



# Effect of $\text{Fe}_2\text{O}_3$ as an Aggregate Replacement on Mechanical, and Gamma/ Neutron Radiation Shielding Properties of Phosphoaluminate Glasses

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## Abstract

In the present work, we examined the impact of  $\text{Fe}_2\text{O}_3$  on the mechanical and photon shielding characteristics of lead-phosphoaluminate glasses. Due to water corrosion, the use of lead-phosphosilicate glasses may be limited. The addition of  $\text{Fe}_2\text{O}_3$  significantly improves its water resistance. The radiation and mechanical of  $20\text{PbO} - 45\text{P}_2\text{O}_5 - 15\text{Al}_2\text{O}_3 - (20-x)\text{Na}_2\text{O} - x\text{Fe}_2\text{O}_3$  glass system doped with  $x\text{Fe}_2\text{O}_3$  reflect the originality of this article. The molar volume of these samples is declining whereas the density is an increment. Ultrasonic velocity and elastic modulus were found to be enhanced. The shielding parameters were established using the Phy-X / PSD. The mass attenuation coefficient is the highest in the sample with the maximum  $\text{Fe}_2\text{O}_3$  content. The ( $Z_{\text{eff}}$ ) and ( $N_{\text{eff}}$ ) values decreased and then increased slowly at lower energy. Because of the Compton scattering interaction, the ( $Z_{\text{eq}}$ )-value decreases as the energy and  $\text{Fe}_2\text{O}_3$  content increase. Small deviations from the glass samples are observed at higher energy levels to decrease the value ( $\Sigma R$ ). Finally, the increment of  $\text{Fe}_2\text{O}_3$  in prepared glasses increases the  $\gamma$ -radiation & neutronattenuation rate.

**Keywords** Phosphoaluminate · Elastic modulus · Shielding · Neutron

## 1 Introduction

Glass is an amorphous material that melts without crystallizing. High-manufacture phosphate glasses are used intended for numerous configurations [1–7]. The features of iron-phosphosilicate mixed glass networks are different

from those of single glass networks [8–16]. There are several physical-chemical features of the transition metal ions (TMIs) doped phosphosilicate glasses that lead to a wide range of discussions of those samples in material knowledge. In detail, transition metal oxides (TMO) are widely perceived in phosphate glasses that are used to improve their chemical resistance.  $\text{Fe}_2\text{O}_3$  and  $\text{PbO}$  are important elements because of their physical and mechanical characteristics.  $\text{Fe}_2\text{O}_3$  and  $\text{PbO}$  glasses have specific characteristics as a result of their mechanical and radiation applications [17–24].

Iron alkaline phosphosilicate glasses have significant scientific and technological advancements. The structural benefits involved with the existence of  $\text{PO}_4$  are responsible for this significance. Besides phosphate glass, the presence of TMIs, for example,  $\text{Fe}_2\text{O}_3$  and  $\text{PbO}$  can provide new possibilities to extend these glasses' features. Heavy metal oxide doped glasses as  $\text{PbO}$  exhibition these glasses are highly optical, and mechanical because they act as a former and modifier. The presence of TMIs, such as  $\text{Fe}_2\text{O}_3$  and  $\text{PbO}$ , in phosphosilicate glasses, can provide novel potentials for extending the features of these glasses [17–23].

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Radiation has an incredible influence and has extremely large requests in our daily lives for everything we do. Radiation depletion can be used to determine the risk impacts on living organisms. As a result of its special properties in our lives, the application of radiation has enhanced, and the application of radiation shielding is increasing day by day. Many researchers used the glasses for various radiation protection [25–29].

The addition of  $\text{Fe}_2\text{O}_3$  enhances the strength of the glass materials are used in gamma-ray shielding.  $\text{Fe}_2\text{O}_3$  is commonly used in phosphate glasses to increase their chemical resistance to moisture attacks. Phosphate glasses containing alkali, alkaline earth metals and TMIs are having great importance as they are used as cathode materials in batteries. Among the various TMIs, the  $(\text{Fe}_2\text{O}_3)$  ions have a vigorous bearing on the innumerable properties particularly mechanical, optical and structural properties of glassy materials and which can exist in two different oxidations  $\text{Fe}^{2+}$  and  $\text{Fe}^{3+}$  states with different co-ordinations or environments. By keeping in view all the above methodologies, the radiation, and mechanical features of  $20\text{PbO} - 45\text{P}_2\text{O}_5 - 15\text{Al}_2\text{O}_3 - (20-x)\text{Na}_2\text{O} - x\text{Fe}_2\text{O}_3$  glass system doped with  $x\text{Fe}_2\text{O}_3$  reflect the originality of this article.

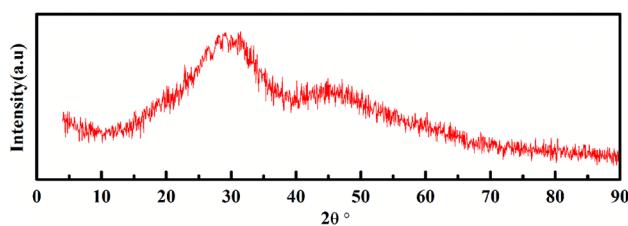
## 2 Materials and Methods

The melting and quenching process was used to synthesize iron-lead-phosphoaluminate glasses with a chemical formula of  $45\text{P}_2\text{O}_5 - 15\text{Al}_2\text{O}_3 - 20\text{PbO} - (20-x)\text{Na}_2\text{O} - x\text{Fe}_2\text{O}_3$  ( $0 \leq x \leq 2$ ) mol%. The mixture in the alumina crucible was preheated for 1 h in an electric furnace at  $450^\circ\text{C}$  to remove moisture,  $\text{CO}_2$ , &  $\text{NH}_3$ . As a result, the melting process began right away in the same furnace, which was kept at  $1150^\circ\text{C}$  for 1 h. The melted glass is quenched in a mould (inner size: Height 2 cm x thickness 1 cm x 1 cm) and annealed at  $400^\circ\text{C}$  for 2 h to reduce internal thermal stress. Glass samples in Table 1 were prepared by traditional technique as the following equation:  $\text{Na}_2\text{CO}_3 + \text{Fe}_2\text{O}_3 + \text{PbO} + \text{Al}_2\text{O}_3 + 2(\text{NH}_4)_2\text{HPO}_4 \xrightarrow[-(4\text{NH}_3 + 6\text{H}_2\text{O} + \text{CO}_2)]{\Delta \text{at } 450^\circ\text{C}} [\text{Na}_2\text{O} + \text{Fe}_2\text{O}_3 + \text{PbO} + \text{P}_2\text{O}_5 + \text{Al}_2\text{O}_3] \xrightarrow{\Delta \text{at } 1150^\circ\text{C}} \text{glasses}$

