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Synthesis of Magnetic Chitosan-Fly Ash/Fe₃O₄ Composite **for Adsorption of Reactive Orange 16 Dye: Optimization by Box–Behnken Design**

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Abstract

A hybrid composite biopolymer of magnetic chitosan-fly ash/Fe₃O₄ (CS-FA/Fe₃O₄) was prepared to be an effective composite biosorbent for the removal of reactive orange 16 (RO16) dye from aqueous media. Various analytical techniques such as XRF, BET, XRD, FTIR, and SEM–EDX were utilized to characterize of CS -FA/Fe₃O₄ composite. The effects of adsorption process parameters namely adsorbent dose (A: 0.04–0.12 g), solution pH (B: 4–10), temperature (C: 30–50 °C), and time (E: 20–90 min) were optimized by using Box–Behnken design (BBD) in response surface methodology (RSM). The experimental results indicate that the highest RO16 removal was 73.1% by signifcant interaction between BC (p-value=0.0002) and AD (p-value = 0.022). The optimum RO16 dye removal conditions were recorded at solution pH \sim 4, adsorbent dose (0.08 g), temperature (30 °C), and time (55 min). The adsorption process was well described by pseudo-second order (PSO) kinetic and Freundlich isotherm model. The adsorption capacity of CS-FA/Fe₃O₄ composite for RO16 dye was 66.9 mg/g at 30 °C. The mechanism of the RO16 dye adsorption included many interactions such as electrostatic, $n-\pi$ interaction, H-bonding, and Yoshida H-bonding. Furthermore, the $CS-FA/Fe_3O_4$ composite exhibited a high ability to separate from the aqueous solution after adsorption process by external magnetic feld.

Keywords Magnetic chitosan · Fly ash · Reactive orange 16 dye · Adsorption · Response surface methodology

Introduction

Organic dyes are widely utilized in various industries such as printing, textile, leather, paint, and pharmaceuticals [[1\]](#page-12-0). The discharge of these dyes without treatment into water is one of the environmental problems due to its risks on aquatic life and human's health [[2\]](#page-12-1). Therefore, it is necessary to remove these dyes before releasing it into the environment. Several methods have been applied to remove these dyes prior to discharge into water such as photocatalytic [\[3](#page-12-2)], adsorption [\[4](#page-12-3), [5](#page-12-4)], oxidation [\[6](#page-12-5)], and flocculation [\[7](#page-12-6)]. Adsorption is considered one of the most efficient methods used to remove

dyes because of the simplicity of design, non-generation of toxic materials, low cost, and high efficiency $[8-10]$ $[8-10]$ $[8-10]$.

Chitosan (CS) is a cationic polysaccharide composed of D-glucosamine units [\[11](#page-12-9)]. CS can be obtained from the deacetylation of chitin, which is the second most abundant biopolymer in nature after cellulose [\[12](#page-12-10)]. CS has various interesting properties such as biodegradability, non-toxicity, biocompatibility, and antimicrobial activity [[13](#page-12-11), [14](#page-12-12)]. The uniqueness of CS molecular structure comes from the availability of amino $(-NH_2)$ and hydroxyl $(-OH)$ groups [\[15](#page-12-13)], which are represented active adsorption sites for the removal several of water pollutants such as dyes [[16\]](#page-12-14) and metal ions [\[17\]](#page-12-15). However, the application of natural CS as a biosorbent in wastewater treatment technologies still limited due to the high swelling index, solubility in various organic acids, low surface area, and considerable leachability [[18](#page-12-16)].

In general, various successful treatment methods are frequently applied to enhance the chemical and structural characteristics of CS such as crosslinking reaction, which is convenient and feasible pathway to reduce its solubility in acidic medium and to minimize the hydrophobicity

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and swelling index in aqueous solution [\[19](#page-13-0)]. However, the crosslinking reaction generally leads to decrease the adsorption capacity of CS due to blocking its reactive adsorption sites, particularly amino $(-NH₂)$ group when react with dialdehyde crosslinker agent [[20\]](#page-13-1). To overcome this drawback, fabricating CS nanocomposite materials is another promising pathway for enhancing the structural and surface area of CS biopolymer and reducing its internal difusion resistance [\[19](#page-13-0)]. Therefore, various promising materials with multifunctional groups such as $TiO₂$ nanoparticles, clays, and fly ash particles were incorporated into molecular structure of CS to improve its adsorptive and physiochemical properties [\[21–](#page-13-2)[23\]](#page-13-3).

