The Dielectric Properties and Thermal Conductivities of Epoxy Composites Reinforced by Titanium Dioxide

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Received: 7 October 2021 / Accepted: 12 November 2021 / Published online: 20 November 2021 © The Author(s), under exclusive licence to Springer Science+Business Media, LLC, part of Springer Nature 2021

Abstract



To improve the dielectric properties and thermal conductivities of epoxy resins (EP), titanium dioxide superfine powders with microspheres structure (S-TiO₂) were prepared via a hydrothermal process based on the sodium dodecyl benzene sulfonate and hydroxyl silicate. The different content of S-TiO₂ was then employed as modifiers to add into EP resin to prepare the S-TiO₂/EP composites. The structure and morphology of the prepared S-TiO₂ was observed by X-ray diffraction (XRD) and scanning electron microscopy (SEM), and influences of different addition of S-TiO₂ on the thermal conductivity of S-TiO₂/EP composites are researched, while their dielectric constant and dielectric loss are also studied. The results suggested that the reasonable content of S-TiO₂ can endow the S-TiO₂/EP composites with higher dielectric constant without excessive increase their dielectric loss even under the high frequency. Furthermore, the thermal conductivity of S-TiO₂/EP are also be improved, which can be attributed to the good thermal conductivity of S-TiO₂ itself and the thermal conductivity path formed by S-TiO₂ inside the EP matrix.

Keywords Thermal conductivity \cdot Dielectric constant \cdot Dielectric loss \cdot TiO₂ \cdot Epoxy

1 Introduction

With the rapid development of electronic science and technology, various of new energy products emerge one after another, and the electronic devices tend to be miniaturized, integrated and flexible [1, 2]. In order to reduce the damage of material properties caused by a large amount of heat generated during the electrical operation, the excellent thermal conductivity of materials is increasingly required [3, 4]. As one of the universal thermosetting polymers, epoxy (EP) has been widely used as electronic components due to its high mechanical properties, low creep property and good oxidation resistance [5–7]. The thermal conductivity of pure EP is within the range of 0.17–0.23 W/mK, which can basically meet the requirements of common electronic components and materials [8, 9]. However, when used in the field of

Yuan Jia jiayu_an_happy@126.com microelectronics and electrical appliances, their thermal conductivity still needs to be further optimized.

At present, a large number of literature reports have shown that appropriate modification methods can promote the industrial production of heat-conducting EP [10]. All the methods can be fall into two categories. The first is developing the intrinsic thermal conductivity EP, which is to introduce the elements and groups with good thermal conductivity into the main molecule or chain structure of the epoxy resin by forming the molecular bonds [11], or improve the order and high orientation of the structure of the EP [12]. Nevertheless, relying only on the construction of thermal connections in the EP structure cannot meet the needs of greater heat conduction [13, 14]. The second is to fill the fillers with excellent thermal conductivity such as boron nitride, aluminum nitride and alumina in to EP matrix [15-17], which is more simple and more flexible, hence this method has been applied more widely [18]. Although the addition of these fillers significantly improves the thermal conductivity of EP, it will also affect its dielectric properties in a certain extent [19]. Therefore, in order to minimize other additional damage caused by the fillers added into to EP, newer thermal conductivity fillers should be selected and prepared.

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Metals and their oxides are often used as fillers for EP because of their excellent thermal conductivity [20]. Among them, titanium dioxide (TiO₂) is a kind of important inorganic functional material oxide, which exhibits excellent electric chemical and controllability, as while as the stronger photocatalysis [21, 22]. Numbers of research showed that by adding TiO₂ particles, the electrochemical properties of organic resin can be further improved [23, 24]. In addition, the excellent thermal stability of TiO₂ is benefit to the thermal conductivity of resins [25, 26]. From what has been discussed above, a new kind of TiO₂ particles with microspheres structure (S-TiO₂) were prepared via a hydrothermal process in this article, and the S-TiO₂ were then added into EP as modifiers to prepare a kind of novel S-TiO₂/EP composites. The thermal conductivity and dielectric properties of the S-TiO₂/EP composites were measured to research the effect of S-TiO₂ on the EP resins. This study is aiming to provide a new method for the development of new EP composites with the high thermal conductive, high dielectric constant and low dielectric loss, which can be used in microelectronic component fields.