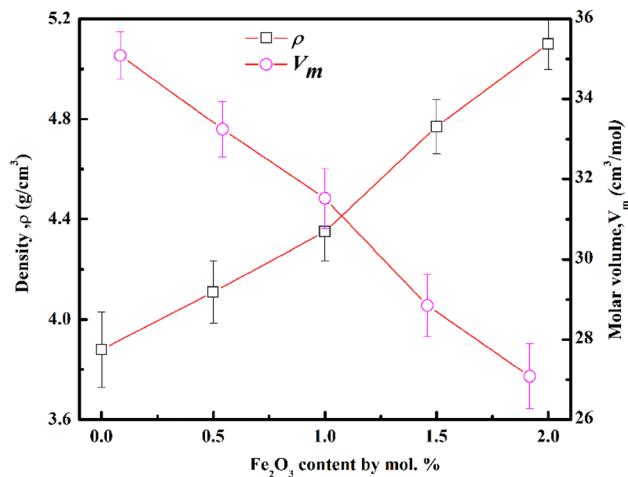
**Table 1** The components of synthesized glasses

Code	Components (mol%)				
	$\text{P}_2\text{O}_5$	$\text{Al}_2\text{O}_3$	PbO	$\text{Na}_2\text{O}$	$\text{Fe}_2\text{O}_3$
G 1	45	15	20	20	0
G 2	45	15	20	19.5	0.5
G 3	45	15	20	19	1
G 4	45	15	20	18.5	1.5
G 5	45	15	20	18	2

$\xrightarrow{\text{annealing at } 400^\circ\text{C}}$  samples. The density is determined using Archimedes Code. Molar volume is established by  $V_m = M/\rho$ . The pulse-echo method was used to obtain longitudinal ( $v_L$ ) and shear ( $v_T$ ) ultrasonic velocities at room temperature. A digital ultrasonic flaw detector (KARL DEUTSCH Echograph model 1085) was used in conjunction with x-cut and y-cut transducers (KARL DEUTSCH) operating at a fundamental frequency of 4 MHz. The ultrasonic velocity measurement has a  $\pm 10$  m/s uncertainty. Elastic moduli were determined as: longitudinal  $L = \rho v_L^2$ , transverse  $G = \rho v_T^2$ , Young's  $Y = (1 + \sigma)2G$ , & bulk  $K = L - \left(\frac{4}{3}\right)G$ . Using the model in refs. [19, 21], it is possible to estimate the elastic moduli of the glasses based on packing density  $V_i$  and dissociation energy  $Gi$ :  $Vi = \left(\frac{3\pi}{4}\right)N_A(mR_A^3 + nR_O^3)m^3 \cdot \text{mol}^{-1}$ ,  $Gi = \left(\frac{1}{V_m}\right)\sum_i GiXi$ . Longitudinal  $L = K + \left(\frac{4}{3}\right)G$ , transverse  $G = 30 * \left(\frac{V_i^2 G_i}{V_i}\right)$  Young's  $Y = 8.36 V_i G_i$ , bulk  $K = 10 V_i^2 G_i$ . Poisson's ratio  $\sigma = \frac{1}{2} - \left(\frac{1}{7.2 * Vi}\right)$ . Impedance;  $Z = v_L \rho$ . Hardness;  $H = \frac{(1-2\sigma)Y}{6(1+\sigma)}$ . Debye:  $\theta_D = \frac{h}{k} \left(\frac{9N_A}{4\pi V_m}\right)^{\frac{1}{3}} M_s$ . Average velocities  $M_s = \frac{1}{3} \left(\left(\frac{1}{v_L^3}\right) + \left(\frac{2}{v_T^3}\right)\right)^{-\frac{1}{3}}$ . Packing density & Oxygen molar volume:  $V_o = \left(\frac{M}{\rho}\right) \left(\frac{1}{\sum x_{ini}}\right)$ ,  $OPD = \left(\frac{1000C}{V_m}\right) \left(\frac{Mol}{L}\right)$ , Fractal bond connectivity ( $d$ ) =  $4(G/K)$ . Phy-X / PSD, by Sakar et al. [29] can compute several shielding factors at (0 MeV-15 MeV). Beer-Lambert law as written in Eq in mathematical form:  $\mu = -\frac{\ln I_b}{I_0}$ , Where  $\mu$  represents the linear attenuation coefficient ( $\text{cm}^{-1}$ )  $I_0$  and  $I$ , respectively, show unattenuated and attenuated photon intensities. Mass attenuation coefficient (MAC) was calculated as follows:  $\left(\frac{\mu}{\rho}\right) = \sum_i w_i \left(\frac{\mu}{\rho}\right)_i$ . Mean free path (MFP), tenth and half-value layer (TVL), (HVL) considered as  $MEP = \left(\frac{1}{\mu}\right)$ , (TVL) (HVL) are calculated by:  $TVL = \left(\frac{\ln 10}{\mu}\right)$ ,  $HVL = \left(\frac{\ln 2}{\mu}\right)$ . The effective atomic number ( $Z_{eff}$ ) is predictable by  $Z_{eff} = \left(\frac{\sigma_a}{\sigma_e}\right)$  where ( $\sigma_a$ ) is the atomic cross-section,  $\sigma_a = \sigma_m \frac{1}{\sum_i n_i} = \left(\frac{\mu}{\rho}\right)_{target} / N_A \sum_i \frac{w_i}{A_i}$ , and  $\sigma_e$  is the electronic cross-section,  $\sigma_e = \frac{1}{N} \sum_i \left(\frac{\mu}{\rho}\right)_i \frac{f_i w A_i}{z_i}$ . Equivalent atomic number  $Z_{eq}$  is predictable by  $Z_{eq} = \frac{Z1(\log R2 - \log R1) + Z2(\log R - \log R1)}{\log R2 - \log R1}$ . Electron density ( $N_{eff}$ ) is predictable by  $N_{eff} = N \frac{Z_{eff}}{\sum_i F_i A_i}$ . Effective removal cross-section ( $\Sigma_R$ ), is predictable as:  $\left(\frac{\Sigma_R}{\rho}\right) = \sum_i w_i \left(\frac{\Sigma_R}{\rho}\right)_i$  and  $R = \sum_i \rho_i \left(\frac{R}{\rho}\right)_i$