In this respect, fy ash (FA) is a by-product generated from combusting of coal in the thermal power plants [\[24](#page-13-4)]. The FA contains mainly of metal oxides such as silica $(SiO₂)$, alumina $(Al₂O₃)$, and magnetite $(Fe₂O₃)$, in addition to unburned carbon [[25,](#page-13-5) [26](#page-13-6)]. FA has many preferable properties to be promising adsorbent such as chemical composition, surface area, porosity, particle size, and water holding capacity [\[23](#page-13-3)]. However, the main technical drawbacks of using bare FA as an adsorbent in wastewater treatment technology were due to the difficulty of filtration and separation processes of ultrafne particles from treated solution during and post treatment process. Recently, the FA and/or CS-FA composite were applied as adsorbents for removal of organic water pollutants from contaminated water [\[27](#page-13-7), [28](#page-13-8)].

Moreover, magnetic nanoparticles (such as $Fe₃O₄$ and $Fe₂O₃$) were introduced as the magnetic core within composite adsorbent in order to achieve the efective separation and easy collection of adsorbents from aqueous media by external magnetic field $[29, 30]$ $[29, 30]$ $[29, 30]$ $[29, 30]$. Fe₃O₄ nanoparticles were widely utilized in preparation of adsorbents due to its exceptional features such as surface functional groups, magnetic response ability, small particle size, biocompatibility, and biodegradability [[31](#page-13-11)]. Recently, magnetic $CS-Fe₃O₄$ composites were widely prepared and used as adsorbents in adsorption technique for removal of dyes [[32\]](#page-13-12), pharmaceuticals [\[33](#page-13-13)], and metal ions [\[34](#page-13-14)].

Therefore, the main objective of this research work was to produce multifunctional performances of recoverable and separable composite magnetic chitosan-fly ash/ $Fe₃O₄$ $(CS-FA/Fe₃O₄)$ as an effective biosorbent to remove of reactive orange 16 (RO16) dye from aqueous media. The key parameters afecting the RO16 dye adsorption such as adsorbent dose, solution pH, temperature, and time were optimized using Box–Behnken design (BBD) in response surface methodology (RSM). Furthermore, the non-linear forms of isotherm and kinetic models were studied. Finally, a suitable mechanism for RO16 dye adsorption by CS-FA/ $Fe₃O₄$ composite was proposed.

Materials and Methods

Materials

The fly ash (FA) was collected from thermal power station situated in Kapar area, Selangor, Malaysia. FA powder was washed with distilled water to remove any soluble substances. Then, FA powder was dried in an oven at 80 °C for 24 h before sieving to certain particles size \leq 250 µm. CS (deacetylation≥75%; medium molecular weight) was obtained from Sigma-Aldrich. Iron(III) chloride hexahydrate (FeCl₃·6H₂O, MW: 270.30 g/mol) was purchased from HmbG Chemicals. Iron(II) chloride tetrahydrate $(FeCl₂·4H₂O, MW:198.81 g/mol)$ was purchased from Bendosen Laboratory Chemicals. Reactive orange 16 dye $(C_{20}H_{17}N_3Na_2O_{11}S_3, MW: 617.54$ g/mol, λ_{max} = 493 nm) was purchased from ACROS, Organics. Acetic acid, Hydrochloric acid, and sodium hydroxide were supplied from R&M Chemicals. All experiments of this research were performed using ultrapure water.

Synthesis of Magnetic Chitosan-Fly Ash/Fe₃O₄ Composite (CS-FA/Fe₃O₄)

1 g of CS fakes and 1 g of FA particles were blended in acetic acid solution (5%, 50 mL). The solution was slowly stirred for 24 h at 25 °C to ensure dissolution of CS fakes and loading of FA particles in the CS molecular structure. After that, 10 mL containing 0.014 mol of $Fe³⁺$ ions and 0.013 mol of Fe^{2+} ions (these ions were prepared by dissolving 3.9 g of FeCl₃·6H₂O and 2.7 g of FeCl₂·4H₂O in distilled water) were added to the solution of CS-FA with gentle stirring for 1 h at 25 °C. The obtained solution was injected into of sodium hydroxide solution (2 M, 1000 mL) by syringe needle (10 mL) with gentle stirring for 6 h, where the magnetic CS-FA/Fe₃O₄ beads were instantaneously formed. The fresh beads of magnetic CS-FA/Fe₃O₄ were washed using distilled water to remove the residue of sodium hydroxide solution. Then, the CS-FA/Fe₃O₄ powder (particle size \leq 250 µm) was achieved by grinding process of $CS\text{-FA/Fe}_3\text{O}_4$ beads. The synthesis steps of CS-FA/Fe₃O₄ and image of CS-FA/Fe₃O₄ beads are presented in Fig. [1.](#page-2-0)

Characterization

The characterization of $CS\text{-FA/Fe}_3\text{O}_4$ composite was performed by various analytical methods and techniques. The chemical composition of FA was determined by X-ray Fluorescence (XRF) analysis. The surface area and pore volume of the CS-FA/Fe₃O₄ composite was determined by Micromeritics ASAP 2060 analyzer using