2 Experimental Methods

2.1 Materials

The EP resin (the purity of > 95 wt%) was purchased from Nantong Xingchen Synthetic Material Co. Ltd. The isophorone diamine (analytical pure) was purchased from Shanghai McLean Biochemical Technology Co., Ltd. The n-butyl titanate (analytical pure) was purchased from Jingzhou fine chemical co., Ltd). The other solvents such as anhydrous ethanol and acetone were supplied by Tianjin Fuchen Chemical Reagents Factory without further purification.

2.2 Preparation of the S-TiO₂

The S-TiO₂ were obtained via the hydrothermal method. 12.5 mL n-butyl titanate and 1.5 mL water were added into a 50 mL hydrothermal kettle, the mixture was then reacted under 180 °C for 24 h. After naturally falling to room temperature, the mixture was centrifuged by anhydrous ethanol and deionized water for three times, respectively. The S-TiO₂ which are white powdery were finally obtained by dried at 60 °C for 12 h. The preparation process is shown in Fig. 1.

2.3 Preparation of the S-TiO₂/EP Composites

The S-TiO₂/EP composites with different content of S-TiO₂ were prepared via the casting method, which is shown in Fig. 2. The EP and isofrone diamine were stirred with the



Fig. 1 The preparation process of $S-TiO_2$



Fig. 2 The preparation process of S-TiO₂/EP

mass ratio of 7:1 in a glass beaker under 70 °C for 10 min, and the prepared S-TiO₂ (with the mass ratio of 0.0 wt%, 1.0 wt%, 2.0 wt%, 3.0 wt%, 4.0 wt%, 5.0 wt% and 6.0 wt%, respectively) in 20 mL acetone were added into the EP. These mixtures were ultrasonic dispersed under 70 °C for 20 min to ensure well-dispersed of S-TiO₂ in the EP matrix, thus the pre-polymer of S-TiO₂/EP can be obtained. These S-TiO₂/EP pre-polymer matrixes were then poured into a pre-heated mould under 80 °C, and degassed at 80 °C for about 30 min in a vacuum drying oven, until the bubbles inside the matrix are completely removed. Finally, the moulds filled with S-TiO₂/EP pre-polymer were put into the blast drying oven, and cured with the cured process of 80 °C/1 h + 100 °C/1 h + 120 °C/2 h.

2.4 Measurements

2.4.1 The X-ray Diffraction (XRD)

The X-ray diffraction (XRD, Bruker D8, Germany) was employed to research the crystal structure of $S-TiO_2$ at room temperature.

2.4.2 Scanning Electron Microscopy (SEM)

The S-3400N II scanning electron microscope (SEM, HITACHI, Japan) was employed to observe the morphology of S-TiO₂, and the surface morphology of the fractured surface of the EP and S-TiO₂/EP samples at room temperature.

2.4.3 Dielectric Properties

The dielectric properties of EP and S-TiO₂/EP composites were measured by dielectric constant dielectric loss tester (ZJD-A type, China Aviation Times Company).

2.4.4 Thermal Conductivity

The thermal conductivities of the EP and S-TiO₂/EP composites were measured by transient fast hot wire method of thermal conductivity tester (KDRX-II, Xiangtan Xiangyi Instrument Co., Ltd, China).



Fig. 3 The XRD result of $S-TiO_2$

Fig. 4 The SEM of $S-TiO_2$

3 Results and Discussion

3.1 Morphology Structure of the S-MoS₂

The crystallographic structure of S-TiO₂ is researched by X-ray diffraction (XRD) as shown in Fig. 3. As can be seen from the figure, the strong diffraction peaks appear at $2\theta = 25.25^{\circ}$, 37.83° , 48.03° , 53.91° , 55.01° , 62.61° , 68.94° , 70.35° , 75.04° can be correspond to standard spectrum (21-1272) of anatase TiO₂ which is (101), (004), (200), (105), (211), (204), (116), (220) and (215), respectively. At the same time, there is no excess impurity peak on the way, indicating that the prepared S-TiO₂ possesses good crystal shape and high purity. In addition, the diffraction peak corresponding to S-TiO₂ is weak and wide, which is caused by the small grain size of the nanoparticles.

To research the morphology of the obtained S-TiO₂ particles, The SEM with different magnification ratios is employed to observe their apparent morphology. It can be seen from Fig. 4A, the surface of the obtained S-TiO₂ particles is more loose and uniform, and the pore size is smaller, indicating that the prepared S-TiO₂ are ultrafine powders, which is benefit to alter their aggregation state in the resin system. In order to further observe the microscopic morphology of S-TiO₂ particles, the SEM of the part marked in red in Fig. 4A was magnified by 25 times, and the results were shown in Fig. 4B. It can be seen that S-TiO₂ nanoparticles are spherical morphology with uniform particle size, which can endow the S-TiO₂ with excellent stability.

