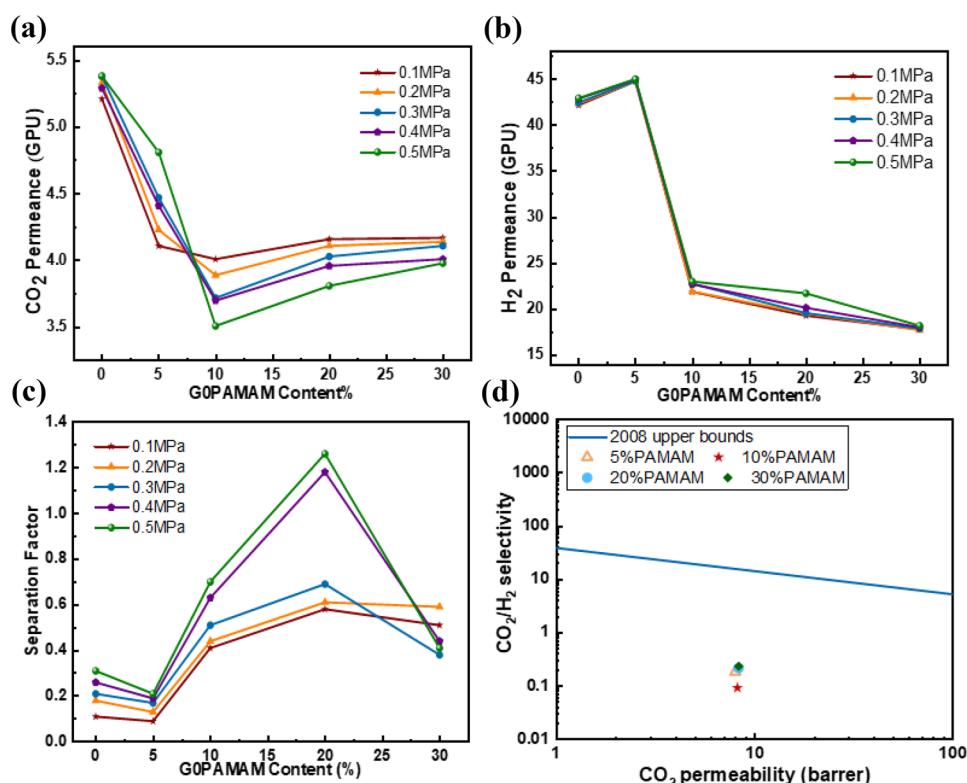
permeance unit. However, CO₂ mainly permeated through the PPCm by the facilitated transport mechanism. Therefore, the separation factor of the PPCm for the CO₂/H₂ mixture was much smaller than that for CO₂/N₂. When the PAMAM content was too much, the effective amine density decreased. And it had resulted in the decline of the separation factors.

In Fig. 7(d), under the same 1 bar = 0.1 MPa, the comparison of the CO₂ separation performance in this work was compared with the upper bound in the literature²⁰. And the numerical gap between the CO₂/H₂ separation performance of the membranes in this work and the upper bound was bigger than that between the CO₂/N₂ separation performance of the membranes in this work and the upper bound in the literature.

Conclusion

In this study, PAMAM was successfully introduced into the PVA/Cu²⁺ base membrane, and the uniformly transparent PPCm was successfully prepared. PAMAM could act

Fig. 7 CO₂/H₂ mixture separation performance of the membranes with different PAMAM concentrations. **a** CO₂ permeance, **b** H₂ permeance, and **c** the separation factors of the CO₂/H₂; **d** comparison of the membranes with 5%, 10%, 15% and 20% PAMAM performance in this work with literature data²⁰ for CO₂/H₂. Feed gas: CO₂/H₂ (50/50 by volume) mixture



as heterogeneous nucleation agents in the PVA/Cu²⁺ base membrane to improve the crystallization of the transfer membrane. The introduction of the mechanical properties of PAMAM reduced the fracture elongation and increased the elastic modulus. The introduction of PAMAM has little effect on the gas permeance unit (GPU) of N₂ and H₂. But it significantly improved the GPU of CO₂. As the content of PAMAM increased, the separation factor of PPCm of CO₂/N₂ and CO₂/H₂ were increased. The separation factor of PPCm of CO₂/N₂ was much larger than that of CO₂/H₂. This membrane can be used for CO₂ capture and separation, and it will make an important contribution to the greenhouse effect.

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Declarations

Competing Interest The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

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