 $(CS-FA/Fe₃O₄)$

Fig. 1 The synthesis steps of CS-FA/Fe₃O₄ composite

nitrogen adsorption/desorption isotherms at 77 K. Scanning electron microscope-energy dispersive X-ray analyze (SEM–EDX, Zeiss Supra 40 VP, Germany) was utilized to determine the morphological characteristics of CS-FA/ $Fe₃O₄$ composite before and after adsorption of RO16 dye molecules. The X-Ray difraction (XRD, X'Pert PRO, PAnalytical) was used to determine the crystallinity of $CS-FA/Fe₃O₄$ composite. pH-potentiometric titration was performed to determine the amine content in $CS-FA/Fe₃O₄$ composite based on the method published by Vieira and Beppu [[35\]](#page-13-15). The point of zero charge (pH_{pzc}) for CS-FA/ $Fe₃O₄$ composite was calculated based on the reported method [[36\]](#page-13-16). The surface functional groups of CS-FA/ $Fe₃O₄$ composite before and after RO16 dye adsorption were determined using Fourier Transform Infrared (FTIR) spectroscopy (Perkin-Elmer, Spectrum RX I).

Design of Experiments

Four independent variables namely adsorbent dose (A), solution pH (B) , temperature (C) , and time (D) were optimized by using Box–Behnken design (BBD) in response surface methodology (RSM) for the RO16 dye adsorption onto CS -FA/Fe₃O₄ composite. Design-Expert software (version 11, Stat-Ease, Minneapolis, USA) was used to design of experiments and analysis of the experimental results. The levels and ranges of independent variables and their codes are shown in Table [1.](#page-2-1) A second-order polynomial model was utilized to estimate the RO16 dye removal as presented in the following Eq. ([1\)](#page-2-2).

$$
Y = \beta_0 + \sum \beta_i X_i + \sum \beta_{ii} X_i^2 + \sum \sum \beta_{ij} X_i X_j \tag{1}
$$

Table 1 Codes and actual variables and their levels in BBD

	Codes Variables	Level $1(-1)$ Level $2(0)$ Level $3(+1)$		
A	Adsorbent dose (g) 0.04		0.08	0.12
B	рH	4.0	7.0	10
C	Temperature $(^{\circ}C)$	30	40	50
Ð	Time (min)	20	55	90

where, *Y* is the response (dye removal), β_0 is the model constant, β_i is the linear coefficient of the input parameter, β_{ii} is the quadratic coefficient of the input parameter, and β_{ij} is the interaction coefficient between the input parameters, while X_i and X_j represent the independent variables. A total of 29 experiments (runs) are designed by BBD to optimize and evaluate the four independent variables including A: adsorbent dose (0.04–0.12 g), B: solution pH (4–10), C: temperature (30–50 °C), and D: time (20–90 min) on the RO16 dye removal. Noteworthy, the ranges and levels for BBD-RSM were pre-determined to be the best. The actual experimental design and values of RO16 dye removal are given in Table [2](#page-3-0). A certain amount of $CS-FA/Fe₃O₄$ composite was

Table 2 The 4-varibles BBD matrix and experimental data for RO16 removal efficiency

Run	A: Adsor- bent dose (g)	B: pH	C: Temp $({}^{\circ}C)$	D: Time (min)	RO16 removal $(\%)$
$\mathbf{1}$	0.04	$\overline{4}$	40	55	45.0
$\mathfrak{2}$	0.12	$\overline{4}$	40	55	62.6
3	0.04	10	40	55	15.2
$\overline{4}$	0.12	10	40	55	23.5
5	0.08	7	30	20	25.5
6	0.08	7	50	$20\,$	10.2
7	0.08	7	30	90	35.0
8	0.08	7	50	90	22.4
9	0.04	7	40	20	7.90
10	0.12	7	40	20	13.6
11	0.04	7	40	90	12.4
12	0.12	7	40	90	45.2
13	0.08	$\overline{4}$	30	55	73.1
14	0.08	10	30	55	16.2
15	0.08	$\overline{4}$	50	55	25.7
16	$0.08\,$	10	50	55	22.2
17	0.04	7	30	55	15.9
18	0.12	7	30	55	32.7
19	0.04	τ	50	55	14.7
20	0.12	7	50	55	33.3
21	0.08	$\overline{4}$	40	20	36.3
22	0.08	10	40	20	15.8
23	0.08	$\overline{\mathcal{L}}$	40	90	48.6
24	0.08	10	40	90	17.2
25	$0.08\,$	7	40	55	15.2
26	$0.08\,$	7	40	55	14.8
27	$0.08\,$	7	40	55	15.9
28	0.08	7	40	55	14.6
29	0.08	7	40	55	15.4

added to the Erlenmeyer fasks (125 mL) containing RO16 dye solution (50 mL). These fasks were agitated at fxed shaking speed of 100 strokes/min using water bath (WNB7- 45, Memmert, Germany). After that, the adsorbents were separated by an external magnetic feld and the solution was filtered by syringe filter $(0.45 \mu m)$. Finally, the concentrations of RO16 dye were calculated by UV–Vis spectroscopy (HACH DR 2800) at λ_{max} 493 nm. The RO16 dye removal (DR%) was calculated using the following Eq. [\(2](#page-3-1)).

$$
DR\% = \frac{(C_o - C_e)}{C_o} \times 100\tag{2}
$$

where C_o (mg/L) is the RO16 dye initial concentration and C_e (mg/L) is the concentration of the RO16 dye at equilibrium.

