**ORIGINAL PAPER** 



# Synthesis of Magnetic Chitosan-Fly Ash/Fe<sub>3</sub>O<sub>4</sub> Composite for Adsorption of Reactive Orange 16 Dye: Optimization by Box–Behnken Design

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### Abstract

A hybrid composite biopolymer of magnetic chitosan-fly ash/Fe<sub>3</sub>O<sub>4</sub> (CS-FA/Fe<sub>3</sub>O<sub>4</sub>) was prepared to be an effective composite biosorbent for the removal of reactive orange 16 (RO16) dye from aqueous media. Various analytical techniques such as XRF, BET, XRD, FTIR, and SEM–EDX were utilized to characterize of CS-FA/Fe<sub>3</sub>O<sub>4</sub> composite. The effects of adsorption process parameters namely adsorbent dose (A: 0.04–0.12 g), solution pH (B: 4–10), temperature (C: 30–50 °C), and time (E: 20–90 min) were optimized by using Box–Behnken design (BBD) in response surface methodology (RSM). The experimental results indicate that the highest RO16 removal was 73.1% by significant interaction between BC (p-value=0.0002) and AD (p-value=0.022). The optimum RO16 dye removal conditions were recorded at solution pH~4, adsorbent dose (0.08 g), temperature (30 °C), and time (55 min). The adsorption process was well described by pseudo-second order (PSO) kinetic and Freundlich isotherm model. The adsorption capacity of CS-FA/Fe<sub>3</sub>O<sub>4</sub> composite for RO16 dye was 66.9 mg/g at 30 °C. The mechanism of the RO16 dye adsorption included many interactions such as electrostatic, n– $\pi$  interaction, H-bonding, and Yoshida H-bonding. Furthermore, the CS-FA/Fe<sub>3</sub>O<sub>4</sub> composite exhibited a high ability to separate from the aqueous solution after adsorption process by external magnetic field.

Keywords Magnetic chitosan · Fly ash · Reactive orange 16 dye · Adsorption · Response surface methodology

# Introduction

Organic dyes are widely utilized in various industries such as printing, textile, leather, paint, and pharmaceuticals [1]. The discharge of these dyes without treatment into water is one of the environmental problems due to its risks on aquatic life and human's health [2]. Therefore, it is necessary to remove these dyes before releasing it into the environment. Several methods have been applied to remove these dyes prior to discharge into water such as photocatalytic [3], adsorption [4, 5], oxidation [6], and flocculation [7]. Adsorption is considered one of the most efficient methods used to remove dyes because of the simplicity of design, non-generation of toxic materials, low cost, and high efficiency [8-10].

Chitosan (CS) is a cationic polysaccharide composed of D-glucosamine units [11]. CS can be obtained from the deacetylation of chitin, which is the second most abundant biopolymer in nature after cellulose [12]. CS has various interesting properties such as biodegradability, non-toxicity, biocompatibility, and antimicrobial activity [13, 14]. The uniqueness of CS molecular structure comes from the availability of amino ( $-NH_2$ ) and hydroxyl (-OH) groups [15], which are represented active adsorption sites for the removal several of water pollutants such as dyes [16] and metal ions [17]. However, the application of natural CS as a biosorbent in wastewater treatment technologies still limited due to the high swelling index, solubility in various organic acids, low surface area, and considerable leachability [18].

In general, various successful treatment methods are frequently applied to enhance the chemical and structural characteristics of CS such as crosslinking reaction, which is convenient and feasible pathway to reduce its solubility in acidic medium and to minimize the hydrophobicity

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and swelling index in aqueous solution [19]. However, the crosslinking reaction generally leads to decrease the adsorption capacity of CS due to blocking its reactive adsorption sites, particularly amino  $(-NH_2)$  group when react with dial-dehyde crosslinker agent [20]. To overcome this drawback, fabricating CS nanocomposite materials is another promising pathway for enhancing the structural and surface area of CS biopolymer and reducing its internal diffusion resistance [19]. Therefore, various promising materials with multifunctional groups such as TiO<sub>2</sub> nanoparticles, clays, and fly ash particles were incorporated into molecular structure of CS to improve its adsorptive and physiochemical properties [21–23].

In this respect, fly ash (FA) is a by-product generated from combusting of coal in the thermal power plants [24]. The FA contains mainly of metal oxides such as silica (SiO<sub>2</sub>), alumina (Al<sub>2</sub>O<sub>3</sub>), and magnetite (Fe<sub>2</sub>O<sub>3</sub>), in addition to unburned carbon [25, 26]. FA has many preferable properties to be promising adsorbent such as chemical composition, surface area, porosity, particle size, and water holding capacity [23]. However, the main technical drawbacks of using bare FA as an adsorbent in wastewater treatment technology were due to the difficulty of filtration and separation processes of ultrafine particles from treated solution during and post treatment process. Recently, the FA and/or CS-FA composite were applied as adsorbents for removal of organic water pollutants from contaminated water [27, 28].

Moreover, magnetic nanoparticles (such as  $Fe_3O_4$  and  $Fe_2O_3$ ) were introduced as the magnetic core within composite adsorbent in order to achieve the effective separation and easy collection of adsorbents from aqueous media by external magnetic field [29, 30].  $Fe_3O_4$  nanoparticles were widely utilized in preparation of adsorbents due to its exceptional features such as surface functional groups, magnetic response ability, small particle size, biocompatibility, and biodegradability [31]. Recently, magnetic CS– $Fe_3O_4$  composites were widely prepared and used as adsorbents in adsorption technique for removal of dyes [32], pharmaceuticals [33], and metal ions [34].

