

# $P_1$ -Nonconforming Quadrilateral Finite Volume Methods for the Semilinear Elliptic Equations

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**Abstract** In this paper we use  $P_1$ -nonconforming quadrilateral finite volume methods with interpolated coefficients to solve the semilinear elliptic problems. Two types of control volumes are applied. Optimal error estimates in  $H^1$ -norm on the quadrilateral mesh and superconvergence of derivative on the rectangular mesh are derived by using the continuity argument, respectively. In addition, numerical experiments are presented adequately to confirm the theoretical analysis and optimal error estimates in  $L^2$ -norm is also observed obviously. Compared with the standard  $Q_1$ -conforming quadrilateral element, numerical results of the proposed finite volume methods show its better performance than others.

**Keywords** Semilinear elliptic equations · Finite volume methods ·  $P_1$ -nonconforming quadrilateral element ·  $Q_1$ -conforming quadrilateral element · Superconvergence

## 1 Introduction

Finite volume methods (FVM) is an important and commonly used method for solving many practical problems in scientific and engineering computations. It is also known as the Marker-and-Cell methods [9, 15], the generalized difference methods [23, 45], finite volume element methods (FVEM) [4–6, 26, 43], covolume methods [10–12] or box methods

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[2, 14, 35]. Its main virtues are the local conservation and the capability of discretizing domains with complex geometry. In general, it represents the conservation of a quantity of interest, such as mass, momentum or energy in fluid mechanics. The integral formulation of a finite volume scheme for a problem is obtained by integrating the problem over a control volume or a dual element. In fact, FVM might be regarded as a special class of Petrov-Galerkin methods where the trial function spaces are connected with the test function spaces associated with the dual partitions induced by the control volumes [21, 42]. Usually, we use different polynomial functions as trial and test spaces over the original partition and its dual partition, respectively. It is different from the standard finite element methods (FEM) which only use simple polynomial function spaces over the original partition. Although FEM is flexible to deal with the complex domains and various boundary conditions, and the theory on the convergence and stability of FEM is well established, the main drawback of FEM might be the loss of the local conservation property which can be fundamental for the simulation of many physical models, e.g., in computational fluid dynamics, hyperbolic equations, heat transfer and modeling of fuel cells [9, 15, 19, 23, 44]. Of course, one of the main limitation of FVM is the low order approximation. For most existing FVM, the test space is either a piecewise constant or a linear finite element spaces.

In this paper we shall devote ourself to study the semilinear elliptic problems by using FVM and FEM, respectively. Now a lot of numerical methods have been proposed and developed to solve the semilinear problems. Among them, FEM with interpolated coefficients is an effective and excellent method. In 1980, this method was introduced and analyzed firstly for the semilinear parabolic problems by Zlamal [46]. Later, Larson, Thomee and Zhang [22] studied the semidiscrete linear triangular FEM with interpolated coefficients, and Chen, Larson and Zhang [8] derived almost optimal order convergence on a uniform triangular mesh by using the piecewise linear finite element space and superconvergence techniques. Xiong and Chen [37–39] studied the superconvergence of triangular quadratic FEM for the nonlinear ordinary differential equation and the  $Q_1$ -conforming rectangular FEM with interpolated coefficients for the semilinear elliptic problem, respectively. Recently Xiong and Chen [40, 41] put the interpolation idea into FVEM for solving two-point boundary value problem of the semilinear differential equations and studied the  $Q_1$ -conforming rectangular FVEM with interpolated coefficients for the semilinear elliptic equation.

On the quadrilateral mesh, Li and Li [24] studied the generalized difference methods for the Poisson equation under some assumptions on the regularity of solutions and restrictions on the quadrilateral subdivision of a convex polygon domain. Zhu and Li [45] obtained a superconvergence result of the generalized difference methods in a discrete norm. Wang [36] constructed a mixed FVEM based on the rectangular mesh for the biharmonic equations by using  $Q_1$ -conforming element.

In 2003, Park and Sheen [34] introduced the nonparametric  $P_1$ -nonconforming quadrilateral FEM to solve the second-order elliptic problems independently by a novel approach. Unlike the usual conforming and nonconforming quadrilateral elements, their element only consists of piecewise linear polynomials that are continuous at the midpoints of edges. One of the benefits of using this element is convenient to use the rectangular or quadrilateral mesh with much less degrees of freedom than the usual quadrilateral nonconforming elements. Note that for  $Q_1$ -conforming quadrilateral element, they have the same degrees of freedom for different boundary conditions. On the other hand, from different points of view, the different  $P_1$ -nonconforming quadrilateral finite element can also be found in some references, e.g. the RQC4 element proposed in [44] (has been published 20 years ago). Furthermore, motivated by references [33, 34, 44], the parametric constrained nonconforming rotated  $Q_1$  element are presented in [20] and the nonconforming double set parameter rotated  $Q_1$  element are also presented in [28–32]. In 2006, Mao, Chen and Sun [31] presented

a four-parameter quadrilateral nonconforming element with double set parameter by using different motivation and ideas (It is originated from the nonconforming rotated  $Q_1$  element and bilinear element, they call it QB element) and proved that it is an anisotropic and superconvergent nonconforming quadrilateral element. Note that QB element is equivalent to  $P_1$ -nonconforming quadrilateral element [34] under the rectangular meshes.

Later, Man and Shi [27] studied FVEM of  $P_1$ -nonconforming quadrilateral element for the elliptic problems based on a dual partition of overlapping type and obtain optimal error estimates under additional assumptions on the source term and the partition. Moreover, Grajewski, Hron and Turek [18] examined in detail the numerical behavior of Park-Sheen element with special emphasis on the treatment of Dirichlet boundary conditions and made several numerical examples for the  $P_1$ -nonconforming FEM on the quadrilateral meshes. Recently, Feng, Kim, Nam and Sheen [16] used the locally stabilized  $P_1$ -nonconforming quadrilateral and hexahedral FEM to solve the Stokes equations and obtained optimal error estimate for velocity and pressure. In this paper, we shall use  $P_1$ -nonconforming quadrilateral element to solve the semilinear elliptic problems by FVM and FEM on the rectangular mesh, respectively. Furthermore, we apply  $Q_1$ -conforming quadrilateral element to the same problems by FVM and FEM, respectively.

The outline of this paper is organized as follows. In Sect. 2, we shall introduce the FVM with interpolated coefficients and two types of control volumes for the semilinear elliptic equations. In Sect. 3, we will give preliminaries and some lemmas. In Sect. 4, we derive optimal error estimate in  $H^1$ -norm on the quadrilateral mesh. Next we will prove superconvergence of derivative on the rectangular mesh in Sect. 5. The theoretical results are investigated in detail by numerical experiments. In addition, numerical comparisons of the standard  $Q_1$ -conforming quadrilateral FVM (or FEM) and  $P_1$ -nonconforming quadrilateral FVM (or FEM) are presented in Sect. 6. Finally, conclusions are given in Sect. 7.

## 2 FVM with Interpolated Coefficients

Now we consider the following second order semilinear elliptic equation

$$-\Delta u + f(u) = g, \quad \text{in } \Omega \subset \mathbb{R}^2 \tag{1}$$

with homogenous boundary condition of Dirichlet type, i.e.,  $u|_{\partial\Omega} = 0$  and  $g \in L^2(\Omega)$ . Assume that  $f'(s) > 0$  for  $s \in (-\infty, +\infty)$  and  $f''(s)$  is continuous with respect to  $s$ , and  $\Omega = (0, 1) \times (0, 1)$ .

Finite volume approximations rely on the local conservation property expressed by the differential equation. Namely, integrating equation (1) over any control volume  $V \subset \Omega$  with piecewise smooth boundary  $\partial V$  and using the Green formula, we obtain

$$-\int_{\partial V} \frac{\partial u}{\partial n} ds + \int_V f(u) dx dy = \int_V g dx dy, \quad \forall V \subset \Omega, \tag{2}$$

where  $n$  denotes the unit exterior normal to  $\partial V$ . The FVM of problem (2) consists of replacing the exact solution  $u$  by the finite-dimensional space of piecewise smooth functions and using a finite set of control volumes. In this paper, we shall use the rectangular partition of  $\Omega$  and the piecewise linear interpolation with interpolated coefficients for  $u$  firstly.

Given a quasi-uniform rectangular partition  $T_h$  for  $\Omega$ , and the nodes are  $(x_i, y_j)$ ,  $i = 0, 1, 2, \dots, N_x$ ,  $j = 0, 1, 2, \dots, N_y$ . Denote  $h_{x_i} = x_i - x_{i-1}$ ,  $i = 1, 2, \dots, N_x$ ,  $h_{y_j} = y_j - y_{j-1}$ ,  $j = 1, 2, \dots, N_y$ , and  $h = \max_{i,j} \{h_{x_i}, h_{y_j}\}$ . For any rectangular element  $\tau_{ij} =$

$[x_{i-1}, x_i] \times [y_{j-1}, y_j] \in T_h$ , let  $Z_h(\tau_{ij})$  and  $E_h(\tau_{ij})$  be the set of nodes and sides of  $\tau_{ij}$  respectively. Setting  $Z_h = \bigcup_{\tau_{ij} \in T_h} Z_h(\tau_{ij})$  and  $E_h = \bigcup_{\tau_{ij} \in T_h} E_h(\tau_{ij})$ . Further let  $Z_h^{in}$  and  $E_h^{in}$  be the set of interior nodes and sides of  $T_h$  respectively. We denote the set of all middle point of sides  $e \in E_h$  (or  $E_h^{in}$ ) with each node  $z_j$  by  $M_h$  (or  $M_h^{in}$ ), and denote the subset of  $E_h$  consisting of those sides that have  $z_j$  is a endpoint of sides  $e$  by  $E_h(j)$ . Moreover, we denote the set of midpoints of sides  $e \in E_h(j)$  by  $M_h(j)$ . In what follows, we use  $\tau$  with or without subscripts to denote a element, possibly different at different occurrences in this paper, that may be a rectangular element, a trapezoidal element or a quadrilateral element.

Now we introduce  $P_1$ -nonconforming quadrilateral finite element space [34] and dual partition  $T_h^*$  associated with the quadrilateral partition  $T_h$ . Setting

$$S_h = \{v_h : \Omega \rightarrow R : v_h|_\tau \in P_1(\tau) \text{ for all } \tau \in T_h \text{ and } v_h \text{ is continuous at every } m_i \in M_h^{in}\},$$

$$S_{0h} = \{v_h \in S_h | v_h(m_i) = 0 \text{ for any } m_i \in M_h \setminus M_h^{in}\},$$

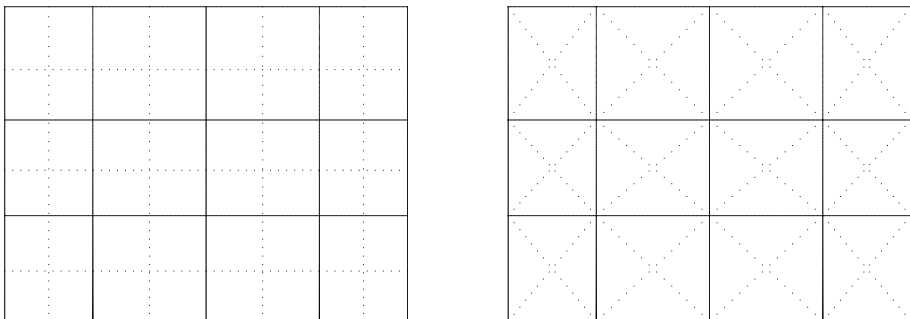
where  $P_1(\tau) = \text{span}\{1, x, y\}$ . Let  $\phi_j \in S_{0h}$  be such that

$$\phi_j(m) = \begin{cases} 1, & \text{if } m \in M_h(j), \\ 0, & \text{if } m \in M_h \setminus M_h(j). \end{cases}$$

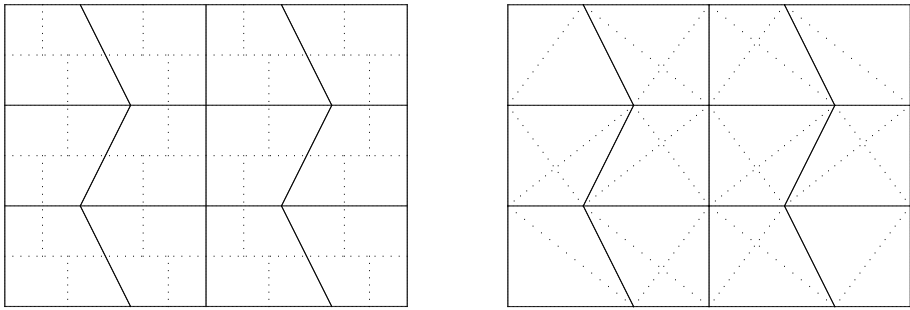
It is pointed out that if  $T_h$  is decomposed into parallelograms,  $\phi_j$  is continuous at  $z_j$  for all  $j$ . However,  $\phi_j$  may not be continuous in general. Under the assumption that each interior edge has at least one interior vertex as its endpoint, all functions associated with the interior nodes  $Z_h^{in}$  form the basis of  $S_{0h}$ .