The adsorptive removal of RO16 dye by bare fly ash powder (FA), $CS/Fe₃O₄$, and CS-FA/Fe₃O₄ composite was pre-determined and compared. The RO16 dye removal was 28.9%, 39.9%, and 68.2% for the fy ash powder (FA), CS/ $Fe₃O₄$, and CS-FA/Fe₃O₄ composite adsorbents, respectively. This results show clearly the synergistic efect of incorporating FA powder into polymeric matrix of CS/ $Fe₃O₄$ on the adsorptive property of the composite CS-FA/ $Fe₃O₄$ for removal of RO16 dye.

Batch Adsorption Study

The RO16 dye adsorption onto CS-FA/Fe₃O₄ composite was studied in batch mode. According to Table [2](#page-3-0) containing values of RO16 dye removal efficiency, the highest RO16 dye removal (%) can be obtained from run 13 under the following conditions: adsorbent dose (A: 0.08 g/L), pH (B: 4), temperature (C: 30 °C), and time (D: 55 min). Thus, these optimum conditions of adsorption key parameters were kept constant in the experiments of batch adsorption study. Adsorption experiments of RO16 dye were carried out using the same procedure mentioned above at diferent RO16 dye initial concentrations (20–150 mg/L) and contact time (0–660 min). The adsorption capacity of CS-FA/Fe₃O₄ composite for RO16 dye at equilibrium, q_e (mg/g) was determined according to the following Eq. ([3](#page-3-2)).

$$
q_e = \frac{(C_o - C_e)V}{W}
$$
 (3)

where, $V(L)$ is volume of RO16 dye solution and $W(g)$ is the weight of CS -FA/Fe₃O₄ composite. Adsorption experiments were conducted in duplicate under identical conditions and the results are reported as an average value.

Results and Discussion

Characterization

Physicochemical Properties

The elemental composition of FA was determined by XRF analysis and presented in Table [3](#page-4-0). The result of analysis indicates the presence of Si, P, K, Ca, Al, Fe, Ti, Ag, Sr, and Zr mainly in structure of FA. Thus, it can be concluded that FA consist of metal oxides such SiO_2 , AL_2O_3 , Fe_2O_3 , CaO, TiO₂, P_2O_3 and K₂O. The textural properties of FA, magnetic CS, and CS-FA/Fe₃O₄ composite are presented in Table [4.](#page-4-1) The BET surface area analysis (Table [4\)](#page-4-1) shows that the FA has surface area $4.74 \text{ (m}^2\text{/g)}$, while BET surface area of magnetic CS and CS-FA/Fe₃O₄ composite were 2.22 m²/g and 8.57 m^2/g , respectively. The results reflect a relatively high surface area of CS -FA/Fe₃O₄ composite compared to $CS/Fe₃O₄$ which can be attributed to the interfacial interaction between FA and the molecular structure of CS [[37\]](#page-13-17). Furthermore, CS-FA/Fe₃O₄ composite is a mesoporous material in accordance with the classifcation of IUPAC (USA) [\[38](#page-13-18)]. The potentiometric titrations showed the CS/Fe₃O₄ has 45.6% amino group (–NH₂) content, while CS-FA/Fe₃O₄ composite was 39.5% . The decreasing in amine $(-NH₂)$ content of the matrix of CS after incorporation of FA particles can be attributed to the physical loading of FA into molecular structure of $CS/Fe₃O₄$, and also to the chemical interactions between silicon matrix and/or negative charge of FA with basic sites of amino group in CS molecular struc-ture [\[39\]](#page-13-19). The results indicate that CS-FA/Fe₃O₄ composite has a relatively high content of amino $(-NH₂)$ group. The protonation of amino $(-NH_2)$ group into $(-NH_3^+)$ in acidic environment can play an important role in the adsorption of RO16 dye due to electrostatic attraction between cationic amino groups $(-NH_3^+)$ of CS-FA/Fe₃O₄ composite and RO16 dye anions.