Therefore, the main objective of this research work was to produce multifunctional performances of recoverable and separable composite magnetic chitosan-fly ash/Fe<sub>3</sub>O<sub>4</sub> (CS-FA/Fe<sub>3</sub>O<sub>4</sub>) as an effective biosorbent to remove of reactive orange 16 (RO16) dye from aqueous media. The key parameters affecting the RO16 dye adsorption such as adsorbent dose, solution pH, temperature, and time were optimized using Box–Behnken design (BBD) in response surface methodology (RSM). Furthermore, the non-linear forms of isotherm and kinetic models were studied. Finally, a suitable mechanism for RO16 dye adsorption by CS-FA/ Fe<sub>3</sub>O<sub>4</sub> composite was proposed.

# **Materials and Methods**

### Materials

The fly ash (FA) was collected from thermal power station situated in Kapar area, Selangor, Malaysia. FA powder was washed with distilled water to remove any soluble substances. Then, FA powder was dried in an oven at 80 °C for 24 h before sieving to certain particles size  $\leq 250 \ \mu m$ . CS (deacetylation > 75%; medium molecular weight) was obtained from Sigma-Aldrich. Iron(III) chloride hexahydrate (FeCl<sub>3</sub>·6H<sub>2</sub>O, MW: 270.30 g/mol) was purchased from HmbG Chemicals. Iron(II) chloride tetrahydrate (FeCl<sub>2</sub>·4H<sub>2</sub>O, MW:198.81 g/mol) was purchased from Bendosen Laboratory Chemicals. Reactive orange 16 dye  $(C_{20}H_{17}N_3Na_2O_{11}S_3, MW: 617.54 \text{ g/mol}, \lambda_{max} = 493 \text{ nm})$  was purchased from ACROS, Organics. Acetic acid, Hydrochloric acid, and sodium hydroxide were supplied from R&M Chemicals. All experiments of this research were performed using ultrapure water.

# Synthesis of Magnetic Chitosan-Fly Ash/Fe<sub>3</sub>O<sub>4</sub> Composite (CS-FA/Fe<sub>3</sub>O<sub>4</sub>)

1 g of CS flakes and 1 g of FA particles were blended in acetic acid solution (5%, 50 mL). The solution was slowly stirred for 24 h at 25 °C to ensure dissolution of CS flakes and loading of FA particles in the CS molecular structure. After that, 10 mL containing 0.014 mol of Fe<sup>3+</sup> ions and 0.013 mol of Fe<sup>2+</sup> ions (these ions were prepared by dissolving 3.9 g of FeCl<sub>3</sub>·6H<sub>2</sub>O and 2.7 g of FeCl<sub>2</sub>·4H<sub>2</sub>O in distilled water) were added to the solution of CS-FA with gentle stirring for 1 h at 25 °C. The obtained solution was injected into of sodium hydroxide solution (2 M, 1000 mL) by syringe needle (10 mL) with gentle stirring for 6 h, where the magnetic CS-FA/Fe<sub>3</sub>O<sub>4</sub> beads were instantaneously formed. The fresh beads of magnetic CS-FA/Fe<sub>3</sub>O<sub>4</sub> were washed using distilled water to remove the residue of sodium hydroxide solution. Then, the CS-FA/Fe<sub>3</sub>O<sub>4</sub> powder (particle size  $\leq 250 \ \mu$ m) was achieved by grinding process of CS-FA/Fe<sub>3</sub>O<sub>4</sub> beads. The synthesis steps of CS-FA/Fe $_3O_4$  and image of CS-FA/Fe $_3O_4$  beads are presented in Fig. 1.

### Characterization

The characterization of CS-FA/Fe<sub>3</sub>O<sub>4</sub> composite was performed by various analytical methods and techniques. The chemical composition of FA was determined by X-ray Fluorescence (XRF) analysis. The surface area and pore volume of the CS-FA/Fe<sub>3</sub>O<sub>4</sub> composite was determined by Micromeritics ASAP 2060 analyzer using



Fig. 1 The synthesis steps of CS-FA/Fe<sub>3</sub>O<sub>4</sub> composite

nitrogen adsorption/desorption isotherms at 77 K. Scanning electron microscope-energy dispersive X-ray analyze (SEM-EDX, Zeiss Supra 40 VP, Germany) was utilized to determine the morphological characteristics of CS-FA/ Fe<sub>3</sub>O<sub>4</sub> composite before and after adsorption of RO16 dye molecules. The X-Ray diffraction (XRD, X'Pert PRO, PAnalytical) was used to determine the crystallinity of CS-FA/Fe<sub>3</sub>O<sub>4</sub> composite. pH-potentiometric titration was performed to determine the amine content in CS-FA/Fe<sub>3</sub>O<sub>4</sub> composite based on the method published by Vieira and Beppu [35]. The point of zero charge (pH<sub>nzc</sub>) for CS-FA/ Fe<sub>3</sub>O<sub>4</sub> composite was calculated based on the reported method [36]. The surface functional groups of CS-FA/ Fe<sub>3</sub>O<sub>4</sub> composite before and after RO16 dye adsorption were determined using Fourier Transform Infrared (FTIR) spectroscopy (Perkin-Elmer, Spectrum RX I).