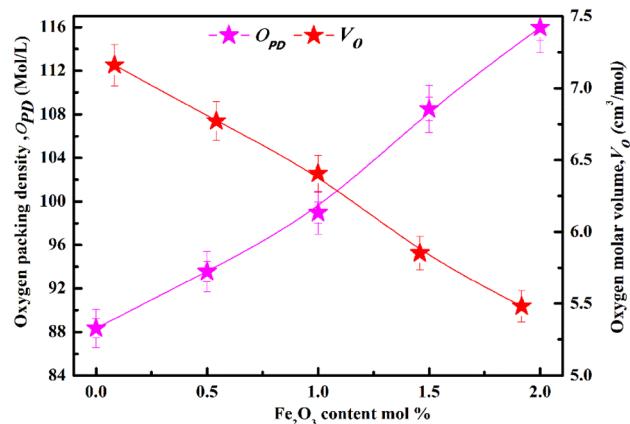
**Fig. 1** XRD of G 3 synthesized glasses



**Fig. 2**  $\rho$  &  $V_m$  of prepared samples

**Table 2** Various physical constraints

Samples	G 1	G 2	G 3	G 4	G 5
No	3.1	3.15	3.2	3.25	3.3
$(N_i) (10^{21} \text{ ions}/\text{cm}^3)$	—	1.43	3	4.93	6.97
$R_i (\text{\AA})$	—	9.03	7.05	5.97	5.32
$r_i (\text{\AA})$	—	10.45	8.17	6.94	6.19
$r_p (\text{\AA})$	—	3.00	2.35	1.99	1.78
$(d_{P-P}) \text{ nm}$	0.55	0.53	0.52	0.50	0.48



**Fig. 3**  $V_o$  &  $OPD$  of prepared glasses

### 3 Results and Discussion

#### 3.1 Physical Properties

The XRD of the glass system is illustrated in Fig. 1, the amorphous state of all glasses is detected. Figure 2 illustrates the molar volume ( $V_m$ ) and glass density ( $\rho$ ) as  $\text{Fe}_2\text{O}_3$  concentration increases. The results demonstrate that  $\rho$  is increasing, while  $V_m$  decreases. Several factors, such as density and molecular mass, have a direct impact on the ( $\rho$ ) and ( $V_m$ ). The density of  $\text{Na}_2\text{O}$  and  $\text{Fe}_2\text{O}_3$ , (2.27, 5.25), and molecular weights (61.69, 159.688). The atomic radii of [Fe (0.83 $\text{\AA}$ ) & Na (1.8 $\text{\AA}$ )] [30–35]. Fe-ions concentration was calculated as  $Ni = \left( \frac{6.023 \times 10^{23} \times \text{mol fraction of cation} \times \text{valency of cation}}{V_m} \right)$ . It is well-known that  $\text{Fe}^{3+}$  concentration increments due to the decreasing of  $V_m$ . Inter-ionic distance ( $R_i$ ) calculated as  $R_i = \left( \frac{1}{\text{content of Pb}} \right)^{\frac{1}{3}}$ , it is well-known that  $R_i$  declined, this decline is associated with reductions of  $V_m$ . P – P separation ( $d_{P-P}$ ) could be estimated by  $(dP - P) = \left( \frac{V_m^B}{N} \right)^{\frac{1}{3}}$  and  $V_m^B = \frac{V_m}{2(1-2X_n)}$ . The values of ( $dP - P$ ) increased due to the decrease of  $V_m$ . Radius Polaron  $r_p$  & distance inter-nuclear  $r_i$  are predictable by  $r_p = \frac{1}{2} \left( \frac{\pi}{6N} \right)^{\frac{1}{3}}$ ,  $r_i = \left( \frac{1}{N} \right)^{\frac{1}{3}}$ . It is men-

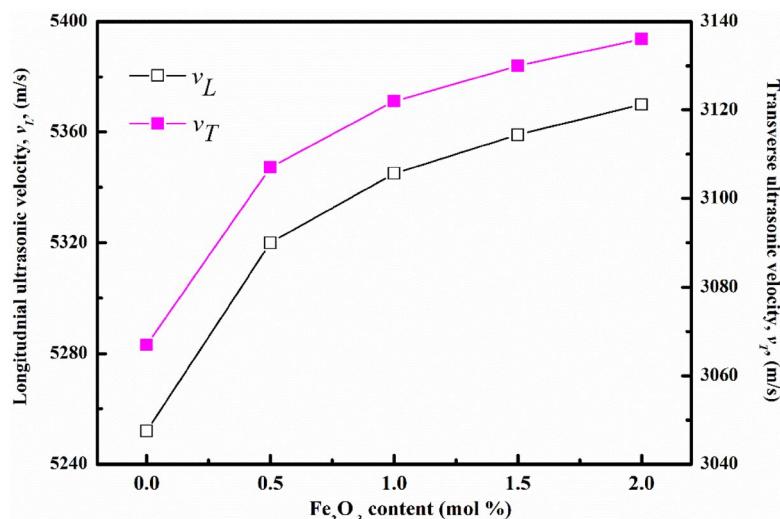
tioned that, with the increases of  $\text{Fe}^{3+}$  these values become smaller, due to reduction of  $V_m$ . Table 2 documents these estimations. The variations in  $V_o$  and  $OPD$  are exemplified in Fig. 3. The  $V_o$  values are decreased, while  $OPD$  increased.

#### 3.2 Mechanical Properties

Figure 4 exemplifies the velocities ( $v_L$ ,  $v_T$ ) of glasses. With an increase in  $\text{Fe}_2\text{O}_3$  content, each velocity is increased and documented in Table 3 [36–43]. Arrange  $v_L$  between 5252, 5370 m/s and  $v_T$  3067, 3136 m/s. When  $\text{Fe}_2\text{O}_3$  is increased, the network glass modifier increases, explaining the observed variations in ( $v_L$ ,  $v_T$ ) of the glasses. This oxide causes bond lengths to shorten and ultrasonic velocities to increase by increasing the stretching force constantly. Furthermore, the increased in  $v_L$  and  $v_T$  of the investigated glasses can be linked to the higher bond strength of Fe–O than Na–O.