XRD Analysis

The XRD pattern of the FA was given in Fig. [2.](#page-4-2) The FA profile shows sharp peaks at $2\theta=16^\circ$, 22° , 26° , 33° , 39° , 41° , 50°, 60°, 61°, and 68°. These peaks refect that the FA consisted primarily of crystalline phases like alumina $(A₁, O₃)$, quartz (SiO_2) , and hematite (Fe_2O_3) [[40\]](#page-13-20). The XRD pattern of CS/Fe₃O₄ shows sharp characteristic peaks at $2\theta = 30^{\circ}$, 35°, 43°, 53°, 57°, and 62°, which are consistent with the

Fig. 2 XRD patterns of **a** FA, **b** CS/Fe₃O₄, and **c** CS-FA/Fe₃O₄ composite

peaks of the $Fe₃O₄$ standard cards (JCPDS file No. 19-629) for the (220), (311), (400), (422), (511), and (440) crystal surfaces, respectively [\[41\]](#page-13-21). The XRD pattern of CS-FA/ $Fe₃O₄$ composite shows similar profile to the CS/Fe₃O₄, except a sharp peak related to FA was appeared in pattern of CS-FA/Fe₃O₄ composite with obvious shift from $2\theta = 26^\circ$ to $2\theta = 27^\circ$, indicating a successful interaction between FA and CS/Fe₃O₄.

FTIR Analysis

FTIR spectra of FA, CS-FA/Fe₃O₄ composite, and CS-FA/ Fe3O4 composite after adsorption of RO16 dye are presented in Fig. [3](#page-5-0). The FTIR spectrum of FA displayed characteristic peaks at 1070 cm−1 and 790 cm−1 for bond stretching of asymmetric Si–O–Si and symmetric Si–O–Si, respectively [[23\]](#page-13-3). The peaks in region between 3600 and 3770 cm^{-1} indicates the stretching vibrations of OH [\[42\]](#page-13-22). The FTIR

Fig. 3 FTIR spectra of **a** FA, **b** CS-FA/Fe₃O₄ composite, and **c** CS -FA/Fe₃O₄ composite after adsorption of RO16 dye

spectrum of CS -FA/Fe₃O₄ composite showed major bands for CS polymer which can be assigned as follows: 3600 cm−1 (stretching vibrations of –NH and –OH bonds), 2870 cm−1 (stretching vibrations of C–H in –CH and –CH₂), 1650 cm⁻¹ (bending vibration of N–H), 1380 cm−1 (stretching vibration of C–N), and 1090 cm^{-1} (skeletal vibration of C–O) [\[37](#page-13-17)]. The peak at 553 cm⁻¹ corresponds to Fe–O bond [[43](#page-13-23)]. The FTIR spectrum of CS -FA/Fe₃O₄ composite after adsorption of RO16 dye did not show much diference in bands position compare to spectrum of $CS-FA/Fe₃O₄$ composite before RO16 dye adsorption, except slight shifting of some bands due to involvement the functional groups of CS-FA/ $Fe₃O₄$ composite in the RO16 dye adsorption process. Furthermore, the band at 1500 cm^{-1} can be attributed to the aromatic rings (C=C) of RO16 dye adsorbed on the surface of CS-FA/Fe₃O₄ composite.

SEM–EDX Analysis

SEM–EDX analysis was carried out in order to investigate the surface morphological structure of FA, $CS/Fe₃O₄$, CS -FA/Fe₃O₄ composite, and CS-FA/Fe₃O₄ composite after adsorption of RO16 dye along with chemical composition. Figure [4](#page-6-0)a–d shows the SEM images and EDX analysis of FA, CS/Fe₃O₄, CS-FA/Fe₃O₄ composite and CS-FA/Fe₃O₄ composite after adsorption of RO16 dye, respectively. Figure [4](#page-6-0)a shows that the fy ash particles in diferent particle sizes were clearly visible in spherical shape (as highlighted in red cycles) with regular and smooth surface. The EDX analysis shows that the FA contains the elements C, O, Al and Si. In fact, the presence of C element within the elements of the analysis of EDX indicates to presence of unburned carbon, which plays an important role in adsorp-tion process [[44](#page-13-24)]. The surface morphology of $CS/Fe₃O₄$ (Fig. [4b](#page-6-0)) shows regular, compact, and homogenous surface, indicating equal distribution of magnetic $Fe₃O₄$ particles into molecular structure of CS. The EDX analysis shows that the $CS/Fe₃O₄$ contains the elements of CS biopolymer such as C, O, and N, in addition to presence element Fe corresponds to the magnetic $Fe₃O₄$. The surface morphology of CS-FA/Fe₃O₄ composite as shown in Fig. [4c](#page-6-0) appeared as irregular and heterogeneous surface with many visible cavities and pores. The appearance of spherical particles in the image indicates successful incorporation FA particles into molecular structure of CS. The EDX analysis shows a slight decrease in the elemental content of C which can be attributed to the loading of FA into molecular structure of $CS/Fe₃O₄$. The surface of CS-FA/Fe₃O₄ after the adsorption of RO16 dye (Fig. [4d](#page-6-0)) was turned to be less porous with evanescence of crevices on the CS-FA/Fe₃O₄ surface, indicating the RO16 dye molecules adsorbed on the CS-FA/ $Fe₃O₄$ surface. The EDX analysis shows the presence of S

Fig. 4 SEM images and EDX spectra of a FA, b CS/Fe₃O₄, c CS-FA/Fe₃O₄ composite, and d CS-FA/Fe₃O₄ composite after adsorption of RO16 dye

element belongs to RO16 dye and reconfrms the RO16 dye adsorption by CS -FA/Fe₃O₄ surface.