# **Design of Experiments**

Four independent variables namely adsorbent dose (A), solution pH (B), temperature (C), and time (D) were

optimized by using Box–Behnken design (BBD) in response surface methodology (RSM) for the RO16 dye adsorption onto CS-FA/Fe<sub>3</sub>O<sub>4</sub> composite. Design-Expert software (version 11, Stat-Ease, Minneapolis, USA) was used to design of experiments and analysis of the experimental results. The levels and ranges of independent variables and their codes are shown in Table 1. A second-order polynomial model was utilized to estimate the RO16 dye removal as presented in the following Eq. (1).

$$Y = \beta_0 + \sum \beta_i X_i + \sum \beta_{ii} X_i^2 + \sum \sum \beta_{ij} X_i X_j$$
(1)

 Table 1
 Codes and actual variables and their levels in BBD

Variables	Level 1 (-1)	Level 2 (0)	Level 3 (+1)
Adsorbent dose (g)	0.04	0.08	0.12
pH	4.0	7.0	10
Temperature (°C)	30	40	50
Time (min)	20	55	90
	Variables Adsorbent dose (g) pH Temperature (°C) Time (min)	VariablesLevel 1 (- 1)Adsorbent dose (g)0.04pH4.0Temperature (°C)30Time (min)20	Variables         Level 1 (-1)         Level 2 (0)           Adsorbent dose (g)         0.04         0.08           pH         4.0         7.0           Temperature (°C)         30         40           Time (min)         20         55

where, *Y* is the response (dye removal),  $\beta_0$  is the model constant,  $\beta_i$  is the linear coefficient of the input parameter,  $\beta_{ii}$  is the quadratic coefficient of the input parameter, and  $\beta_{ij}$  is the interaction coefficient between the input parameters, while  $X_i$  and  $X_j$  represent the independent variables. A total of 29 experiments (runs) are designed by BBD to optimize and evaluate the four independent variables including A: adsorbent dose (0.04–0.12 g), B: solution pH (4–10), C: temperature (30–50 °C), and D: time (20–90 min) on the RO16 dye removal. Noteworthy, the ranges and levels for BBD-RSM were pre-determined to be the best. The actual experimental design and values of RO16 dye removal are given in Table 2. A certain amount of CS-FA/Fe<sub>3</sub>O<sub>4</sub> composite was

 Table 2
 The 4-varibles BBD matrix and experimental data for RO16 removal efficiency

Run	A: Adsor- bent dose (g)	B: pH	C: Temp (°C)	D: Time (min)	RO16 removal (%)
1	0.04	4	40	55	45.0
2	0.12	4	40	55	62.6
3	0.04	10	40	55	15.2
4	0.12	10	40	55	23.5
5	0.08	7	30	20	25.5
6	0.08	7	50	20	10.2
7	0.08	7	30	90	35.0
8	0.08	7	50	90	22.4
9	0.04	7	40	20	7.90
10	0.12	7	40	20	13.6
11	0.04	7	40	90	12.4
12	0.12	7	40	90	45.2
13	0.08	4	30	55	73.1
14	0.08	10	30	55	16.2
15	0.08	4	50	55	25.7
16	0.08	10	50	55	22.2
17	0.04	7	30	55	15.9
18	0.12	7	30	55	32.7
19	0.04	7	50	55	14.7
20	0.12	7	50	55	33.3
21	0.08	4	40	20	36.3
22	0.08	10	40	20	15.8
23	0.08	4	40	90	48.6
24	0.08	10	40	90	17.2
25	0.08	7	40	55	15.2
26	0.08	7	40	55	14.8
27	0.08	7	40	55	15.9
28	0.08	7	40	55	14.6
29	0.08	7	40	55	15.4

added to the Erlenmeyer flasks (125 mL) containing RO16 dye solution (50 mL). These flasks were agitated at fixed shaking speed of 100 strokes/min using water bath (WNB7-45, Memmert, Germany). After that, the adsorbents were separated by an external magnetic field and the solution was filtered by syringe filter (0.45  $\mu$ m). Finally, the concentrations of RO16 dye were calculated by UV–Vis spectroscopy (HACH DR 2800) at  $\lambda_{max}$  493 nm. The RO16 dye removal (DR%) was calculated using the following Eq. (2).

$$DR\% = \frac{\left(C_o - C_e\right)}{C_o} \times 100 \tag{2}$$

where  $C_o$  (mg/L) is the RO16 dye initial concentration and  $C_e$  (mg/L) is the concentration of the RO16 dye at equilibrium.

The adsorptive removal of RO16 dye by bare fly ash powder (FA), CS/Fe<sub>3</sub>O<sub>4</sub>, and CS-FA/Fe<sub>3</sub>O<sub>4</sub> composite was pre-determined and compared. The RO16 dye removal was 28.9%, 39.9%, and 68.2% for the fly ash powder (FA), CS/ Fe<sub>3</sub>O<sub>4</sub>, and CS-FA/Fe<sub>3</sub>O<sub>4</sub> composite adsorbents, respectively. This results show clearly the synergistic effect of incorporating FA powder into polymeric matrix of CS/ Fe<sub>3</sub>O<sub>4</sub> on the adsorptive property of the composite CS-FA/ Fe<sub>3</sub>O<sub>4</sub> for removal of RO16 dye.