Next we define a control volume  $V_{z_j}$  of node  $z_j \in Z_h^{in}$ , which includes  $z_j$  and four midpoints of  $M_h(j)$ . For boundary nodes, their control volumes should be modified correspondingly. All the control volumes constitute the dual partition  $T_h^*$ . In this paper we only consider two types of dual partitions. One is the nonoverlapping rectangular control volumes of interior vertices, and it is shown in the left subfigure of Fig. 1. The other is the overlapping quadrilateral control volumes of interior vertices which consist of four diagonals, and it is so called diagonal box [35] and shown in the right subfigure of Fig. 1.

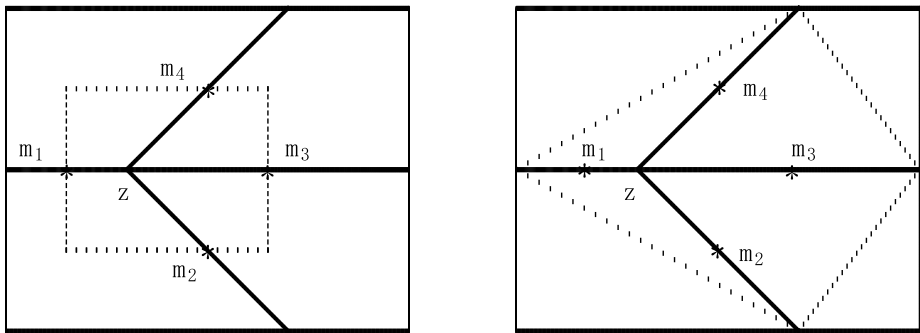
*Remark 2.1* Moreover, we consider a trapezoidal mesh in Fig. 2 which appear in [16, 20] and two types of control volumes in Fig. 3. The trapezoidal element is an extension of the original two dimensional rectangular element, where  $\theta \in [0, 1]$  is a relax parameter that



**Fig. 1** *Left:* A rectangular mesh with nonoverlapping control volumes of interior vertices. *Right:* A rectangular mesh with overlapping control volumes of interior vertices

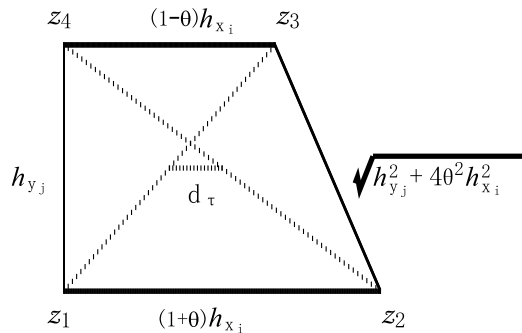


**Fig. 2** *Left:* A trapezoid mesh with nonoverlapping control volumes. *Right:* A trapezoid mesh with overlapping control volumes



**Fig. 3** *Left: (I).* A sample nonoverlapping control volume  $V_z$ , where  $m_i, i = 1, 2, 3, 4$ , is midpoint. *Right: (II).* A sample overlapping control volume  $V_z$

**Fig. 4** The shape of a trapezoid element  $\tau$



depict the shape of a element,  $z_i, i = 1, 2, 3, 4$ , are vertices of  $\tau$ , and the length of the edge  $z_2z_3$  equates  $\sqrt{h_{y_j}^2 + 4\theta^2 h_{x_i}^2}$  in Fig. 4. When  $\theta = 0$ , the trapezoidal mesh degenerates to a rectangular mesh. When  $\theta = 1$ , the trapezoidal mesh degenerates to a triangle mesh.

*Remark 2.2* For the low order conforming quadrilateral element,  $Q_1(\tau) = span\{1, x, y, xy\}$ . If we use  $Q_1$ -conforming element and the trapezoidal mesh in Fig. 2, then when  $\theta = 1$ , the trapezoid is degenerated into the right triangle. In this case, the  $Q_1$ -conforming quadrilateral

element is well-defined and it degenerates to the  $P_1$ -conforming triangular element [1, 13, 32]. For the  $P_1$ -nonconforming quadrilateral element, it has the same conclusion. Note that the smallness of the quantity  $d_\tau$ , the distance between the two midpoints of the two diagonals of  $\tau$ , is a good indicator of almost parallelogram [1, 11, 13, 20]. Here the midpoints distance  $d_\tau = \theta h_{x_i}$  in Fig. 4. Obviously,  $d_\tau \rightarrow 0$  as  $\theta \rightarrow 0$ ,  $Q_1(\tau)$  and  $P_1(\tau)$  do work very well.

Now we introduce the standard notations and definitions for the Sobolev spaces  $H^{m,p}(\Omega)$ , and their associated norms  $\|\cdot\|_{m,p}$  and seminorms  $|\cdot|_{m,p}$ ,  $m \geq 0$ . If  $p = 2$ , the subscript  $p$  may be omitted, in which case the norms, inner products and seminorms are denoted by  $\|\cdot\|_m$ ,  $(\cdot, \cdot)_m$  and  $|\cdot|_m$ , respectively. If  $m = 0$ , the subscript  $m$  may be omitted. The space  $H^0(\Omega)$  coincides with  $L^2(\Omega)$ , in which case the norm and inner product are denoted by  $\|\cdot\|_0$  and  $(\cdot, \cdot)$ , respectively. The space  $H_0^1(\Omega)$  is the subspace of  $H^1(\Omega)$  consisting of functions with vanishing on  $\partial\Omega$ . Further we shall denote with  $p'$  the adjoint number of  $p$ , i.e.  $\frac{1}{p} + \frac{1}{p'} = 1$ ,  $p, p' \geq 1$ . In what follows, we use  $C$ , with or without subscripts to denote a generic positive constant, possibly different at different occurrences in this paper, that is independent of the mesh parameter  $h$  but may depend on the domain  $\Omega$ .

Let  $S_{0h}$  be the piecewise linear finite element space over the original partition  $T_h$  and  $S_h^* \subset L^2(\Omega)$  be the piecewise constant space over the dual partition  $T_h^*$ , respectively. Suppose  $z \in Z_h$  and denote the basis function of  $S_h$  at the vertex  $z$  by  $\phi_z$ . Define  $V_z$  by the corresponding dual element of vertex  $z$  and  $\chi_z$  by the characteristic function over  $V_z$ . Define the interpolation operator  $I_h : H^2(\Omega) \cap H_0^1(\Omega) \rightarrow S_{0h}$  as in [34] such that

$$I_h\varphi(m) = \frac{1}{2}(\varphi(z_1) + \varphi(z_2)), \quad \forall m \in M_h,$$

where  $z_1$  and  $z_2$  are the endpoints of an edge with  $m$  as its midpoint. For any  $\varphi \in H^2(\Omega) \cap H_0^1(\Omega)$ , its interpolation can be expressed as

$$I_h\varphi = \frac{1}{2} \sum_{z \in Z_h} \varphi(z)\phi_z, \quad \forall \varphi \in H^2(\Omega) \cap H_0^1(\Omega). \tag{3}$$

It has the following approximation property

$$\|\varphi - I_h\varphi\| + h\|\varphi - I_h\varphi\|_{1,h} \leq Ch^2\|\varphi\|_2, \quad \forall \varphi \in H^2(\Omega) \cap H_0^1(\Omega).$$

Define a one-to-one operator  $I_h^* : S_{0h} \rightarrow S_h^*$  by

$$I_h^*\varphi = \sum_{z \in Z_h} \varphi(z)\chi_z, \quad \forall \varphi \in S_{0h}. \tag{4}$$

It has the following approximation property [27]

$$\|\varphi - I_h^*\varphi\|_{0,q} \leq Ch|\varphi|_{1,q,h}, \quad \forall \varphi \in S_{0h}, \quad 1 < q < \infty.$$

In the finite volume discretization, we require the number of dual element should equal to the number of unknowns to obtain a unique approximate solution. For  $P_1$ -nonconforming quadrilateral element, the basis functions are corresponding to the vertices while continuous at the midpoints of the partition. So the standard finite volume scheme of problem (2) can read, finding  $\bar{u}_h = \sum_{z_i \in Z_h^{in}} \bar{u}_{z_i} \phi_{z_i} \in S_{0h}$ , such that

$$-\int_{\partial V_{z_i}} \frac{\partial \bar{u}_h}{\partial n} ds + \int_{V_{z_i}} f(\bar{u}_h) dx dy = \int_{V_{z_i}} g dx dy, \quad \forall z_i \in Z_h^{in}. \tag{5}$$

For convenience, we now define the finite volume scheme with interpolated coefficients, finding  $u_h = \sum_{z_i \in Z_h^{in}} u_{z_i} \phi_{z_i} \in S_{0h}$ , such that

$$-\int_{\partial V_{z_i}} \frac{\partial u_h}{\partial n} ds + \int_{V_{z_i}} J_h f(u_h) dx dy = \int_{V_{z_i}} g dx dy, \quad \forall z_i \in Z_h^{in}, \tag{6}$$

where  $J_h f(u_h) = \sum_{z_i \in Z_h^{in}} f(u_{z_i}) \phi_{z_i}$ .

Obviously, the nonlinear systems of FVM with interpolated coefficients (6) is simpler than that of the standard FVM (5) (or FEM) for the semilinear elliptic problems. If we use the Newton (or Newton-like) iteration method and  $P_1$ -nonconforming quadrilateral element to solve equations (6), it is easy to calculate its Jacobian matrix and stiffness matrix.