Figures 5 and 6 show elastic moduli with  $\text{Fe}_2\text{O}_3$  content (experimentally and theoretically). Elastic modulus values decreased with the reduction of  $\text{Fe}_2\text{O}_3$  content. This behavior is attributed to an increment in coordination number as  $\text{Fe}_2\text{O}_3$  rises, in addition to the increase in the average force and cross-link density. As  $\text{Na}_2\text{O}$  replaces  $\text{Fe}_2\text{O}_3$ ,  $V_m$  reduces,

**Fig. 4** ( $v_L$ & $v_T$ ) of synthesized glasses



and the  $\rho$  rises, attempting to make the glass matrices extra compact. The above results are listed in Table 3. This could be because the elastic moduli are dependent on the density values, which are increased when Fe<sub>2</sub>O<sub>3</sub> is added to the glasses, compacting the glass structure, and increasing network rigidity.

Mechanical values ( $V_i$ ), ( $G_i$ ), ( $H$ ), ( $\alpha_p$ ), ( $Z$ ), ( $O_{PD}$ ), ( $V_o$ ), and ( $\sigma$ ) are listed in Table 4. ( $V_i$ ), ( $H$ ), ( $\alpha_p$ ), ( $Z$ ), ( $O_{PD}$ ), ( $d$ ), and ( $\sigma$ ) is increased with Fe<sub>2</sub>O<sub>3</sub>, whereas ( $G_i$ ) decrements. The content of the network modifier (NWM) is linked to an enhancement in the glass structure's rigidity. The addition of Fe<sub>2</sub>O<sub>3</sub> also increased crosslink density and sample compactness due to the current glassy samples' small variability in configuration. The fractal bond connectivity ( $d$ ) is an important parameter that connects the elastic properties of the glasses to their structures. The values of ( $d$ ) around 3. The structure of the glassy samples will be converted into a 3D network as the Fe<sub>2</sub>O<sub>3</sub> content increases.

### 3.3 Radiation Properties

In terms of  $\gamma$ -shielding, a lead phosphosilicate glass system doped with Fe<sub>2</sub>O<sub>3</sub> has been explored [44–60]. The MAC of the glass under consideration is the first criterion to be explained. Figure 7 illustrates the MAC of the glasses and estimated by  $(\frac{\mu}{\rho}) = \sum_i w_i (\frac{\mu}{\rho})_i$ . Table 5 presents values of MAC. The reducing order of the samples is (G1) > (G2) > (G3) > (G4) > (G5), because of the atomic number variance between Fe and Na, this is not a significant increase. It is demonstrated that the MAC of the glass system increased at low energy and then stayed constant at higher energy [32, 34, 36–38, 41–43]. MAC trend with energy is the same as observable and is monitored by the major procedures of common gamma-ray interaction as photoelectric (PE) effect,

Compton effect (CE), and pair production (PP) effect. MAC of glasses under-investigated compared to other samples are presented in Table 6.

Figure 8 shows the  $Z_{eff}$  of studied samples with  $\gamma$ -energy. The glass with the code G1 possesses the maximum score, whereas G5 possesses the minimum. The trend order of the samples is (G1)  $Z_{eff} >$  (G2)  $Z_{eff} >$  (G3)  $Z_{eff} >$  (G4)  $Z_{eff} >$  (G5)  $Z_{eff}$ . The obtained results for  $Z_{eff}$  values are shown in Table 7. The rate of  $\gamma$ -radiation attenuation for the glasses is accelerated as a result of the addition of Fe<sub>2</sub>O<sub>3</sub> to the glasses [32, 34, 36–38, 41–43]. Figure 9 represents the ( $N_{eff}$ ) with energy. ( $N_{eff}$ ) has the same behaviour as  $Z_{eff}$  [44–60].

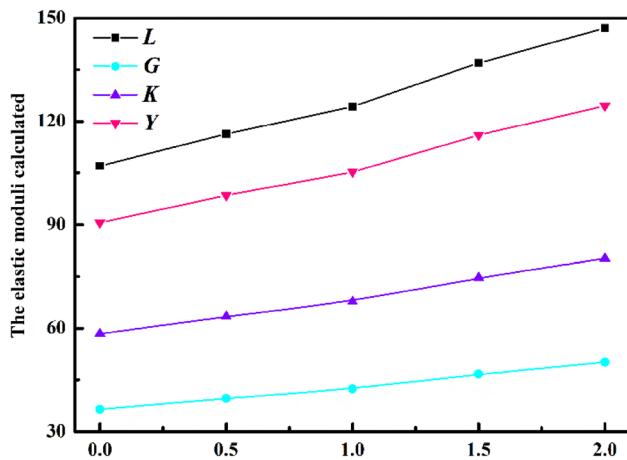
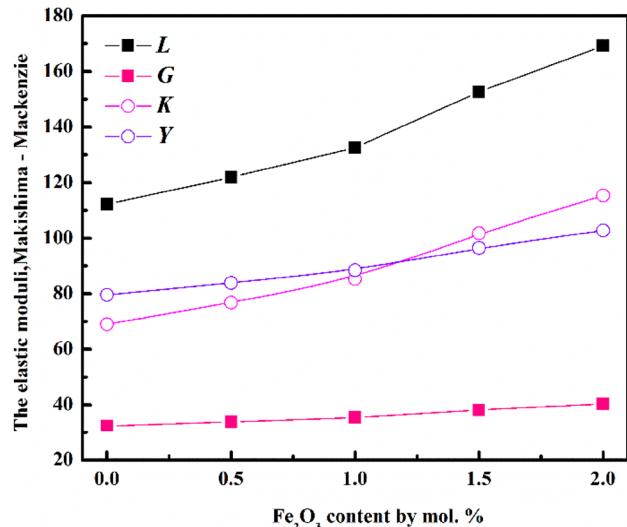
The ( $Z_{eq}$ ) values of prepared samples were represented in Fig. 10. It is illustrated that ( $Z_{eq}$ ) increased with energy and with the replacement of Na<sub>2</sub>O with Fe<sub>2</sub>O<sub>3</sub>. The ( $Z_{eq}$ ) values are reduced with energy increased and with the Fe<sub>2</sub>O<sub>3</sub> content because of the Compton scattering interaction. The highest ( $Z_{eq}$ ) value is 1 MeV for prepared samples. The obtained results for  $Z_{eff}$  values are shown in Table 8 [44–60].