### **Batch Adsorption Study**

The RO16 dye adsorption onto CS-FA/Fe<sub>3</sub>O<sub>4</sub> composite was studied in batch mode. According to Table 2 containing values of RO16 dye removal efficiency, the highest RO16 dye removal (%) can be obtained from run 13 under the following conditions: adsorbent dose (A: 0.08 g/L), pH (B: 4), temperature (C: 30 °C), and time (D: 55 min). Thus, these optimum conditions of adsorption key parameters were kept constant in the experiments of batch adsorption study. Adsorption experiments of RO16 dye were carried out using the same procedure mentioned above at different RO16 dye initial concentrations (20–150 mg/L) and contact time (0–660 min). The adsorption capacity of CS-FA/Fe<sub>3</sub>O<sub>4</sub> composite for RO16 dye at equilibrium,  $q_e$ (mg/g) was determined according to the following Eq. (3).

$$q_e = \frac{\left(C_o - C_e\right)V}{W} \tag{3}$$

where, V (L) is volume of RO16 dye solution and W (g) is the weight of CS-FA/Fe<sub>3</sub>O<sub>4</sub> composite. Adsorption experiments were conducted in duplicate under identical conditions and the results are reported as an average value.

# **Results and Discussion**

### Characterization

#### **Physicochemical Properties**

The elemental composition of FA was determined by XRF analysis and presented in Table 3. The result of analysis indicates the presence of Si, P, K, Ca, Al, Fe, Ti, Ag, Sr, and Zr mainly in structure of FA. Thus, it can be concluded that FA consist of metal oxides such SiO<sub>2</sub>, AL<sub>2</sub>O<sub>3</sub>, Fe<sub>2</sub>O<sub>3</sub>, CaO, TiO<sub>2</sub>, P<sub>2</sub>O<sub>3</sub> and K<sub>2</sub>O. The textural properties of FA, magnetic CS, and CS-FA/Fe<sub>3</sub>O<sub>4</sub> composite are presented in Table 4. The BET surface area analysis (Table 4) shows that the FA has surface area  $4.74 \text{ (m}^2\text{/g)}$ , while BET surface area of magnetic CS and CS-FA/Fe<sub>3</sub>O<sub>4</sub> composite were 2.22  $m^2/g$ and 8.57  $m^2/g$ , respectively. The results reflect a relatively high surface area of CS-FA/Fe<sub>3</sub>O<sub>4</sub> composite compared to CS/Fe<sub>3</sub>O<sub>4</sub> which can be attributed to the interfacial interaction between FA and the molecular structure of CS [37]. Furthermore, CS-FA/Fe<sub>3</sub>O<sub>4</sub> composite is a mesoporous material in accordance with the classification of IUPAC (USA) [38]. The potentiometric titrations showed the  $CS/Fe_3O_4$  has 45.6% amino group ( $-NH_2$ ) content, while CS-FA/Fe<sub>3</sub>O<sub>4</sub> composite was 39.5%. The decreasing in amine  $(-NH_2)$ content of the matrix of CS after incorporation of FA particles can be attributed to the physical loading of FA into molecular structure of  $CS/Fe_3O_4$ , and also to the chemical interactions between silicon matrix and/or negative charge of FA with basic sites of amino group in CS molecular structure [39]. The results indicate that  $CS-FA/Fe_3O_4$  composite has a relatively high content of amino  $(-NH_2)$  group. The protonation of amino (-NH<sub>2</sub>) group into (-NH<sub>3</sub><sup>+</sup>) in acidic environment can play an important role in the adsorption of RO16 dye due to electrostatic attraction between cationic amino groups (-NH<sub>3</sub><sup>+</sup>) of CS-FA/Fe<sub>3</sub>O<sub>4</sub> composite and RO16 dye anions.

Table 3	XRF analysis for FA
sample	

Element	Conc.	Unit
Al	0.94	%
Si	4.71	%
Р	0.32	%
Κ	0.98	%
Ca	2.01	%
Ti	1.08	%
Fe	5.07	%
Sr	0.29	%
Zr	0.18	%
Ag	0.12	%

Table 4 Textural properties of FA,  $CS/Fe_3O_4$ , and  $CS-FA/Fe_3O_4$  composite

Sample name	BET surface area (m <sup>2</sup> /g)	Mean pore diameter (nm)
FA	4.74	6.62
CS/Fe <sub>3</sub> O <sub>4</sub>	2.22	49.5
CS-FA/Fe <sub>3</sub> O <sub>4</sub>	8.57	7.84

#### **XRD** Analysis

The XRD pattern of the FA was given in Fig. 2. The FA profile shows sharp peaks at  $2\theta = 16^{\circ}$ ,  $22^{\circ}$ ,  $26^{\circ}$ ,  $33^{\circ}$ ,  $39^{\circ}$ ,  $41^{\circ}$ ,  $50^{\circ}$ ,  $60^{\circ}$ ,  $61^{\circ}$ , and  $68^{\circ}$ . These peaks reflect that the FA consisted primarily of crystalline phases like alumina (Al<sub>2</sub>O<sub>3</sub>), quartz (SiO<sub>2</sub>), and hematite (Fe<sub>2</sub>O<sub>3</sub>) [40]. The XRD pattern of CS/Fe<sub>3</sub>O<sub>4</sub> shows sharp characteristic peaks at  $2\theta = 30^{\circ}$ ,  $35^{\circ}$ ,  $43^{\circ}$ ,  $53^{\circ}$ ,  $57^{\circ}$ , and  $62^{\circ}$ , which are consistent with the



Fig. 2 XRD patterns of a FA, b CS/Fe<sub>3</sub>O<sub>4</sub>, and c CS-FA/Fe<sub>3</sub>O<sub>4</sub> composite

peaks of the Fe<sub>3</sub>O<sub>4</sub> standard cards (JCPDS file No. 19-629) for the (220), (311), (400), (422), (511), and (440) crystal surfaces, respectively [41]. The XRD pattern of CS-FA/ Fe<sub>3</sub>O<sub>4</sub> composite shows similar profile to the CS/Fe<sub>3</sub>O<sub>4</sub>, except a sharp peak related to FA was appeared in pattern of CS-FA/Fe<sub>3</sub>O<sub>4</sub> composite with obvious shift from  $2\theta = 26^{\circ}$ to  $2\theta = 27^{\circ}$ , indicating a successful interaction between FA and CS/Fe<sub>3</sub>O<sub>4</sub>.