### 3 Preliminaries and Lemmas

Below we shall presume that the exact solution  $u$  of problem (1) is sufficiently smooth for our purpose. Next we introduce some bilinear forms and lemmas in this section. Defining

$$a(u, I_h^* \varphi_h) = - \sum_{z \in Z_h} \varphi_h(z) \int_{\partial V_z \setminus \partial T_h} \frac{\partial u}{\partial n} ds, \quad \forall \varphi_h \in S_{0h},$$

$$(u, I_h^* \varphi_h) = \sum_{z \in Z_h} \varphi_h(z) \int_{V_z} u dx dy, \quad \forall \varphi_h \in S_{0h},$$

and taking  $V = V_z$ , then problem (2) is rewritten as follows

$$a(u, I_h^* \varphi_h) + (f(u), I_h^* \varphi_h) = (g, I_h^* \varphi_h), \quad \forall \varphi_h \in S_{0h}. \tag{7}$$

Similarly, equation (6) is equivalent to finding  $u_h \in S_{0h}$ , such that

$$a(u_h, I_h^* \varphi_h) + (J_h f(u_h), I_h^* \varphi_h) = (g, I_h^* \varphi_h), \quad \forall \varphi_h \in S_{0h}. \tag{8}$$

Assume that  $T_h$  is a quasi-uniform trapezoid partition (see Fig. 2), the following two lemmas are suitable for the usual trapezoid mesh with rectangular control volumes. In terms of properties of interpolation and the bilinear form  $a(\cdot, \cdot)$ , we have

#### Lemma 3.1

$$a(\varphi_h, I_h^* \varphi_h) = |\varphi_h|_1^2, \quad \forall \varphi_h \in S_{0h}, \tag{9}$$

$$a(u_h - I_h u, I_h^* \varphi_h) \leq Ch \|u\|_2 |\varphi_h|_1, \quad \forall u \in H^2(\Omega) \cap H_0^1(\Omega), \varphi_h \in S_{0h}. \tag{10}$$

*Proof* For all  $\varphi_h \in S_{0h}$ , we can write it as follows

$$\varphi_h|_\tau = u_1 \phi_1 + u_2 \phi_2 + u_3 \phi_3 + u_4 \phi_4,$$

where  $u_k$  denotes the coefficient of the basis function  $\phi_k$ ,  $k = 1, 2, 3, 4$ . So we have

$$|\varphi_h|_1^2 = \sum_{\tau \in T_h} |\varphi_h|_{1,\tau}^2 = \sum_{\tau \in T_h} \int_\tau \left( \frac{\partial \varphi_h}{\partial x} \right)^2 dx dy + \int_\tau \left( \frac{\partial \varphi_h}{\partial y} \right)^2 dx dy = \sum_{\tau \in T_h} (\alpha_1 + \alpha_2),$$

where

$$\begin{aligned}\alpha_1 &= \int_{\tau} \left( \frac{\partial \varphi_h}{\partial x} \right)^2 dx dy = \int_{\tau} \frac{1}{h_{x_i}^2} (u_2 + u_3 - u_1 - u_4)^2 dx dy \\ &= \frac{h_{y_j}}{h_{x_i}} (u_2 + u_3 - u_1 - u_4)^2, \\ \alpha_2 &= \int_{\tau} \left( \frac{\partial \varphi_h}{\partial y} \right)^2 dx dy = \int_{\tau} \frac{1}{h_{y_j}^2} (u_3 + u_4 - u_1 - u_2)^2 dx dy \\ &= \frac{h_{x_i}}{h_{y_j}} [u_3 + u_4 - u_1 - u_2 - \theta(u_1 - u_2 - u_3 + u_4)]^2.\end{aligned}$$

On the other hand, we have

$$\begin{aligned}a(\varphi_h, I_h^* \varphi_h) &= - \sum_{z \in Z_h} \varphi_h(z) \int_{\partial V_z \setminus \partial T_h} \frac{\partial \varphi_h}{\partial n} ds \\ &= - \sum_{\tau \in T_h} \sum_{i=1}^4 \varphi_h(z_i) \int_{\partial V_{z_i} \cap \tau} \frac{\partial \varphi_h}{\partial n} ds \\ &= - \sum_{\tau \in T_h} [\varphi_h(z_1) \beta_1 + \varphi_h(z_2) \beta_2 + \varphi_h(z_3) \beta_3 + \varphi_h(z_4) \beta_4],\end{aligned}$$

where

$$\begin{aligned}\beta_1 &= \int_{\partial V_{z_1} \cap \tau} \frac{\partial \varphi_h}{\partial n} ds = \frac{h_{y_j}}{2h_{x_i}} (u_2 + u_3 - u_1 - u_4) \\ &\quad + \frac{h_{x_i}}{2h_{y_j}} (1 + \theta) [u_3 + u_4 - u_1 - u_2 + \theta(u_2 + u_3 - u_1 - u_4)], \\ \beta_2 &= \int_{\partial V_{z_2} \cap \tau} \frac{\partial \varphi_h}{\partial n} ds = \frac{h_{y_j}}{2h_{x_i}} (u_1 + u_4 - u_2 - u_3) \\ &\quad + \frac{h_{x_i}}{2h_{y_j}} (1 - \theta) [u_3 + u_4 - u_1 - u_2 + \theta(u_2 + u_3 - u_1 - u_4)], \\ \beta_3 &= \int_{\partial V_{z_3} \cap \tau} \frac{\partial \varphi_h}{\partial n} ds = \frac{h_{y_j}}{2h_{x_i}} (u_1 + u_4 - u_2 - u_3) \\ &\quad + \frac{h_{x_i}}{2h_{y_j}} (1 + \theta) [u_1 + u_2 - u_3 - u_4 + \theta(u_1 + u_4 - u_2 - u_3)], \\ \beta_4 &= \int_{\partial V_{z_4} \cap \tau} \frac{\partial \varphi_h}{\partial n} ds = \frac{h_{y_j}}{2h_{x_i}} (u_2 + u_3 - u_1 - u_4) \\ &\quad + \frac{h_{x_i}}{2h_{y_j}} (1 - \theta) [u_1 + u_2 - u_3 - u_4 + \theta(u_1 + u_4 - u_2 - u_3)]\end{aligned}$$



and

$$\begin{aligned} \varphi_h(z_1) &= \frac{1}{2}(3u_1 + u_2 - u_3 + u_4) + \frac{\theta}{2}(u_1 + u_4 - u_2 - u_3), \\ \varphi_h(z_2) &= \frac{1}{2}(u_1 + 3u_2 + u_3 - u_4) + \frac{\theta}{2}(u_2 + u_3 - u_1 - u_4), \\ \varphi_h(z_3) &= \frac{1}{2}(-u_1 + u_2 + 3u_3 + u_4) + \frac{\theta}{2}(u_1 + u_4 - u_2 - u_3), \\ \varphi_h(z_4) &= \frac{1}{2}(u_1 - u_2 + u_3 + 3u_4) + \frac{\theta}{2}(u_2 + u_3 - u_1 - u_4). \end{aligned}$$

From above equalities, we obtain

$$\begin{aligned} \alpha_1 + \alpha_2 &= -[\varphi_h(z_1)\beta_1 + \varphi_h(z_2)\beta_2 + \varphi_h(z_3)\beta_3 + \varphi_h(z_4)\beta_4] \\ &= \frac{h_{y_j}}{h_{x_i}}(u_2 + u_3 - u_1 - u_4)^2 + \frac{h_{x_i}}{h_{y_j}}[u_3 + u_4 - u_1 - u_2 - \theta(u_1 - u_2 - u_3 + u_4)]^2. \end{aligned}$$

The desired result (9) is derived from above formulations. From [27, 36] we also have (10). □

*Remark 3.1* From [36, 41], the following result is classical for the semilinear elliptic equation (1) by using  $Q_1$ -conforming rectangular element, i.e.,

$$a(\varphi_h, \tilde{I}_h^* \varphi_h) \geq \frac{1}{2} |\varphi_h|_1^2, \quad \forall \varphi_h \in \tilde{S}_{0h},$$

where  $\tilde{S}_{0h}$  is the piecewise bilinear finite element space over the rectangular partition and  $\tilde{I}_h^* : C(\Omega) \rightarrow S_h^*$  is the interpolation operator correspondingly. From equation (9), we know that  $a(\cdot, \cdot)$  has better coercivity and stability for  $P_1$ -nonconforming rectangular element.

*Remark 3.2* In fact, for the general quadrilateral mesh with two types of control volumes in Fig. 3, if we use  $P_1$ -nonconforming quadrilateral FVM to solve the semilinear elliptic equation (1), then we can obtain the same properties of bilinear form  $a(\cdot, \cdot)$  by the symbolic computation and the similar technique in [27, 36], i.e., (9) and (10) hold.

Form [16, 27], we have following useful lemma.

**Lemma 3.2** *The semi-norm  $|\cdot|_1$  and the norm  $\|\cdot\|_1$  are equivalent in the space  $S_{0h}$ , that is, there exists positive constants  $C_1$  and  $C_2$ , such that*

$$C_1 |\varphi_h|_1 \leq \|\varphi_h\|_1 \leq C_2 |\varphi_h|_1, \quad \forall \varphi_h \in S_{0h}.$$

**Lemma 3.3** *For the quasi-uniform rectangular mesh, the operator  $I_h^*$  has following properties*

$$\int_{\tau} I_h^* v_h dx dy = \int_{\tau} v_h dx dy, \quad \forall v_h \in S_{0h}, \quad \forall \tau \in T_h, \tag{11}$$

$$\int_{z_k z_{k+1}} I_h^* v_h ds = \int_{z_k z_{k+1}} v_h ds, \quad \forall v_h \in S_{0h}, \quad \forall \tau \in T_h, \tag{12}$$

$$\|v_h - I_h^* v_h\|_{0,p,\tau} \leq Ch \|v_h\|_{1,p,\tau}, \quad \forall v_h \in S_{0h}, \forall \tau \in T_h, 1 < p < \infty. \tag{13}$$

*Proof* Consider  $\tau \in T_h$  (as in Fig. 4), where  $z_5 = z_1$  and  $\theta = 0$ . For all  $v_h \in S_{0h}$ , we have

$$v_h|_\tau = u_1\phi_1 + u_2\phi_2 + u_3\phi_3 + u_4\phi_4$$

and

$$\begin{aligned} \int_\tau I_h^* v_h dx dy &= \frac{h_{x_i} h_{y_j}}{4} [v_h(z_1) + v_h(z_2) + v_h(z_3) + v_h(z_4)] \\ &= \frac{h_{x_i} h_{y_j}}{4} (2u_1 + 2u_2 + 2u_3 + 2u_4) \\ &= \frac{h_{x_i} h_{y_j}}{2} (u_1 + u_2 + u_3 + u_4), \\ \int_\tau v_h dx dy &= \int_\tau (u_1\phi_1 + u_2\phi_2 + u_3\phi_3 + u_4\phi_4) dx dy \\ &= \frac{h_{x_i} h_{y_j}}{2} (u_1 + u_2 + u_3 + u_4). \end{aligned}$$

The equation (11) is derived from above two equalities.

On one hand, for  $k = 1$  and  $k = 3$ , we have

$$\begin{aligned} \int_{z_k z_{k+1}} v_h ds &= \int_{z_k z_{k+1}} (u_1\phi_1 + u_2\phi_2 + u_3\phi_3 + u_4\phi_4) ds = (u_k + u_{k+1})h_{x_i}, \\ \int_{z_k z_{k+1}} I_h^* v_h ds &= \frac{h_{x_i}}{2} [v_h(z_k) + v_h(z_{k+1})] = \frac{h_{x_i}}{2} (2u_k + 2u_{k+1}) = (u_k + u_{k+1})h_{x_i}. \end{aligned}$$

On the other hand, for  $k = 2$  and  $k = 4$ , we have

$$\begin{aligned} \int_{z_k z_{k+1}} v_h ds &= \int_{z_k z_{k+1}} (u_1\phi_1 + u_2\phi_2 + u_3\phi_3 + u_4\phi_4) ds = (u_k + u_{k+1})h_{y_j}, \\ \int_{z_k z_{k+1}} I_h^* v_h ds &= \frac{h_{y_j}}{2} [v_h(z_k) + v_h(z_{k+1})] = \frac{h_{y_j}}{2} (2u_k + 2u_{k+1}) = (u_k + u_{k+1})h_{y_j}, \end{aligned}$$

where  $u_5 = u_1$ . Equation (12) is derived from above four equalities. □

Apply the similar technique in [7, 27], we also obtain inequality (13).