(TVL), and (HVL) of prepared samples are shown in Fig. 11,&12. The shielding capacity of glasses possessing lowering HVL is the greatest. In this regard, of all the synthesized glasses, G5 appeared to be the most effective at shielding against gamma ionizing radiation. The trend order of the samples is (G1)  $HVL >$  (G2)  $HVL >$  (G3)  $HVL >$  (G4)  $HVL >$  (G5)  $HVL$ . Table 9 summarises the HVL results. TVL& HVL possess the same trend as the synthesized samples [44–60].

Figure 13 depicts the change in MFP. MFP values increased as photon energy increased. Additionally, MFP decreased as Fe<sub>2</sub>O<sub>3</sub> content increased. This information reveals that as the photon's energy increases, it becomes capable of transmitting the prepared sample on purpose. For the best attenuation capabilities, G5 glass is recommended.

**Table 3** Mechanical parameters values

code	$V_L$ m/s	$V_T$	L				G				K				Y				L <sub>M</sub>				G <sub>M</sub>				K <sub>M</sub>				Y <sub>M</sub>										
			L <sub>M</sub>	G <sub>M</sub>	K <sub>M</sub>	Y <sub>M</sub>	L	G	K	Y	L <sub>M</sub>	G <sub>M</sub>	K <sub>M</sub>	Y <sub>M</sub>	L	G	K	Y	L <sub>M</sub>	G <sub>M</sub>	K <sub>M</sub>	Y <sub>M</sub>	L	G	K	Y	L <sub>M</sub>	G <sub>M</sub>	K <sub>M</sub>	Y <sub>M</sub>											
G 1	5252	3067	107.02	36.50	58.36	90.60	112.16	32.37	68.99	79.56	116.32	39.68	98.49	121.93	33.86	76.78	83.91	124.28	42.40	67.74	105.24	132.52	35.41	85.31	88.41	136.99	46.73	74.68	116.00	152.69	38.21	101.74	96.5	147.07	50.16	80.19	124.51	169.176	40.365	115.36	102.75
G 2	5320	3107	116.32	39.68	63.42	98.49	121.93	33.86	76.78	83.91	124.28	42.40	67.74	105.24	132.52	35.41	85.31	88.41	136.99	46.73	74.68	116.00	152.69	38.21	101.74	96.5	147.07	50.16	80.19	124.51	169.176	40.365	115.36	102.75							
G 3	5345	3122	136.99	46.73	74.68	116.00	152.69	38.21	101.74	96.5	147.07	50.16	80.19	124.51	169.176	40.365	115.36	102.75	136.99	46.73	74.68	116.00	152.69	38.21	101.74	96.5	147.07	50.16	80.19	124.51	169.176	40.365	115.36	102.75							
G 4	5359	3130	136.99	46.73	74.68	116.00	152.69	38.21	101.74	96.5	147.07	50.16	80.19	124.51	169.176	40.365	115.36	102.75	136.99	46.73	74.68	116.00	152.69	38.21	101.74	96.5	147.07	50.16	80.19	124.51	169.176	40.365	115.36	102.75							
G 5	5370	3136	147.07	50.16	80.19	124.51	169.176	40.365	115.36	102.75	147.07	50.16	80.19	124.51	169.176	40.365	115.36	102.75	147.07	50.16	80.19	124.51	169.176	40.365	115.36	102.75	147.07	50.16	80.19	124.51	169.176	40.365	115.36	102.75							

**Fig. 5** (L, G, K&Y) of prepared glasses**Fig. 6** (L, G, K&Y) of prepared glasses as calculated by Makishima and Mackenzie

It is well known that MEP and shielding have a relationship, with lower MFP values indicating better shielding material.

Figure 14 shows the ( $\Sigma R$ ) of fabricated samples. At lower energy, it is detected that ( $\Sigma R$ ) increment with energy. At higher energies, glass samples show minor deviations as ( $\Sigma R$ ) decreases. Figure 15 depicts the Fast neutron removal cross-section (FNRCS).

of the glass system. It should be noted that as the Fe<sub>2</sub>O<sub>3</sub> content increment, the FNRCS values increment [44–60]. In terms of FNRCS, the glasses are arranged in the following order: G5 > G4 > G3 > G2 > G1. The Fe<sub>2</sub>O<sub>3</sub> content of the glasses supports this conclusion.

Samples name/ parameters	$V_i \times 10^{-6}, (m^3)$	$G_i,$ (kcal/kJ)	$d$	$\sigma$	$Z \times 10^7 (kg \cdot m^{-2} \cdot s^{-1})$	$\theta_D$ (K)	$H,$ (GPa)	$T_s,$ (°C)
G 1	0.73	13.13	2.5	0.241	2.04	434.37	6.30	1016.77
G 2	0.77	13.12	2.5	0.241	2.19	448.35	6.85	1045.09
G 3	0.81	13.11	2.5	0.241	2.32	458.90	7.32	1056.84
G 4	0.88	13.1	2.5	0.241	2.56	474.21	8.07	1063.89
G 5	0.94	13.1	2.5	0.241	2.74	485.61	8.65	1069.61