BBD Model Analysis

The individual and interactive effects of the independent factors including adsorbent dose (A), solution pH (B), temperature (C) and time (D) on the RO16 dye removal were investigated using BBD-RSM. Analysis of variance (ANOVA) was employed to analyze the experimental results of RO16 dye removal statistically as shown in Table [5.](#page-7-0) Based on Table [5](#page-7-0) (ANOVA analysis), the F-value of model and the corresponding p-value are 17.7 and < 0.0001 , respectively. These values indicate that the model is statistically signif-cant [\[45\]](#page-13-25). The coefficient of determination (R^2) value was close to the unity, indicating to the high correlation between the values of actual and the predicted. Generally, the terms of model with p-value less than 0.05 (Prob $>$ F $<$ 0.0500) are signifcant on the RO16 dye removal under chosen conditions. According to Table [5](#page-7-0), the BBD model terms of A, B, C, E, A^2 , B^2 , C^2 , AD and BC are significant on the RO16 dye removal. However, the terms of BBD model with p-value larger than 0.05 were excluded from second-order polynomial model in order to achieve ftting of the BBD model. Thus, the equation of second-order polynomial model between tested factors and the RO16 dye removal (response) was obtained and described in the following Eq. ([4\)](#page-7-1):

RO16 removal (
$$
%
$$
) = +15.18 + 8.32A – 15.10B
-5.83C + 5.96D + 6.78AD
+ 13.35BC + 4.74A² + 14.66B²
+ 5.35C² (4)

Validation of model can be also achieved by graphical methods through investigation in the nature of residuals distribution of the model, and relationship between values of the predicted and actual RO16 dye removal. Figure [5a](#page-8-0) shows normal probability plot of residuals for the model. It was observed from Fig. [5a](#page-8-0), the perfect normal distributions of the residuals, where points seem conspicuously close to a straight line. This observation indicates to the accuracy of the assumptions and independence of the residuals [\[46](#page-13-26)]. The relationship between the values of predicted and actual RO16 dye removal (%) is shown in Fig. [5b](#page-8-0) which indicates the values of predicted and actual are close to each other, and confrming the statistical validation of the model.

Interactive Efects of Two Variables on RO16 Dye Removal

The interaction effect between any two independent variables on the RO16 dye removal was evaluated. The interaction effect between solution $pH(B)$ and temperature (C) on the RO16 dye removal was significant (p-value = 0.0002), while the other factors (adsorbent dose 0.08 g and time 55 min) remained constant. The plots of three-dimensional (3D) response surfaces and two dimensional (2D) contour for the impacts and interaction of solution pH (B) and temperature (C) on RO16 dye removal $(\%)$ were shown in Fig. [6a](#page-10-0), b, respectively. According to Fig. [6](#page-10-0)a, b can be noticed that the lowering solution pH from 10 to 4 is responsible for increasing the RO16 dye removal (%) from 7.90 to 73.1%. The pHpzc value of CS-FA/Fe₃O₄ composite was 7 as depicted in Fig. [6c](#page-10-0). This result elucidates that the CS-FA/ $Fe₃O₄$ composite has a cationic character and reinforced the availability of the amino $(-NH_3^+)$ cationic group on the $CS-FA/Fe₃O₄$ surface, and in a good agreement with the potentiometric titrations test. The surface of $CS-FA/Fe₃O₄$ composite can be converted to positive charge at pH value below the pHpzc, thus promoting the adsorption of anions RO16 dye species. As a result, a strong electrostatic interaction can be occurred between protonated amino $(-NH₃)$ functional group of CS -FA/Fe₃O₄ composite and sulfonate $(-SO_3^-)$ groups of the RO16 dye, thus increasing the RO16 dye removal as shown in Eq. [\(5](#page-7-2)).

$$
R - NH_3^+ + RO16 - SO_3^- \leftrightarrow R - NH_3^+ - SO_3^- - RO16 \quad (5)
$$

Furthermore, it was observed from Fig. [6](#page-10-0)a, b the highest RO16 dye removal was achieved at temperature 30 °C,

Fig. 5 a Normal probability plot of residuals for BBD model, **b** plot of the relationship between the predicted and actual values of RO16 dye removal (%)

indicating the RO16 dye adsorption process onto the CS-FA/ $Fe₃O₄$ surface was an exothermic in nature [\[47](#page-13-27)].