*Remark 3.3* If we use the trapezoidal mesh with rectangular control volumes to instead of rectangular mesh in Fig. 2, equation (11) can rewrite as

$$\left| \int_\tau I_h^* v_h dx dy - \int_\tau v_h dx dy \right| \leq Ch^2 \|v_h\|_{1,\tau}, \quad \forall v_h \in S_{0h}, \tau \in T_h. \tag{14}$$

For all  $\tau \in T_h$  as in Fig. 4, we have

$$v_h|_\tau = u_1\phi_1 + u_2\phi_2 + u_3\phi_3 + u_4\phi_4.$$

By simple computation, we obtain

$$\begin{aligned} \int_{\tau} I_h^* v_h dx dy &= \frac{h_{x_i} h_{y_j}}{4} [v_h(z_1)(1 + \theta) + v_h(z_2) + v_h(z_3) + v_h(z_4)(1 - \theta)] \\ &= \frac{h_{x_i} h_{y_j}}{4} [(2 + \theta + \theta^2)u_1 + (2 + \theta - \theta^2)u_2 + (2 - \theta - \theta^2)u_3 \\ &\quad + (2 - \theta + \theta^2)u_4]. \\ \int_{\tau} v_h dx dy &= \int_{\tau} (u_1 \phi_1 + u_2 \phi_2 + u_3 \phi_3 + u_4 \phi_4) dx dy \\ &= h_{x_i} h_{y_j} \left[ \frac{3 + \theta}{6} (u_1 + u_2) + \frac{3 - \theta}{6} (u_3 + u_4) \right]. \end{aligned}$$

By combining of these results, we obtain

$$\begin{aligned} &\left| \int_{\tau} I_h^* v_h dx dy - \int_{\tau} v_h dx dy \right| \\ &= \frac{h_{x_i} h_{y_j}}{4} \left| \theta^2 (u_1 + u_4 - u_2 - u_3) + \frac{\theta}{3} (u_1 + u_2 - u_3 - u_4) \right| \\ &= \frac{h_{x_i} h_{y_j}}{4} \left| \frac{2\theta^2}{3} (u_1 + u_4 - u_2 - u_3) + \frac{\theta}{3} [(1 + \theta)(u_1 - u_3) + (1 - \theta)(u_2 - u_4)] \right| \\ &\leq \frac{h^2}{4} \left\{ \frac{8\theta^4}{9} (u_1 + u_4 - u_2 - u_3)^2 + \frac{2\theta^2}{9} [(1 + \theta)(u_1 - u_3) + (1 - \theta)(u_2 - u_4)]^2 \right\}^{\frac{1}{2}} \\ &\leq Ch^2 \{ (u_1 + u_4 - u_2 - u_3)^2 + [(1 + \theta)(u_1 - u_3) + (1 - \theta)(u_2 - u_4)]^2 \}^{\frac{1}{2}} \\ &= Ch^2 |v_h|_{1,\tau} \leq Ch^2 \|v_h\|_{1,\tau}. \end{aligned}$$

By symbolic computation, we have the same result (12) for the trapezoidal mesh with rectangular control volumes. Here

$$\begin{aligned} \int_{z_1 z_2} v_h ds &= \int_{z_1 z_2} (u_1 \phi_1 + u_2 \phi_2 + u_3 \phi_3 + u_4 \phi_4) ds = (u_1 + u_2)(1 + \theta)h_{x_i}, \\ \int_{z_1 z_2} I_h^* v_h ds &= \frac{(1 + \theta)h_{x_i}}{2} [v_h(z_1) + v_h(z_2)] = \frac{(1 + \theta)h_{x_i}}{2} (2u_1 + 2u_2) = \int_{z_1 z_2} v_h ds, \\ \int_{z_2 z_3} v_h ds &= \int_{z_2 z_3} (u_1 \phi_1 + u_2 \phi_2 + u_3 \phi_3 + u_4 \phi_4) ds \\ &= (u_2 + u_3) \sqrt{h_{y_j}^2 + 4\theta^2 h_{x_i}^2}, \\ \int_{z_2 z_3} I_h^* v_h ds &= \frac{\sqrt{h_{y_j}^2 + 4\theta^2 h_{x_i}^2}}{2} [v_h(z_2) + v_h(z_3)] = \frac{\sqrt{h_{y_j}^2 + 4\theta^2 h_{x_i}^2}}{2} (2u_2 + 2u_3) \\ &= \int_{z_2 z_3} v_h ds, \end{aligned}$$

$$\int_{z_3z_4} v_h ds = \int_{z_3z_4} (u_1\phi_1 + u_2\phi_2 + u_3\phi_3 + u_4\phi_4) ds = (u_3 + u_4)(1 - \theta)h_{x_i},$$

$$\int_{z_3z_4} I_h^* v_h ds = \frac{(1 - \theta)h_{x_i}}{2} [v_h(z_3) + v_h(z_4)] = \frac{(1 - \theta)h_{x_i}}{2} (2u_3 + 2u_4) = \int_{z_3z_4} v_h ds,$$

$$\int_{z_4z_1} v_h ds = \int_{z_4z_1} (u_1\phi_1 + u_2\phi_2 + u_3\phi_3 + u_4\phi_4) ds = (u_4 + u_1)h_{y_j},$$

$$\int_{z_4z_1} I_h^* v_h ds = \frac{h_{y_j}}{2} [v_h(z_4) + v_h(z_1)] = \frac{h_{y_j}}{2} (2u_4 + 2u_1) = \int_{z_4z_1} v_h ds.$$

Moreover, we use inequality (14) and apply the similar technique in [7, 27], and also obtain inequality (13) for the trapezoidal mesh with rectangular control volumes.

It is pointed out that we can obtain the similar results (12), (13) and (14) by using symbolic computation on the general quadrilateral mesh for  $P_1$ -nonconforming quadrilateral FVM with two types of control volumes.

By using the similar technique in [7, 27], we also have the following result.

**Lemma 3.4** *Assume  $v, w$  are sufficiently smooth functions. Let  $I_h w \in S_{0h}$  be the interpolation of  $w$ , then*

$$|(v \cdot (w - I_h w), \varphi_h)| \leq Ch^2 \|w\|_{2,p} \|\varphi_h\|_{1,p'}, \quad \forall \varphi_h \in S_{0h} \tag{15}$$

for  $\frac{1}{p} + \frac{1}{p'} = 1, 1 < p \leq \infty$ .

**Lemma 3.5** *Assume  $w \in H^2(\Omega) \cap H_0^1(\Omega)$ , then there exists a positive constant  $C$  independent of the mesh size  $h$ , such that*

$$|(w - I_h w, I_h^* \varphi_h)| \leq Ch^2 \|w\|_2 \|\varphi_h\|_1, \quad \forall \varphi_h \in S_{0h}. \tag{16}$$

*Proof* Using Lemma 3.4 and the Schwartz inequality, we obtain

$$\begin{aligned} |(w - I_h w, \varphi_h - I_h^* \varphi_h)| &\leq \sum_{\tau \in T_h} \int_{\tau} |w - I_h w| |\varphi_h - I_h^* \varphi_h| dx dy \\ &\leq \sum_{\tau \in T_h} C_{\tau} h^3 \|w\|_{2,\tau} \|\varphi_h\|_{1,\tau} \leq Ch^3 \|w\|_2 \|\varphi_h\|_1. \end{aligned} \tag{17}$$

By using (17) and (15) with  $v \equiv 1$  and  $p = 2$ , we get the desired result (16). □

### 4 Error Estimates

In this section, we provide some error estimates for the finite volume scheme (6). Firstly we introduce an auxiliary bilinear form

$$A(u; w, I_h^* \varphi_h) = a(w, I_h^* \varphi_h) + (f'(u)w, I_h^* \varphi_h),$$

where  $u$  is the exact solution of problem (2). For the auxiliary bilinear form  $A(u; \cdot, \cdot)$ , we have following positive definite properties.

**Lemma 4.1** For  $u \in H_0^1(\Omega)$ ,  $A(u; w_h, I_h^* w_h)$  is positive definite for sufficiently small  $h$ , i.e., there exists a positive constant  $\gamma$ , such that

$$A(u; w_h, I_h^* w_h) \geq \gamma(u, f) \|w_h\|_1^2. \tag{18}$$

*Proof* We rewrite  $A(u; w_h, I_h^* w_h)$  as follows

$$A(u; w_h, I_h^* w_h) = a(w_h, I_h^* w_h) + (f'(u)w_h, w_h) - (f'(u)w_h, w_h - I_h^* w_h). \tag{19}$$

From Lemmas 3.1 and 3.2, we have

$$a(w_h, I_h^* w_h) \geq C_1 \|w_h\|_1^2. \tag{20}$$

Note that  $f'(s) > 0$  and let  $C_2 = \inf_{z \in \Omega} f'(u(z))$ , then we have

$$(f'(u)w_h, w_h) \geq C_2 \|w_h\|_0^2 \geq 0. \tag{21}$$

In terms of (11) in Lemma 3.3, Remarks 3.1 and 3.2, we obtain

$$\begin{aligned} |(f'(u)w_h, w_h - I_h^* w_h)| &= \left| \sum_{\tau \in T_h} \int_{\tau} f'(u)w_h(w_h - I_h^* w_h) dx dy \right| \\ &\leq \sum_{\tau \in T_h} \left[ \left| \int_{\tau} (f'(u)w_h - C_{\tau})(w_h - I_h^* w_h) dx dy \right| + Ch^2 \|w_h\|_{1,\tau}^2 \right] \\ &\leq \sum_{\tau \in T_h} [C_3 h |f'(u)w_h|_{1,\tau} h |w_h|_{1,\tau} + Ch^2 \|w_h\|_{1,\tau}^2] \\ &\leq \max_{\Omega} (|f''(u)\nabla u|, |f'(u)|) \sum_{\tau \in T_h} C_4 h^2 \|w_h\|_{1,\tau}^2 + Ch^2 \|w_h\|_1^2 \\ &\leq C_5 h^2 \|w_h\|_1^2, \end{aligned} \tag{22}$$

where  $C_{\tau}$  is the value of  $f'(u)w_h$  at the center point in  $\tau \in T_h$ . Using (20), (21) and (22), we obtain

$$A(u; w_h, I_h^* w_h) \geq C_1 \|w_h\|_1^2 - C_5 h^2 \|w_h\|_1^2 = (C_1 - C_5 h^2) \|w_h\|_1^2,$$

which implies the desired result (18) for sufficiently small  $h$ . □

Next we derive the main result of this section.

**Theorem 4.1** Assume  $u \in H^2(\Omega) \cap H_0^1(\Omega)$  is the solution of problem (1) and  $T_h$  is quasi-uniform rectangular or trapezoidal partition of domain  $\Omega$ , then the approximate solution  $u_h \in S_{0h}$  of FVM with interpolated coefficients (6) converges to the exact solution  $u$  and has the following estimate

$$\|u - u_h\|_1 \leq C(u, f)h \tag{23}$$

for sufficiently small  $h$ .