3.2 Dielectric Properties of the Materials

The dielectric constant of S-TiO₂/EP composites with different S-TiO₂ content was measured with frequency, and the corresponding curve was as shown in Fig. 5. It can be observed from the figure that the dielectric constant of





Fig. 5 The dielectric permittivity of S-TiO₂/EP with different content of S-TiO₂ varies by frequency

S-TiO₂/EP composites increases with the increase of S-TiO₂ content, but the increase amplitude is not high, indicating that even the addition of S-TiO₂ can increase the dielectric constant of S-TiO₂/EP composites to a certain extent, but it is still within the range of use. At the same time, the dielectric constant did not increase or decrease significantly with the increase of frequency, and the dielectric constant was still low above 1000 kHz, indicating that even with the addition of a certain amount of S-TiO₂, the S-TiO₂/EP composites were still difficult to turn polarization at high frequency, so it had a low dielectric constant drop. The low dielectric constant of S-TiO₂/EP composites at high frequencies can greatly meet the needs of their use as high frequency insulating electronic materials.

Figure 6 shows the curve of dielectric loss of EP and S-TiO₂/EP composites with different S-TiO₂ content as a function of frequency. As can be observed from the figure, when S-TiO₂ content was lower than 4.0 wt%, the dielectric loss of S-TiO₂/EP composite was close to that of pure EP, and even showed a lower trend at a certain frequency. However, as the S-TiO₂ content continues to further increase, the

dielectric loss of S-TiO₂/EP composites began to increase, this is because of excessive S-TiO₂ inside the composites prone to stack, and caused a local interfacial area overlap, which provides a good path for carriers to form the current conduction, thereby the dielectric loss of S-TiO₂/EP composite became to increase. In addition, it also can be observed from the figure, with the increase of frequency, the dielectric loss of EP and S-TiO₂/EP composites also began to increase, this phenomenon is mainly due to the increase of the frequency can cause the acceleration of internal polarity molecular motion, and the heat generated by the friction between the molecular chain also increased, which resulted in the increase of dielectric loss by the composite. However, the presence of S-TiO₂ that inhibit the movement of carriers to a certain extent, while the dielectric loss of S-TiO₂/EP composites does not increase too much, thus it can meet the requirements of its use as a high frequency circuit.

3.3 Thermal Conductivities of the Materials

The effect of S-TiO₂ doges on the thermal conductivities of S-TiO₂/EP composites are also researched, and the results are shown in Fig. 7. As can be seen from the figure that the thermal conductivities of S-TiO₂/EP composites increase by the increase of S-TiO₂ content, and reached the maximum value of 0.1976 W/mK when the content of S-TiO₂ is 4.0 wt%, increased as much as 16.2% compared with pure EP resin, suggesting that the properly addition of S-TiO₂ can obviously improve the thermal conductivities of EP. The enhanced thermal conductivity of S-TiO₂/EP composites can be attributed to the essential excellent thermal conductivity of S-TiO₂. To further research the reasons for the improvement of thermal conductivity of the materials, the fracture surface morphology of EP resin and S-TiO₂/EP composites filled with 4.0 wt% S-TiO₂ are observed by SEM. As can be seen from the figure, the surface of pure EP resin is very flat, while the surface of the S-TiO₂/EP composite can be observed with regular bumps, which is caused by the



Fig.6 The dielectric loss of S-TiO₂/EP with different content of S-TiO₂ varies with frequency



Fig. 7 The thermal conductivities of S-TiO_2/EP with different content of S-TiO_2

uniform dispersion of S-TiO₂ inside the resin. The uniform dispersion of S-TiO₂ can provide a good thermal conduction path for heat conduction inside the resin, which is conducive to the improvement of thermal conductivity of the material. However, when the content of S-TiO₂ further increased to 5.0 wt%, the thermal conductivity of the S-TiO₂/EP composites began to decrease significantly. This phenomenon is due to the presence of a small amount of hydroxyl groups on the surface of the S-TiO₂ prepared by the method of hydrating heat. Therefore, excessive S-TiO₂ is unevenly dispersed in the EP matrix, resulting in some voids. The defects caused by such voids will hinder the heat transfer and ultimately lead to the decrease of the thermal conductivity of the S-TiO₂/EP composites (schematic diagram of heat conduction mechanism is shown in Fig. 9). Even as so, $S-TiO_2/EP$ composites with high content of S-TiO₂ still exhibit better thermal conductivity than that of pure EP resin.