Another significant interaction (p -value = 0.022) on the RO16 dye removal (%) was between adsorbent dose (A) and time (D), while the other parameters (solution pH 7 and temperature 40 °C) remained constant. The plots of threedimensional (3D) response surfaces and two dimensional (2D) contour for the impacts and interaction of adsorbent dose (A) and time (D) on RO16 dye removal $(\%)$ were shown in Fig. [6](#page-10-0)d, e, respectively. As depicted in Fig. [6d](#page-10-0), e, the dye removal $(\%)$ was gradually increased by increasing adsorbent dose which can be attributed to the increase in the available surface area of CS-FA/Fe3O4 in dye solution, and also higher CS-FA/Fe3O4 dose indicates a greater number of active adsorption sites available. Moreover, the RO 16 dye removal was increased by increasing the contact time from 20 to 90 min, with longer contact time the RO16 dye molecules will get sufficient time to move deeper toward inner active adsorption sites on the surface of CS-FA/Fe3O4.

Adsorption Study

The effect of initial RO16 dye concentration and contact time on adsorption equilibrium was investigated. The adsorption capacity, $q_t(mg/g)$ against time at several initial RO16 concentrations of 20, 40, 60, 80, 100 and 150 mg/L was investigated as depicted in Fig. [7a](#page-10-1), while the other optimum factors

like adsorbent dose $=0.08$ g, solution pH 4, and tempera-ture = 30 °C were kept constant. It is observed from Fig. [7a](#page-10-1) that the quantity of RO16 dye molecules uptake onto surface of CS-FA/Fe₃O₄ composite raised from 12.4 to 45.7 mg/g by increasing the initial RO16 dye concentrations from 20 to 150 mg/L. This can be attributed to the higher concentration gradient which provides a driving force to move the RO16 molecules towards active adsorption sites [[48](#page-13-28)].

Adsorption Kinetics

In order to understand the controlling mechanism of the adsorption process of RO16 dye molecules on the CS-FA/ $Fe₃O₄$ composite, the non-linear pseudo-first-order (PFO) and non-linear pseudo-second-order (PSO) kinetic models were utilized to analyze the experimental data of the RO16 dye adsorption on CS -FA/Fe₃O₄ composite at different initial RO16 dye concentrations [\[49](#page-13-29)]. The non-linear equations of the kinetic models PFO [\[50](#page-13-30)] and PSO [\[51](#page-13-31)] are expressed in Eqs. (6) (6) (6) and (7) (7) as follows:

$$
q_t = q_e (1 - \exp^{-k_1 t})
$$
\n⁽⁶⁾

$$
q_t = \frac{q_e^2 k_2 t}{1 + q_e k_2 t} \tag{7}
$$

Fig. 7 a Effect of the contact time on RO16 adsorption at different initial concentrations, and **b** adsorption isotherms of RO16 dye by CS-FA/Fe₃O₄ composite (adsorbent dose = 0.16 g, pH of solution = 4, temperature=30 \degree C, agitation speed=100 strokes and volume of solution = 100 mL)

where, q_t (mg/g) is the amount of RO16 dye adsorbed at time (t), and q_e (mg/g) is the amount of RO16 dye adsorbed at equilibrium. k_1 (1/min) is the rate constant of PFO, and $k₂$ (g/mg min) is the rate constant of PSO. The parameters of kinetic models and R^2 values are recorded in Table [6.](#page-10-2) According to experimental data (Table [6\)](#page-10-2) can be concluded that the adsorption of RO16 dye molecules by the CS-FA/ $Fe₃O₄$ composite follows PSO model due to the higher correlation coefficient (R^2) values, in addition to the calculated q_e ($q_{e,cal}$) values fitted well with the experimental q_e ($q_{e,exp}$) values. This result indicates that the adsorption of RO16 dye by CS-FA/Fe₃O₄ composite was the chemisorption process involving the electrostatic interaction between the positively charged available on the surface of CS-FA/Fe₃O₄ composite and the RO16 dye anions [\[52](#page-13-32)].

Adsorption Isotherms

Adsorption isotherm is essential to understand the interaction between the RO16 dye molecules and the CS-FA/ $Fe₃O₄$ composite [\[53](#page-13-33), [54\]](#page-13-34). In order to evaluate the adsorption capacity of $CS\text{-FA/Fe}_3\text{O}_4$ composite for RO16 dye, non-linear equilibrium models of Langmuir, Freundlich, and Temkin were utilized to ft the experimental data. The nonlinear equations of the equilibrium models Langmuir [[55](#page-13-35)], Freundlich [[56\]](#page-13-36), and Temkin [[57\]](#page-14-0) are presented in Eqs. [\(8](#page-10-3)), (9) (9) , and (10) (10) , respectively.