*Proof* Subtracting (8) from (7), we obtain the following error equation

$$a(u - u_h, I_h^* \varphi_h) + (f(u) - J_h f(u_h), I_h^* \varphi_h) = 0. \tag{24}$$

Define

$$f(u) - J_h f(u_h) = (f(u) - J_h f(u)) + J_h(f(u) - f(u_h)) = \lambda_1 + \lambda_2, \tag{25}$$

where  $\lambda_1 = f(u) - J_h f(u)$ . Next we analyze the function  $f(u) - J_h f(u_h)$ . By using Taylor expansion in  $\tau \in T_h$ , we have

$$\begin{aligned} \lambda_2 &= J_h(f(u) - f(u_h)) = \sum_{z \in Z_h(\tau)} (f(u(z)) - f(u_h(z))) \phi_z \\ &\leq f'(u)(I_h u - u_h) + \delta_1 \max_{\tau} |I_h u - u_h| + \delta_2 \max_{\tau} |I_h u - u_h|^2 \\ &= f'(u)(I_h u - u_h) + \lambda_3, \end{aligned} \tag{26}$$

where

$$\begin{aligned} \lambda_3 &= \delta_1 \max_{\tau} |I_h u - u_h| + \delta_2 \max_{\tau} |I_h u - u_h|^2, \\ \delta_1 &= C \max_{z', z'' \in \tau} |f'(u(z')) - f'(u(z''))| = o(h), \\ \delta_2 &= \frac{1}{2} f''(\xi) = o(1). \end{aligned}$$

Substituting (26) into (24), we have

$$A(u; u_h - I_h u, I_h^* \varphi_h) = a(u - I_h u, I_h^* \varphi_h) + (\lambda_1 + \lambda_3, I_h^* \varphi_h).$$

Letting  $\zeta = u_h - I_h u \in S_{0h}$  and taking  $\varphi_h = \zeta$ , from Lemmas 3.5 and 4.1, we obtain

$$\gamma \|\zeta\|_1^2 \leq Ch \|\zeta\|_1 + C(h \|\zeta\|_{0,\infty} + \|\zeta\|_{0,\infty}^2) \|\zeta\|_{0,1}.$$

Recalling for Bramble [3], that

$$\|\zeta\|_{0,\infty} \leq C |\ln h|^{1/2} \|\nabla \zeta\| \leq C |\ln h|^{1/2} \|\zeta\|_1$$

hold for all  $\zeta \in S_{0h}$  and using the well know Sobolev inequality

$$\|v\|_{0,p} \leq C \|v\|_1, \quad \forall 1 \leq p < \infty,$$

we get

$$\gamma \|\zeta\|_1^2 \leq Ch \|\zeta\|_1 + C(h |\ln h|^{1/2} \|\zeta\|_1 + |\ln h| \|\zeta\|_1^2) \|\zeta\|_1.$$

Omitting the common factor  $\|\zeta\|_1$ , we have

$$\gamma \|\zeta\|_1 \leq Ch + Ch |\ln h|^{1/2} \|\zeta\|_1 + C |\ln h| \|\zeta\|_1^2 \tag{27}$$

for sufficiently small  $h$ .

Omitting the second term of the right-side of (27), we get

$$\|\zeta\|_1 \leq C_1 h + C_2 |\ln h| \|\zeta\|_1^2. \tag{28}$$

Next we adopt a continuity argument by imitating the method in [17] and prove

$$\|\zeta\|_1 \leq \|I_h u - u_h\| \leq 2C_1 h. \tag{29}$$

For all  $b \in [0, 1]$ , considering the following auxiliary semilinear elliptic problems ( $P^b$ ): Find  $u^b$  such that

$$\begin{cases} -\Delta u^b + bf(u^b) = bg & \text{in } \Omega, \\ u^b = 0 & \text{on } \partial\Omega. \end{cases} \tag{30}$$

Obviously, when  $b = 1$ , this is the original problem (1). And when  $b = 0$ , we have the exact solution  $u^0 = 0$ . We shall assume the following condition on  $\Omega = (0, 1) \times (0, 1)$ .  $\forall b \in [0, 1]$ , there exist a solution  $u^b$  of problem ( $P^b$ ) and a positive constant  $\xi$ , such that the set

$$N_\xi = \left\{ \omega \mid \omega \in H^2(\Omega) \cap H_0^1(\Omega), \max_\Omega |u - \omega| < \xi \right\}$$

is some neighborhood of the exact solution  $u$  of problem (1).

We approximate the problem ( $P^b$ ): Find  $u_h^b \in S_{0h}$ , such that

$$a(u_h^b, I_h^* v_h) + b(J_h f(u_h^b), I_h^* v_h) = b(g, I_h^* v_h), \quad \forall v_h \in S_{0h}. \tag{31}$$

We intend to show that ( $P_h^b$ ) is solvable. For each  $h$ , we define the set  $F_h \subset [0, 1]$  by

$$F_h = \{b \in [0, 1] \mid (P_h^b) \text{ has a solution } u_h^b \in N_\xi \text{ and } \|I_h u^b - u_h^b\|_1 \leq 2C_1 h \text{ holds}\},$$

where  $C_1$  is the constant appearing in (28). Next we show that the set  $F_h$  has the following properties.

- (i)  $F_h$  is not empty. In fact, for  $b = 0$ ,  $u^b = 0$  and  $u_h^b = 0$  are the solutions of continuous and the discrete problems, respectively.
- (ii)  $F_h$  is open in  $[0, 1]$ . If  $b \in F_h$ , then ( $P_h^b$ ) is solvable. Using the monotonicity condition, we obtain the solvability of ( $P_h^{\tilde{b}}$ ) for all points  $\tilde{b}$  in a neighborhood of  $b$ . By the implicit function theorem,  $u_h^{\tilde{b}}$  depends continuously on  $\tilde{b}$ . Thus properly shorten the neighborhood such that the strict inequality  $\|I_h u^b - u_h^b\|_1 \leq 2C_1 h$  and  $u_h^b \in N_\xi$  is still valid and we have  $\tilde{b} \in F_h$  for these  $\tilde{b}$ .
- (iii)  $F_h$  is closed. Let  $b(j) \in F_h$  and  $b(j) \rightarrow b$ ,  $j \rightarrow \infty$ . Since  $u_h^{b(j)} \in N_\xi$ , there is a cluster point  $u_h^b$  which is the unique solution of ( $P_h^b$ ) and satisfies  $\|I_h u^b - u_h^b\|_1 \leq 2C_1 h$ . Recalling for (28), we conclude

$$\|I_h u^b - u_h^b\|_1 \leq C_1 h + 4C_2 C_1^2 |\ln h| h^2 \leq C_1 (1 + 4C_1 C_2 |\ln h|) h.$$

Then for sufficiently small  $h$ , we have  $4C_1 C_2 |\ln h| h \leq 1$  and  $\|I_h u^b - u_h^b\|_1 \leq 2C_1 h$ , i.e., the strict inequality holds.

Form (i)–(iii), we know that for sufficiently small  $h$ , the set  $F_h$  is not empty, closed and open with respect to  $b$  and thus must coincide with  $[0, 1]$ . Note that for  $b = 1$ , ( $P_h^1$ ) is solvable. We prove that (29) and  $u_h \in N_\xi$  hold for appropriately small  $h$ .

Finally, the desired result (23) follows from (29) and the approximation property

$$\|u - I_h u\|_1 \leq Ch \|u\|_2. \tag{32}$$

□

### 5 Superconvergence of Derivative

In this section we show superconvergence of derivative of the finite volume scheme (6) on the rectangular mesh. First we give the superclose property of derivative for  $I_h u$ .

**Lemma 5.1** [20, 25] *For sufficiently smooth function  $u$ , let  $I_h u \in S_{0h}$  be the interpolation of  $u$  on the rectangular mesh, then we have superclose property*

$$|\nabla(u - I_h u)| = o(h^2 |\ln h|) \tag{32}$$

for the center points in all  $\tau \in T_h$ .

For the FVM with interpolated coefficients (6) on the rectangular mesh for the semilinear elliptic problem, we have the following superconvergence results of derivative.

**Theorem 5.1** *Assume that  $u \in W^\infty_3(\Omega)$ ,  $f'(s) > 0$  for  $s \in (-\infty, +\infty)$  and  $f''(s)$  is continuous with respect to  $s$ , and  $g \in W^1_0(\Omega)$ . Assume that the rectangular partition  $T_h$  of  $\Omega$  is the quasi uniform. Then the FVM with interpolated coefficients (6) for the semilinear elliptic problem has superconvergence of derivative, i.e.,*

$$|\nabla(u - u_h)| = o(h^2 |\ln h|)$$

hold for all center points of  $\tau \in T_h$ .

*Proof* Choosing  $v = v_h \in S_{0h}$  in (7), we obtain

$$a(u, v_h) + (f(u), v_h) = (g, v_h). \tag{33}$$

Subtracting (8) from (33), we have

$$\begin{aligned} a(u - u_h, v_h) + a(u, v_h - I_h^* v_h) + a(u_h - u, v_h - I_h^* v_h) + (f(u) - J_h f(u), v_h) \\ + (J_h f(u), v_h - I_h^* v_h) + (J_h(f(u) - f(u_h)), I_h^* v_h) = (g, v_h) - (g, I_h^* v_h). \end{aligned} \tag{34}$$

Let  $\eta = u - I_h u$ ,  $\zeta = u_h - I_h u$ . It follows from (34), (25) and (26) that

$$\begin{aligned} A(u; \zeta, v_h) &= a(\zeta, v_h) + (f'(u)\zeta, v_h) \\ &= a(\eta, v_h) + a(u, v_h - I_h^* v_h) + a(u_h - u, v_h - I_h^* v_h) + (\lambda_1, v_h) \\ &\quad + (J_h f(u), v_h - I_h^* v_h) + (\lambda_3, I_h^* v_h) + (g, I_h^* v_h - v_h). \end{aligned} \tag{35}$$

Recalling [7], we get

$$|a(\eta, v_h)| = \left| \int_\Omega \nabla \eta \nabla v_h dx dy \right| \leq Ch^2 \|u\|_{3,\infty} \|v_h\|_{1,1}. \tag{36}$$

Using Lemma 3.4 with  $p = +\infty$ , we have

$$|(\lambda_1, v_h)| = |(f(u) - J_h f(u), v_h)| \leq Ch^2 \|f(u)\|_{2,\infty} \|v_h\|_{1,1}. \tag{37}$$



In terms of Lemma 3.3 and the trace theorem, we have

$$\begin{aligned}
 |a(u, v_h - I_h^* v_h)| &= \left| \sum_{V \in T_h^*} \left( \int_V \nabla u \nabla v_h dx dy - v_h(z) \int_{\partial V} \frac{\partial u}{\partial n} ds \right) \right| \\
 &= \left| \sum_{V \in T_h^*} \int_{\partial V} \frac{\partial u}{\partial n} (v_h - v_h(z)) ds \right| \\
 &= \left| \sum_{\tau \in T_h} \sum_{i=1}^4 \int_{\partial V_{z_i} \cap \tau} \left( \frac{\partial u}{\partial n} - w_\tau \right) (v_h - I_h^* v_h) ds \right| \\
 &\leq Ch^2 \|u\|_{2,\infty} \|v_h\|_{1,1},
 \end{aligned} \tag{38}$$

where  $w_\tau$  is the value of  $\frac{\partial u}{\partial n}$  at the midpoint on the edge  $z_i z_{i+1}$ ,  $i = 1, 2, 3, 4$ , and  $z_5 = z_1$ . Analogously, we get

$$\begin{aligned}
 |a(u_h - u, v_h - I_h^* v_h)| &= \left| \sum_{\tau \in T_h} \sum_{i=1}^4 \int_{z_i z_{i+1}} \frac{\partial(u_h - u)}{\partial n} (v_h - I_h^* v_h) ds \right| \\
 &\leq Ch \|u_h - u\|_{1,\infty} \|v_h\|_{0,1} \\
 &\leq Ch \|u_h - u\|_{1,\infty} \|v_h\|_{1,1}.
 \end{aligned} \tag{39}$$

Using Lemma 3.3, we obtain the following estimates

$$|(J_h f(u), v_h - I_h^* v_h)| \leq Ch^2 \|f(u)\|_{1,\infty} \|v_h\|_{1,1}, \tag{40}$$

$$|(g, v_h - I_h^* v_h)| \leq Ch^2 \|g\|_{1,\infty} \|v_h\|_{1,1}. \tag{41}$$

Substituting from (36)–(41) into (35), we have

$$A(u; \zeta, v_h) \leq Ch^2 \|v_h\|_{1,1} + Ch \|u_h - u\|_{0,\infty} \|v_h\|_{1,1} + C \|\lambda_3\|_{0,\infty} \|v_h\|_{1,1}.$$