### **FTIR Analysis**

FTIR spectra of FA, CS-FA/Fe<sub>3</sub>O<sub>4</sub> composite, and CS-FA/ Fe<sub>3</sub>O<sub>4</sub> composite after adsorption of RO16 dye are presented in Fig. 3. The FTIR spectrum of FA displayed characteristic peaks at 1070 cm<sup>-1</sup> and 790 cm<sup>-1</sup> for bond stretching of asymmetric Si–O–Si and symmetric Si–O–Si, respectively [23]. The peaks in region between 3600 and 3770 cm<sup>-1</sup> indicates the stretching vibrations of OH [42]. The FTIR



Fig.3 FTIR spectra of a FA, b CS-FA/Fe<sub>3</sub>O<sub>4</sub> composite, and c CS-FA/Fe<sub>3</sub>O<sub>4</sub> composite after adsorption of RO16 dye

spectrum of CS-FA/Fe<sub>3</sub>O<sub>4</sub> composite showed major bands for CS polymer which can be assigned as follows: 3600 cm<sup>-1</sup> (stretching vibrations of -NH and -OH bonds), 2870 cm<sup>-1</sup> (stretching vibrations of C-H in -CH and -CH<sub>2</sub>), 1650 cm<sup>-1</sup> (bending vibration of N-H), 1380 cm<sup>-1</sup> (stretching vibration of C–N), and 1090 cm<sup>-1</sup> (skeletal vibration of C–O) [37]. The peak at 553  $\text{cm}^{-1}$  corresponds to Fe–O bond [43]. The FTIR spectrum of CS-FA/Fe<sub>3</sub>O<sub>4</sub> composite after adsorption of RO16 dye did not show much difference in bands position compare to spectrum of CS-FA/Fe<sub>3</sub>O<sub>4</sub> composite before RO16 dye adsorption, except slight shifting of some bands due to involvement the functional groups of CS-FA/ Fe<sub>3</sub>O<sub>4</sub> composite in the RO16 dye adsorption process. Furthermore, the band at  $1500 \text{ cm}^{-1}$  can be attributed to the aromatic rings (C=C) of RO16 dye adsorbed on the surface of CS-FA/Fe<sub>3</sub>O<sub>4</sub> composite.

#### SEM–EDX Analysis

SEM-EDX analysis was carried out in order to investigate the surface morphological structure of FA, CS/Fe<sub>3</sub>O<sub>4</sub>, CS-FA/Fe<sub>3</sub>O<sub>4</sub> composite, and CS-FA/Fe<sub>3</sub>O<sub>4</sub> composite after adsorption of RO16 dye along with chemical composition. Figure 4a-d shows the SEM images and EDX analysis of FA, CS/Fe<sub>3</sub>O<sub>4</sub>, CS-FA/Fe<sub>3</sub>O<sub>4</sub> composite and CS-FA/Fe<sub>3</sub>O<sub>4</sub> composite after adsorption of RO16 dye, respectively. Figure 4a shows that the fly ash particles in different particle sizes were clearly visible in spherical shape (as highlighted in red cycles) with regular and smooth surface. The EDX analysis shows that the FA contains the elements C, O, Al and Si. In fact, the presence of C element within the elements of the analysis of EDX indicates to presence of unburned carbon, which plays an important role in adsorption process [44]. The surface morphology of  $CS/Fe_3O_4$ (Fig. 4b) shows regular, compact, and homogenous surface, indicating equal distribution of magnetic Fe<sub>3</sub>O<sub>4</sub> particles into molecular structure of CS. The EDX analysis shows that the CS/Fe<sub>3</sub>O<sub>4</sub> contains the elements of CS biopolymer such as C, O, and N, in addition to presence element Fe corresponds to the magnetic Fe<sub>3</sub>O<sub>4</sub>. The surface morphology of CS-FA/Fe<sub>3</sub>O<sub>4</sub> composite as shown in Fig. 4c appeared as irregular and heterogeneous surface with many visible cavities and pores. The appearance of spherical particles in the image indicates successful incorporation FA particles into molecular structure of CS. The EDX analysis shows a slight decrease in the elemental content of C which can be attributed to the loading of FA into molecular structure of CS/Fe<sub>3</sub>O<sub>4</sub>. The surface of CS-FA/Fe<sub>3</sub>O<sub>4</sub> after the adsorption of RO16 dye (Fig. 4d) was turned to be less porous with evanescence of crevices on the CS-FA/Fe<sub>3</sub>O<sub>4</sub> surface, indicating the RO16 dye molecules adsorbed on the CS-FA/ Fe<sub>3</sub>O<sub>4</sub> surface. The EDX analysis shows the presence of S



Fig. 4 SEM images and EDX spectra of a FA, b CS/Fe<sub>3</sub>O<sub>4</sub>, c CS-FA/Fe<sub>3</sub>O<sub>4</sub> composite, and d CS-FA/Fe<sub>3</sub>O<sub>4</sub> composite after adsorption of RO16 dye

element belongs to RO16 dye and reconfirms the RO16 dye adsorption by CS-FA/Fe<sub>3</sub>O<sub>4</sub> surface.