3.4 Mechanical Properties of the Materials

When used as electronic and electrical materials, the mechanical property of EP composites is also very important. Figure 10 shows the influence of different contents of S-TiO₂ on the flexural strength of S-TiO₂/EP composites. It can be seen from the figure that the flexural strength of S-TiO₂/EP composites increases firstly and then decreases slightly with the further increase of S-TiO₂ content. When S-TiO₂ content increased to 4.0 wt%, the flexural strength of S-TiO₂/EP composite reached the maximum of 96.18 MPa, which was increased by 29.4% compared with that of pure EP resin (74.32 MPa). This indicates that the reasonable addition of S-TiO₂ can effectively improve the mechanical properties of EP resin. It is because when the reasonable addition of S-TiO₂ is added into EP resin, the ultrafine S-TiO₂ is conducive to the uniform dispersion in the resin matrix, and the spherical structure of S-TiO₂ can be



Fig. 9 Schematic diagram of heat conduction mechanism

deformed under the action of external forces, effectively resisting the damage of external forces on the composites. However, when further increasing the S-TiO₂ content, the flexural strength of S-TiO₂/EP composite no longer increases, even started to decline slightly, the reason for this is that too much S-TiO₂ in the composites start to serious reunion, caused the internal defects of S-TiO₂/EP composite, which seriously affect their mechanical properties.

It can also be observed from the SEM result as shown in Fig. 8A that, the fracture morphology of pure EP resin has a very smooth cross section and smooth structure, showing an obvious river-like morphology, which is a typical brittle fracture characteristic, indicating that pure EP resin exhibits limited mechanical properties. However, when the appropriate content of S-TiO₂ (4.0 wt%) was added, the fracture surface of S-TiO₂/EP composite (as shown in Fig. 8B) became very rough and appeared obvious fish scale shape. At the same time, more dense dimples were observed than pure EP, showing typical ductile fracture characteristics, indicating that the mechanical properties of the S-TiO₂/EP composites increased after the addition of S-TiO₂. At the same time, it can also be observed from Fig. 8B that there are a small number of obvious protrusions on the fracture surface and the distribution is relatively uniform. Such protrusions are attributed to the S-TiO₂ particles, which indicates that S-TiO₂ has achieved good dispersion in the EP composites.



Fig.8 SEM of fracture surfaces taken from the resins (**A** EP, **B** S-TiO₂/EP composites with 4.0 wt% S-TiO₂)



Fig. 10 The flexural strength of the S-TiO_2/EP composites with different content $S\text{-}TiO_2$

4 Conclusions

A novel S-TiO₂ dioxide superfine powders with microspheres structure (S-TiO₂) were prepared via hydrothermal process, and the S-TiO₂ was then employed as modifiers to prepare S-TiO₂/EP composites by blending with EP matrix. The results suggested that dielectric constant of S-TiO₂/ EP composites was improved and their dielectric loss can still remain a low level even under high frequency. Furthermore, the reasonable addition of S-TiO₂ can also enhance the thermal conductivity of S-TiO₂/EP, thermal conductivities of S-TiO2/EP composites reached the maximum value of 0.1976 W/mK when the content of S-TiO₂ is 4.0 wt%, increased as much as 16.2% compared with pure EP resin, which is owning to the good thermal conductivity of S-TiO₂ itself and the thermal conductivity path formed by S-TiO₂ inside the EP matrix. However, excessive addition of $S-TiO_2$ is detrimental to the thermal conductivity of S-TiO₂/EP composites, which is attributed to the voids inside the materials caused by the agglomeration of S-TiO₂. Meanwhile, the flexural strength of S-TiO₂/EP composite with 4.0 wt% S-TiO₂ also reached the maximum of 96.18 MPa, increased by 29.4% compared to pure EP resin (74.32 MPa). The purpose of this study is to prepare a kind of resin composites with good thermal conductivity and excellent dielectric properties which can be used in high frequency electric field.

Acknowledgements This work was financially supported by the Natural Science Research Program of Shaanxi Province (2021JQ-798), the Scientific Research Program of Education Department of Shaanxi Province (21JK0870), Xi 'an Association for Science and Technology Young Talent Promotion Project (095920211335), the Environmental Pollution Monitoring and Control Innovation Team of Education Department of Shaanxi Province (51), and the Research Team of Xi'an University (XAWLKYTD018).

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