Note that

$$\|u_h - u\|_{0,\infty} \leq \|\eta\|_{0,\infty} + \|\zeta\|_{0,\infty} \leq C(u)h^2 + \|\zeta\|_{0,\infty}$$

and

$$\|\lambda_2\|_{0,\infty} \leq Ch \|\zeta\|_{0,\infty} + Ch \|\zeta\|_{0,\infty}^2,$$

this yields

$$A(u; \zeta, v_h) \leq Ch^2 \|v_h\|_{1,1} + Ch \|\zeta\|_{1,\infty} \|v_h\|_{1,1} + C \|\zeta\|_{1,\infty} \|v_h\|_{1,1}. \tag{42}$$

Choosing  $v_h = G_h$  as the discrete Green function with respect to the bilinear form  $A(u_h; \cdot, \cdot)$ , and noting that  $\|G_h\|_{1,1} \leq |\ln h|$  (see [7]), we get

$$\|\zeta\|_{1,\infty} \leq Ch^2 |\ln h| + Ch \|\zeta\|_{1,\infty} |\ln h| + C \|\zeta\|_{1,\infty}^2 |\ln h|.$$

For sufficiently small  $h$ , omitting the second term of the right-side, we have

$$\|\zeta\|_{1,\infty} \leq Ch^2 |\ln h| + C \|\zeta\|_{1,\infty}^2 |\ln h|. \tag{43}$$

Similarly, we adopt the continuity argument in the proof of Theorem 4.1 and obtain

$$|\nabla\zeta|_{0,\infty} \leq \|\zeta\|_{1,\infty} \leq Ch^2|\ln h|. \quad (44)$$

Using (32) and (44), we obtain

$$|\nabla(u - u_h)| \leq |\nabla(u - I_h u)| + |\nabla\zeta| = |\nabla(u - I_h u)| + o(h^2|\ln h|),$$

i.e.,

$$|\nabla(u - u_h)| = o(h^2|\ln h|),$$

for all the center points of  $\tau \in T_h$ . This completes the proof of the theorem.  $\square$

*Remark 5.1* For  $Q_1$ -conforming rectangular element, if  $I_h u \in \tilde{S}_{0h}$  is the Lagrange interpolation of  $u$ , then the following superclose property [40]

$$|\nabla(u - I_h u)| = o(h^2)$$

holds for the center points for all  $\tau \in T_h$ . Moreover, the similar superconvergence result of derivative in Theorem 5.1 also holds.

## 6 Numerical Experiments

In this section, we present one test problem to illustrate the theoretical results obtained in the previous section. In our numerical experiments, we consider the following semilinear elliptic problem on a unit square domain  $\Omega$  in  $R^2$ :

$$-\Delta u + u^3 = g, \quad \text{in } \Omega, \quad u = 0, \quad \text{on } \partial\Omega \quad (45)$$

where the exact solution is given by

$$u(x, y) = y(1 - x)\sin(x(1 - y)),$$

and the right-hand side function  $g$  is generated by problem (45). Here we use the nonuniform triangulations of  $\Omega$  into quadrilaterals [16]. The quadrilateral meshes are depicted in Fig. 5. Each element is a right trapezoid whose the shape is controlled by a relax parameter  $\theta \in [0, 1]$ , see Fig. 6. Here, for any fixed  $\theta$ , the meshes do not satisfy the nearly parallelogram condition when  $h$  decreases. When  $\theta = 0$ , each element is a rectangle. When  $\theta = 1$ , each element is a right triangle.

Firstly, we apply  $P_1$ -nonconforming quadrilateral FVM to the test problem (45) based on nonoverlapping control volume ( $I$ ) and overlapping control volume ( $II$ ) in Fig. 3, respectively. And then we use  $P_1$ -nonconforming quadrilateral FEM to the test problem (45). Numerical results on the trapezoidal meshes are presented in Tables 1, 2 and 3 in terms of the  $H^1$ -seminorm convergence rates. Here we only present five cases for  $\theta = 0, \frac{1}{4}, \frac{1}{2}, \frac{3}{4}$  and 1. From these tables, we observe that the convergence rates are optimal on these general quadrilateral meshes, which confirms well our theoretical analysis. But the relatively errors  $\frac{|u - u_h|}{|u|}$  of three methods by using  $P_1$ -nonconforming quadrilateral element increase as  $\theta$  increases, respectively.

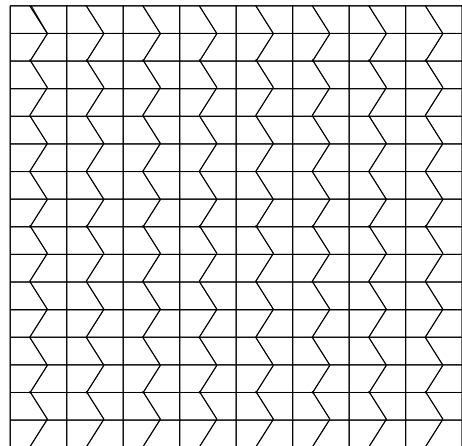
**Table 1** FVM with  $P_1$ -nonconforming quadrilateral element based on nonoverlapping control volume

$N$	$\theta = 0$		$\theta = \frac{1}{4}$		$\theta = \frac{1}{2}$		$\theta = \frac{3}{4}$		$\theta = 1$	
	$\frac{ u-u_h }{ u }$	Rate	$\frac{ u-u_h }{ u }$	Rate	$\frac{ u-u_h }{ u }$	Rate	$\frac{ u-u_h }{ u }$	Rate	$\frac{ u-u_h }{ u }$	Rate
4	2.3883e-1	–	2.4899e-1	–	2.7641e-1	–	3.1922e-1	–	3.7512e-1	–
8	1.1924e-1	1.0032	1.2495e-1	0.9947	1.4099e-1	0.9713	1.6606e-1	0.9428	1.9891e-1	0.9153
16	5.9588e-2	1.0007	6.2512e-2	0.9992	7.0766e-2	0.9945	8.3675e-2	0.9889	1.0059e-1	0.9835
32	2.9790e-2	1.0002	3.1259e-2	0.9999	3.5412e-2	0.9988	4.1907e-2	0.9976	5.0420e-2	0.9965
64	1.4895e-2	1.0000	1.5629e-2	1.0000	1.7709e-2	0.9998	2.0961e-2	0.9995	2.5224e-2	0.9992

**Table 2** FVM with  $P_1$ -nonconforming quadrilateral element based on overlapping control volume

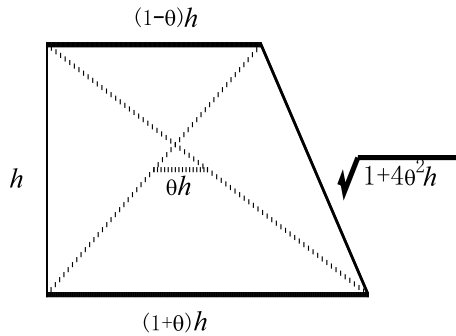
$N$	$\theta = 0$		$\theta = \frac{1}{4}$		$\theta = \frac{1}{2}$		$\theta = \frac{3}{4}$		$\theta = 1$	
	$\frac{ u-u_h }{ u }$	Rate	$\frac{ u-u_h }{ u }$	Rate	$\frac{ u-u_h }{ u }$	Rate	$\frac{ u-u_h }{ u }$	Rate	$\frac{ u-u_h }{ u }$	Rate
4	2.3508e-1	–	2.4722e-1	–	2.7963e-1	–	3.2832e-1	–	3.8870e-1	–
8	1.1876e-1	0.9851	1.2535e-1	0.9797	1.4354e-1	0.9620	1.7100e-1	0.9411	2.0529e-1	0.9210
16	5.9527e-2	0.9964	6.2882e-2	0.9952	7.2194e-2	0.9915	8.6229e-2	0.9877	1.0374e-1	0.9847
32	2.9782e-2	0.9991	3.1466e-2	0.9989	3.6147e-2	0.9980	4.3198e-2	0.9972	5.1991e-2	0.9967
64	1.4894e-2	0.9998	1.5736e-2	0.9997	1.8079e-2	0.9996	2.1608e-2	0.9994	2.6099e-2	0.9993

**Fig. 5** Nonuniform quadrilateral mesh



Secondly, we apply  $Q_1$ -conforming quadrilateral FVM to the test problem (45) based on nonoverlapping control volume ( $I$ ) and overlapping control volume ( $II$ ) in Fig. 3, respectively. And then we use  $Q_1$ -conforming quadrilateral FEM to the test problem (45). Numerical results on the trapezoidal meshes are presented in Tables 4–6 in terms of the  $H^1$ -seminorm convergence rates. In Table 4, we present five cases for  $\theta = 0, \frac{1}{4}, \frac{1}{2}, \frac{3}{4}$  and 1. We observe from Table 4 that the convergence rates are optimal on these general quadrilateral meshes, which confirm our theoretical analysis. In Tables 5–6, we only present five cases for  $\theta = 0, \frac{1}{32}, \frac{1}{16}, \frac{1}{8}$  and  $\frac{1}{4}$ , since numerical results of the last two of these methods are not good as  $\theta \geq \frac{1}{4}$ . We observe from Tables 5–6 that the convergence rates are not optimal on these

**Fig. 6** The shape of quadrilateral element



**Table 3** FEM with  $P_1$ -nonconforming quadrilateral element

$N$	$\theta = 0$		$\theta = \frac{1}{4}$		$\theta = \frac{1}{2}$		$\theta = \frac{3}{4}$		$\theta = 1$	
	$\frac{ u-u_h }{ u }$	Rate	$\frac{ u-u_h }{ u }$	Rate	$\frac{ u-u_h }{ u }$	Rate	$\frac{ u-u_h }{ u }$	Rate	$\frac{ u-u_h }{ u }$	Rate
4	2.3507e-1	–	2.4638e-1	–	2.7643e-1	–	3.2167e-1	–	3.7855e-1	–
8	1.1876e-1	0.9851	1.2476e-1	0.9817	1.4114e-1	0.9667	1.6708e-1	0.9450	2.0002e-1	0.9204
16	5.9527e-2	0.9964	6.2561e-2	0.9959	7.1067e-2	0.9930	8.4194e-2	0.9888	1.0112e-1	0.9840
32	2.9782e-2	0.9991	3.1302e-2	0.9990	3.5573e-2	0.9984	4.2170e-2	0.9975	5.0685e-2	0.9965
64	1.4894e-2	0.9998	1.5653e-2	0.9999	1.7791e-2	0.9997	2.1093e-2	0.9995	2.5356e-2	0.9992

**Table 4** FVM with  $Q_1$ -conforming quadrilateral element based on nonoverlapping control volume

$N$	$\theta = 0$		$\theta = \frac{1}{4}$		$\theta = \frac{1}{2}$		$\theta = \frac{3}{4}$		$\theta = 1$	
	$\frac{ u-u_h }{ u }$	Rate	$\frac{ u-u_h }{ u }$	Rate	$\frac{ u-u_h }{ u }$	Rate	$\frac{ u-u_h }{ u }$	Rate	$\frac{ u-u_h }{ u }$	Rate
4	1.7619e-1	–	1.8098e-1	–	1.9647e-1	–	2.2359e-1	–	2.5768e-1	–
8	8.7787e-2	1.0051	9.0160e-2	1.0046	9.7879e-2	1.0052	1.0988e-1	1.0249	1.2303e-1	1.0666
16	4.3856e-2	1.0012	4.5036e-2	1.0014	4.8874e-2	1.0019	5.4672e-2	1.0071	6.0756e-2	1.0179
32	2.1923e-2	1.0003	2.2512e-2	1.0004	2.4428e-2	1.0005	2.7302e-2	1.0018	3.0283e-2	1.0045
64	1.0961e-2	1.0001	1.1255e-2	1.0001	1.2213e-2	1.0001	1.3647e-2	1.0005	1.5130e-2	1.0011

general quadrilateral meshes and decrease as  $\theta$  increases. Furthermore, the relatively errors  $\frac{|u-u_h|}{|u|}$  of three methods by using  $Q_1$ -conforming quadrilateral element increase similarly as  $\theta$  increases, respectively.