# **BBD Model Analysis**

The individual and interactive effects of the independent factors including adsorbent dose (A), solution pH (B), temperature (C) and time (D) on the RO16 dye removal were investigated using BBD-RSM. Analysis of variance (ANOVA) was employed to analyze the experimental results of RO16 dye removal statistically as shown in Table 5. Based on Table 5 (ANOVA analysis), the F-value of model and the corresponding p-value are 17.7 and < 0.0001, respectively. These values indicate that the model is statistically significant [45]. The coefficient of determination  $(R^2)$  value was close to the unity, indicating to the high correlation between the values of actual and the predicted. Generally, the terms of model with p-value less than 0.05 (Prob > F < 0.0500) are significant on the RO16 dye removal under chosen conditions. According to Table 5, the BBD model terms of A, B, C, E,  $A^2$ ,  $B^2$ ,  $C^2$ , AD and BC are significant on the RO16 dye removal. However, the terms of BBD model with p-value larger than 0.05 were excluded from second-order polynomial model in order to achieve fitting of the BBD model. Thus, the equation of second-order polynomial model between tested factors and the RO16 dye removal (response) was obtained and described in the following Eq. (4):

	Table 5	Analysis of variance (	ANOVA	) for the removal	of RO16 dy	ye
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Source	Sum of squares	Df	Mean square	F-value	P-value
Model	6854.35	14	489.60	17.69	< 0.0001
A-Adsorbent dose	830.00	1	830.00	30.00	< 0.0001
B-pH	2736.12	1	2736.12	98.89	< 0.0001
C-Temp	407.17	1	407.17	14.72	0.0018
D-Time	426.02	1	426.02	15.40	0.0015
AB	21.62	1	21.62	0.7815	0.3916
AC	0.81	1	0.81	0.0293	0.8666
AD	183.60	1	183.60	6.64	0.0220
BC	712.89	1	712.89	25.76	0.0002
BD	29.70	1	29.70	1.07	0.3177
CD	1.82	1	1.82	0.0659	0.8012
$A^2$	145.43	1	145.43	5.26	0.0379
$\mathbf{B}^2$	1394.05	1	1394.05	50.38	< 0.0001
$C^2$	185.49	1	185.49	6.70	0.0214
$D^2$	3.62	1	3.62	0.1310	0.7228
Residual	387.37	14	27.67		
Cor Total	7241.72	28			

RO16 removal (%) = 
$$+15.18 + 8.32A - 15.10B$$
  
- 5.83C + 5.96D + 6.78AD  
+ 13.35BC + 4.74A<sup>2</sup> + 14.66B<sup>2</sup>  
+ 5.35C<sup>2</sup> (4)

Validation of model can be also achieved by graphical methods through investigation in the nature of residuals distribution of the model, and relationship between values of the predicted and actual RO16 dye removal. Figure 5a shows normal probability plot of residuals for the model. It was observed from Fig. 5a, the perfect normal distributions of the residuals, where points seem conspicuously close to a straight line. This observation indicates to the accuracy of the assumptions and independence of the residuals [46]. The relationship between the values of predicted and actual RO16 dye removal (%) is shown in Fig. 5b which indicates the values of predicted and actual are close to each other, and confirming the statistical validation of the model.

# Interactive Effects of Two Variables on RO16 Dye Removal

The interaction effect between any two independent variables on the RO16 dye removal was evaluated. The interaction effect between solution pH (B) and temperature (C) on the RO16 dye removal was significant (p-value = 0.0002), while the other factors (adsorbent dose 0.08 g and time 55 min) remained constant. The plots of three-dimensional (3D) response surfaces and two dimensional (2D) contour for the impacts and interaction of solution pH (B) and temperature (C) on RO16 dye removal (%) were shown in Fig. 6a, b, respectively. According to Fig. 6a, b can be noticed that the lowering solution pH from 10 to 4 is responsible for increasing the RO16 dye removal (%) from 7.90 to 73.1%. The pHpzc value of CS-FA/Fe<sub>3</sub>O<sub>4</sub> composite was 7 as depicted in Fig. 6c. This result elucidates that the CS-FA/ Fe<sub>3</sub>O<sub>4</sub> composite has a cationic character and reinforced the availability of the amino (-NH<sub>3</sub><sup>+</sup>) cationic group on the CS-FA/Fe<sub>3</sub>O<sub>4</sub> surface, and in a good agreement with the potentiometric titrations test. The surface of CS-FA/Fe<sub>3</sub>O<sub>4</sub> composite can be converted to positive charge at pH value below the pHpzc, thus promoting the adsorption of anions RO16 dye species. As a result, a strong electrostatic interaction can be occurred between protonated amino (-NH<sub>3</sub>) functional group of CS-FA/Fe<sub>3</sub>O<sub>4</sub> composite and sulfonate  $(-SO_3^{-})$  groups of the RO16 dye, thus increasing the RO16 dye removal as shown in Eq. (5).

$$R - NH_3^+ + RO16 - SO_3^- \leftrightarrow R - NH_3^+ - SO_3^- - RO16$$
 (5)

Furthermore, it was observed from Fig. 6a, b the highest RO16 dye removal was achieved at temperature 30 °C,



Fig. 5 a Normal probability plot of residuals for BBD model, b plot of the relationship between the predicted and actual values of RO16 dye removal (%)

indicating the RO16 dye adsorption process onto the CS-FA/  $Fe_3O_4$  surface was an exothermic in nature [47].