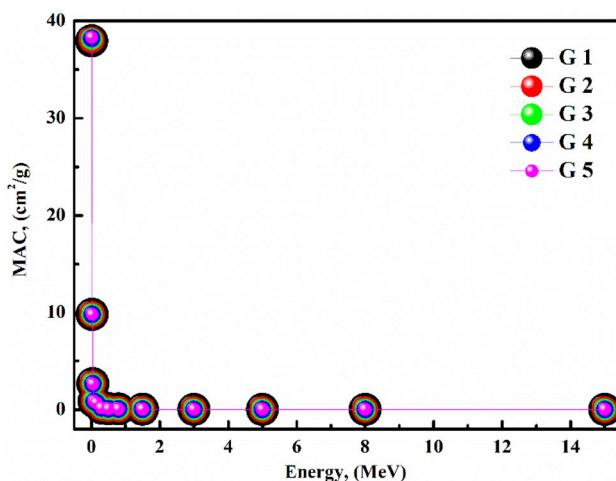


Fig. 7 MAC of prepared samples

Table 5 MAC of the glasses

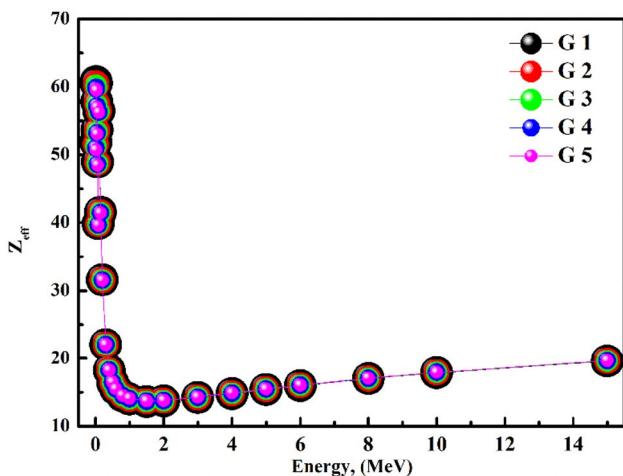
Energy	G 1	G 2	G 3	G 4	G 5
0.015	37.940	38.032	38.123	38.213	38.303
0.02	28.033	28.036	28.038	28.040	28.042
0.03	9.825	9.823	9.820	9.818	9.815
0.04	4.689	4.687	4.685	4.682	4.680
0.05	2.666	2.664	2.662	2.661	2.659
0.06	1.700	1.699	1.697	1.696	1.695
0.08	0.869	0.868	0.867	0.867	0.866
0.1	1.804	1.799	1.794	1.789	1.784
0.15	0.709	0.707	0.705	0.704	0.702
0.2	0.390	0.389	0.388	0.387	0.386
0.3	0.196	0.196	0.196	0.195	0.195
0.4	0.136	0.136	0.136	0.136	0.136
0.5	0.109	0.109	0.109	0.109	0.109
0.6	0.093	0.093	0.093	0.093	0.093
0.8	0.076	0.076	0.075	0.075	0.075
1	0.065	0.065	0.065	0.065	0.065
1.5	0.051	0.051	0.051	0.051	0.051
2	0.045	0.045	0.045	0.045	0.045
3	0.038	0.038	0.038	0.038	0.038
4	0.034	0.034	0.034	0.034	0.034
5	0.033	0.033	0.033	0.033	0.033
6	0.032	0.032	0.032	0.032	0.032
8	0.031	0.031	0.031	0.031	0.031
10	0.031	0.031	0.031	0.031	0.031
15	0.032	0.032	0.032	0.032	0.032

#### 4 Conclusions

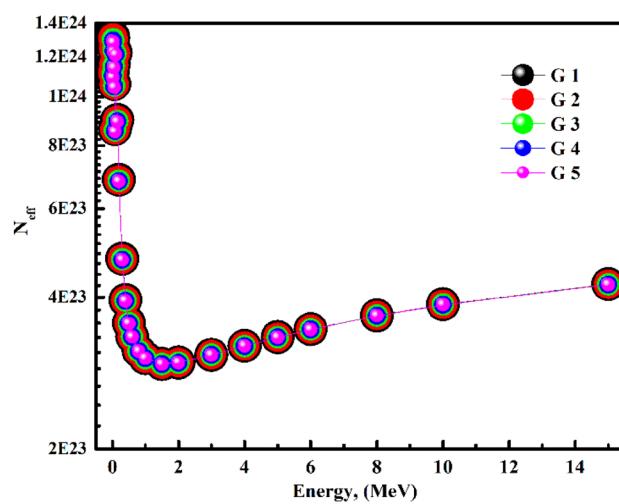
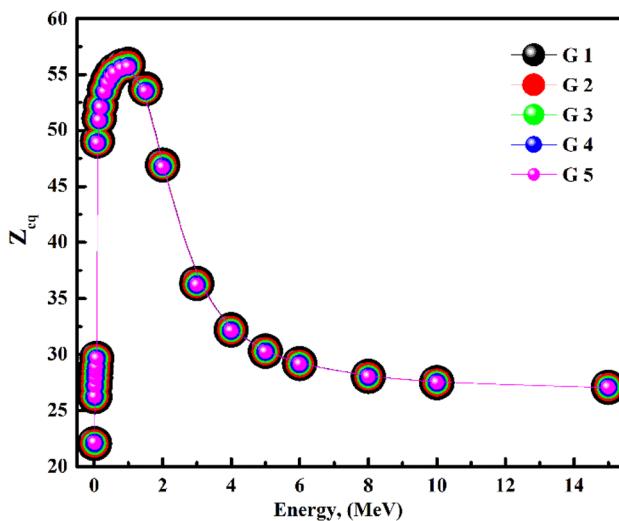
The melt quenching procedure was used to manufacture a set of phosphate glasses with the following formulation:

**Table 6** MAC (in  $\text{cm}^2/\text{g}$ ) of prepared samples in assessment with diverse glasses

Samples	MAC, (MeV)	
	0.02	10
G 5 (Currently working)	28.042	0.031
66B <sub>2</sub> O <sub>3</sub> -5Al <sub>2</sub> O <sub>3</sub> -29Na <sub>2</sub> O	1.074	0.020
5Bi <sub>2</sub> O <sub>3</sub> -61B <sub>2</sub> O <sub>3</sub> -5Al <sub>2</sub> O <sub>3</sub> -29Na <sub>2</sub> O	5.059	0.022
10Bi <sub>2</sub> O <sub>3</sub> -56B <sub>2</sub> O <sub>3</sub> -5Al <sub>2</sub> O <sub>3</sub> -29Na <sub>2</sub> O	9.043	0.023
0PbO-30SiO <sub>2</sub> -46.67B <sub>2</sub> O <sub>3</sub> -23.33Na <sub>2</sub> O	1.386	0.023
5PbO-25SiO <sub>2</sub> -46.67B <sub>2</sub> O <sub>3</sub> -23.33Na <sub>2</sub> O	5.167	0.021
10PbO-20SiO <sub>2</sub> -46.67B <sub>2</sub> O <sub>3</sub> -23.33Na <sub>2</sub> O	8.952	0.024
49.46SiO <sub>2</sub> -26.38Na <sub>2</sub> O-23.08CaO-1.07P <sub>2</sub> O <sub>5</sub>	3.982	0.024
47.84SiO <sub>2</sub> -26.67Na <sub>2</sub> O-23.33CaO-2.16P <sub>2</sub> O <sub>5</sub>	3.985	0.023
44.47SiO <sub>2</sub> -27.26Na <sub>2</sub> O-23.85CaO-4.42P <sub>2</sub> O <sub>5</sub>	4.057	0.024
40.96SiO <sub>2</sub> -27.87Na <sub>2</sub> O-24.39CaO-6.78P <sub>2</sub> O <sub>5</sub>	4.113	0.024
37.28SiO <sub>2</sub> -28.52Na <sub>2</sub> O-24.95CaO-9.25P <sub>2</sub> O <sub>5</sub>	4.061	0.024
48.98SiO <sub>2</sub> -26.67Na <sub>2</sub> O-23.33CaO-1.02P <sub>2</sub> O <sub>5</sub>	3.983	0.023
43.66SiO <sub>2</sub> -28.12Na <sub>2</sub> O-24.60CaO-3.62P <sub>2</sub> O <sub>5</sub>	4.100	0.024
38.14SiO <sub>2</sub> -29.62Na <sub>2</sub> O-25.91CaO-6.33P <sub>2</sub> O <sub>5</sub>	4.190	0.022
40.71SiO <sub>2</sub> -28.91Na <sub>2</sub> O-25.31CaO-5.07 P <sub>2</sub> O <sub>5</sub>	4.131	0.022