Thirdly, we present numerical results in Tables 7–12 in terms of the  $L^2$ -norm convergence rates. We observe from these tables that the convergence rates are optimal on these general quadrilateral meshes only for  $P_1$ -nonconforming quadrilateral FVM based on nonoverlapping control volume ( $I$ ) and overlapping control volume ( $II$ ) and  $P_1$ -nonconforming quadrilateral FEM, and  $Q_1$ -conforming quadrilateral FVM based on nonoverlapping control volume ( $I$ ). For other two methods, we can not obtain good numerical results as  $\theta \geq \frac{1}{4}$  in Tables 11–12. The convergence rates of the last two of these methods decrease as  $\theta$  increases. Furthermore the relatively errors  $\frac{\|u-u_h\|_0}{\|u\|_0}$  of six methods by using  $P_1$ -nonconforming quadrilateral element and  $Q_1$ -conforming quadrilateral element increase as  $\theta$  increases, respectively. Moreover, we find that the results of FVE (or FEM)

**Table 5** FVM with  $Q_1$ -conforming quadrilateral element based on overlapping control volume

$N$	$\theta = 0$		$\theta = \frac{1}{32}$		$\theta = \frac{1}{16}$		$\theta = \frac{1}{8}$		$\theta = \frac{1}{4}$	
	$\frac{ u-u_h }{ u }$	Rate	$\frac{ u-u_h }{ u }$	Rate	$\frac{ u-u_h }{ u }$	Rate	$\frac{ u-u_h }{ u }$	Rate	$\frac{ u-u_h }{ u }$	Rate
4	1.8057e-1	–	1.8066e-1	–	1.8079e-1	–	1.8131e-1	–	1.8409e-1	–
8	8.8289e-2	1.0322	8.8331e-2	1.0322	8.8439e-2	1.0316	8.8872e-2	1.0286	9.0863e-2	1.0187
16	4.3917e-2	1.0075	4.3940e-2	1.0074	4.4005e-2	1.0070	4.4275e-2	1.0052	4.5468e-2	0.9988
32	2.1931e-2	1.0018	2.1949e-2	1.0014	2.2002e-2	1.0000	2.2220e-2	0.9946	2.3129e-2	0.9752
64	1.0962e-2	1.0005	1.0985e-2	0.9986	1.1053e-2	0.9932	1.1324e-2	0.9752	1.2362e-2	0.9038

**Table 6** FEM with  $Q_1$ -conforming quadrilateral element

$N$	$\theta = 0$		$\theta = \frac{1}{32}$		$\theta = \frac{1}{16}$		$\theta = \frac{1}{8}$		$\theta = \frac{1}{4}$	
	$\frac{ u-u_h }{ u }$	Rate	$\frac{ u-u_h }{ u }$	Rate	$\frac{ u-u_h }{ u }$	Rate	$\frac{ u-u_h }{ u }$	Rate	$\frac{ u-u_h }{ u }$	Rate
4	1.7619e-1	–	1.7644e-1	–	1.7706e-1	–	1.7943e-1	–	1.8889e-1	–
8	8.7787e-2	1.0051	8.8356e-2	0.9978	9.0019e-2	0.9760	9.6322e-2	0.8974	1.1765e-1	0.6830
16	4.3855e-2	1.0012	4.5287e-2	0.9642	4.9318e-2	0.8681	6.2742e-2	0.6184	0.9820e-2	0.2607
32	2.1923e-2	1.0003	2.5044e-2	0.8570	3.2512e-2	0.6015	5.2512e-2	0.2568	0.9571e-2	0.3711
64	1.0961e-2	1.0001	1.6541e-2	0.5960	2.7056e-2	0.2650	5.0358e-2	0.0604	0.9649e-2	–0.012

**Table 7** FVM with  $P_1$ -nonconforming quadrilateral element based on nonoverlapping control volume

$N$	$\theta = 0$		$\theta = \frac{1}{4}$		$\theta = \frac{1}{2}$		$\theta = \frac{3}{4}$		$\theta = 1$	
	$\frac{ u-u_h }{ u }$	Rate	$\frac{ u-u_h }{ u }$	Rate	$\frac{ u-u_h }{ u }$	Rate	$\frac{ u-u_h }{ u }$	Rate	$\frac{ u-u_h }{ u }$	Rate
4	6.5202e-2	–	7.5280e-2	–	1.0452e-1	–	1.6836e-1	–	2.6297e-1	–
8	1.6180e-2	2.0107	1.9475e-2	1.9506	2.9217e-2	1.8388	4.9105e-2	1.7776	7.8978e-2	1.7354
16	4.0630e-3	1.9936	4.9271e-3	1.9828	7.5049e-3	1.9609	1.2756e-2	1.9447	2.0766e-2	1.9272
32	1.0460e-3	1.9576	1.2487e-3	1.9803	1.8770e-3	1.9994	3.9140e-3	1.9977	5.2293e-3	1.9896
64	2.9930e-4	1.8503	3.3409e-4	1.9023	4.6295e-4	2.0195	7.7547e-4	2.0422	1.2796e-3	2.0309

**Table 8** FVM with  $P_1$ -nonconforming quadrilateral element based on overlapping control volume

$N$	$\theta = 0$		$\theta = \frac{1}{4}$		$\theta = \frac{1}{2}$		$\theta = \frac{3}{4}$		$\theta = 1$	
	$\frac{ u-u_h }{ u }$	Rate	$\frac{ u-u_h }{ u }$	Rate	$\frac{ u-u_h }{ u }$	Rate	$\frac{ u-u_h }{ u }$	Rate	$\frac{ u-u_h }{ u }$	Rate
4	5.8302e-2	–	7.6605e-2	–	1.2680e-1	–	2.1466e-1	–	3.3036e-1	–
8	1.4740e-2	1.9839	2.0596e-2	1.8951	3.7260e-2	1.7669	6.6243e-2	1.6962	1.0586e-1	1.6419
16	3.6962e-3	1.9956	5.2518e-3	1.9715	9.7184e-3	1.9388	1.7528e-2	1.9181	2.8414e-2	1.8975
32	9.2977e-4	1.9911	1.3079e-3	2.0056	2.4262e-3	2.0020	4.4100e-3	1.9908	7.1993e-3	1.9807
64	2.4837e-4	1.9044	3.2265e-4	2.0192	5.7964e-4	2.0655	1.0687e-3	2.0449	1.7676e-3	2.0261

with  $P_1$ -nonconforming quadrilateral element are similar to the results of FVE with  $Q_1$ -conforming quadrilateral element. As expected, the errors become smaller as the meshes are refined.

**Table 9** FEM with  $P_1$ -nonconforming quadrilateral element

$N$	$\theta = 0$		$\theta = \frac{1}{4}$		$\theta = \frac{1}{2}$		$\theta = \frac{3}{4}$		$\theta = 1$	
	$\frac{ u-u_h }{ u }$	Rate	$\frac{ u-u_h }{ u }$	Rate	$\frac{ u-u_h }{ u }$	Rate	$\frac{ u-u_h }{ u }$	Rate	$\frac{ u-u_h }{ u }$	Rate
4	5.8301e-2	–	7.4998e-2	–	1.1518e-1	–	1.8540e-1	–	2.8177e-1	–
8	1.4740e-2	1.9839	1.9843e-2	1.9182	3.2922e-2	1.8067	5.5775e-2	1.7330	8.8058e-2	1.6780
16	3.6962e-3	1.9956	5.0363e-3	1.9782	8.5216e-3	1.9491	1.4663e-2	1.9274	2.3488e-2	1.9066
32	9.2977e-4	1.9911	1.2558e-3	2.0038	2.1273e-3	2.0028	3.6834e-3	1.9931	5.9380e-3	1.9838
64	2.4837e-4	1.9044	3.1321e-4	2.0034	5.1284e-4	2.0525	8.9529e-4	2.0406	1.4541e-3	2.0298

**Table 10** FVM with  $Q_1$ -conforming quadrilateral element based on nonoverlapping control volume

$N$	$\theta = 0$		$\theta = \frac{1}{4}$		$\theta = \frac{1}{2}$		$\theta = \frac{3}{4}$		$\theta = 1$	
	$\frac{ u-u_h }{ u }$	Rate	$\frac{ u-u_h }{ u }$	Rate	$\frac{ u-u_h }{ u }$	Rate	$\frac{ u-u_h }{ u }$	Rate	$\frac{ u-u_h }{ u }$	Rate
4	5.1254e-2	–	6.5901e-2	–	9.2076e-2	–	1.2492e-1	–	1.6231e-1	–
8	1.2510e-2	2.0345	1.5988e-2	2.0433	2.2080e-2	2.0601	2.9670e-2	2.0739	3.8447e-2	2.0778
16	3.1072e-3	2.0095	3.9642e-3	2.0119	5.4567e-3	2.0166	7.3133e-3	2.0204	9.4783e-3	2.0202
32	7.7549e-4	2.0024	9.8897e-4	2.0030	1.3602e-3	2.0042	1.8222e-3	2.0048	2.3636e-3	2.0036
64	1.9379e-4	2.0006	2.4711e-4	2.0008	3.3982e-4	2.0010	4.5525e-4	2.0010	5.9080e-4	2.0002

**Table 11** FVM with  $Q_1$ -conforming quadrilateral element based on overlapping control volume

$N$	$\theta = 0$		$\theta = \frac{1}{32}$		$\theta = \frac{1}{16}$		$\theta = \frac{3}{8}$		$\theta = \frac{1}{4}$	
	$\frac{ u-u_h }{ u }$	Rate	$\frac{ u-u_h }{ u }$	Rate	$\frac{ u-u_h }{ u }$	Rate	$\frac{ u-u_h }{ u }$	Rate	$\frac{ u-u_h }{ u }$	Rate
4	2.7044e-2	–	2.8855e-2	–	3.0713e-2	–	3.4931e-2	–	4.4806e-2	–
8	6.1174e-3	2.1443	6.6195e-3	2.1240	7.1292e-3	2.1071	8.2743e-3	2.0778	1.1753e-2	2.0241
16	1.4482e-3	2.0393	1.6167e-3	2.0337	1.7483e-3	2.0278	2.0696e-3	1.9993	3.2522e-3	1.8536
32	3.6974e-4	2.0101	4.0175e-4	2.0087	4.3988e-4	1.9908	5.9398e-4	1.8009	1.4053e-3	1.2105
64	9.2206e-5	2.0025	1.0136e-4	1.9869	1.2925e-4	1.7669	3.1461e-4	0.9169	1.1162e-3	0.3324

**Table 12** FEM with  $Q_1$ -conforming quadrilateral element

$N$	$\theta = 0$		$\theta = \frac{1}{32}$		$\theta = \frac{1}{16}$		$\theta = \frac{3}{8}$		$\theta = \frac{1}{4}$	
	$\frac{ u-u_h }{ u }$	Rate	$\frac{ u-u_h }{ u }$	Rate	$\frac{ u-u_h }{ u }$	Rate	$\frac{ u-u_h }{ u }$	Rate	$\frac{ u-u_h }{ u }$	Rate
4	5.1295e-2	–	5.2526e-2	–	5.4197e-2	–	5.8785e-2	–	7.2364e-2	–
8	1.2705e-2	2.0134	1.2958e-2	2.0192	1.3236e-2	2.0338	1.3959e-2	2.0743	1.7108e-2	2.0806
16	3.1684e-3	2.0036	3.1714e-3	2.0307	3.1400e-3	2.0756	3.9742e-3	1.8124	1.2042e-2	0.5058
32	7.9158e-4	2.0009	7.4859e-4	2.0829	1.0088e-3	1.6381	3.6072e-3	0.1398	1.4301e-2	–0.247
64	1.9786e-4	2.0002	2.5507e-4	1.5533	9.6791e-4	0.0597	3.9956e-3	–0.148	1.5411e-2	–0.108

Finally, we present the superconvergence of derivative of six methods. Here  $E_{Du}$  denotes the mean relative error of derivative of  $u_h$  at center points of the quadrilateral mesh.