Another significant interaction (p-value = 0.022) on the RO16 dye removal (%) was between adsorbent dose (A) and time (D), while the other parameters (solution pH 7 and temperature 40 °C) remained constant. The plots of threedimensional (3D) response surfaces and two dimensional (2D) contour for the impacts and interaction of adsorbent dose (A) and time (D) on RO16 dye removal (%) were shown in Fig. 6d, e, respectively. As depicted in Fig. 6d, e, the dye removal (%) was gradually increased by increasing adsorbent dose which can be attributed to the increase in the available surface area of CS-FA/Fe3O4 in dye solution, and also higher CS-FA/Fe3O4 dose indicates a greater number of active adsorption sites available. Moreover, the RO 16 dye removal was increased by increasing the contact time from 20 to 90 min, with longer contact time the RO16 dye molecules will get sufficient time to move deeper toward inner active adsorption sites on the surface of CS-FA/Fe3O4.

# **Adsorption Study**

The effect of initial RO16 dye concentration and contact time on adsorption equilibrium was investigated. The adsorption capacity,  $q_t$ (mg/g) against time at several initial RO16 concentrations of 20, 40, 60, 80, 100 and 150 mg/L was investigated as depicted in Fig. 7a, while the other optimum factors like adsorbent dose = 0.08 g, solution pH 4, and temperature = 30 °C were kept constant. It is observed from Fig. 7a that the quantity of RO16 dye molecules uptake onto surface of CS-FA/Fe<sub>3</sub>O<sub>4</sub> composite raised from 12.4 to 45.7 mg/g by increasing the initial RO16 dye concentrations from 20 to 150 mg/L. This can be attributed to the higher concentration gradient which provides a driving force to move the RO16 molecules towards active adsorption sites [48].

### **Adsorption Kinetics**

In order to understand the controlling mechanism of the adsorption process of RO16 dye molecules on the CS-FA/ $Fe_3O_4$  composite, the non-linear pseudo-first-order (PFO) and non-linear pseudo-second-order (PSO) kinetic models were utilized to analyze the experimental data of the RO16 dye adsorption on CS-FA/Fe<sub>3</sub>O<sub>4</sub> composite at different initial RO16 dye concentrations [49]. The non-linear equations of the kinetic models PFO [50] and PSO [51] are expressed in Eqs. (6) and (7) as follows:

$$q_t = q_e (1 - \exp^{-k_1 t})$$
(6)

$$q_t = \frac{q_e^2 k_2 t}{1 + q_e k_2 t}$$
(7)







**Fig. 7 a** Effect of the contact time on RO16 adsorption at different initial concentrations, and **b** adsorption isotherms of RO16 dye by CS-FA/Fe<sub>3</sub>O<sub>4</sub> composite (adsorbent dose=0.16 g, pH of solution=4, temperature=30 °C, agitation speed=100 strokes and volume of solution=100 mL)

where,  $q_t$  (mg/g) is the amount of RO16 dye adsorbed at time (t), and  $q_e$  (mg/g) is the amount of RO16 dye adsorbed at equilibrium.  $k_1$  (1/min) is the rate constant of PFO, and  $k_2$  (g/mg min) is the rate constant of PSO. The parameters of kinetic models and  $R^2$  values are recorded in Table 6. According to experimental data (Table 6) can be concluded that the adsorption of RO16 dye molecules by the CS-FA/ Fe<sub>3</sub>O<sub>4</sub> composite follows PSO model due to the higher correlation coefficient ( $R^2$ ) values, in addition to the calculated  $q_e$  ( $q_{e,cal}$ ) values fitted well with the experimental  $q_e$  ( $q_{e,exp}$ ) values. This result indicates that the adsorption of RO16 dye by CS-FA/Fe<sub>3</sub>O<sub>4</sub> composite was the chemisorption process involving the electrostatic interaction between the positively charged available on the surface of CS-FA/Fe<sub>3</sub>O<sub>4</sub> composite and the RO16 dye anions [52].

### **Adsorption Isotherms**

Adsorption isotherm is essential to understand the interaction between the RO16 dye molecules and the CS-FA/  $Fe_3O_4$  composite [53, 54]. In order to evaluate the adsorption capacity of CS-FA/Fe<sub>3</sub>O<sub>4</sub> composite for RO16 dye, non-linear equilibrium models of Langmuir, Freundlich, and Temkin were utilized to fit the experimental data. The nonlinear equations of the equilibrium models Langmuir [55], Freundlich [56], and Temkin [57] are presented in Eqs. (8), (9), and (10), respectively.

$$q_e = \frac{q_{\max} K_a C_e}{1 + K_a C_e} \tag{8}$$

$$q_e = K_f C_e^{1/n} \tag{9}$$

$$q_e = \frac{RT}{b_T} \ln(K_T C_e) \tag{10}$$

where  $q_e$  (mg/g) is the amount of RO16 dye adsorbed at equilibrium,  $C_e$  (mg/L) is the concentration of RO16 dye at equilibrium,  $q_{\text{max}}$  (mg/g) is the maximum adsorption capacity, and  $K_a$  (L/mg) is Langmuir constant.  $K_f$  (mg/g) (L/mg)<sup>1/n</sup> is the Freundlich constant, n is the dimensionless constant