**Fig. 8** ( $Z_{\text{eff}}$ ) of prepared glasses

$x20\text{PbO} - 45\text{P}_2\text{O}_5 - 15\text{Al}_2\text{O}_3 - (20-x)\text{Na}_2\text{O} - x\text{Fe}_2\text{O}_3$  ( $0 \leq x \leq 2$ ). The mechanical and radiation characteristics of these glasses were examined. The density, ultrasonic velocity, and elastic moduli are incremented as the Fe<sub>2</sub>O<sub>3</sub> expands. Experimental results and calculated elastic moduli values using the Makishima-Mackenzie theoretical model are deemed acceptable. The parameters like MAC, LAC, TVL, HVL, MFP, and  $\sum R$  are computed to estimate the capabilities of glasses doped with Fe<sub>2</sub>O<sub>3</sub> to shield radiation. The results show that as the Fe<sub>2</sub>O<sub>3</sub> content increases, the values of MAC and  $\sum R$  decrement. The G5 glass sample shields photons and neutrons better than

**Fig. 9** ( $N_{\text{eff}}$ ) of the synthesized samples**Fig. 10** ( $Z_{\text{eq}}$ ) of the synthesized samples

other glass samples, according to this investigation. The parameters' analysis revealed that the glasses under consideration are strong candidates for radiation shielding. Finally, the increase of Fe<sub>2</sub>O<sub>3</sub> in prepared glasses increase  $\gamma$ -radiation attenuation rate.

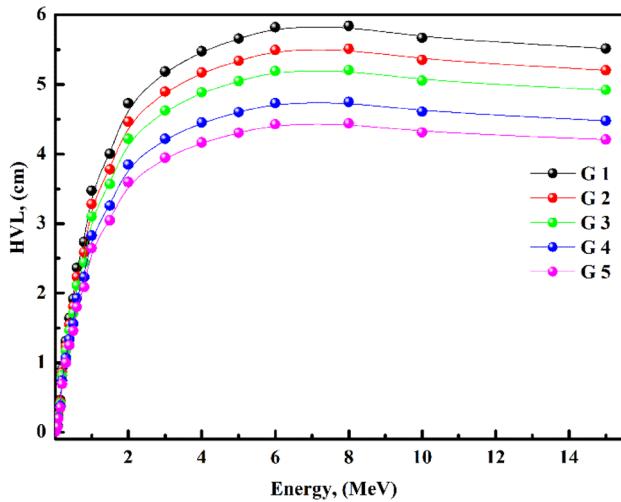
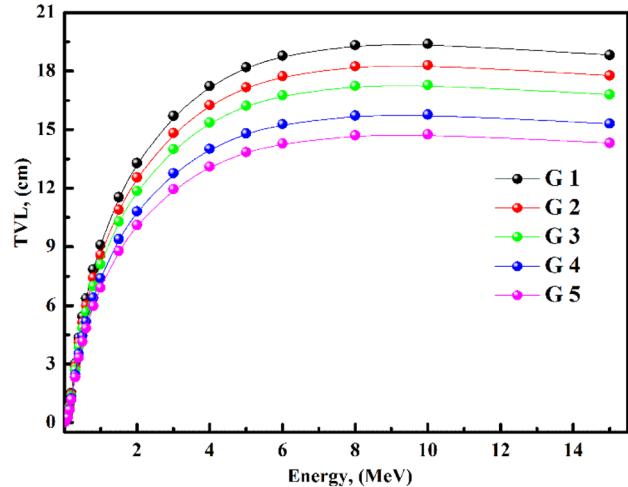
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**Table 7**  $Z_{eff}$  of the glasses

Energy	G 1	G 2	G 3	G 4	G 5
0.015	51.85	51.56	51.27	51.00	50.72
0.02	60.77	60.49	60.21	59.94	59.67
0.03	60.48	60.22	59.97	59.72	59.48
0.04	57.80	57.59	57.38	57.18	56.97
0.05	53.68	53.52	53.36	53.20	53.04
0.06	48.94	48.82	48.70	48.59	48.47
0.08	39.83	39.78	39.72	39.66	39.60
0.1	56.46	56.41	56.35	56.29	56.24
0.15	41.53	41.50	41.47	41.44	41.41
0.2	31.60	31.59	31.57	31.56	31.54
0.3	22.03	22.03	22.04	22.04	22.04
0.4	18.23	18.24	18.25	18.26	18.27
0.5	16.43	16.44	16.45	16.47	16.48
0.6	15.44	15.46	15.48	15.49	15.51
0.8	14.46	14.48	14.49	14.51	14.53
1	13.99	14.01	14.03	14.05	14.06
1.5	13.62	13.64	13.66	13.68	13.69
2	13.71	13.73	13.75	13.77	13.79
3	14.21	14.22	14.24	14.26	14.28
4	14.80	14.82	14.84	14.86	14.87
5	15.39	15.41	15.43	15.45	15.47
6	15.97	15.99	16.00	16.02	16.04
8	17.00	17.02	17.04	17.06	17.08
10	17.90	17.92	17.94	17.95	17.97
15	19.62	19.64	19.65	19.67	19.69