**Table 13** Mean relative error of derivative at the central point of partition for  $P_1$ -nonconforming quadrilateral FVM with nonoverlapping control volume

$N$	$\theta = 0$		$\theta = \frac{1}{4}$		$\theta = \frac{1}{2}$		$\theta = \frac{3}{4}$		$\theta = 1$	
	$E_{Du}$	Rate	$E_{Du}$	Rate	$E_{Du}$	Rate	$E_{Du}$	Rate	$E_{Du}$	Rate
4	4.6618e-2	–	1.2343e-1	–	2.0473e-1	–	2.8420e-1	–	3.5022e-1	–
8	1.4235e-2	1.7115	5.8244e-2	1.0835	1.0955e-1	0.9021	1.5158e-1	0.9069	1.8451e-1	0.9246
16	3.6987e-3	1.9443	2.9543e-2	0.9793	5.6957e-2	0.9437	7.9237e-2	0.9358	9.5695e-2	0.9472
32	1.0064e-3	1.8778	1.5060e-2	0.9720	2.9259e-2	0.9610	4.0781e-2	0.9583	4.9267e-2	0.9578
64	3.1655e-4	1.6687	7.6500e-3	0.9724	1.4898e-2	0.9738	2.0769e-2	0.9735	2.5099e-2	0.9730

**Table 14** Mean relative error of derivative at the central point of partition for  $P_1$ -nonconforming quadrilateral FVM with overlapping control volume

$N$	$\theta = 0$		$\theta = \frac{1}{4}$		$\theta = \frac{1}{2}$		$\theta = \frac{3}{4}$		$\theta = 1$	
	$E_{Du}$	Rate	$E_{Du}$	Rate	$E_{Du}$	Rate	$E_{Du}$	Rate	$E_{Du}$	Rate
4	3.6501e-2	–	9.7746e-2	–	1.6695e-1	–	2.5406e-1	–	3.5997e-1	–
8	9.7271e-3	1.9078	4.8802e-2	1.0021	9.1540e-2	0.8670	1.2803e-1	0.9887	1.6610e-1	1.1158
16	2.5840e-3	1.9124	2.5446e-2	0.9395	4.7608e-2	0.9432	6.4667e-2	0.9854	8.1747e-2	1.0228
32	7.1634e-4	1.8509	1.3003e-2	0.9686	2.4361e-2	0.9666	3.2829e-2	0.9781	4.1281e-2	0.9857
64	2.3768e-4	1.5916	6.5917e-3	0.9801	1.2372e-2	0.9775	1.6626e-2	0.9816	2.0903e-2	0.9818

**Table 15** Mean relative error of derivative at the central point of partition for  $P_1$ -nonconforming quadrilateral FEM

$N$	$\theta = 0$		$\theta = \frac{1}{4}$		$\theta = \frac{1}{2}$		$\theta = \frac{3}{4}$		$\theta = 1$	
	$E_{Du}$	Rate	$E_{Du}$	Rate	$E_{Du}$	Rate	$E_{Du}$	Rate	$E_{Du}$	Rate
4	3.6486e-2	–	1.0352e-1	–	1.7815e-1	–	2.4520e-1	–	3.1933e-1	–
8	9.7252e-3	1.9076	5.3475e-2	0.9529	1.0143e-1	0.8126	1.3970e-1	0.8116	1.6787e-1	0.9274
16	2.5839e-3	1.9122	2.7949e-2	0.9361	5.3409e-2	0.9253	7.3343e-2	0.9296	8.7808e-2	0.9349
32	7.1634e-4	1.8509	1.4321e-2	0.9647	2.7516e-2	0.9568	3.7843e-2	0.9546	4.5191e-2	0.9883
64	2.3768e-4	1.5916	7.2834e-3	0.9754	1.4015e-2	0.9733	1.9274e-2	0.9733	2.3006e-2	0.9740

Numerical results of the superconvergence of derivative are presented in Tables 13–16. We observe from these tables that the superconvergence points of derivative exist if and only if  $\theta = 0$  for these methods. For other cases, there are no similar superconvergences at the nodes of the partition and the midpoints of edges. Furthermore, we can obtain better convergence of derivative of  $u_h$  at center points as  $\theta$  increases for  $P_1$ -nonconforming quadrilateral FVM and  $P_1$ -nonconforming quadrilateral FEM, and  $Q_1$ -conforming quadrilateral FVM with nonoverlapping control volume. On the other hand, we can observe that numerical results are not good as  $\theta \geq \frac{1}{4}$  in Tables 17–18 for other two methods.

*Remark 6.1* The smallness of the quantity  $d_\tau$  is a good indicator of almost parallelogram. From Fig. 6, we obtain the midpoints distance  $d_\tau = \theta h$ . On one hand, if  $\theta = o(h)$ , i.e.,  $d_\tau = o(h^2)$  satisfies the usual Bi-section condition [20], we can obtain good numerical results. On the other hand, if  $\theta \rightarrow 0$ , i.e.,  $d_\tau \rightarrow 0$ , then we have good numerical results similarly. In a

**Table 16** Mean relative error of derivative at the central point of partition for  $Q_1$ -conforming quadrilateral FVM with nonoverlapping control volume

$N$	$\theta = 0$		$\theta = \frac{1}{4}$		$\theta = \frac{1}{2}$		$\theta = \frac{3}{4}$		$\theta = 1$	
	$E_{Du}$	Rate	$E_{Du}$	Rate	$E_{Du}$	Rate	$E_{Du}$	Rate	$E_{Du}$	Rate
4	4.3958e-2	–	9.6325e-2	–	1.7191e-1	–	2.3491e-1	–	2.7949e-1	–
8	1.1518e-2	1.9323	4.6292e-2	1.0572	8.9263e-2	0.9455	1.2368e-1	0.9255	1.4710e-1	0.9260
16	3.0116e-3	1.9353	2.2976e-2	1.0106	4.5761e-2	0.9640	6.3831e-2	0.9543	7.6020e-2	0.9523
32	7.7410e-4	1.9599	1.1525e-2	0.9954	2.3302e-2	0.9736	3.2578e-2	0.9704	3.8825e-2	0.9694
64	1.9652e-4	1.9779	5.8262e-3	0.9841	1.1849e-2	0.9754	1.6580e-2	0.9744	1.9764e-2	0.9741

**Table 17** Mean relative error of derivative at the central point of partition for  $Q_1$ -conforming quadrilateral FVM with overlapping control volume

$N$	$\theta = 0$		$\theta = \frac{1}{32}$		$\theta = \frac{1}{16}$		$\theta = \frac{1}{8}$		$\theta = \frac{1}{4}$	
	$E_{Du}$	Rate	$E_{Du}$	Rate	$E_{Du}$	Rate	$E_{Du}$	Rate	$E_{Du}$	Rate
4	3.6645e-2	–	3.7460e-2	–	4.3507e-2	–	5.8696e-2	–	9.4814e-2	–
8	9.6639e-3	1.9151	1.2052e-2	1.6361	1.5943e-2	1.4483	2.5579e-2	1.1983	4.8917e-2	0.9548
16	2.5188e-3	1.9398	4.1869e-3	1.5253	6.5071e-3	1.2928	1.2045e-2	1.0865	2.5289e-2	0.9518
32	6.4923e-4	1.9160	1.6473e-3	1.3458	2.9344e-3	1.1490	5.9721e-3	1.0121	1.2916e-2	0.9694
64	1.6522e-4	1.9744	7.2941e-4	1.1753	1.4277e-3	1.0393	3.0379e-3	0.9752	6.7100e-3	0.9448

**Table 18** Mean relative error of derivative at the central point of partition for  $Q_1$ -conforming quadrilateral FEM

$N$	$\theta = 0$		$\theta = \frac{1}{32}$		$\theta = \frac{1}{16}$		$\theta = \frac{1}{8}$		$\theta = \frac{1}{4}$	
	$E_{Du}$	Rate	$E_{Du}$	Rate	$E_{Du}$	Rate	$E_{Du}$	Rate	$E_{Du}$	Rate
4	4.4148e-2	–	4.7424e-2	–	5.4727e-2	–	7.8010e-2	–	1.1311e-1	–
8	1.1793e-3	1.9044	1.6687e-2	1.5069	2.4987e-2	1.1311	4.5375e-2	0.7818	8.9740e-2	0.5469
16	3.0952e-3	1.9298	7.4370e-3	1.1660	1.3944e-2	0.8415	2.8542e-2	0.6688	6.1612e-2	0.5425
32	7.9596e-4	1.9593	3.8950e-3	0.9331	8.0240e-3	0.7972	1.7908e-2	0.6724	4.4086e-2	0.4829
64	2.0204e-4	1.9780	2.1575e-3	0.8523	4.8484e-3	0.7268	1.2367e-2	0.5341	3.6057e-2	0.2900

word, the convergence rate of the  $P_1$ -nonconforming quadrilateral element is independent of the mesh distortion parameter  $\theta$ . These numerical results coincide with the theoretical results.

*Remark 6.2* In 2005, Hu and Shi [20] defined a constrained nonconforming rotated  $Q_1$ -element (CNR- $Q_1$ ) and analyzed the superconvergence of the CNR- $Q_1$  element for the linear elliptic problems. They pointed out the CNR- $Q_1$  element is equivalent to the  $P_1$ -nonconforming element [34] on the rectangle mesh. They have the same properties on the rectangle mesh. For the general quadrilateral mesh, it is still unknown whether there are similar results. From numerical experiments in [20], we know the relative errors of  $P_1$ -nonconforming quadrilateral element is smallest on the general quadrilateral mesh for Poisson equation, and the convergence rate of  $P_1$ -nonconforming element is independent of the



mesh distortion parameter. From Tables 1–18, we can obtain the similar numerical laws for the semilinear elliptic problems by  $P_1$ -nonconforming quadrilateral element.

*Remark 6.3* Recently, Mao et al. give a more general framework to construct effective FEM by using the different ideas, and novel DSP element and QB element are proposed in [29, 31, 32]. In fact, QB element is equivalent to the nonparametric  $P_1$ -nonconforming quadrilateral element [34] under rectangular meshes, but for general quadrilateral meshes, they are not equivalent. Moreover, the nonparametric  $P_1$ -nonconforming quadrilateral element has the optimal convergence without the Bi-section condition on the meshes and it can be implemented easily.

*Remark 6.4* In our numerical experiments, the number of unknown variables is same for every method. And the number of nonzero elements of the coefficient matrix is the least by using  $P_1$ -nonconforming element. Each line has at most five nonzero elements by using  $P_1$ -nonconforming element and at most nine nonzero elements by using  $Q_1$ -conforming element on the rectangle mesh. For other cases, each line of the coefficient matrix has at most nine nonzero elements by using  $P_1$ -nonconforming element and  $Q_1$ -conforming element respectively.

## 7 Conclusions

In conclusion,  $P_1$ -nonconforming quadrilateral element is a simple and stable element. Numerical analysis and examples have demonstrated excellent stability and convergence properties of the nonconforming FEM and FVM by using the nonoverlapping control volumes and overlapping control volumes, respectively. Moreover,  $P_1$ -nonconforming quadrilateral element has better convergence of derivative.

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