$$
q_e = \frac{q_{\text{max}} K_a C_e}{1 + K_a C_e} \tag{8}
$$

$$
q_e = K_f C_e^{1/n} \tag{9}
$$

$$
q_e = \frac{RT}{b_T} \ln(K_T C_e) \tag{10}
$$

where q_e (mg/g) is the amount of RO16 dye adsorbed at equilibrium, C_e (mg/L) is the concentration of RO16 dye at equilibrium, q_{max} (mg/g) is the maximum adsorption capacity, and K_a (L/mg) is Langmuir constant. K_f (mg/g) (L/mg)^{1/n} is the Freundlich constant, *n* is the dimensionless constant

Table 6 PFO and PSO kinetic parameters for RO16 dye adsorption on CS -FA/Fe₃O₄ composite

Table 7 Parameters of the Langmuir, Freundlich, and Temkin isotherm models for RO16 dye adsorption on $CS-FA/Fe₃O₄$ composite at 30 °C

Adsorption isotherm	Parameter	Value 66.9	
Langmuir	q_m (mg/g)		
	K_a (L/mg)	0.02	
	R^2	0.93	
Freundlich	K_f (mg/g) (L/mg) ^{1/n}	4.76	
	n	1.94	
	R^2	0.96	
Temkin	$K_T(L/mg)$	0.96	
	b_T (J/mol)	208	
	R^2	0.88	

indicates to the adsorption intensity. K_T (L/mg) is Temkin constant, $T(K)$ is temperature, $R(8.314$ J/molK) is the universal gas constant, and b_T (J/mol) is heat of adsorption. The non-linear curves of the equilibrium models are shown in Fig. [7](#page-10-1)b. The parameters of equilibrium models are recorded in Table [7](#page-11-0). According to the R^2 values (Table 7) obtained from the isotherm models, it observed that the Freundlich isotherm has highest correlation $(R^2 0.96)$, which indicated that the RO16 dye adsorption occurred on heterogeneous surface [\[58\]](#page-14-1). The maximum adsorption capacity (q_{max}) of CS-FA/Fe₃O₄ composite for RO16 dye was 66.9 mg/g at 30 °C. It can be deduced that the CS-FA/Fe₃O₄ composite was a potential and efective biosorbent for removal of RO16 dye from aqueous media.

Adsorption Mechanism

Adsorption mechanism of RO16 dye on CS-FA/Fe₃O₄ composite surface by diferent types of interactions is shown in Fig. [8](#page-11-1). An electrostatic attraction (Fig. [8](#page-11-1)a) is considered from the most interaction that can be occurred between RO16 dye and surface of adsorbent. This mechanism involves the electrostatic interaction between RO16 dye anions with positively charged available on the CS-FA/Fe₃O₄

Fig. 8 Illustration of the possible adsorption mechanism between CS-FA/Fe₃O₄ composite and RO16 dye: **a** electrostatic attraction, **b** dipole– dipole hydrogen bonding interactions, **c** Yoshida H-bonding, and **d** *n*–π stacking interactions

composite surface. Adsorption mechanism also includes H-bonding interactions such as dipole–dipole hydrogen bonding (Fig. [8b](#page-11-1)), and Yoshida H-bonding (Fig. [8c](#page-11-1)). Dipole–dipole hydrogen bonding happens between H atom available on the surface of CS-FA/Fe₃O₄ composite, and N atoms in the RO16 dye structure, while Yoshida H-bonding happens between –OH available on the surface of CS-FA/ $Fe₃O₄$ composite, and the aromatic rings of RO16 dye.[\[59](#page-14-2)]. Finally, $n-\pi$ interaction comes from delocalization of the lone pair electron of O and N atoms into the π orbital of the dye aromatic rings as shown in Fig. [8](#page-11-1)d [[60\]](#page-14-3). According to the above, it can be concluded that these interactions are efective in enhancing adsorption process of RO16 dye on the surface of CS-FA/Fe₃O₄ composite.

Conclusion

Magnetic fly ash/Fe₃O₄ particles (CS-FA/Fe₃O₄) composite was successfully synthesized and applied as an efective bioadsorbent for the removal of RO16. The incorporation of FA particles in magnetic CS leads to enhance surface area of $CS\text{-FA/Fe}_3\text{O}_4$ composite. The CS-FA/ $Fe₃O₄$ composite was easily separated and collected from the aqueous solution after adsorption process by external magnetic feld. Analysis of variance (ANOVA) showed the F-value of model and the corresponding p-value are 17.7 and < 0.0001 , indicating the model is statistically signifcant. The experimental results indicate that the highest RO16 dye removal of 73.1% was observed by significant interaction between BC ($pH \times$ temperature, p -value = 0.0002) and AD (adsorbent dose x time, $p-value = 0.022$. The optimum conditions of adsorption process parameters were $pH \sim 4$, adsorbent dose (0.08 g), temperature (30 \degree C) and time (55 min). The kinetics and isotherms models results indicated that the adsorption was afected by chemisorption and heterogeneous mode of adsorption. The q_{max} of CS-FA/Fe₃O₄ composite for RO16 dye was 66.9 mg/g at 30 °C.

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