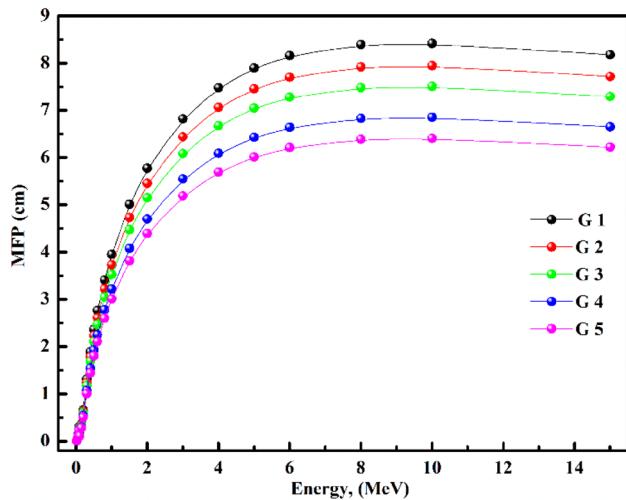
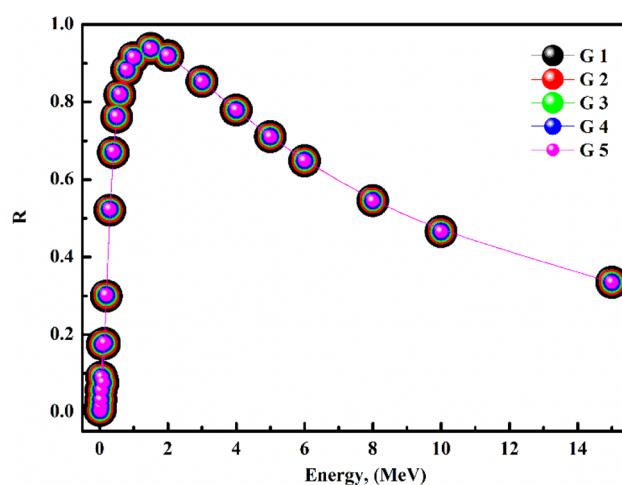
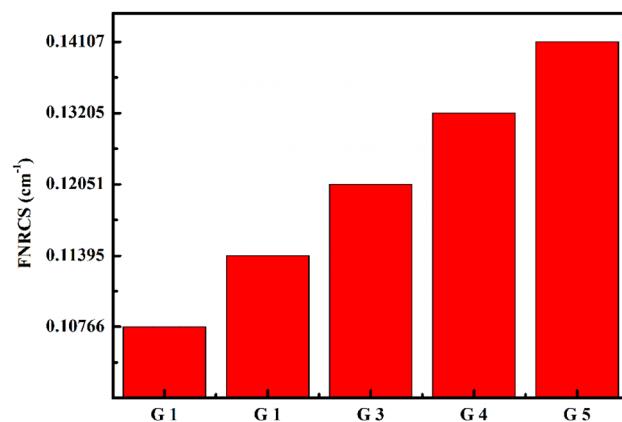
**Table 8**  $Z_{eq}$  of the glasses

Energy	G 1	G 2	G 3	G 4	G 5
0.015	22.07	22.09	22.11	22.13	22.15
0.02	26.25	26.25	26.25	26.25	26.25
0.03	27.23	27.23	27.23	27.23	27.23
0.04	27.94	27.94	27.93	27.93	27.93
0.05	28.50	28.49	28.49	28.48	28.47
0.06	28.95	28.94	28.93	28.93	28.92
0.08	29.69	29.68	29.67	29.66	29.65
0.1	49.04	48.99	48.95	48.90	48.85
0.15	51.07	51.02	50.97	50.92	50.87
0.2	52.24	52.19	52.13	52.08	52.03
0.3	53.63	53.58	53.52	53.47	53.42
0.4	54.45	54.40	54.35	54.29	54.24
0.5	54.99	54.94	54.88	54.83	54.78
0.6	55.35	55.29	55.24	55.19	55.14
0.8	55.74	55.68	55.63	55.58	55.52
1	55.90	55.84	55.79	55.74	55.68
1.5	53.70	53.65	53.59	53.54	53.49
2	46.91	46.86	46.81	46.75	46.70
3	36.34	36.31	36.28	36.24	36.21
4	32.22	32.20	32.18	32.16	32.14
5	30.30	30.29	30.28	30.27	30.25
6	29.20	29.19	29.18	29.17	29.16
8	28.05	28.05	28.04	28.04	28.04
10	27.50	27.50	27.50	27.50	27.49
15	27.08	27.08	27.08	27.08	27.08

**Fig. 11** HVL of the synthesized samples**Fig. 12** TVL of the synthesized samples

**Table 9** HVL of the glasses

Energy	G 1	G 2	G 3	G 4	G 5
0.015	0.005	0.004	0.004	0.004	0.004
0.02	0.006	0.006	0.006	0.005	0.005
0.03	0.018	0.017	0.016	0.015	0.014
0.04	0.038	0.036	0.034	0.031	0.029
0.05	0.067	0.063	0.060	0.055	0.051
0.06	0.105	0.099	0.094	0.086	0.080
0.08	0.206	0.194	0.184	0.168	0.157
0.1	0.099	0.094	0.089	0.081	0.076
0.15	0.252	0.238	0.226	0.207	0.194
0.2	0.458	0.434	0.411	0.375	0.352
0.3	0.910	0.860	0.814	0.743	0.696
0.4	1.310	1.238	1.171	1.069	1.001
0.5	1.639	1.549	1.465	1.337	1.251
0.6	1.915	1.809	1.710	1.561	1.460
0.8	2.365	2.234	2.111	1.926	1.802
1	2.739	2.586	2.444	2.229	2.086
1.5	3.475	3.281	3.100	2.828	2.645
2	4.002	3.779	3.571	3.257	3.046
3	4.728	4.464	4.218	3.847	3.598
4	5.186	4.896	4.626	4.219	3.947
5	5.477	5.170	4.885	4.455	4.167
6	5.657	5.340	5.046	4.602	4.304
8	5.819	5.493	5.190	4.733	4.427
10	5.837	5.511	5.207	4.748	4.441
15	5.669	5.351	5.056	4.610	4.312

**Fig. 13** MFP of the synthesized samples**Fig. 14** (ΣR) of the synthesized samples**Fig. 15** FNRCS of the synthesized samples

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## Declarations

**Conflict of interest** The authors declare that they have no conflict of interest.

**Compliance with Ethical Standards** The manuscript has not been published elsewhere.

**Declaration of Competing Interest** There are no known competing financial interests among the authors.

**Consent to Participate** The author's consent to participate & publication.

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