Concentration	$q_{\rm eexp}$ . (mg/g)	PFO			PSO	PSO		
(mg/L)		$q_{\rm e\ cal}({\rm mg/g})$	<i>k</i> <sub>1</sub> (1/min)	$R^2$	$\overline{q_{\rm ecal}({\rm mg/g})}$	$k_2 \times 10^{-2}$ (g/mg min)	<i>R</i> <sup>2</sup>	
20	12.4	12.2	0.18	0.98	12.5	3.0	0.99	
40	16.8	16.4	0.08	0.96	17.1	0.8	0.99	
60	24.6	23.7	0.04	0.78	24.7	0.3	0.95	
80	28.6	27.3	0.03	0.93	29.1	0.2	0.98	
100	32.2	30.2	0.02	0.90	32.3	0.14	0.96	
150	45.7	40.5	0.03	0.88	43.4	0.11	0.95	

6

Table 6PFO and PSO kineticparameters for RO16 dyeadsorption on CS-FA/Fe3O4composite

Table 7 Parameters of the Langmuir, Freundlich, and Temkin isotherm models for RO16 dye adsorption on CS-FA/Fe $_3O_4$  composite at 30 °C

Adsorption isotherm	Parameter	Value
Langmuir	$q_m (mg/g)$	66.9
	$K_a$ (L/mg)	0.02
	$R^2$	0.93
Freundlich	$K_f (mg/g) (L/mg)^{1/n}$	4.76
	n	1.94
	$R^2$	0.96
Temkin	$K_T$ (L/mg)	0.96
	$b_{\rm T}$ (J/mol)	208
	$R^2$	0.88

indicates to the adsorption intensity.  $K_T$  (L/mg) is Temkin constant, T (K) is temperature, R (8.314 J/molK) is the universal gas constant, and  $b_T$  (J/mol) is heat of adsorption. The non-linear curves of the equilibrium models are shown in

Fig. 7b. The parameters of equilibrium models are recorded in Table 7. According to the  $R^2$  values (Table 7) obtained from the isotherm models, it observed that the Freundlich isotherm has highest correlation ( $R^2$  0.96), which indicated that the RO16 dye adsorption occurred on heterogeneous surface [58]. The maximum adsorption capacity ( $q_{max}$ ) of CS-FA/Fe<sub>3</sub>O<sub>4</sub> composite for RO16 dye was 66.9 mg/g at 30 °C. It can be deduced that the CS-FA/Fe<sub>3</sub>O<sub>4</sub> composite was a potential and effective biosorbent for removal of RO16 dye from aqueous media.

#### **Adsorption Mechanism**

Adsorption mechanism of RO16 dye on CS-FA/Fe<sub>3</sub>O<sub>4</sub> composite surface by different types of interactions is shown in Fig. 8. An electrostatic attraction (Fig. 8a) is considered from the most interaction that can be occurred between RO16 dye and surface of adsorbent. This mechanism involves the electrostatic interaction between RO16 dye anions with positively charged available on the CS-FA/Fe<sub>3</sub>O<sub>4</sub>



**Fig.8** Illustration of the possible adsorption mechanism between CS-FA/Fe<sub>3</sub>O<sub>4</sub> composite and RO16 dye: **a** electrostatic attraction, **b** dipole–dipole hydrogen bonding interactions, **c** Yoshida H-bonding, and **d** n- $\pi$  stacking interactions

composite surface. Adsorption mechanism also includes H-bonding interactions such as dipole–dipole hydrogen bonding (Fig. 8b), and Yoshida H-bonding (Fig. 8c). Dipole–dipole hydrogen bonding happens between H atom available on the surface of CS-FA/Fe<sub>3</sub>O<sub>4</sub> composite, and N atoms in the RO16 dye structure, while Yoshida H-bonding happens between –OH available on the surface of CS-FA/ Fe<sub>3</sub>O<sub>4</sub> composite, and the aromatic rings of RO16 dye.[59]. Finally, n– $\pi$  interaction comes from delocalization of the lone pair electron of O and N atoms into the  $\pi$  orbital of the dye aromatic rings as shown in Fig. 8d [60]. According to the above, it can be concluded that these interactions are effective in enhancing adsorption process of RO16 dye on the surface of CS-FA/Fe<sub>3</sub>O<sub>4</sub> composite.

# Conclusion

Magnetic fly ash/Fe<sub>3</sub>O<sub>4</sub> particles (CS-FA/Fe<sub>3</sub>O<sub>4</sub>) composite was successfully synthesized and applied as an effective bioadsorbent for the removal of RO16. The incorporation of FA particles in magnetic CS leads to enhance surface area of CS-FA/Fe<sub>3</sub>O<sub>4</sub> composite. The CS-FA/ Fe<sub>3</sub>O<sub>4</sub> composite was easily separated and collected from the aqueous solution after adsorption process by external magnetic field. Analysis of variance (ANOVA) showed the F-value of model and the corresponding p-value are 17.7 and < 0.0001, indicating the model is statistically significant. The experimental results indicate that the highest RO16 dye removal of 73.1% was observed by significant interaction between BC (pH × temperature, p-value = 0.0002) and AD (adsorbent dose x time, p-value = 0.022). The optimum conditions of adsorption process parameters were pH ~ 4, adsorbent dose (0.08 g), temperature (30 °C) and time (55 min). The kinetics and isotherms models results indicated that the adsorption was affected by chemisorption and heterogeneous mode of adsorption. The  $q_{max}$  of CS-FA/Fe<sub>3</sub>O<sub>4</sub> composite for RO16 dye was 66.9 mg/g at 30 °C.

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